FINAL MITIGATION PLAN

601 East Stream Restoration Union County, North Carolina EEP Project Identification Number 95756

> Yadkin River Basin 03-07-14 Cataloging Unit 03040105 Contract #004925 RFP #16-004110



Prepared for:



SEAL 1-39-2014

NC Department of Environment and Natural Resources Ecosystem Enhancement Program 1652 Mail Service Center Raleigh, NC 27699-1652

January 2014

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NC Department of Environment and Natural Resources Ecosystem Enhancement Program

1652 Mail Service Center Raleigh, NC 27699-1652

Prepared by:



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January 2014

IRTR PROCESS SUMMARY

The NCIRT Review comments and intent to approve letter for the 601 East Mitigation Site dated January 6, 2014 is included in the following pages to document the IRT Review process for this project. The following is a list of revisions that have been made to the Mitigation Plan in response to these comments:

- 1. The on-site sediment loss/bank erosion has been quantified for the recent degradation in the upper project reach in Section 7.2.1, page 40.
- 2. Performance information has been added to the document addressing on site sediment reduction Section 9.0, Page 49.
- 3. Dense planting of shrubs outside and around the BMP's on the ephemeral section of Reach 1a was added in the document Section 7.2.1, Page 40.
- 4. The performance standards wording was changed in Section 9, Page 49 to reflect the NCEEP Monitoring Requirements and Performance Standards for Stream and Wetland Mitigation Dated November 7, 2011. (Section IV C.)



DEPARTMENT OF THE ARMY

WILMINGTON DISTRICT, CORPS OF ENGINEERS 69 DARLINGTON AVENUE WILMINGTON, NORTH CAROLINA 28403-1343

21 January, 2014

Regulatory Division

Re: NCIRT Review and USACE Approval of the 601 East Draft Mitigation Plan; SAW 2013-00265; EEP IMS # 95756

Mr. Tim Baumgartner North Carolina Ecosystem Enhancement Program 1652 Mail Service Center Raleigh, NC 27699-1652

Dear Mr. Baumgartner:

The purpose of this letter is to provide the North Carolina Ecosystem Enhancement Program (NCEEP) with all comments generated by the North Carolina Interagency Review Team (NCIRT) during the 30-day comment period for the 601 East Draft Mitigation Plan, which closed on 3 January, 2014. These comments are attached for your review.

Based on our review of these comments, we have determined that no major concerns have been identified with the Draft Mitigation Plan. However, the minor issues with the Draft as discussed in the attached comment memo must be addressed in the Final Mitigation Plan.

The Final Mitigation Plan is to be submitted with the Preconstruction Notification (PCN) Application for Nationwide permit approval of the project along with a copy of this letter and a summation of the addressed comments. If it is determined that the project does not require a Department of the Army permit, you must still provide a copy of the Final Mitigation Plan, along with a copy of this letter, to the appropriate USACE field office at least 30 days in advance of beginning construction of the project. Please note that this approval does not preclude the inclusion of permit conditions in the permit authorization for the project, particularly if issues mentioned above are not satisfactorily addressed. Additionally, this letter provides initial approval for the Mitigation Plan, but this does not guarantee that the project will generate the requested amount of mitigation credit. As you are aware, unforeseen issues may arise during construction or monitoring of the project that may require maintenance or reconstruction that may lead to reduced credit.

Thank you for your attention to this matter, and if you have any questions regarding this letter, the mitigation plan review process, or the requirements of the Mitigation Rule, please call me at 919-846-2564.

Sincerely,

Digitally signed by CRUMBLEY.TYLER.AUTR Y.1007509975 Date: 2014.01.21 09:13:10 -05'00'

Tyler Crumbley Regulatory Specialist

Enclosures

Electronic Copies Furnished:

NCIRT Distribution List CESAW-RG/H. Wicker CESAW-RG-A/S. Kichefski NCEEP/P. Wiesner

DEPARTMENT OF THE ARMY WILMINGTON DISTRICT, CORPS OF ENGINEERS 69 DARLINGTON AVENUE WILMINGTON, NORTH CAROLINA 28403-1343

CESAW-RG/Crumbley

6 January, 2014

MEMORANDUM FOR RECORD

SUBJECT: 601 East- NCIRT Comments During 30-day Mitigation Plan Review

PURPOSE: The comments listed below were posted to the NCEEP Mitigation Plan Review Portal during the 30-day comment period in accordance with Section 332.8(g) of the 2008 Mitigation Rule.

NCEEP Project Name: 601 East Stream Restoration Project, Union County, NC

USACE AID#: SAW-2013-00265

NCEEP #: 95756

30-Day Comment Deadline: 3 January, 2014

1. Eric Kulz, NCDWR, 19 December, 2013:

 As stated for previous projects, DWR continues to have concerns regarding restoration, particularly P1 restoration, on incised intermittent channels (project proposes 350 LF of P1 on Reach 1a). Our concern remains that constructing an offline channel at a higher elevation can sometimes result in removing the groundwater discharge altogether, converting a jurisdictional intermittent channel into a non-jurisdictional ephemeral feature. It should be noted that credit loss (and the potential need for compensatory mitigation) could result if the proposed work results in the conversion of an intermittent stream to an ephemeral feature. DWR wants to ensure the written record for this project includes our concern.

T. Crumbley, USACE, 2 January, 2014:

• The District concurs with the comment provided by NCDWR with regard to Priority 1 restoration on incised intermittent channels. During the field meeting on 29 January, 2013 several issues with the project were discussed:

- a. There was concern from NCIRT on disconnecting the intermittent section of Reach 1a (above cross-section #1) from the groundwater source. It was stated that credits will not be generated on reaches that have been converted from intermittent to ephemeral.
- b. It was suggested by the NCIRT to quantify the on-site sediment loss/bank erosion prior to restoration and potentially tie a performance standard to incorporate onsite reduction versus watershed input.
- c. USFWS suggested planting dense shrubs along with trees on the outside/around the BMP on ephemeral section of Reach 1a to prevent additional rill or gully formation. Specifically utilizing species that will attenuate sediment.
- d. USFWS also suggested that a neotropical migrant bird study be conducted prior to construction.
- A brief discussion on impacts to existing wetlands is presented in the Draft plan, but any impacts (eg. filling, draining, converting) to current waters of the U.S. (streams, wetlands and open waters) must be accounted for and discussed in the Pre-Construction Notification (PCN) and the loss or conversion of those waters must be replaced on-site. (the conversion of ponds to stream is considered an impact, but the functional uplift provided allows for this conversion to be conducted under NWP 27. These impacts do, however need to be accounted for in the PCN).
- Section 9, pg. 46. Performance Standards: Should reference the "Ecosystem Enhancement Program Monitoring Requirements and Performance Standards for Stream and Wetland Mitigation" Dated November 7, 2011. (Section IV C.) *All monitoring and performance standard requirements need to comply with this EEP/District guidance unless the project was instituted prior to the release of this guidance*

Digitally signed by CRUMBLEY.TYLER.AUT RY.1007509975 Date: 2014.01.21

09:13:34 -05'00'

Tyler Crumbley Regulatory Specialist,

Regulatory Division



Environmental Banc & Exchange Capital • Experience • Expertise

January 13, 2014

Paul Wiesner, Western Program Manager NC Ecosystem Enhancement Program 5 Ravenscroft Drive, Suite 102 Asheville, NC 28801

Reference:

Response to 601 East-NCIRT Comments During 30-day Mitigation Plan Review

Draft Mitigation Plan and Preliminary Plan Set for the

601 East Stream Restoration Project

Yadkin River Basin - CU#03040105-Union County

NCEEP Project ID No. 95756

Contract #004925

Dear Mr. Wiesner:

Please find attached the responses to comments received for the above referenced project. The following responses are listed in the order of the comments received.

1. Eric Kulz, NCDWR, 19, December, 2013:

R: It is understood that credits will not be generated on reaches that have been converted from intermittent to ephemeral. Only the upper portion of Reach 1a will be restored above the present ground elevation. A series of 5 basins have been designed above Reach 1a. These basins will function to trap sediment as well as to provide groundwater recharge areas as the water is stored and allowed to drain into the soils below. We expect Reach 1a to remain intermittent.

2. T. Crumbley, USACE, 2 January, 2014:

a R: See response 1 above.

b R:The on-site sediment loss/bank erosion has been quantified as follows:
Based on surveyed cross sections of the incised channel and an assumed pre-degradation top of bank elevation a sediment loss volume of 167 tons was estimated to have occurred along 335 feet of channel length between 2008 and 2010 at the top of the stream. A series of five (5) stormwater BMP basins have been designed throughout the ephemeral channel reach to detain future sediment moving through the system. The basins have a total capacity to hold 206 tons of sediment. After the initial degradation within this area between 2008 and 2011 occurred, significant sediment loss was not observed in 2012 or 2013. It is anticipated that the due to the continued farming of the land outside of the conservation easement that the draws to the south and east of the restoration project will continue to introduce excess sediment to the stream. It is not anticipated that the sediment loss will be as significant as the degradation that occurred between 2008 and 2010 due to the observations that were made in 2012 and 2013. The designed basins have ample storage capacity to capture sediment and provide ground water recharge as water is stored and allowed to drain into the soils below upstream of the intermittent channel. This change was added to the mitigation plan Section 7.2.1, Page 40.

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The tributaries outside of the conservation easement will be observed yearly and the monitoring report will document the function of the upstream basins in capturing excess sediment produced by observed degradation. The reconstructed stream efficiency for sediment transport will be documented annually through the visual assessment. A specific performance standard will not be added. This change was noted in the mitigation plan Section 9.0, Page 49.

c R: A dense planting of shrubs along with trees on the outside and around the BMP's on the ephemeral section of Reach 1a will be provided. Shrubs will be used to attenuate sediment. This change was noted in the mitigation plan Section 7.2.1 Page 40.

d R: The existing nesting habitat, which consists of primarily privet, will be removed this winter prior to spring. As such, there will no nesting habitat in the construction zone. Further, there will remain extensive habitat along the relic stream channel as well as the riparian buffer along Lanes Creek.

Impacts to existing wetlands:

R: It is understood that the conversion of wetlands will be reported in the PCN. It is anticipated with that raising the stream channel and restoration to the relic channel will create/restore additional wetlands throughout the length of the project. As such, there will not only be a gain of wetlands, but a functional uplift to the entire system.

Section 9, pg 49. Performance Standards:

Cara Conde for David Godley

R: The performance standards wording in this section has been added as requested.

Please call me if you have any questions.

Thanks,

David Godley Senior Project Manger



EXECUTIVE SUMMARY

Environmental Banc & Exchange (EBX) proposes to restore and enhance Tanyard Branch an unstable stream in Union County. The 601 East Stream Restoration Site is located approximately 1,500 feet east of the intersection of Pageland Highway and Landsford Road at the latitude 34° 50' 21.62" N and longitude 80° 25' 32.26" W. The conservation easement consists of 12.78 acres of existing agricultural land currently in crop production surrounding Tanyard Branch an unstable stream. This mitigation plan describes the details, methods and protocols proposed to generate approximately 3,680 stream mitigation credits, which includes approximately 215 linear feet of ephemeral channel with buffer restoration and best management practices to filter sediment; 2,892 linear feet of Priority I restoration; 480 linear feet of Priority 3 restoration; and 400 linear feet of Stream Enhancement Level I.

General Site Conditions

The historic land use at the project site has consisted primarily of agricultural row crops. Additional land use practices, including the maintenance and removal of riparian vegetation and the relocating, dredging, and straightening of Tanyard Branch have contributed to unstable channel characteristics and degraded water quality. Current conditions at the 601 East Stream Restoration Site contains incised channels with unstable banks and a small to no riparian buffer. Just south of Landsford Road the stream has been impacted by the presence of invasive exotic plants. The uppermost reach of Tanyard Branch is in a confined valley with a steep slope. Recent improvement on Pageland Highway (US 601) has caused significant degradation of the ephemeral and intermittent segments of the stream in recent years. The lower segment of the project is separated by 1,100 feet of stream that is located in a substantially wooded buffer not included in the proposed project. The lower reach consists of a straightened channel that has been diverted from its original location within the floodplain.

Restoration Concept

The stream restoration proposed for this project has been selected to minimize the impact on adjacent land. The stream has been designed to incorporate enhancement practices where it is beneficial to the stream. Where restoration was determined to be warranted, consideration was given to which reaches could best be served by maintaining as much of the existing channel pattern as possible. The ephemeral channel has been designed with protective buffers and BMPs to trap incoming excess sediment within the channel to aid in stabilizing the upper most reach of the project and address existing stressors. Tanyard Branch has been designed with two reaches in both the upper and lower parts of the project. The top of the upper reach from the ephemeral channel to the existing woods at the spring house has been designed as a Type B4 stream. Below the woods to Landsford Road the stream has been designed as a Type C4. The lower reach has been designed as a Type C4 from the wood line for a distance of approximately 1078 feet. The last 480 feet of the stream has been designed as a Priority 3 restoration, Type B4, to transition the stream through a deeply incised reach to Lanes Creek.

The restoration reaches will include the installation of rock, brush, and wood structures. Brush toe structures will be installed within the perennial stream on selected meander

bends to provide bank stability and aquatic habitat. Constructed riffles will be used for grade control to prevent head cut formation. Log vanes with rootwads will be installed in two meander bends in the lower reach to direct the flow away from the outside of the bend and provide toe and bank protection. On-site material including brush, logs, and bed material will be used to the maximum extent possible. In-stream structures will be designed to improve aquatic habitat.

This mitigation plan has been written in conformance with the requirements of the following:

Federal rule for compensatory mitigation project sites as described in the Federal Register Title 33 Navigation and Navigable Waters Volume 3 Chapter 2 Section § 332.8 paragraphs (c)(3) through (c)(14).

NCDENR Ecosystem Enhancement Program In-Lieu Fee Instrument signed and dated July 28, 2010

These documents govern NCEEP operations and procedures for the delivery of compensatory mitigation.

TABLE OF CONTENTS

1.0	RESTORATION PROJECT GOALS AND OBJECTIVES	10
2.0	SITE SELECTION	12
2.1 2.2 2.3	DIRECTIONS TO SITE	12 17
2.4	PROJECT SITE PHOTOS	
3.0	SITE PROTECTION INSTRUMENT	
4.0	BASELINE INFORMATION	
4.1 4.2	PROJECT INFORMATIONREACH SUMMARY INFORMATION	
4.3	WETLAND SUMMARY INFORMATION	32
4.4	REGULATORY CONSIDERATIONS	
5.0	DETERMINATION OF CREDITS	
6.0	CREDIT RELEASE SCHEDULE	
7.0	MITIGATION WORK PLAN	
7.1 7.2	DESCRIPTION OF TARGET STREAM AND VEGETATION COMMUNITIES DESIGN NARRATIVE	
8.0	MAINTENANCE PLAN	
9.0	PERFORMANCE STANDARDS	
10.0	MONITORING REQUIREMENTS	
11.0	LONG-TERM MANAGEMENT PLAN	
12.0	ADAPTIVE MANAGEMENT PLAN	52
13.0	FINANCIAL ASSURANCES	52
14.0	OTHER INFORMATION	53
14.1		
14.2	REFERENCE	53
FIGU	RES	
FIGUR	RE 1: PROJECT SITE VICINITY MAP	18
FIGUR	RE 2: PROJECT SITE WATERSHED MAP	19
FIGUR	RE 3: PROJECT SITE NRCS SOIL SURVEY MAP	20
FIGUR	RE 4: EXISTING HYDROLOGIC FEATURES	21
FIGUR	RE 5: HISTORICAL AERIAL PHOTO 1938	22
FIGUR	RE 6: HISTORICAL AERIAL PHOTO 1951	23
FIGUR	RE 7: HISTORICAL AERIAL PHOTO 1969	24
FIGUR	RE 8: HISTORICAL AERIAL PHOTO 1998	25
FIGUR	RE 9: HISTORICAL AERIAL PHOTO 2006	26
FIGUR	RE 10: SITE PROTECTION INSTRUMENT	30

FIGURE 11: PROPOSED HYDROLOGIC FEATURES MAP47
APPENDICIES
APPENDIX A. SITE PROTECTION INSTRUMENT
APPENDIX B. BASELINE INFORMATION DATA
B1. WETLAND DETERMINATION DATA FORM
B2. STREAM IDENTIFICATION FORMS
B3. CATEGORICAL EXCLUSION FORM
B4. FLOODPLAIN REQUIREMENT CHECKLIST
B5. CHANNEL CROSS SECTION COMPARISON 2008-2012
APPENDIX C. MITIGATION WORK PLAN DATA AND ANALYSES
C1. CHANNEL MORPHOLOGY TABLES
C2. Hydraulic Modeling
C3. CHANNEL STABILITY (BEHI)
C4. ASSESSMENT DATA
C5. EXISTING CONDITIONS PLAN SHEETS
C6. Design Calculations
C7. REFERENCE REACH DATA

APPENDIX D. PROJECT PLAN SHEETS

APPENDIX E. PRELIMINARY MONITORING PLANS

1.0 RESTORATION PROJECT GOALS AND OBJECTIVES

The North Carolina Ecosystem Enhancement Program (NCEEP) develops River Basin Restoration Priorities (RBRP) to guide its restoration activities within each of the state's 54 cataloging units. RBRP delineate specific watersheds that exhibit both the need and opportunity for wetland, stream, and riparian buffer restoration. These watersheds are called Targeted Local Watersheds (TLWs) and receive priority for NCEEP planning and restoration project funds.

The 2003 Yadkin Pee-Dee River Basin Watershed Restoration Plan first identified HUC 03040105081010 (Upper Lanes Creek) as a TLW

(<u>http://www.nceep.net/services/restplans/yadkinpeedee%202003.pdf</u>) and was subsequently updated in 2009

(http://www/nceep.net/services/restplans/Yadkin_Pee_Dee_RBRP_2009_Final_pdf). In 2009 the watershed was characterized by 2 percent impervious surface, 53 percent non-forested buffer, and 44 percent agriculture area with 9 percent of the streams listed as impaired for Aquatic Life by the North Carolina Division of Water Quality (NCDWQ). The 2009 Yadkin Pee-Dee RBRP identified agricultural practices and development impacts as potential stressors within the TLW. The 601 East Stream Restoration Site (hereafter referred to as the "Site") was identified as a stream restoration opportunity to improve water quality and habitat within the Upper Lane's Creek TLW.

The project goals address the stressors identified in the TLW and include the following:

- Reduce water quality stressors originating in and around the project area affecting the project reaches and downstream watercourses, which includes populations of the Savannah Lilliput (Toxolasma pullus) and the Carolina Creekshell (Vilosa vaughiana), both listed species of concern. Specifically, this will involve:
 - a. Reducing turbidity and sediment loading
 - b. Input reductions of nutrients and crop protection chemicals
 - c. Improving thermoregulation
- 2. Improving aquatic habitat quality and diversity within the project reaches
- 3. Improving recruitment of instream fine organic matter (FOM) in the near term and both FOM and large wood in the long term
- 4. Improving terrestrial habitat diversity and quality in the vicinity of project reaches
- 5. Establishing habitat continuity between the reach headwaters and Lanes Creek
- 6. Improving flood flow attenuation and floodplain interaction

The project goals will be addressed through the following project objectives:

Objectives	Relative Support of Stated Goals		
	High	Mod	Low
Restore or enhance reach pattern, dimension, and profile	6,2		3
Stabilize eroding stream banks	1,2		
Install stream structures to maintain grad and improve bedform complexity	2,6	3	
Implement BMP detention devices on lateral agricultural drainages	6	1	
Install a diverse, native riparian buffer	1-5	6	
Remove invasive and/or exotic plant species	4	5	
Secure a protective conservation easement and establish fencing as needed	1-6		

2.0 SITE SELECTION

2.1 Directions to Site

The 601 East Stream Restoration Site is located approximately 10 miles southeast of Monroe and 0.25 miles east of the intersection of Pageland Highway (US 601) and Landsford Road (NC 1005) in Union County, North Carolina. From Charlotte take US-74 E towards Monroe. After approximately 25 miles turn right onto US 601 S/Pageland Hwy, continue on US 601 S for approximately 10 miles then make a slight right onto Landsford Road (NC 1005). The Site is located at the crossing of Landsford Road and Tanyard Branch at latitude 34° 50' 21.62" N and longitude 80° 25' 32.26" W.

2.2 Site Selection

2.2.1 Description

The project stream on the property is named Tanyard Branch which is a tributary to Lanes Creek. The Site is located on predominately agricultural land. The upper reach of the project is a first order stream. The lower reach of the project begins at the junction of two tributaries. The landowner to the northeast of the lower reach utilizes his land for livestock grazing. The livestock on this property is contained by fencing and does not have access to Tanyard Branch.

Historic land use at the Site has consisted primarily of agriculture crop production. Additional land use practices, including the maintenance and removal of riparian vegetation and the relocating, dredging, and straightening of on-site streams have contributed to unstable channel characteristics and degraded water quality.

2.2.2 <u>USGS Hydrologic Unit Code and NCDWQ River Basin Designations</u>

The project area is located within the United States Geological Survey (USGS) Hydrologic Unit 03040105 (Rocky River Basin) of the greater Yadkin Pee-Dee River Basin. The Rocky River Basin covers 1,417 square miles (3,670 square kilometers) and portions of seven North Carolina counties, in addition to areas of South Carolina. The subject stream is mapped as a UT to Lanes Creek (DWQ Stream Index Number 13-17-40-(1)) – identified as Tanyard Branch in this document based on deed records. Lanes Creek is classified as "WS-V". The "WS-V" classification indicates waters that are protected as water supplies which are generally upstream and draining to Class WS-IV waters or waters used by industry to supply their employees with drinking water or as waters formerly used as water supply. These waters are also protected for Class C uses.

Class C waters are protected for uses such as secondary recreation, fishing, wildlife, fish consumption, aquatic life including propagation, survival and maintenance of biological integrity, and agriculture. Secondary recreation includes wading, boating, and other uses involving human body contact with water where such activities take place in an infrequent, unorganized, or incidental manner (NCDWQ).

Tanyard Branch has no NCDWQ stream impairment rating however Lanes Creek is classified as an impacted stream due turbidity, fecal coliform bacteria, and low-dissolved oxygen due to agriculture and pasture land use practices within the watershed. Impaired streams are those streams not meeting their associated water quality standards in more than 10 percent of the samples taken within the assessment period (January 1, 2002 through December 31, 2006) and impacted streams are those not meeting water quality standards in 7 to 9 percent of the samples.

2.2.3 <u>Watershed Characterization</u>

The Site is characteristic of the Piedmont region with moderate rainfall with annual precipitation averaging 45 to 50 inches per year. Elevations within the Site range from 550 feet at the headwaters extent of Tanyard Branch to 500 feet where Tanyard Branch converges with Lanes Creek. The Site encompasses approximately 3,400 linear feet of Tanyard Branch. The drainage area of Tanyard Branch at the culvert at Landsford Road is 0.27 square miles and to the downstream end of the Site is 0.56 square miles. Land use within the watershed consists of primarily agricultural use with some single family residential. Impervious area covers less than 2 percent of the total watershed. Land use changes are not anticipated in the watershed of this headwater stream in the near future as the watershed consists of primarily active agricultural crop production. Low density residential development is a possibility for the watershed due to the sites proximity to US 601.

2.2.4 Physiography, Geology, and Soils

The Site lies within the Carolina Slate Belt system of the Piedmont Geographical Province and is composed of gently sloping terrain with parent material consisting of a Metamudstone and Meta-Argillic metamorphic rock.

The valleys within the Site headwaters are Type II-colluvial valleys, which are moderately steep, gentle-sloping side-slopes. The valley type changes to a Type VIII, a wide alluvial moderate to gentle sloping valley within a well-developed floodplain adjacent to Lanes Creek.

The Union County Soil Survey identifies seven soil types within the Site (Table 1).

Table 1. Soils in the study area.

Soil Series	Mapping Unit	Drainage Class	Hydric Status
Badin channery silt loam	Ва	Well Drained	Non-Hydric
Badin channery silty clay loam	Bd	Well Drained	Non-Hydric
Chewacla silt loam	Ch	Somewhat Poorly Drained	Hydric*
Cid channery silt loam	Cm	Moderately Well Drained	Non-Hydric
Misenheimer-Cid complex	Mh	Moderately Well Drained	Non-Hydric
Tatum gravelly silt loam	Та	Well Drained	Non-Hydric
Tatum gravelly silty clay loam	Tb	Well Drained	Non-Hydric

^{* -} Soils which are primarily nonhydric, but which may contain hydric inclusions

2.2.5 Historical Land Use and Development Trends

Historic aerial photographs of the Site from 1938, 1951, 1969, 1998, 2006, and 2011 were examined. In the 1938 photograph (Figure 5), the southern parcel is moderately vegetated and the stream has been diverted into a farm pond. The northern parcel is clear of vegetation and actively being farmed; and it appears the stream is flowing through its current channel. By 1951 (Figure 6), the stream is still impounded on the southern parcel and vegetation has matured; the northern parcel is still clear of vegetation and actively farmed. The 1969 photograph (Figure 7) is of poorer quality, but one is able to discern the absence of the farm pond. Vegetation on the southern parcel looks similar to 1951; however, on the northern parcel, vegetation has increased in relation to actively farmed areas. The 1998 photograph (Figure 8) shows the most area covered with vegetation of the six photographs. The southern parcel has what appears to be a mature forested buffer on the stream; while the northern parcel has also been allowed to revert to a forested state. At some point between the 1998 photograph and the 2006 photograph (Figure 9), the vegetated buffer on both the southern and northern parcels was removed. The 2011 photograph (Figure 10) is very similar to the 2006 photograph; the upstream erosion of the start of the stream channel is evident from the photograph. Aerial photographs are included in Appendix F.

The historic land use at the Site has consisted primarily of agriculture use. Additional land use practices, including the maintenance and removal of riparian vegetation and the relocating and straightening of on-site streams have contributed to unstable channel characteristics and degraded water quality. Historic wetlands were likely drained in order to maximize agricultural production.

2.2.6 Existing Site Conditions

In order to assess the existing geomorphic conditions data was collected on the channel above Landsford Road in 2013 that included the longitudinal profile, cross sections at 27 locations, pebble counts in the intermittent and perennial Type B reaches and the Type C reach, and soil samples for sieve analysis on bank and point bar locations. Data was collected on the existing stream below Landsford Road that included the longitudinal profile, cross sections at 19 locations on the relic channel and 9 locations on the existing active channel, pebble count data, and soil bank and depositional bar samples for sieve analysis.

Cross section information was collected for the project site in 2008 for an earlier proposal submittal. The intermittent and ephemeral streams at the top of the project were observed to have incised significantly when additional data was collected in 2012. Research was completed to determine the stressor that caused the dramatic change in the stream. Improvements were made to Highway 601 during this time frame. The roadway was widened and storm drainage added during the improvements produced higher volumes of stormwater flows from the road system to Tanyard Branch. Due to the additional stormwater amounts and the lack of vegetation present on the stream banks, the stream channel incised for approximately 500 linear feet. Approximately 50 percent of the incision is located within the ephemeral and 50 percent in the intermittent channel. Evidence of excess sediment wash filling in the downstream channel is visible in a 100 foot stream segment immediately downstream of the incision. The ephemeral,

intermittent, and perennial stream origins were identified in the IRT field review meeting held on January 29, 2013. The comparison of the 2008 and 2012 cross sections have been included in Appendix B.

Reach A includes 215 feet of ephemeral channel that is located directly above the intermittent channel at the top of the reach. This area has experienced severe erosion in the past 5 years and has eroded to a "G" Type channel passing extensive sediment downstream. The average valley slope is 2% and the bank heights extend up to 3.8 feet.

Reach 1 is located at the upper most limit of the project and includes 430 feet of intermittent and 1005 feet of perennial stream. This reach extends just into the existing wood line at the spring house. Reach 1 classifies as a Type G4 stream at the top, a degraded Type C4b in the sediment depositional area, and as a degraded Type B4 stream for the majority of its length. The average valley slope is 2 percent. The bank height ratio ranges from 0.4 in the depositional area to 2 in the severely incised stream segments. The landowner has added field stones at locations along the stream length creating a series of check dams within the incised channel. The stones have effectively trapped some of the sediment that has washed through the system during the past 5 years in which observations have been made. The stream throughout this reach, except for a 200 foot segment, is typically disconnected from the floodplain. The present sediment loads are being routed by the incised channel without significant accumulation of depositional material and the overall profile trend is degradation.

Reach 2 begins inside the wooded area at the spring house. The valley slope reduces to 0.84 percent and it widens out throughout this reach. The stream classification changes to a degraded Type C4/E4 in Reach 2. The stream segment through the woods has good pattern however has banks that are eroding and some vertical instability is present. The stream beyond the woods has been severely impacted by sediment and exotic invasive species. A defined channel is not present through much of this reach. The present sediment loads are not effectively being routed through much of this reach and are accumulating as depositional material.

The stream continues below Landsford Road through a wooded buffer for approximately 1,100 linear feet. The buffer extends from 50 to 100 feet on the western side of the stream. The eastern buffer is limited to an existing width of 10 to 20 feet. The topography rises in elevation at a steep rate to the existing agricultural fields to the west. The floodplain to the east is flat. The existing channel has pattern, connection with the floodplain, and is reasonably stable throughout this area. This segment of stream is not included in the restoration project.

Reach 3 begins at the edge of the wooded area just after the junction of two stream tributaries in which the drainage area approximately doubles. Just below the confluence the stream has been impacted by an existing culvert farm crossing, providing access to farm fields east and west of the stream. Beyond the culvert the active channel has been diverted from its original path and flows north to Lanes Creek. This channel is straight, varies in depth from 2 to 6 feet, and borders the existing agricultural field. A relic

channel is located to the west of the existing pipe crossing. Approximately 200 feet of the old channel has been filled in and is currently under crop production. The average valley slope is 0.67 percent. The relic channel is a degraded Type C, for approximately two thirds of its length that has fairly good access to the stream with bank height ratios from 1 to 1.3. The present sediment loads are being routed by the incised channel with some accumulation of depositional material just downstream of the culvert plunge pool where the channel widens out significantly and a portion of the flow is diverted to the floodplain and relic channel. Cross sections taken in the active channel and the relic channel confirm that a portion of flow is currently being diverted to the relic channel through the floodplain during storm events. The floodplain is lower to the west of the active channel allowing for this flow divergence.

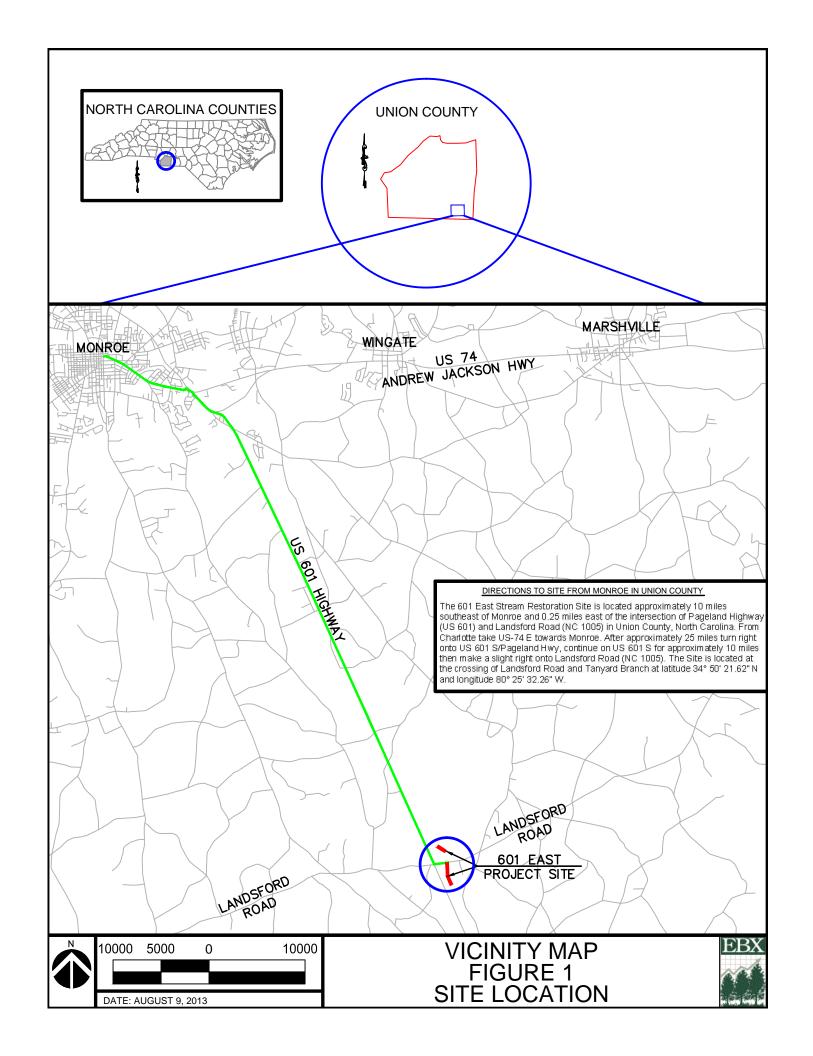
Reach 4 is located in the lower one third of the channel. The valley slope remains at 0.67 percent however the stream becomes increasing incised, Type G, within this reach until it attains a channel depth of 6 feet at the confluence with Lanes Creek. The deeply incised channel has steep banks with limited vegetation. The overall profile trend of this stream segment is degradational.

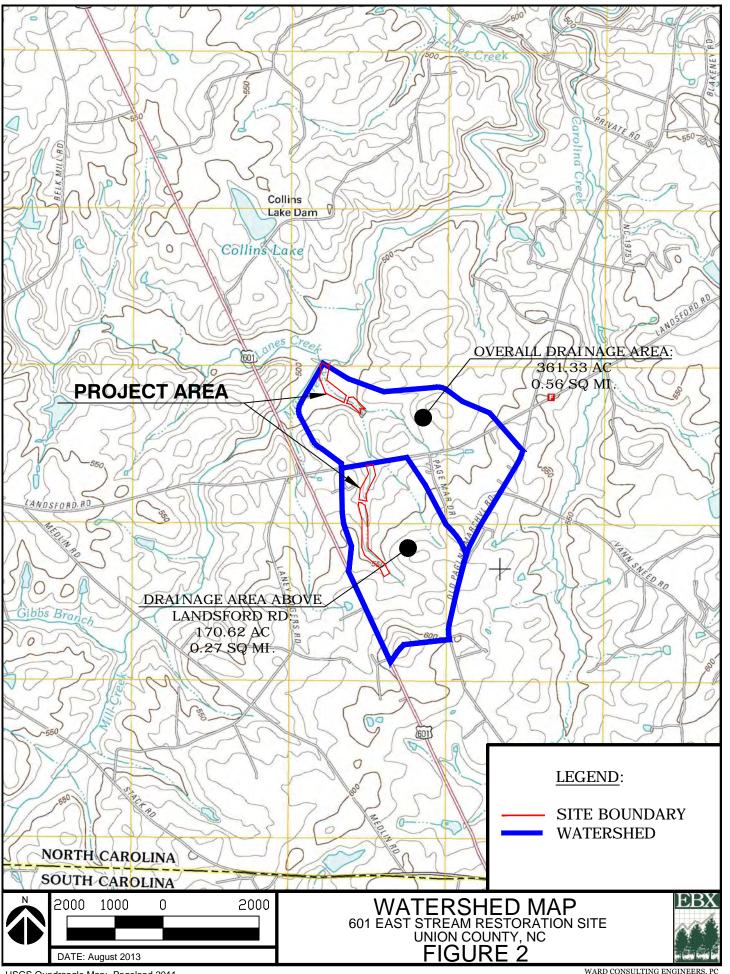
Tanyard Branch contains a very narrow buffer throughout the Site consisting of a mixture of tree species typical of a Piedmont Headwater Forest and Piedmont Alluvial Forest community within Reach 1,transitioning to a Piedmont Alluvial Forest within Reach 2, and continuing within Reach 3 and 4. These communities are located along a very narrow and fragmented riparian buffer along Tanyard Branch throughout the Site. Canopy trees are very sparse throughout consisting of green ash (*Fraxinus pennsylvanica*), red maple (*Acer rubrum*),willow oak (*Quercus phellos*), sycamore (*Platanus occidentalis*), sweetgum (*Liquidambar styraciflua*), and eastern cottonwood (*Populus deltoides*). The subcanopy and shrub layer consisted of black willow (Salix nigra), elderberry (*Sambucus canadensis*), eastern red cedar (*Juniperus virginiana*), silky dogwood (*Cornus amomum*), tag alder (*Alnus serrulata*), silverling (*Baccharis halimifolia*), and Chinese privet (*Ligustrum sinenge*). Chinese privet is the dominant woody species within Reach 3 and 4 of the Site.

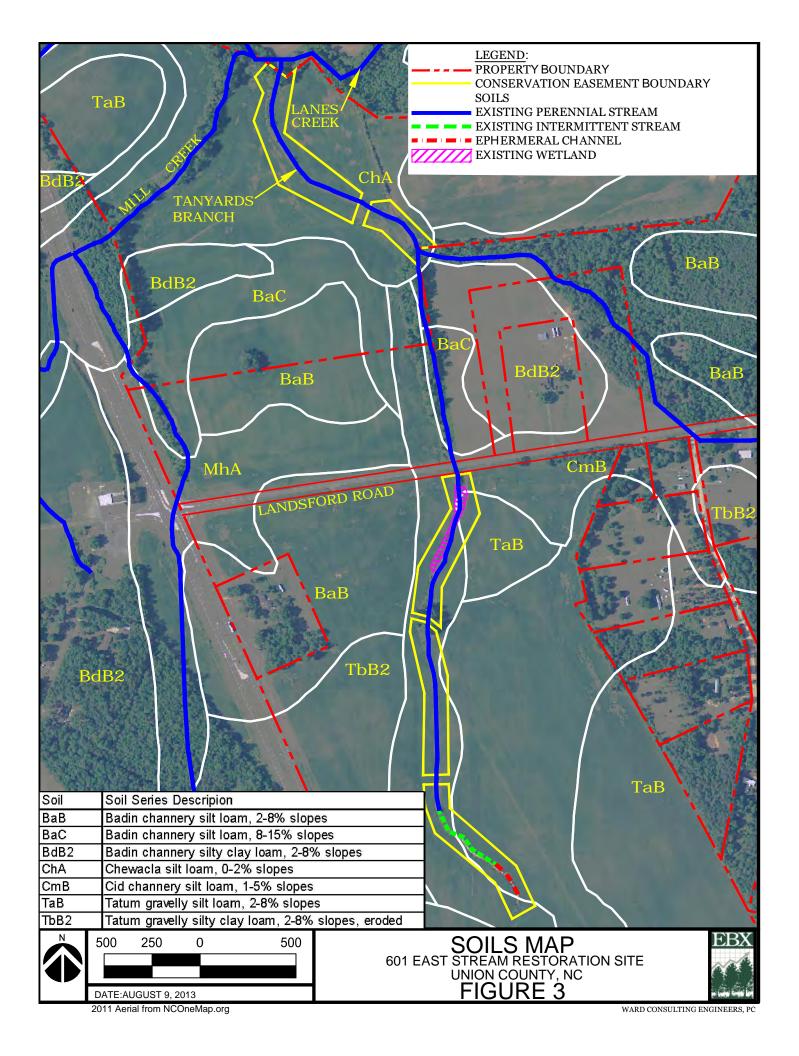
One wetland, a non-tidal freshwater marsh, occurs along Tanyard Branch. Located within Reach 3, this wetland is a small wetland, approximately 0.43 acre that encompasses Tanyard Branch just upstream of Landsford Rd. This wetland is a linear feature of alluvial deposits resultant of upstream channel degradation. Tanyard Branch becomes a braided stream as it enters this depositional area, and then converges back into a defined channel approximately 70 linear feet upstream of Landsford Rd. Vegetation is mostly herbaceous within the wetland having some small trees, such as Black Willow and Red Maple along the margins. Common Cattail (*Typha latifolia*) dominates the herbaceous layer, with Bulrush (*Scirpus cyperinus*), Common Rush (*Juncus effusus*) and Sedges (*Carex* sp.). Parrot feather (*Myriophyllum aquaticum*) an invasive exotic submerged aquatic plant that grows in slow moving water, was ubiquitous throughout Wetland A.

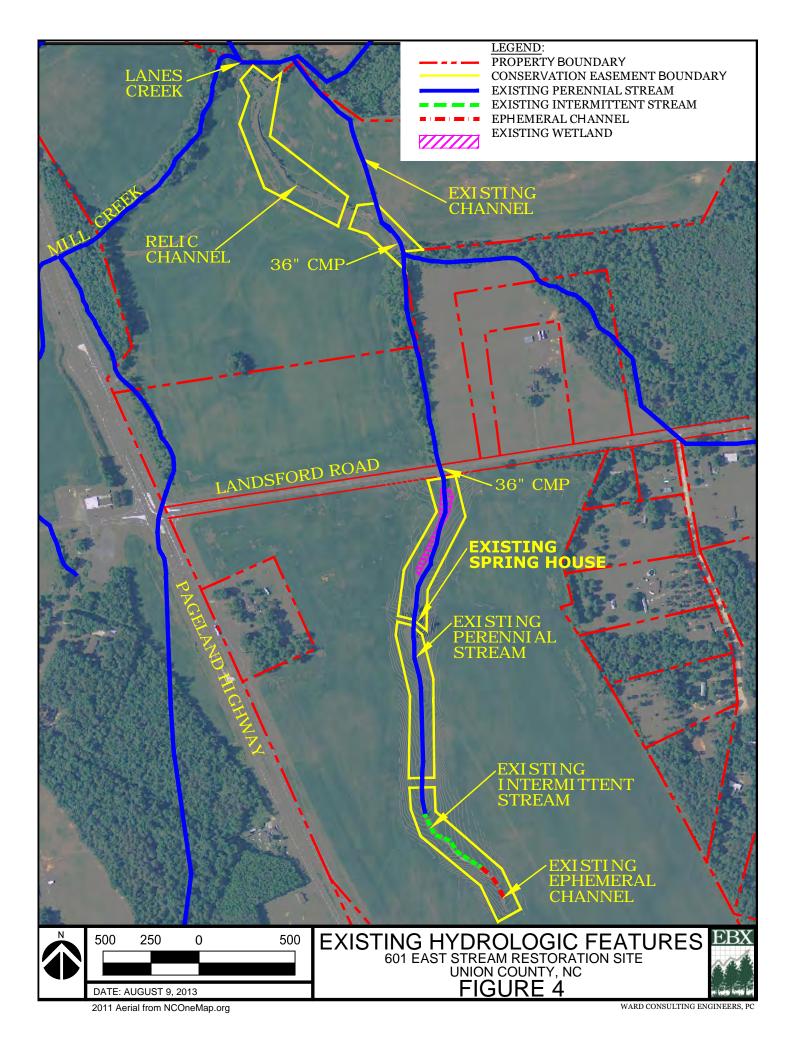
2.3 Project Site Figures

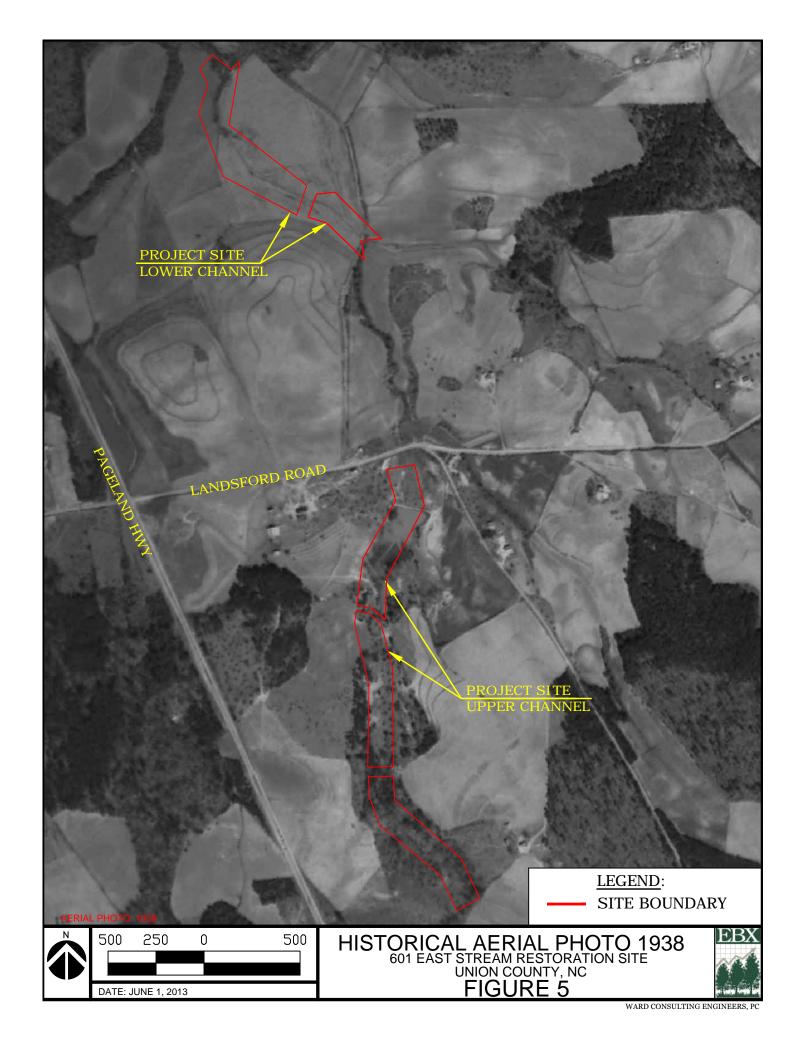
The following figures Project Site Vicinity Map, Project Site Watershed Map, Project site NRCS Soil Survey Map, Existing Hydrologic Features, and Historical Aerial Photos (1938, 1951, 1969, 1998, and 2006) follow.

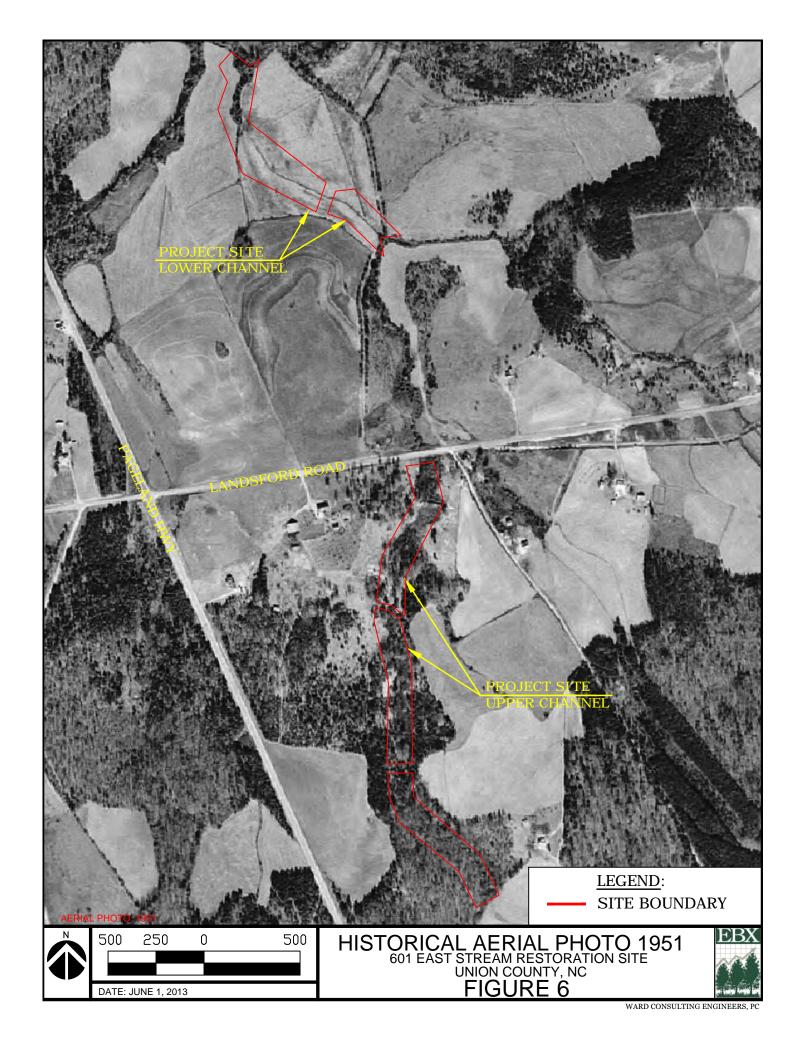


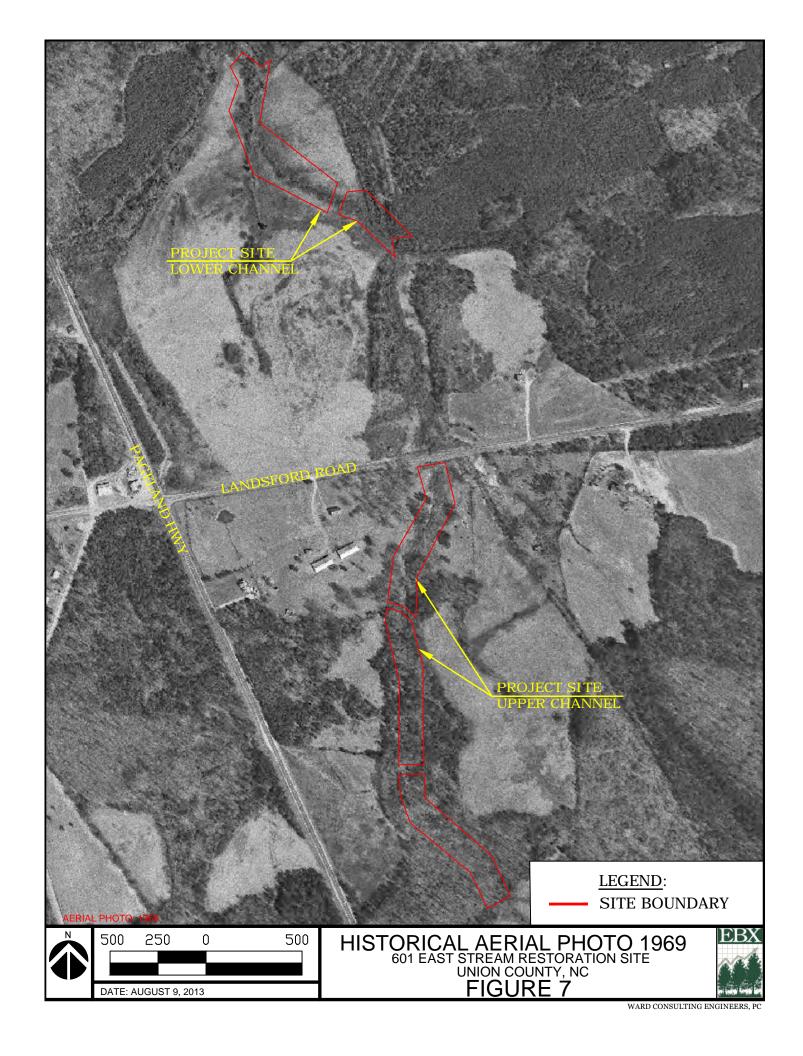


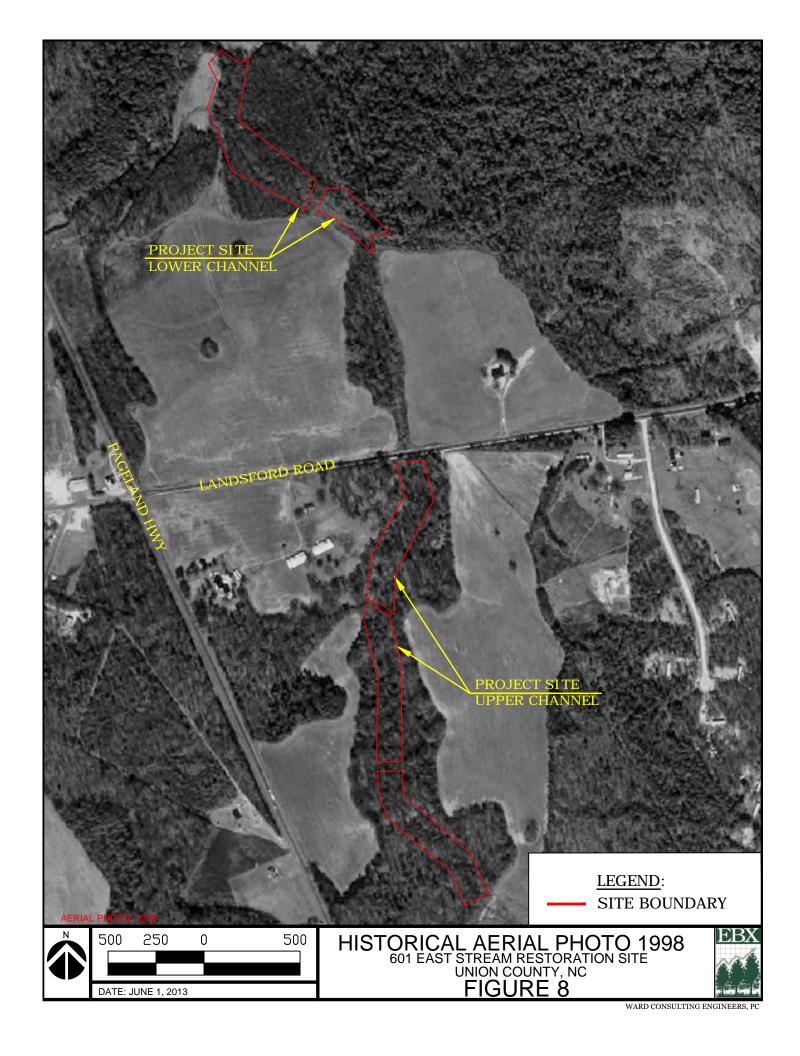


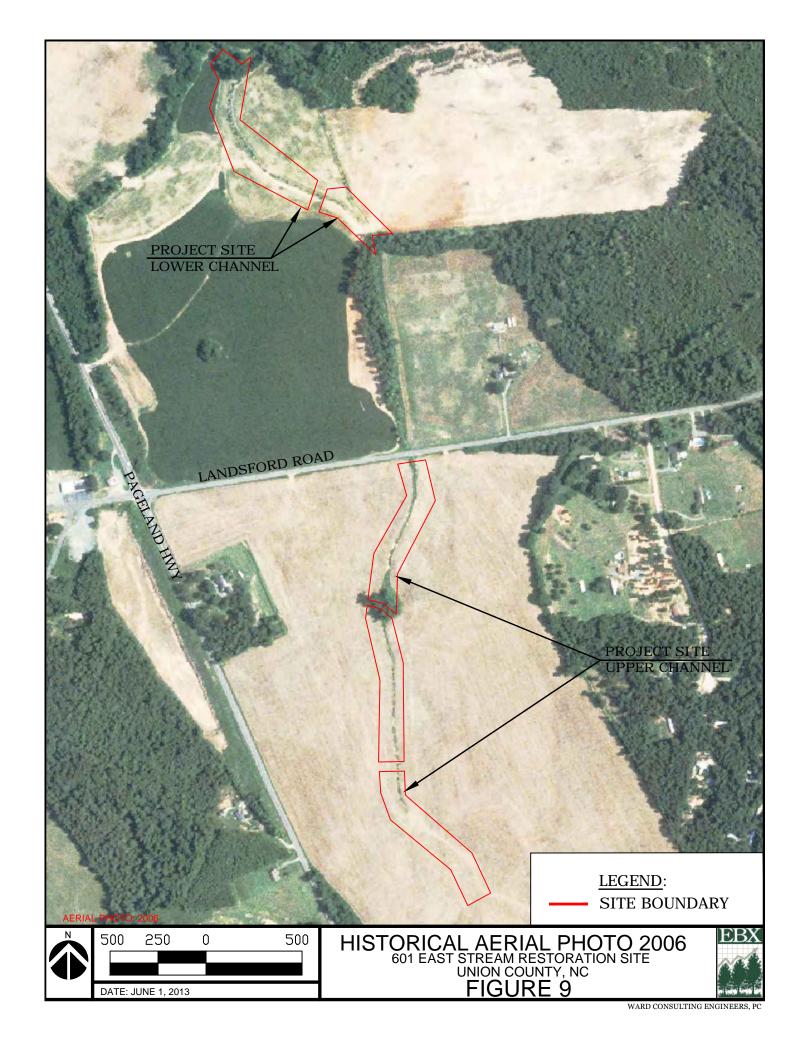












2.4 Project Site Photos

Site Photographs Nov 12, 2012



Photo Point 1. Uppermost head cut top of project- Ephemeral Channel



Photo Point 2. Ephemeral channel in foreground, intermittent channel origin.



Photo Point 3. Origin of perennial stream



Photo Point 4. Stream in woods by spring house.



Photo Point 5. South facing view of old spring house with Tanyard Branch in the foreground.



Photo Point 6. Wetland area undefined channel by Landsford Road.



Photo Point 7. Channel upstream of Landsford Road at culvert.



Photo Point 8. Pipe at outlet at existing Farm Crossing Lower Reach



Photo Point 9. Existing channel at outlet of plunge pool at farm crossing viewing incised channel downstream



Photo Point 10. Head of Relic Channel as viewed from active channel.



Photo Point 11. Relic Channel with Chinese Privet as the dominant vegetation.

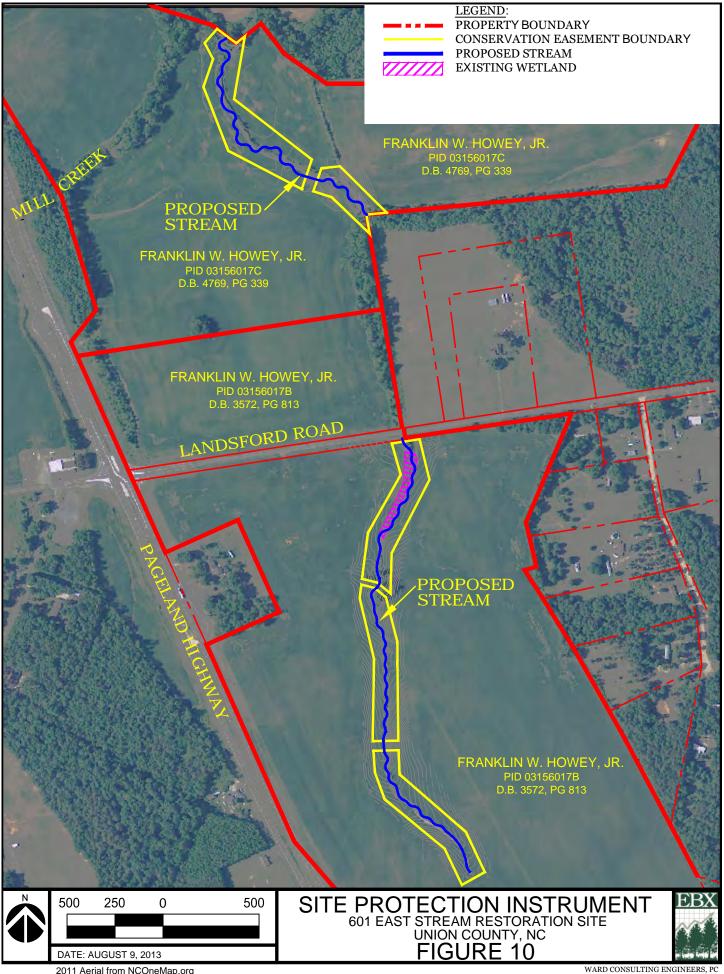
3.0 SITE PROTECTION INSTRUMENT

The land required for the construction, management, and stewardship of this mitigation project includes portions of the following parcels. A copy of the land protection instrument(s) is included in the appendices.

	Landowner	PIN	County	Site Protection Instrument	Deed Book and Page Number	Acreage protected
Parcel A	Franklin W. Howey Jr.	03156017B	Union	Conservation Easement	DB 3572 PG 813	7.76
Parcel B	Franklin W. Howey Jr.	03156017C	Union	Conservation Easement	DB 4769 PG 339	5.02

When available, the recorded document(s) will be provided. If the recorded document(s) are not available, the template documents will be provided.

All site instruments require 60-day advance notification to the Corps and the State prior to any action to void, amend, or modify the document. No such action shall take place unless approved by the State.



4.0 BASELINE INFORMATION

4.1 Project Information					
Project Name	601 East Stream Restoration Site	601 East Stream Restoration Site			
County	Union County				
Project Area (acres)	12.78				
Project Coordinates (latitude and longitude)	34° 50' 21.62" N, 80° 25' 32.26"N				
Project Watersh	ed Summary Information				
Physiographic Province	Piedmont				
River Basin	Yadkin River Basin				
USGS Hydrologic Unit 8-Digit	USGS Hydrologic Unit 14-digit	03040105081010			
DWQ Sub-basin	03-04-14				
Project Drainage Area (acres)	361.33				
Project drainage Area Percentage of Impervious Area	2%				
CGIA Land Use Classification	2.01.01.07 Annual Row Crop Rotation				

4.2 Reach Summary Information

Parameters	Reach 1	Reach 2	Reach 3	Reach 4
Length of reach (LF)	1418	906	1080	Relic Channel
Valley Classification	II	II	VIII	VIII
Drainage area (acres)	109	135	333	359
NCDWQ stream identification score	Intermittent: 19.5 Perennial: 33.5	33.5	33.5	33.5
NCDWQ Water Quality Classification	13-17-40-(1)	13-17-40-(1)	13-17-40-(1)	13-17-40-(1)
Morphological Description (stream type)	G4/B4/C4b	C4/E4/DA	C4/G4	G4
Evolutionary trend (reference channel evolution model used)	G	C/DA	G	G
Underlying mapped soils	Intermittent: Tatum gravelly silty clay loam Perrenial: Cid channery silt loam	Cid channery silt loam, Tatum gravelly silt loam	Chewacla silt loam	Chewacla silt loam
Drainage class	Well Drained	Moderately Well Drained	Somewhat Poorly Drained	Somewhat Poorly Drained
Soil Hydric status	Non Hydric	Non Hydric	Non Hydric	Non Hydric
Slope	2%	0.84%	0.67%	1.25%
FEMA classification	N/A	N/A	N/A	N/A
Native vegetation community	Agriculture along upstream portion of Intermittent channel. The remaining stream buffer within this reach is composed of Willow Oak, Red Maple, River Birch, Black Willow, Elderberry, and Blackberry.	Canopy species include Willow Oak, Black Willow, Red Maple, Sweetgum, Eastern Red Cedar, Tag Alder, and Silky Dogwood. Wetland A is composed of Cattails, spike rush arrow-arum, and duckweed.	Canopy species include Red Maple, Hackberry, Willow Oak, and Sweetgum. The presence of Chinese privet outcompete any shrub and herb layer.	Canopy species include Red Maple, Hackberry, Willow oak, and Sweetgum. The presence of Chinese privet outcompete any shrub and herb layer.
Percent composition of exotic invasive vegetation	0%	50% of Parrot feather	5% of Japanese stilt grass, 80% Chinese privet, and kudzu	80% Chinese privet

Parameters	Wetland 1			
Size of Wetland (acres)	0.43 ac			
Wetland Type (non-	Non-Tidal Freshwater Marsh			
riparian, riparian				
riverine, or riparian non-				
riverine)				
Mapped Soil Series	Cid channery Silt Loam			
Drainage class	Moderately Well Drained to Somewhat Poorly Drained			
Soil Hydric Status	Non-Hydric			
Source of Hydrology	Tanyard Branch headwaters, groundwater, and adjacent runoff			
Hydrologic Impairment	Wetland A formed from accumulating sediments filling the channel resulting in a braided channel system through the wetland.			
Native vegetation community	Herbaceous-Vegetation is domninated by herbaceous vegetation such as Cattail (<i>Typha latifolia</i>), Bulrush (<i>Scirpus cyperinus</i>), Common Rush (<i>Juncus effuses</i>). Some tree species such as Black Willow (<i>Salix nigra</i>), and Red Maple (<i>Acer rubrum</i>) are present in the wetland margins.			
Percent composition of exotic invasive vegetation	95% -The invasive Parrot Feather (<i>Miriophyllum aquaticum</i>) is dominant throughout the wetland where there is standing water.			

4.4 Regulatory Considerations

Regulation	Applicable?	Resolved?	Supporting Documentation
Waters of the United States-Section 404	Yes	To Be Permitted.	
Waters of the United States – Section 401	Yes	To Be Permitted.	
Endangered Species Act	No	Yes	ERTR
Historic Preservation Act	No	Yes	ERTR
Costal Zone Management Act (CZMA)/Costal Area Management Act (CAMA)	No	N/A	
FEMA Floodplain Compliance	No	N/A	
Essential Fisheries Habitat	No	N/A	

5.0 DETERMINATION OF CREDITS

Mitigation credits presented in these tables are projections based upon site design. Upon completion of site construction the project components and credits data will be revised to be consistent with the as-built condition.

	601 East Stream Restoration, Union County EEP Project Number 95756										
	Mitigation Credits										
	Stream	m	Riparia	n Wetland	Non-riparian Wetland		Buffer	Nitrogen Nutrient Offset	Phosphorous Nutrient Offset		
Туре	R	RE	R	RE	R	RE					
Totals	3680										

Project Components Project Restoration -or-Restoration Existing Approach (PI, Component -or-Stationing/Location Restoration Footage or Mitigation Ratio Footage/Acreage PII etc.) Reach ID Equivalent Acreage Buffer Reach A establishment and 5+45 - 7+60215 215 1:5 **Ephemeral** BMP sediment import reduction Reach 1a 336 P1 R 7+60 - 11+10350 1:1 Intermittent Reach 1b 11+10 - 11+95 85 Enhancement E1 85 1:1.5 Intermittent Reach 1c 11+95 - 13+50136 Enhancement E1 155 1:1.5 Perennial Reach 1d 14+00 - 22+00790 P1 R 800 1:1 Perennial Reach 2a 22+00 - 22+4040 Enhancement E1 1:1.5 Perennial Reach 2b 22+80 - 24+00125 Enhancement E1 120 1:1.5 Perennial Reach 2c 24+00 - 31+24669 P1 R 724 1:1 Perennial Reach 3a 80' active channel 43+06 - 46+60 P1 R 368 1:1 Perennial 112' relic channel Reach 3b 47+20 - 53+70502' relic channel P1 R 650 1:1 Perennial Reach 4 P3 R 53+70 - 58+50470' relic channel 480 1:1

Perennial

Component Summation									
Restoration Level	Stream (linear feet)		an Wetland acres)	Non-riparian Wetland (acres)	Buffer (square fo				
		Riverine	Non- Riverine						
Restoration	3372								
Enhancement									
Enhancement I	400	400							
Enhancement II									
Creation									
Preservation/Other	215								
HQ Preservation									
			BMP EI	ements					
Element Location		ation	Purpose/Function		Notes				
FB, LS, S, FS		Ephemeral Channel 5+45 – 7+60		Slowing the water down for settling and filtering excess sediment		Sediment expected from future degradation upstream			

FB, LS, S, FS

BMP Elements
BR = Bioretention cell; SF = Sand Filter; SW = Stormwater Wetland; WDP = Wet Detention Pond; DDP = Dry Detention Pond; FS = Filter Strip; S = Grassed Swale; LS = Level Spread; NI = Natural Infiltration Area; FB = Forested Buffer

6.0 CREDIT RELEASE SCHEDULE

All credit releases will be based on the total credit generated as reported by the as-built survey of the mitigation site. Under no circumstances shall any mitigation project be debited until the necessary DA authorization has been received for its construction or the District Engineer (DE) has otherwise provided written approval for the project in the case where no DA authorization is required for construction of the mitigation project. The DE, in consultation with the Interagency Review Team (IRT), will determine if performance standards have been satisfied sufficiently to meet the requirements of the release schedules below. In cases where some performance standards have not been met, credits may still be released depending on the specifics of the case. Monitoring may be required to restart or to be extended, depending on the extent to which the site fails to meet the specified performance standard. The release of project credits will be subject to the criteria described as follows:

Stream Credits								
Monitoring Year	Credit Release Activity	Interim Release	Total Released					
0	Initial Allocation – see requirements below	30%	30 %					
1	First year monitoring report demonstrates performance standards are being met	10%	40%					
2	Second year monitoring report demonstrates performance standards are being met	10%	50% (60%*)					
3	Third year monitoring report demonstrates performance standards are being met	10%	60% (70%*)					
4	Fourth year monitoring report demonstrates performance standards are being met	5%	65% (75%*)					
5	Fifth year monitoring report demonstrates performance standards are being met	10%	75% (85%*)					
6	Sixth year monitoring report demonstrates performance standards are being met	5%	80% (90*)					
7	Seventh year monitoring report demonstrates performance standards are being met and project has received closeout approval	10%	90% (100%*)					

Initial Allocation of Released Credits

The initial allocation of released credits, as specified in the mitigation plan can be released by the NCEEP without prior written approval of the DE upon satisfactory completion of the following activities:

- a. Approval of the final Mitigation Plan
- Recordation of the preservation mechanism, as well as a title opinion acceptable to the USACE covering the property
- c. Completion of project construction (the initial physical and biological improvements to the mitigation site) pursuant to the mitigation plan; Per the NCEEP Instruments, construction means that a mitigation site has been construction in its entirety, to include planting, and an as-built report that has

- been produced. As-built reports must be sealed by an engineer prior to project closeout, if appropriate but not prior to the initial allocation of released credits.
- d. Receipt of necessary DA permit authorization or written DA approval for projects where DA permit issuance is not required.

Subsequent Credit Releases

All subsequent credit releases must be approved by the DE, in consultation with the IRT, based on a determination that required performance standards have been achieved. For stream projects a reserve of 15% of a site's total stream credits shall be released after two bank-full events have occurred, in separate years, provided the channel is stable and all other performance standards are met. In the event that less than two bank-full events occur during the monitoring period, release of these reserve credits shall be at the discretion of the IRT. As projects approach milestones associated with credit release, the NCEEP will submit a request for credit release to the DE along with documentation substantiating achievement of criteria required release to occur. This documentation will be included with the annual monitoring report.

7.0 MITIGATION WORK PLAN

7.1 Description of Target Stream and Vegetation Communities

Reference reaches were sought to provide a target for design of the proposed streams. Searches were conducted into surrounding watersheds to find suitable references that contained comparable slope, bed material and valley type. A Type C4 reference was located on Underwood Creek a tributary to Little Twelve Mile Creek in Union County. A type B4 reference was located on UT to Richardson Creek a tributary to Rocky River in Anson County. The reference vegetation community data was also collected at the Cold Springs reference site.

7.1.1 Reference Reach

The reference reach was selected to represent the probable configurations for the proposed stream restoration. Detailed geomorphic survey and Level II Rosgen classifications were conducted on both reference reaches. Reference reach data has been included in Appendix C.

7.1.1.1 UT to Underwood Creek Reference

The reference reach is located in an undisturbed segment of UT to Underwood Creek. This area has remained wooded as far back as 1951 as evidenced by the aerial photography that was obtained. The UT to Underwood creek has many characteristics in common with the 601 East watershed including valley type, valley slope, and drainage area of 0.5 square miles.

The UT to Underwood Creek reach is representative of a C4 channel in a mildly sloped valley with a broad floodplain. Bed material, channel slope and valley form of this stream are consistent with the Site and provide reasonable model for the potential channel forms that can be expected at the site. The UT to Underwood Creek reach has a range of D50 of 20.4 millimeters (mm) to 38.1 mm, D84 of 31.5 mm to 90 mm, channel slope of 0.48 percent, width/depth ratio of 7.7 to 15.6, and sinuosity of 1.2. The channel has a wide bankfull width/depth ratio range and a low bank height that allows floodwater to access the floodplain. The profile consists of a well developed riffle pool sequence located at the appropriate locations within the channel. The stream is located in the same physiographic region, the Carolina Slate Belt, as Tanyard Branch. While UT to Underwood Creek classifies as an "E4/C4" type channel, using the range of numbers from the morphological tables that are more closely associated with a "C" type channel, the proposed restoration channels will be designed to fall into the "C" classification.

Discharge and Bankfull Verification

The drainage area at the downstream limit of the reference reach is approximately 0.43 square miles. The estimated bankfull discharge is approximately 40 cubic feet per second (cfs). The discharge was estimated from eleven field cross sections taken along the channel. Bankfull was located at the top of the existing channel which is at the existing floodplain elevation. Bankfull verification on UT to Underwood Creek was completed with a comparison of field surveyed stream cross sections for typical bankfull

width, area, depth, and discharge relationships. The watershed predicted discharges were compared with the bankfull channel capacities generated from field cross sections for verification. The Rural Piedmont Curves developed by the North Carolina State University (NCSU) Water Quality Group were used to verify acceptable limits of morphological characteristics based on a hydro-physiographic region and drainage area. UT to Underwood Creek's average cross sectional values for bankfull area, width, depth and discharge fell within the confidence limits on the North Carolina Rural Regional Curves

Channel Stability Assessment

Visual observations of UT to Underwood Creek reference show that the stream has adequate root depth and density, moderate bank slopes, low bank heights and good vegetative surface protection. This indicates that the creek has low bank erosion potential degrades slowly and contributes little sediment to the stream waters.

Limited Reference Reach

Through the course of conducting the reference reach searches, several streams were identified as possessing qualities of stability and natural form. However these reaches were determined to not be suitable references for the project due to differences in stream type, valley form, or valley slope.

Reference Vegetation Community

Plant community classifications follow those presented by Schafale and Weakley (1990) where possible. The dominant flora observed, or likely to occur, in each community are described and discussed. Scientific nomenclature and the common names (when applicable) are provided. Plant taxonomy typically follows (Weakley 2008). All subsequent references to the same organism will include the common name only. Published range distributions and habitat analysis are used in estimating flora expected to be present within the project site.

The vegetative community species composition is similar to that of the Piedmont Alluvial Forest located within the conservation easement. The canopy is composed of tree species including but not limited to green ash, sweetgum, red maple, red elm, and southern hackberry. Subcanopy and shrub species observed include ironwood (*Carpinus caroliniana*) saplings of red maple and sweetgum. This community has a dense shrub layer dominated by Chinese privet. Herbaceous species observed in this community include the invasive species, Japanese honeysuckle (*Lonicera japonica*).

7.1.1.2 UT to Richardson Creek

The reference reach is located in an undisturbed segment of UT to Richardson Creek. This area has remained wooded as far back as 1951 as evidenced by the aerial photography that was obtained. The UT to Richardson Creek has many characteristics in common with the 601 East watershed including valley type, valley slope, and drainage area.

The UT to Richardson Creek reach is representative of a B4/C4b channel in a moderately sloped valley with a narrow constrained floodplain. Bed material, channel

slope and valley form of this stream are consistent with the Site and provide reasonable model for the potential channel forms that can be expected at the Site. The UT to Richardson Creek reach has a range of D50 of 18.6 mm to 28.9 mm, D84 of 61.3 mm to 64.8 mm, channel slope of 1.8 percent, width/depth ratio of 8 to 17, and sinuosity of 1.16. The channel has a high bankfull width/depth ratio range and a low bank height that allows floodwater to access the floodplain. The profile consists of a well developed riffle pool sequence located at the appropriate locations within the channel. The stream is located in the same physiographic region, the Carolina Slate Belt, as Tanyard Branch.

Discharge and Bankfull Verification

The drainage area at the downstream limit of the reference reach is approximately 0.15 square miles. The estimated bankfull discharge is approximately 27 cfs. The discharge was estimated from twelve field cross sections taken along the channel. Bankfull was located at the top of the existing channel which is at the existing floodplain elevation. Bankfull verification on UT to Richardson Creek was completed with a comparison of field surveyed stream cross sections for typical bankfull width, area, depth, and discharge relationships. The watershed predicted discharges were compared with the bankfull channel capacities generated from field cross sections for verification. The Rural Piedmont Curves developed by the North Carolina State University (NCSU) Water Quality Group were used to verify acceptable limits of morphological characteristics based on a hydro-physiographic region and drainage area. UT to Underwood Creek's average cross sectional values for bankfull area, width, depth and discharge fell within the confidence limits on the North Carolina Rural Regional Curves.

Channel Stability Assessment

Visual observations of UT to Richardson Creek reference show that the stream has adequate root depth and density, moderate bank slopes, low bank heights and good vegetative surface protection. This indicates that the creek as low bank erosion potential degrades slowly and contributes little sediment to the stream waters.

Limited Reach Reference

Through the course of conducting the reference reach searches, several streams were identified as possessing qualities of stability and natural form. However these reaches were determined to be not suitable references for the project due to differences in stream type, valley form, or valley slope.

Reference Vegetation Community

Plant community classifications follow those presented by Schafale and Weakley (1990) where possible. The dominant flora observed, or likely to occur, in each community are described and discussed. Scientific nomenclature and the common names (when applicable) are provided. Plant taxonomy typically follows (Weakley 2008). All subsequent references to the same organism will include the common name only. Published range distributions and habitat analysis are used in estimating flora expected to be present within the project site.

A plant community survey was performed within the forested community along the Tanyard Branch downstream of Landsford Rd where a stream buffer is present. This

small stream plant community, common to the Piedmont region, is located within what closely resembles a Piedmont Alluvial Forest as described by Schafale and Weakley (Draft May 2012). Canopy species observed included sycamore, hackberry, red maple,river birch, green ash, eastern red cedar, willow oak, and tulip poplar (*Liriodendron tulipifera*). Subcanopy species included American holly (*Ilex opaca*), iron wood, and Chinese privet. Herbaceous species included were sparse consisting mostly of Japanese honeysuckle. The Piedmont Alluvial Forest community proposed for Reach 3 and 4 will be modeled after this community. The Piedmont Headwater Forest community proposed for Reach 1 and 2 will be modeled after typical species expected to occur within these communities and the native woody species already observed along Tanyard Branch within these reaches. Canopy species typical of a Piedmont Headwater Forest consist of willow oak, red maple, sweetgum, common elderberry, ironwood, and white oak, all of which were observed within Reach 1 and 2.

7.2 Design Narrative

7.2.1 Restoration Approach

Tanyard Branch is divided into an ephemeral channel Reach A and four (4) Intermittant or Perennial numbered (1-4) reaches for design with two reaches above Landsford Road and two reaches below. Above Landsford Road the stream valley changes from a Type B to a Type C stream. The ephemeral channel Reach A is located at the top of the project. The ephemeral channel is 215 linear feet in length and improvements include BMPs and buffers to prevent future erosion and sediment input from the existing roadway drainage stressor. Reach 1 is located is the first segment below the ephemeral channel and Reach 2 begins in the woods adjacent to the spring house to Landsford Road. Tanyard Branch below Landsford Road begins as a Type C channel and then changes to a Type B channel in the lower one third of its length with a Priority III restoration approach to transition the stream to the much lower elevation of Lanes Creek.

A concern with the project in the headwater areas was the stability of the ephemeral channel and the extensive erosion that had occurred in the last 5 years due to recent roadway improvements in the watershed. Additionally upstream of the proposed buffers the land will continue in agricultural crop production. The project approach for the ephemeral stream, Reach A, is to stabilize the area from future incision with a series of energy dissipaters to provide vertical stability and as well as provide sediment settling capacity for anticipated future sediment import from continued ephemeral channel erosion outside of the conservation easement. Two hundred and fifteen feet (215') of ephemeral channel has been included in the design. This channel length will have 50 foot vegetative buffers restored along its length and will be included within the conservation easement. A dense planting of shrubs along with trees on the outside and around the BMP's on the ephemeral section of Reach 1a will be provided. Shrubs will be used to attenuate sediment.

Based on surveyed cross sections of the incised channel and an assumed predegradation top of bank elevation a sediment loss volume of 167 tons was estimated to have occurred along 335 feet of channel length between 2008 and 2010 at the top of the stream. A series of five (5) stormwater BMP basins have been designed throughout the ephemeral channel reach to detain future sediment moving through the system. The basins have a total capacity to hold 206 tons of sediment. After the initial degradation within this area between 2008 and 2011 occurred, significant sediment loss was not observed in 2012 or 2013. It is anticipated that the due to the continued farming of the land outside of the conservation easement that the draws to the south and east of the restoration project will continue to introduce excess sediment to the stream. It is not anticipated that the sediment loss will be as significant as the degradation that occurred between 2008 and 2010 due to the observations that were made in 2012 and 2013. The designed basins have ample storage capacity to capture sediment and provide ground water recharge as water is stored and allowed to drain into the soils below upstream of the intermittent channel.

A Mitigation ratio of 1:5 has been requested for the 215 linear feet of channel. The improvements in the ephemeral channel add to the functional uplift of the project, provide additional buffer to adjacent agricultural land, and will reduce sediment import to the downstream restored stream. The buffers and sediment reduction will reduce the amount of pesticide and fertilizers entering the stream.

Several draws input drainage from the agricultural fields into the stream along the length. Depressed areas at each draw will be excavated to create diffuse sheet flow over an extended rim of the depression. These draws do not currently support wetlands. The sheet diffused flow will have reduced velocities and aid in preventing rills within the conservation easement to the new channel. The recommended approach is for a combination of restoration and enhancement of reaches 1 & 2 and full restoration of reaches 3 & 4.

Reach 1 will feature Priority 1 restoration and enhancement Level 1. Reach 1 will be reconstructed as a Priority I restoration with a B4 stream. A priority one is appropriate for this design stream type "B" as the proposed design will raise the channel to reconnect the stream with the current floodplain. A "B" type stream is appropriate for this valley slope. This will provide for the construction of the proper cross sectional geometry, reducing stress on the banks and eliminating bank scour. In addition the bed will be stabilized with constructed functional riffles. Riffles constructed from rock materials supplemented with native gravel and cobble materials will provide immediate habitat features and functional lift. The upper 350 feet of Reach 1 is intermittent. The enhancement E1 portion of Reach 1 includes 290 total linear feet of stream that is currently connected to the floodplain and will be enhanced with the correct stream pattern and dimension. Additionally a 50 foot exclusion for a piped farm crossing of the stream is located within Reach 1.

Reach 1 has been broken down into the following components. Reach 1a is a 350 foot segment to be restored as a P1 restoration approach. Reach 1b is an 85 foot segment of intermittent stream that is currently connected to the floodplain where enhancement E1 is proposed. The perennial stream begins at Reach 1c. This reach includes 155 feet of stream which is currently connected to the floodplain where enhancement E1 is

proposed. Reach 1d is an 800 foot segment of perennial channel length with a P1 restoration approach.

Reach 2 begins where the valley flattens out and becomes broad and therefore a C4 stream type is proposed for this reach. The upstream segment of Reach 2 is located in an existing wooded area of the stream. Enhancement E1 is proposed for 200 linear feet through the wooded area in which the stream cross section and vertical alignment will be adjusted within the existing stream pattern. A forty (40) foot easement exclusion is proposed with in the E1 portion of Reach 2 for an existing spring house that is located adjacent to the stream. The spring house provides water to the residence located at 6915 Pageland Hwy owned by Mary C. and Don E. Taylor Pin Number 03156017A, DB 3572, PG 810. Therefore underground electric and water distribution lines are located within this exclusion area. Reach 2a includes 40 feet of stream enhancement E1 below Reach 1d and above the spring house exclusion. Reach 2b includes 120 feet of enhancement E1 below the spring house exclusion. Priority I restoration is proposed for the remaining 724 linear feet of this reach. This reach has been identified as 2c and it extends to Landsford Road. The stream in Reach 2c has been located adjacent to the existing wetlands that have formed in the existing depositional area. The proposed restoration will preserve the majority of the wetlands and improve sediment transport. A 10 foot exclusion has been provided between the conservation easement and right-ofway on Landsford Road for future roadway expansion.

Reach 3 begins below an existing wooded stream segment approximately 1,200 linear feet below Landsford Road. This reach starts just below the confluence of Tanyard Branch and a tributary that approximately doubles the drainage. Reach 3 is proposed as a C4 stream. The stream will be reconnected to the relic channel on the Site. Through this restoration the stream will placed into its historical location and removed from the agricultural ditch location that was constructed on the property. The issue affecting the ecological function on this reach is the extreme topographic separation of Tanyard Branch from the adjacent floodplain. In order to reconnect Tanyard Branch with the contiguous natural terrain and improve floodplain groundwater hydrology, a Priority I approach is recommended for a distance of 1078 linear feet. A 60 foot easement exclusion is proposed within this stream length for a farm crossing. Reach 3 has been broken into two segments; Reach 3a includes 368 feet above the farm crossing exclusion and Reach 3b 650 feet below. The existing channel below the proposed diversion into the relic channel will be filled for approximately 250 feet to accommodate the new stream alignment and provide farming access to the eastern half of the property. The remaining channel will remain open and in its existing condition.

Reach 4 includes the last 480 linear feet of stream in the lower reach. A Priority 3 restoration approach as a Type B4 stream is proposed for Reach 4. To improve the transition of the stream to the lower elevation of Lanes Creek and overall channel stability the floodplain will be graded to create a confined valley. The restoration will address the degraded conditions of severe channel incision, unstable banks, and improper channel dimensions which are negatively affecting stream function. A Priority 3 approach will be required to convert the existing G channel to a B Type stream.

7.2.2 Restoration Method

Restoration of Type C4 streams will consist of constructing a moderate to high sinuosity stream with a moderate to high width-depth ratio (13 to 14) and a riffle-pool bed profile that will access the floodplain at bankfull flows. Restoration of Type B4 streams will consist of constructing a low to moderate sinuosity (1.1 to 1.17) stream with a moderate width-depth ratio (13 to 16) that accesses the floodplain at greater-than bankfull flows. For streams with average channel slopes from 1.2 to 4 percent the bed profile form is in a range that is transitioning from riffle-pool morphology at the lower slopes to step-pool morphology at the steeper slopes. The profile for Tanyard Branch is at the lower end of the slope range and therefore is proposed as riffle-pool morphology. Exploration for buried bed material will be conducted in proximity of the channel work to harvest available bed material for reuse in the constructed channel. It is anticipated that the existing bed material is insufficient for the proposed work and therefore will be supplemented with off-site material or material quarried on site of appropriate size.

Constructed riffles will primarily be used to provide vertical stability to the channel, assist in maintaining, riffle, run and pool features and to provide habitat. In an effort to minimize rock used for the project constructed riffles were divided into three groups; Class I, Class II, and Stone & Log riffles. Class II riffles have the largest stone and are used in limited areas that have the highest velocities and shear stresses. Class II riffles are also proposed for Reach 4 that is a Priority 3 Type "B" channel transitioning Tanyard Branch to Lanes Creek. Class I riffles were used primarily in the upper reach Type "B" channel. The stone and log constructed riffles are primarily used in the Type "C" channel where lower velocities and shear stresses were predicted. This stone and log riffle design was used to reduce the rock in the channel and introduce more wood into the design. The "C" Type channels also are adjacent to wetter floodplains that will help in preserving the wood within the riffle structure. The riffle material was selected based on the shear stresses obtained in the HEC-RAS analysis. Within the stream length the shear stress resulted in numbers that required a larger diameter rock to hold the vertical profile at riffle locations than is present in the adjacent medium gravel soils. Additionally material of this size is not readily available as sediment import into the channel in this headwater stream to develop the riffles. Therefore to hold the vertical profile of the restored stream larger stone is required to be added at the riffle locations for long term stability as shown on the plans.

Single wing log vanes will be used to shift the flow away from the outside banks on selected meander bends. Trees will be harvested onsite will be used in the log structures. Brush-toe structures will be installed in the perennial stream outside of selected meander bends to provide bank stability, increase bank roughness, and provide aquatic habitat. Rock toe and grade control structures will be used in the ephemeral channel and intermittent stream segments to provide bank and bed stability. A rock toe is proposed in these reaches due to the concern of wood material rotting away too quickly without continual submergence in water. Small diameter (less than 6") woody plants suitable for transplanting will be harvested on-site where available.

Earthwork activities will include excavation of the proposed channel, partial or complete backfilling of existing channels, and the creation of a wider valley for Priority 3

restoration in Reach 4. Grading work is designed to tie into the natural landscape. During construction, wetland areas will be protected from impact outside of the channel construction area.

Farm crossings will be designed with oversized pipe so that the pipe will be buried below the bed to the channel to allow bed material to pass through the pipe. A boulder grade control structure will be placed downstream of the pipe to hold the low water surface just above the outlet and allow for aquatic passage.

All disturbed areas will be stabilized with temporary and permanent seed and covered with straw or mulch. Live stakes will be installed on the stream banks in accordance with the planting plan and the entire conservation easement will be planted with bare root seedlings. Plantings will be in accordance with the planting plan included in Appendix D.

7.2.3 Data Analysis

Hydraulic and Hydrologic Analysis

A hydrologic analysis was preformed to quantify the bankfull flows and flood flows of the watershed for the upper and lower reaches. Field cross sections were taken at 18 locations in Reach 1, 10 locations in Reach 2, 9 locations in Reach 3 and 8 locations in the relic channel. The existing cross sections and the existing stream longitudinal profile of the channel thalweg and water surface slope were evaluated to determine bankfull elevations and discharges at each location based on field indicators. A bankfull elevation and slope was then set based on the field cross section data. The cross sections and slope were then adjusted to obtain a convergence on discharge predictions and morphological parameters.

Table of Bankfull Data from Collected Field Cross Section Data (Selected Sample Data Cross Sections)

Station	Wbkf	Abkf	dbkf	Q (cfs)
Reach 1				
8+66	7.21	4.82	0.67	24.3
9+90	10.56	5.76	0.55	25.0
11+17	19.4	8.1	0.42	21.7
12+11	42.5	14.53	0.32	28.4
12+84	19	12.89	.0.21	23.7
13+8	20.4	8.8	0.43	21.5
14+50	16.4	9.05	0.55	25.9
16+80	18.9	9.1	0.48	23.3
21+42	6.76	5.91	0.87	24.1
Reach 2				
22+52	8.1	10.7	1.33	26.0
27+96	29.3	22.8	1.78	26.9
30+58	18.89	12.6	0.67	29.6
Reach 3 & 4				
41+39	11.08	15.75	1.42	54.7
43+10	15.64	19.4	1.23	64.8
45+00	15.56	14.53	0.93	59.0
3+80 Relic	11.3	13.5	1.2	50.5

The USGS regional Regression equations for the NC Rural Piedmont hydrologic area were calculated for bankfull data and the Piedmont Regional Curve Data was obtained and compared to the field morphological data. The field discharges were slightly lower than the regional curve average values but compared within 80-90% of the regional curve data and within the confidence limits. The regression equations over predicted the discharges obtained from field data for the watershed.

Design Discharge Analysis Comparisons

Reach 1	Field Morph Data	Regional Curve Data	Regression Equation (1.5- 2yr)	Design Discharge
Q Avg (cfs)	23.67 (18.7–28.4)	23 (8-80)	32-38	24
Reach 2				
Q Avg (cfs)	24 (12-29.6)	29 (9-90)	39-45	26
Reach 3 & 4				
Q Avg (cfs)	54.7	56-60 (18-180)	76-90	55

Discharges were determined at 5 locations in the watershed for the Bankfull, 2xBankfull, 2 year, 5 year, 10 year, and 100 year storm events for input into the HEC-RAS model as shown in the table below.

Table of HEC-RAS Discharges

Upper Reach							
Drainage			2 x	2-	5-	10-	100-
Area (Acres)	Discharge point of interest location	Bankfull	Bankfull	Year	Year	Year	Year
36.2	At beginning of perennial stream	22	44	30	57	81	195
51.44	Above pump house	24	48	38	72	102	242
65.5	At head of Reach 2	26	52	45	84	120	282
84	At Landsford Road	33	66	54	100	140	328
Lower Reach							
175	At end of project	55	110	90	163	227	518

The proposed restored stream conditions were analyzed by creating a HEC-RAS model to reflect the proposed channel geometry, slope, and bed form features. Cross sections were established at all head of riffle, end of riffle, and center of pool locations in the model. The roughness coefficients for the channel were set to reflect anticipated future roughness coefficients. The HEC-RAS model was used to provide assistance in the analysis of sediment transport, verify bankfull flow capacity, determine flood flow conditions for large storm events, and confirm that no hydrologic trespass will occur on adjacent properties. The output files from the proposed HEC-RAS model are included in Appendix C.

7.2.4 Sediment Competence Analysis

Data Collection for sediment competence included riffle pebble counts and bulk samples collected on point bars. The bed material consists of a mix of sand and gravel. Pebble counts taken from the top of the stream to the wooded area in the upper reach reflect the sand that has moved out of the incised intermittent stream segment into the perennial stream below. The material in the intermittent stream reflected a 10% sand and 90% gravel mix. The perennial stream below showed a much higher sand

component, 40%, reflecting recent sediment import from the degraded upstream channel.

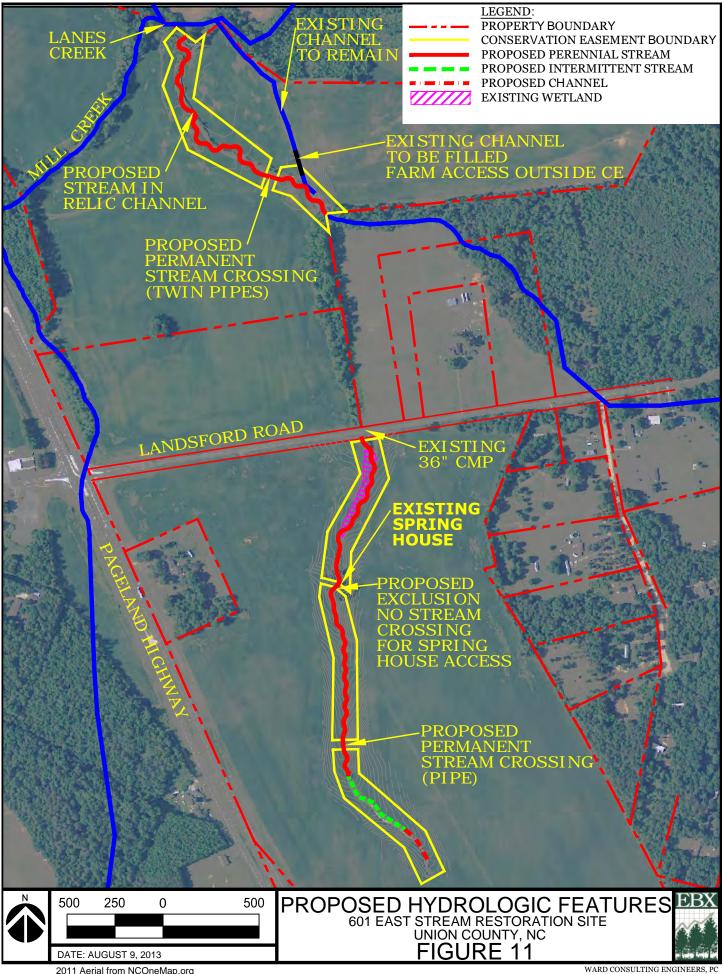
Critical dimensionless shear (Tc*) of 0.035 was calculated using the Andrew's equation (1984). The threshold particle size based on the maximum particle size collected from field point bar samples was a 2 inch (very coarse gravel) particle. The proposed channel depth of flow and water surface slopes were designed to move the threshold particle based on the calculated dimensionless shear stress.

7.2.5 <u>Sediment Capacity Analysis</u>

Bank bulk samples were collected and analyzed for bank material composition to gain a better understanding of the native soils and particle sizes that may be transported to the stream. The samples were taken at two locations in the upper reach and one location in the lower reach. The samples were consistent with a composition of approximately 10% sand, 30% fine gravel, 40% medium gravel and 10% coarse-very coarse gravel.

Tanyard Branch is located at the top of the watershed, and has a low sediment supply and therefore sediment transport was not a significant concern in the design. The soils in the watershed are primarily silt loam. The major import of soils to the stream is through agricultural use of the adjacent land and the buffers will filter much of these sediments. The ephemeral channel has been designed with components to prevent future erosion as well as to trap sediment that may continue to be imported upstream from the recent highway improvements and agricultural operations.

A HEC-RAS model was built to assess the shear stress and stream power of the design for both the upper and lower reaches. Generally the proposed condition model shows a slight decrease in stream power in the larger storm return periods. The decrease in stream power is to be expected in the larger storm events due to the increase in channel width/depth ratio. The stream power values however are sufficiently high to transport the sand/fine gravel particles which constitute the main wash load component. The model results show that the velocities, shear stresses, and stream power are adequate to transport sand and gravel particles. Shear stress and velocities produced by the model were additionally used to size the proposed constructed riffle materials to resist movement. The riffles were sized typically for the 10 year storm event and at critical locations for the 100 year return period. Reach 4 constructed riffles were sized solely for the 100 year storm event. The HEC-RAS model output is included in Appendix C.



8.0 MAINTENANCE PLAN

EBX, NCEEP's full delivery provider, shall monitor the site on a regular basis and shall conduct a physical inspection of the site a minimum of once per year throughout the post-construction monitoring period until performance standards are met. These site inspections may identify site components and features that require routine maintenance. Routine maintenance should be expected most often in the first two years following site construction and may include the following:

Component/Feature	Maintenance through project close-out
Stream	Routine channel maintenance and repair activities may include securing of
	loose coir matting and supplemental installations of live stakes and other
	target vegetation along the channel. Areas where stormwater and floodplain
	flows intercept the channel may also require maintenance to prevent bank
	failures and head-cutting
Wetland	Routine wetland maintenance and repair activities may include securing of
	loose coir matting and supplemental installations of live stakes and other
	target vegetation along the channel. Areas where stormwater and floodplain
	flows intercept the channel may also require maintenance to prevent scour.
Vegetation	Vegetation shall be maintained to ensure the health and vigor of the targeted
	plant community. Routine vegetation maintenance and repair activities may
	include supplemental planting, pruning, mulching, and fertilizing. Exotic
	invasive plant species shall be controlled by mechanical and/or chemical
	methods. Any vegetation control requiring herbicide application will be
	preformed in accordance with NC Department of Agriculture (NCDA) rules and
	regulations.
Site Boundary	Site boundaries shall be identified in the field to ensure clear distinction
	between the mitigation site and adjacent properties. Boundaries may be
	identified by fence, marker, bollard, post, tree-blazing, or other means as
	allowed by site conditions and/or conservation easement. Boundary markers
	disturbed, damaged, or destroyed will be repaired and/or replaced on an as
	needed basis.
Utility Right-of-Way	Utility rights-of-way within the site may be maintained only as allowed by
	Conservation Easement or existing easement, deed restrictions, rights of way,
	or corridor agreements.
Ford Crossing	Ford crossings within the site may be maintained only as allowed by
	Conservation Easement or existing easement, deed restrictions, rights of way,
	or corridor agreements.
Road Crossing	Road crossings within the site may be maintained only as allowed by
	Conservation Easement or existing easement, deed restrictions, rights of way,
	or corridor agreements.
Beaver Management	Beaver activity will be monitored and removed on an as needed basis.
Stormwater Management Device	Storm water management devices will be monitored and maintained per the
	protocols and procedures defined by the NC Division of Water Quality Storm
	Water Best Management Practices Manual.

9.0 PERFORMANCE STANDARDS

Performance standards shall comply with the Ecosystem Enhancement Program Monitoring Requirements and Performance Standards for Stream and Wetland Mitigation Dated November 7, 2011. (Section IV C.)

Morphologic Parameters and Channel Stability

Restored and enhanced streams should demonstrate morphologic stability to be considered successful. Stability does not equate to an absence of change, but rather to sustainable rates of change or stable patterns of variation. Restored streams often demonstrate some level of initial adjustment in the period that follows construction and some subsequent change/variation is also to be expected. However, the observed change should not be unidirectional such that it represents a robust trend. If some trend is evident, it should be modest or indicate migration to another stable form. Annual variation is to be expected, but over time this should demonstrate equilibrium on the reach scale with the maintenance of or even a reduction in the amplitude of variation. Lastly, all of this must be evaluated in the context of hydrologic events to which the system is exposed and the design type/intent (i.e. threshold versus free form alluvial channels).

Dimension

General maintenance of a stable cross-section and hydrologic access to the floodplain features over the course of the monitoring period will generally represent success in dimensional stability. However, some change is natural and expected and can even indicate that the design was successful and appropriate for the hydrologic and sediment regime. Examples include depositional processes resulting in the development of constructive features on the banks and floodplain such as an inner berm, a slightly narrower channel, modest natural levees, and general floodplain deposition.

For stream dimension, cross-sectional overlays and key parameters such as cross-sectional area, and the channel's width to depth ratios should demonstrate modest overall change and patterns of variation that are in keeping with the descriptions in section 3.6.1.

Significant widening of the channel cross-section or <u>trends</u> of increase in the cross sectional area generally represent concern, although some adjustment in this direction is acceptable if the process is arrested after a period of modest adjustment. In the case of riffle cross sections, maintenance of depths that represent small changes to target competence (e.g. consistently low BHRs <1.2) would also reflect stability. Although a pool cross-section may experience periodic infilling due to watershed activity and the timing of events relative to monitoring, the majority of pools within a project stream reach/component should demonstrate maintenance of greater depths and low water surface slopes over time. Rates of lateral migration need to be moderate. Bank pins will be installed to monitor rates of erosion.

Pattern and Profile

Pool depths may vary from year to year, however the majority of pools should maintain depths that are distinct in the profile and are readily observed. Pattern measurement will not be collected unless observations indicate a detectable change based on observations and/or dimension measurements.

Substrate

Generally it is anticipated that the bed materials will coarsen over time. The majority of riffle pebble counts should indicate maintenance or coarsening of the substrate. The D50 and D84 of the substrate should show a coarser distribution of bed materials in riffles and finer size class distribution in pools.

Sediment Transport

Depositional features should be consistent with a stable stream that is effectively managing its sediment load. Point Bar and inner berm features should develop without excessive encroachment of the restored channel. Trends in the development of systemic robust mid-channel or alternating bar features will be considered a destabilizing condition and may require intervention.

The tributaries outside of the conservation easement will be observed yearly and the monitoring report will document the function of the upstream basins in capturing excess sediment produced by observed degradation in the narrative. A specific performance standard has not been added.

Surface Water Hydrology

Monitoring of stream water stages through a staff gauge should show recurrence of bankfull flow on average every 1 to 2 years. Throughout the monitoring period, the surface water stage should achieve bankfull or greater elevations at least twice. The bankfull events must occur during separate monitoring years.

Vegetation

The vegetation monitoring will be conducted according to the Carolina Vegetation Survey (CVS) – EEP protocol Version 4.2 (Lee et al 2008). Vegetation monitoring plots will be 100 square meters in size and will be conducted according to the Level I protocol which has a focus on planted stems only. The purpose of this level of monitoring is to determine the pattern of installation of plant material with respect to species, spacing, density, and to monitor the survival and growth of those installed species. The success criteria for the preferred species in the restoration areas will be based on annual and cumulative survival and growth over seven (7) years. Survival on preferred species must be at a minimum 320 stems/acre at the end of the three years of monitoring and 260 stems/acre after five years. At year 7, density must be no less than 210 seven year-old planted stems/acre. Level II of the CVS protocol, which includes natural stems and planted stems, will be followed for the monitoring year 2 and subsequent years until the project close out year. The number of required plots is based on the mitigation category: stream enhancement, stream restoration, and wetland restoration. A spreadsheet is provided by EEP to calculate to necessary numbers of plots for streams (Lee et al 2008). Ten plots will be required for the restored reach of Tanyard Branch.

10.0 MONITORING REQUIREMENTS

Annual monitoring data will be reported using the EEP monitoring template. The monitoring report shall provide a project data chronology that will facilitate an understanding of project status and trends, population of EEP databases for analysis, research purposes, and assist in decision making regarding project close-out.

Required	Parameter	Quantity	Frequency	Notes
No	Pattern	As per April 2003 WSACE Wilmington District Stream Mitigation Guidelines	Annual	
Yes	Dimension	As per November 2011 NCEEP monitoring requirements	Monitoring Years 1,2,3, 5, and 7	Cross-sections to be monitored over seven (7) years and shall include an assessment of bank height ratio and entrenchment ratio
Yes	Bank Erosion Pins	As per November 2011 NCEEP monitoring requirements	Monitoring Years 1,2,3, 5, and 7	Bank pin arrays shall be installed at pool (bend) monitoring cross-sections; arrays shall be measured at time of cross-section surveys
Yes	Profile	As per April 2003 WSACE Wilmington District Stream Mitigation Guidelines	As-Needed	Longitudinal profile will be collected as a part of the asbuilt survey, visual monitoring will be conducted thereafter.
Yes	Substrate	As per April 2003 WSACE Wilmington District Stream Mitigation Guidelines	Annual	
Yes	Surface Water Hydrology	As per April 2003 WSACE Wilmington District Stream Mitigation Guidelines	Semi-annual	A Crest Gauge will be installed on site; the device will be inspected on a semi-annual basis to document the occurrence of bankfull events on the project.
No	Ground Water Hydrology	Quantity and location of gauges will be determined in consultation with EEP	Annual	Groundwater monitoring gauges with data recording devices will be installed on site; the data will be downloaded on every three months during the growing season
Yes	Vegetation	Quantity and location of gauges will be determined in consultation with EEP	Monitoring Years 1,2,3,5, and 7	Vegetation will be monitored using the Carolina Vegetation Survey (CVS) protocols
Yes	Exotic and nuisance vegetation and Beaver		Annual	Locations of exotic and nuisance vegetation and the occurrence of beaver dams and approximate inundation limits will be mapped.
Yes	Project boundary		Semi-annual	Location of fence damage, vegetation damage, boundary encroachments, etc. will be mapped.

11.0 LONG-TERM MANAGEMENT PLAN

Upon approval for close-out by the Interagency Review Team (IRT) the site will be transferred to the State of North Carolina. This party shall be responsible for periodic inspection of the site to ensure that restrictions required in the conservation easement of the deed restriction document(s) are upheld. Endowment funds required to uphold easement and deed restrictions shall be negotiated prior to site transfer to the responsible party.

12.0 ADAPTIVE MANAGEMENT PLAN

Upon completion of site construction EBX will implement the post-construction monitoring protocols previously defined in this document. Project maintenance will be preformed as described previously in this document. If, during the course of annual monitoring it is determined the site's ability to achieve site performance standards are jeopardized, EBX will notify the NCEEP of the need to develop a Plan of Correction Action. The Plan of Corrective Action will be prepared by an engineering consultant. Once the Corrective Action Plan is prepared and finalized EBX will:

- 1. Notify the NCEEP.
- 2. Revise performance standards, requirements, and monitoring requirements as necessary and/or required by the NCEEP.
- 3. Obtain other permits as necessary.
- 4. Implement the Corrective Action Plan.
- 5. Provide the NCEEP a Record Drawing of Corrective Actions. This document shall depict the extent and nature of the work preformed.

13.0 FINANCIAL ASSURANCES

Pursuant to Section IV H and Appendix III of the Ecosystem Enhancement Program's In-Lieu Fee Instrument dated July 28, 2010, the North Carolina Department of Environment and Natural resources has provided the U.S. Army Corps of Engineers Wilmington District with a formal commitment to fund projects to satisfy mitigation requirements assumed by EEP. This commitment provides financial assurance for all mitigation projects implemented by the program.

14.0 OTHER INFORMATION

14.1 Definitions

Morphological description- the stream type; stream type is determined by quantifying channel entrenchment, dimension, patter, profile, and boundary materials' as described in Rosgen, D. (1996), *Applied River Morphology, 2nd edition*

Native vegetation community – a distinct and reoccurring assemblage of population of plants, animals, bacteria and fungi naturally associated with each other and their population; as described in Schafale, M.P. and Weakley, A. S. (1990), *Classification of the Natural Communities of North Carolina, Third Approximation*

Project Area- includes all protected lands associate with the mitigation project

14.2 Reference

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Appendix A. Site Protection Instrument(s)

(to be included after completion of Task II)

Appendix B. Baseline Information Data

BI. Wetland Determination Data Form

_	ID DETERMINATION D				_
Project/Site: Tamad	Much	City/County	y: UNIDED		Sampling Date: № 🗸 🔊 ३०।
Applicant/Owner:				State: NC	Sampling Point: WA-2
Investigator(s): C. Charles	3	Section, To	ownship, Range:		
Landform (hillslope, terrace, et	a): deflession				Slope (%): 十-2-3/
Subregion (LRR or MLRA):	RO P Lat: 34				Datum: NAD83
Soil Map Unit Name:	Chamsen Sil-	\\ \A\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\		NWI classifica	
Are climatic / hydrologic condit	£ 3		/ No (If	no, explain in Re	
Are Vegetation, Soil _ </td <td></td> <td></td> <td></td> <td></td> <td>esent? Yes No</td>					esent? Yes No
Are Vegetation _^> , Soil				plain any answers	
				s. fransects.	important features, etc.
	/ / /	snowing sample	- Белита		
Hydrophytic Vegetation Prese	1	IS 11	ne Sampled Area	,	
Hydric Soil Present?	Yes N	AAIN	nin a Wetland?	Yes	_ No
Wetland Hydrology Present? Remarks:	Yes No	3			
remarks.	·				
HYDROLOGY					
Wetland Hydrology Indicate	ors:		S	econdary Indicate	ors (minimum of two required)
Primary Indicators (minimum		hat apply)		Surface Soil C	
✓ Surface Water (A1)	True	Aquatic Plants (B14)		Sparsely Vege	itated Concave Surface (B8)
High Water Table (A2)		ogen Sulfide Odor (C		Drainage Patte	
Saturation (A3)	Oxid	ized Rhizospheres on	Living Roots (C3)	Moss Trim Line	es (B16)
Water Marks (B1)	Pres	ence of Reduced Iron	(C4) _	Dry-Season W	/ater Table (C2)
Sediment Deposits (B2)		ent Iron Reduction in T	filled Soils (C6)	Crayfish Burro	
Drift Deposits (B3)		Muck Surface (C7)			ble on Aerial Imagery (C9)
Algal Mat or Crust (B4)	Othe	r (Explain in Remarks			essed Plants (D1)
Iron Deposits (B5)	7.11		<u> </u>	∠ Geomorphic P Challen Applie	
Inundation Visible on Act			 - d	Shallow Aquita _/Microtopograp	
✓ Water-Stained Leaves (E	19)		-	FAC-Neutral T	
Aquatic Fauna (B13)					est (DD)
Field Observations: Surface Water Present?	Yes No Der	oth (inches):			
Water Table Present?		oth (inches):			7
Saturation Present?	Yes No Dep		Wetland Hy	drology Present	7 Yes No
(includes capillary fringe)					1 100 <u>7</u> 100
Describe Recorded Data (stre	aam gauge, monitoring well, a	erial photos, previous	inspections), if availa	ıble:	
Remarks:					
Kemaiks.					
					,

Sampling Point: VEGETATION (Four Strata) - Use scientific names of plants. Absolute Dominant Indicator Dominance Test worksheet: 6×5 m Tree Stratum (Plot size: % Cover Species? Status Number of Dominant Species 1. Jalia Mictor 0136 20 165 That Are OBL, FACW, or FAC: (A) Total Number of Dominant Species Across All Strata: Percent of Dominant Species That Are OBL, FACW, or FAC: (A/B) Prevalence Index worksheet: Total % Cover of: Multiply by: OBL species 20 = Total Cover 5x511 FACW species ___ Sapling/Shrub Stratum (Plot size: FAC species ___ 1) Alia niga FACU species _____ x 4 = UPL species x 5 = __ (A) Column Totals: ____ Prevalence Index = B/A = Hydróphytic Vegetation Indicators: 1 - Rapid Test for Hydrophytic Vegetation 2 - Dominance Test is >50% 3 - Prevalence Index is ≤3.01 4 - Morphological Adaptations (Provide supporting (O = Total Cover data in Remarks or on a separate sheet) Herb Stratum (Plot size: 1. To oben late Folice Problematic Hydrophytic Vegetation (Explain) ¹Indicators of hydric soil and wetland hydrology must be present, unless disturbed or problematic. Definitions of Four Vegetation Strata: Tree – Woody plants, excluding vines, 3 in. (7.8 cm) or more in diameter at breast height (DBH), regardless of height. Sapling/Shrub - Woody plants, excluding vines, less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb - All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall. (@) = Total Cover Woody Vine Stratum (Plot size: Woody vine -- All woody vines greater than 3.28 ft in height. Hydrophytic Vegetation Present? 🗢 _ = Total Cover Remarks: (Include photo numbers here or on a separate sheet.)

	cription: (Describe	to the depi		x Feature		JI GOIIIAII	i tile absence	s of marcators.	·1	
Depth (inches)	Matrix Color (moist)	%	Color (maist)	x reature %	Type ¹	Loc ²	Texture		Remarks	
0-5	104R 5/2	85	1048 36	15	0	M		clowbar		
5-12	1042 5/2	75	1012 5/6	25		M		Un.		
				<u> </u>				· Visto		······································
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	WALLEST TO THE PARTY OF THE PAR									
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1							2			
'Type: C=C Hydric Soll	oncentration, D=Dep	letion, RM=	Reduced Matrix, MS	3=Masked	Sand Gra	lins.		L≕Pore Lining, ators for Prob		ic Soile ³ :
			Dock Surface	/C7\				2 cm Muck (A10	_	
Histosol	i (A1) pipedon (A2)		Dark Surface Polyvalue Be		ce (S8) (M	I RA 147		Coast Prairie Re		,
	istic (A3)		Thin Dark Su					(MLRA 147,		
	n Sulfide (A4)		Loamy Gleye			•	F	Piedmont Flood		19)
	d Layers (A5)		Depleted Mar					(MLRA 136,		
	ick (A10) (LRR N)		Redox Dark					Very Shallow Da		F12)
	d Below Dark Surface	e (A11)	Depleted Dar				(Other (Explain i	n Remarks)	
	ark Surface (A12) Jucky Mineral (S1) (L	RR N	Redox Depre Iron-Mangan			RRN				
	4 147, 148)		MLRA 13		55 (.) <u>2</u>) (.	-,,				
	eleyed Matrix (S4)		Umbric Surfa		MLRA 13	5, 122)	3Inc	dicators of hydr	ophytic vegeta	ation and
	Redox (S5)		Piedmont Flo					etland hydrolog		
	Matrix (S6)		Red Parent N	Aaterial (F	21) (MLR	4 127, 147	7) ur	niess disturbed	or problemation	3.
	Layer (if observed):						Ì		,	
Type:							<u>.</u> .		/	
Depth (in	ches):						Hydric Soi	Present/ Y	es <u>V</u>	No
Remarks:										

B2. NCWAM Stream Identification Forms

NC DWO Stream Identification Form Version 4.11 Project/Site: Town & Board Latitude: 24 23382 Date: 12,200 County: Union Longitude:-{{\bar{\chi}}}.《分學》 Evaluator: Total Points: Stream Determination-(circle one) Other Stream is at least intermittent 19.5 Ephemeral Intermittent Perennial inoclan a e.g. Quad Name: if ≥ 19 or perennial if ≥ 30* Absent Weak Moderate Strong A. Geomorphology (Subtotal =_ 1º. Continuity of channel bed and bank 0. 0 (2) 2. Sinuosity of channel along thalweg 1 3 3. In-channel structure: ex. riffle-pool, step-pool, (2) 0 1 3 ripple-pool sequence 11)>> 0 3 4. Particle size of stream substrate 3 5. Active/relict floodplain 0 (1)**D**-> 2 3 0 6. Depositional bars or benches 0 2 3 7. Recent alluvial deposits (1) 0 (2) 8. Headcuts 1 3 $\langle 0 \rangle \Rightarrow$ 0.5 1.5 9. Grade control 0.5 10. Natural valley 0 1.5 No # 0 \ 11. Second or greater order channel Yes = 3 artificial ditches are not rated; see discussions in manual B. Hydrology (Subtotal = **(**0) 1 2 12. Presence of Baseflow (<u>0</u>) 2 3 13. Iron oxidizing bacteria 1 14. Leaf litter (1.5)0.5 0 15. Sediment on plants or debris Ö (0.5) 1 1.5 (0.5) 16. Organic debris lines or piles 0 1 1.5 No = (0) 17. Soil-based evidence of high water table? Yes = 3 C. Biology (Subtotal =) 3 (2) 0 18. Fibrous roots in streambed (2)0 3 1 19. Rooted upland plants in streambed 2 3 (0)20. Macrobenthos (note diversity and abundance) 21. Aquatic Mollusks 60/ 1 2 3 (O 0.5 1 1.5 22. Fish 23. Crayfish (0)0.5 1 1.5 24. Amphibians Co. 0.5 1 1.5 (O) 0.5 1.5 25. Algae FACW = 0.75; OBL = 1.5 Other = 0 26. Wetland plants in streambed *perennial streams may also be identified using other methods. See p. 35 of manual. Notes: Sketch:

Bank Height (ft)

Bankfull width (ft) 2

Forum Polennical Origina Forum

Water depth (in)

Channel substrate Clay, Silt, Sand, Gravel, Cobble, Bedrock

Velocity - fast, moderate, slow None

Clarity – clear, slightly turbid, turbid $Non \ell$

North Carolina Division of Water Quality - Stream Identification Form; Version 3.1

Date: 7/15/08	Project: EBX	Latitude:
Evaluator: Kate Montieth	site: 601 East	Longitude:
Total Points: Stream is at least intermittent 33,5 if ≥ 19 or perennial if ≥ 30	County: Union	Other e.g. Quad Name;

	A. Geomorphology (Subtotal = 13.5)	Absent	Weak	Woderate	Strong
	1". Continuous bed and bank	0	1	2	(3)
*	2. Sinuosity	0	①	2	3
★★	In-channel structure: riffle-pool sequence	0	1	2	3
	Soil texture or stream substrate sorting	0	1	(2)	3
	Active/relic floodplain	0	1	2	3
	6. Depositional bars or benches	0	(1)	2	3
	7. Braided channel	0	1	2	3
	Recent alluvial deposits	0	1	2	3
	9 " Natural levees	0	1	2	3
	10. Headcuts	Ō	①	2	3
珍幸	11. Grade controls	0	0.5	①	1.5
	12. Natural valley or drainageway	0	(O.)	1	1.5
:	 Second or greater order channel on existing USGS or NRCS map or other documented evidence. 	No:	•	Yes =	3

Man-made ditches are not rated; see discussions in manual

B. Hydrology (Subtotal = 7.5)				
14. Groundwater flow/discharge	0	1	(2)	3
15. Water in channel and > 48 hrs since rain, or Water in channel dry or growing season	0	1	<u> </u>	3
16. Leaflitter	(.5)	1	0.5	0
17. Sediment on plants or debris	(Ö)	0,5	1	1.5
18. Organic debris lines or piles (Wrack lines)	0	(0.9)	1	1.5
19. Hydric soils (redoximorphic features) present?	No = 0		Yes = (1.5)	

20°. Fibrous roots in channel	1 3	2	1	0
21 ⁵ . Rooted plants in channel	3	(2)	1	0
22. Crayfish	0	0.5	1	1.5
23. Bivalves	0	1	2	3
24. Fish	0	0.5	1	1.5
25. Amphibians	Ö	0.5	1	1.5
26. Macrobenthos (note diversity and abundance)	0	0.5	①	1.5
27. Filamentous algae; periphyton	0	1	2	(3)
28. Iron oxidizing bacteria/fungus.	0	0.5	①	1.5
29 ⁶ , Weliand plants in streambed	FAC = 0.5; FA	ACW = 0.75; OB	_= (.5) SAV = 2	2.0; Other = (

billems 20 and 21 focus on the presence of upland plants, Item 29 focuses on the presence of equatic or welland plants.

Notes: (use back side of this form for additional notes.)

Sketch:

Collected right-handed snails; Observed green frog tadpoles and adults; Adult salamander (escaped before ID-ed)

Perennial origin at what appears to be an old headcut – farmer has added pile of rocks to streambed, probably to stop erosion at headcut. No water above headcut; water below headcut

^{*} Stream has been straightened

^{**} Farmer has added rock piles to stream creating riffles and pools and grade control

North Carolina Division of Water Quality - Stream Identification Form; Version 3.1

Date: 7/15/08	Project: EBX	Latitude:
Evaluator: Kate Montieth	Site: 601 East	Longitude:
Total Points: Stream is at least intermittent 19,5 if ≥ 19 or perennial if ≥ 30	County: Union	Other e.g. Quad Name;

A. Geomorphology (Subtotal = 10.5)	Absent	Weak	Moderate	Strong
1 ^a . Continuous bed and bank	0	1	2	(3)
2. Sinuosity	0	1	(2)	3
In-channel structure; riffle-pool sequence	0	①	2	3
Soil texture or stream substrate sorting	0	<u>(1)</u>	2	3
5. Active/relic floodplain	C	1	(2)	3
6. Depositional bars or benches	0	1	2	3
7. Braided channel	(0)	1	2	3
Recent alluvial deposits	0	1	2	3
9° Natural levees	(0)	1	2	3
10. Headcuts	0	<u>(1)</u>	2	3
11. Grade controls	0	0.5	1 1	1,5
12. Natural valley or drainageway	Ō	(0.9	1	1,5
 Second or greater order channel on existing USGS or NRCS map or other documented evidence. 	No =①		Yes	- 3

Man-made ditches are not rated; see discussions in manual

8 H	/drology	(Subtotal =	3	
-----	----------	-------------	---	--

14. Groundwater flow/discharge	(0)	1	2	3
15. Water in channel and > 48 hrs since rain, or Water in channel dry or growing season	0	1	2	3
16. Leaflitter	(1.9)	1	0.5	0
17. Sediment on plants or debris	(O)	0.5	1	1.5
18. Organic debris lines or piles (Wrack lines)	(e)	0.5	1	1.5
19. Hydric soils (redoximorphic features) present?	No = 0		Yes	= (.5)

20°. Fibrous roots in channel	(3)	2	1	0
21 ⁸ . Rooted plants in channel	(3)	2	1	0
22. Crayfish	1 0	0.5	1	1.5
23. Bivalves	(0)	1	2	3
24. Fish	(0)	0.5	1	1.5
25. Amphibians	(0)	0.5	1	1.5
26. Macrobenthos (note diversity and abundance)	0	0.5	1	1.5
27. Filamentous algae; periphyton	(0)	1	2	3
28. Iron oxidizing bacteria/fungus.	0	0.5	1	1.5
20 ^b Metland plants in etraphed	EAC - OF E	AC)A(- D 75, ODL	- 1 F DAVE-1	3 A. Albana

Sketch:

Notes: (use back side of this form for add	itional notes.)
--	-----------------

The stream is in the middle of a corn field. There is no vegetation or biology – just a channel

²⁹ b. Wetland plants in streambed FAC = 0.5; FACW = 0.75; OBL = 1.5 SAV = 2.0; Other = 0 b items 20 and 21 focus on the presence of upland plants, item 29 focuses on the presence of aquatic or wetland plants.

B3. Categorical Exclusion Form

Appendix A

Categorical Exclusion Form for Ecosystem Enhancement Program Projects

Version 1.4

Note: Only Appendix A should to be submitted (along with any supporting documentation) as the environmental document. Project Name: 601 East County Name: Union County EEP Number: RFP#16-004110 / Project # 95756 **Project Sponsor: NCEEP** Project Contact Name: Paul Wiesner Project Contact Address: 5 Ravenscroft Dr., #102, Asheville, NC 28801 Project Contact E-mail: Paul.Wiesner@ncdenr.gov **EEP Project Manager:** Paul Wiesner Project Description For Official Use Only Reviewed By: 5/7/13 Conditional Approved By: **FHWA** Check this box if there are outstanding issues Final Approval By: For Division Administrator

FHWA

Part 2: All Projects	
Regulation/Question	Response
Coastal Zone Management Act (CZMA)	
1. Is the project located in a CAMA county?	Yes No
2. Does the project involve ground-disturbing activities within a CAMA Area of Environmental Concern (AEC)?	Yes No N/A
3. Has a CAMA permit been secured?	Yes No N/A
Has NCDCM agreed that the project is consistent with the NC Coastal Management Program?	Yes No
Comprehensive Environmental Response, Compensation and Liabi	lity Act
(CERCLA)	
Is this a "full-delivery" project?	Yes No
Has the zoning/land use of the subject property and adjacent properties ever been designated as commercial or industrial?	Yes No N/A
3. As a result of a limited Phase I Site Assessment, are there known or potential hazardous waste sites within or adjacent to the project area?	Yes No N/A
4. As a result of a Phase I Site Assessment, are there known or potential hazardous waste sites within or adjacent to the project area?	Yes No N/A
5. As a result of a Phase II Site Assessment, are there known or potential hazardous waste sites within the project area?	Yes No N/A
6. Is there an approved hazardous mitigation plan?	Yes No N/A
National Historic Preservation Act (Section 106)	
Are there properties listed on, or eligible for listing on, the National Register of Historic Places in the project area?	Yes No
Does the project affect such properties and does the SHPO/THPO concur?	Yes No N/A
3. If the effects are adverse, have they been resolved?	Yes No N/A
Uniform Relocation Assistance and Real Property Acquisition Policies Ac Act)	t (Uniform

Is this a "full-delivery" project?	Yes No
Does the project require the acquisition of real estate?	Yes No N/A
3. Was the property acquisition completed prior to the intent to use federal funds?	Yes No N/A
4. Has the owner of the property been informed:* prior to making an offer that the agency does not have condemnation authority; and* what the fair market value is believed to be?	Yes No N/A
The landowner was notified in writing on January 31, 2013.	

Part 3: Ground-Disturbing Activities Regulation/Question	Response
American Indian Religious Freedom Act (AIRFA)	
1. Is the project located in a county claimed as "territory" by the Eastern Band of Cherokee Indians?	Yes No
Is the site of religious importance to American Indians?	Yes No N/A
3. Is the project listed on, or eligible for listing on, the National Register of Historic Places?	Yes No N/A
Have the effects of the project on this site been considered?	Yes No N/A
Antiquities Act (AA)	
Is the project located on Federal lands?	Yes No
2. Will there be loss or destruction of historic or prehistoric ruins, monuments or objects of antiquity?	Yes No N/A
Will a permit from the appropriate Federal agency be required?	Yes No N/A
4. Has a permit been obtained?	Yes No N/A
Archaeological Resources Protection Act (ARPA)	
Is the project located on federal or Indian lands (reservation)?	Yes No

2. Will there be a loss or destruction of archaeological resources?	Yes No N/A
Will a permit from the appropriate Federal agency be required?	Yes No N/A
4. Has a permit been obtained?	Yes No N/A
Endangered Species Act (ESA)	
 Are federal Threatened and Endangered species and/or Designated Critical Habitat listed for the county? 	Yes No
Is Designated Critical Habitat or suitable habitat present for listed species?	Yes No N/A
Are T&E species present or is the project being conducted in Designated Critical Habitat?	Yes No N/A
4. Is the project "likely to adversely affect" the species and/or "likely to adversely modify" Designated Critical Habitat?	Yes No N/A
5. Does the USFWS/NOAA-Fisheries concur in the effects determination?	Yes No N/A
6. Has the USFWS/NOAA-Fisheries rendered a "jeopardy" determination?	Yes No N/A

	Yes
as "territory" by the EBCI? 2. Has the EBCI indicated that Indian sacred sites may be impacted by	No Yes
the proposed project?	No N/A
3. Have accommodations been made for access to and ceremonial use of Indian sacred sites?	Yes No N/A
Farmland Protection Policy Act (FPPA)	
Will real estate be acquired?	Yes No
Has NRCS determined that the project contains prime, unique, statewide or locally important farmland?	Yes No N/A
3. Has the completed Form AD-1006 been submitted to NRCS?	Yes

	N/A	
Fish and Wildlife Coordination Act (FWCA)		
 Will the project impound, divert, channel deepen, or otherwise 	Yes	
control/modify any water body?	No	
2. Have the USFWS and the NCWRC been consulted?	Yes	
	No	
	N/A	
Land and Water Conservation Fund Act (Section 6(f))		
1. Will the project require the conversion of such property to a use other	Yes	
than public, outdoor recreation?	No	
2. Has the NPS approved of the conversion?	Yes	
	No	
	N/A	
Magnuson-Stevens Fishery Conservation and Management Act (Essent	ial Fish	
Habitat)		
Is the project located in an estuarine system?	Yes	
	No	
2. Is suitable habitat present for EFH-protected species?	Yes	
	No	
	N/A	
3. Is sufficient design information available to make a determination of the	Yes	
effect of the project on EFH?	No	
	N/A	
4. Will the project adversely affect EFH?	Yes	
	No	
	N/A	
5. Has consultation with NOAA-Fisheries occurred?	Yes	
	No	
	N/A	
Migratory Bird Treaty Act (MBTA)		
1. Does the USFWS have any recommendations with the project relative	Yes	
to the MBTA?	No	
2. Have the USFWS recommendations been incorporated?	Yes	
	No	
	N/A	
Wilderness Act	1	
1. Is the project in a Wilderness area?	Yes	
The same for a design of a second sec	No	
2. Has a special use permit and/or easement been obtained from the	Yes	
manualinio receiai acency c	No	

B4. Floodplain Requirement Checklist





EEP Floodplain Requirements Checklist

This form was developed by the National Flood Insurance program, NC Floodplain Mapping program and Ecosystem Enhancement Program to be filled for all EEP projects. The form is intended to summarize the floodplain requirements during the design phase of the projects. The form should be submitted to the Local Floodplain Administrator with three copies submitted to NFIP (attn. State NFIP Engineer), NC Floodplain Mapping Unit (attn. State NFIP Coordinator) and NC Ecosystem Enhancement Program.

Project Location

Name of project:	601 East Stream Restoration		
Name if stream or feature:	Tanyard Branch		
County:	Union County		
Name of river basin:	Yadkin River Basin		
Is project urban or rural?	Rural		
Name of Jurisdictional municipality/county:	Union County		
DFIRM panel number for entire site:	371053900J, 3710546000		
Consultant name:	Ward Consulting Engineers, P.C.		
Phone number:	919-870-0526		
Address:	4805 Green Road, Suite 100 Raleigh, NC 27616-2848		

Design Information

Provide a general description of project (one paragraph). Include project limits on a reference orthophotograph at a scale of 1" = 500".

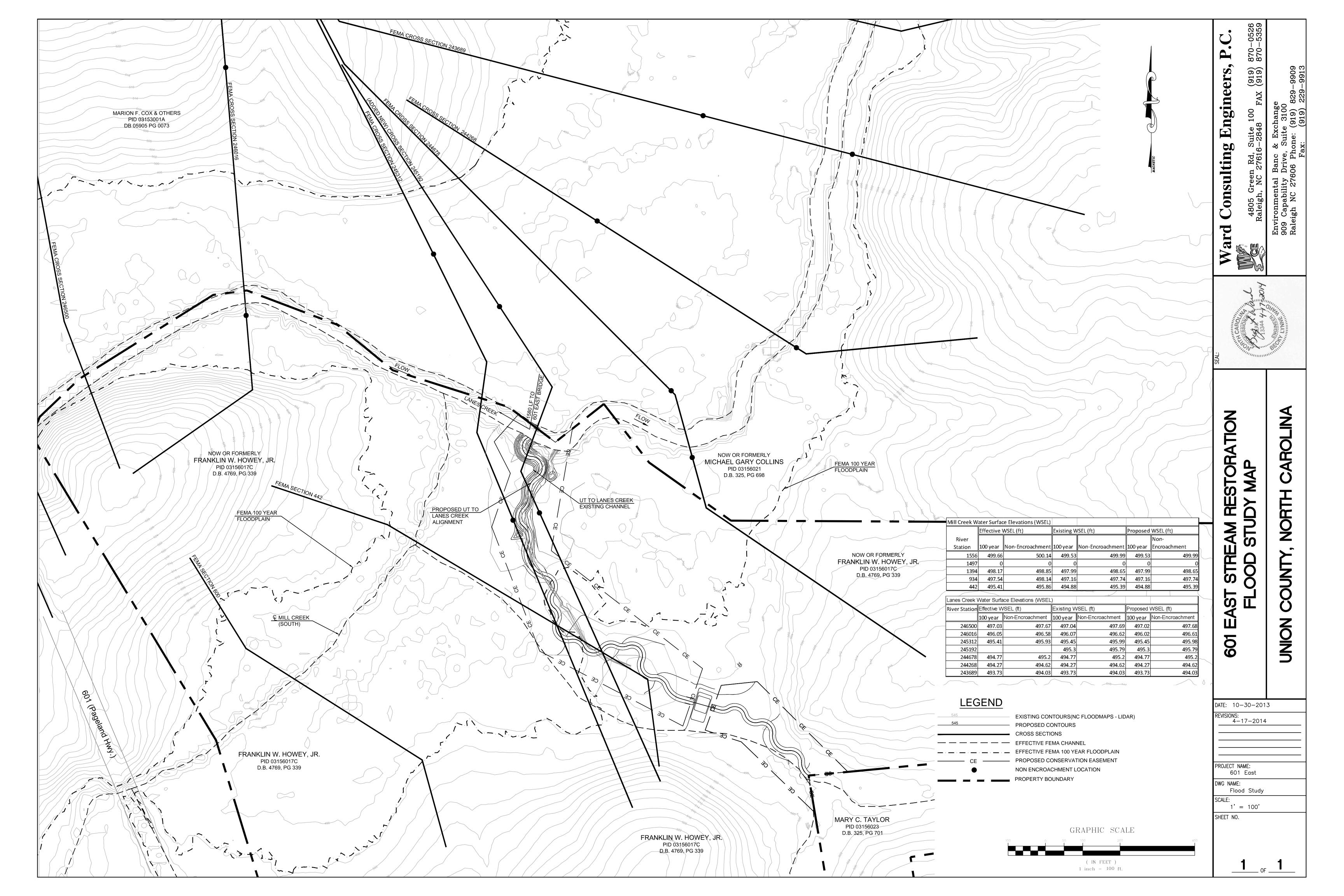
Summarize stream reaches or wetland areas according to their restoration priority.

Reach	Length	Priority	
Reach 1a & 1d	1150	P1	
Reach 1b & 1c	240	EI	
Reach 2a & 2b	160	E1	
Reach 2c	724	PI	
Reach 3a & 3b	1018	PI	
Reach 4	480	P3	

Floodplain Information

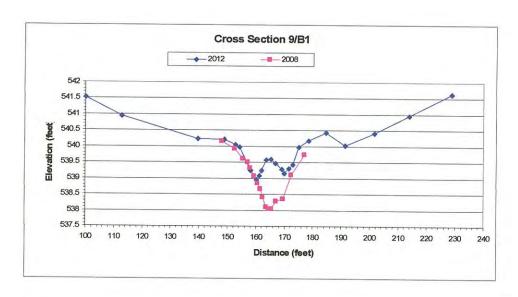
, variabilitativa.	
Is project located in a Specia	ıl Flood Hazard Area (SFHA)?
Yes C No	
If project is located in a SFH Redelineation	A, check how it was determined:
☐ Detailed Study	
Limited Detail Study (La	anes Creek & Mill Creek South)
☐ Approximate Study	
☐ Don't know	
List flood zone designation:	
Check if applies:	
▼ AE Zone	
← Floodway	
Non-Encroachment	(Lanes Creek)
○ None	
☐ A Zone	
C Local Setbacks Rec	quired
	Required
If local setbacks are required	, list how many feet:
Does proposed channel boun encroachment/setbacks?	dary encroach outside floodway/non-

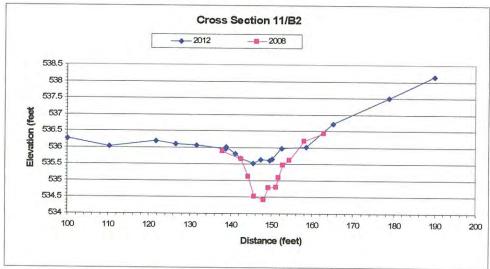
• Yes	C No
Land Acquisition	(Check)
☐ State owned (fe	e simple)
☐ Conservation ea	sment (Design Bid Build)
Conservation Ea	asement (Full Delivery Project)
	et property is state-owned, then all requirements should be addressed to f Administration, State Construction Office (attn: Herbert Neily,
Is community/cou	inty participating in the NFIP program?
	C No
	ty is not participating, then all requirements should be addressed to NFIP Engineer, (919) 715-8000)
Name of Local Florence Number: 70	oodplain Administrator: Lee Jenson 04-283-3605
	Floodplain Requirements
This section to be	filled by designer/applicant following verification with the LFPA
□ No Action	Three by designer appreant following verification with the El 171
No Rise CLan	nes Creek)
☐ Letter of Map R	evision
Conditional Lett	er of Map Revision
Cother Requirem	ents
List other requirer	ments:
not other require.	
Comments:	
Name: Book	L. Ward P.E. Signature: Ley L Ward
- Cong	
Title:	Date: 11-14-2013

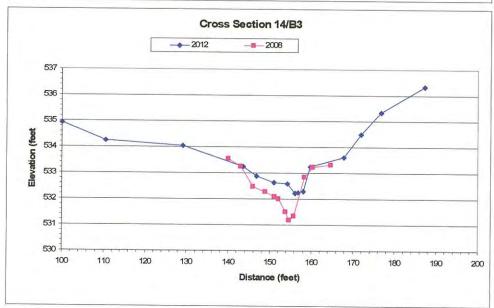


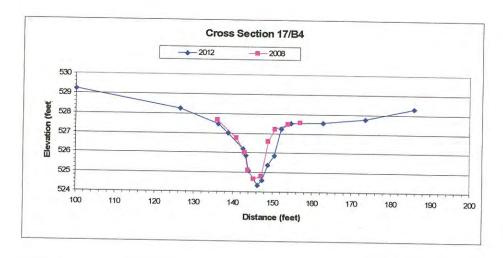
EEP Floodplain Requirements Checklist Project General Description

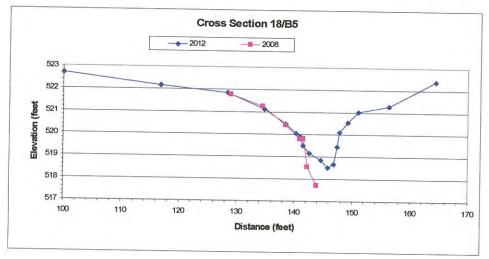
The 601 East project will be constructed on Tanyard Branch which is not a FEMA regulated stream. The project below Landsford Road ties into Lanes Creek which is a FEMA regulated stream. Lanes Creek is a limited detail study with non encroachment limits set at cross section 2465 approximately 1600 feet upstream and cross section 2443 approximately 800 feet downstream of the tie in location. A floodway is not delineated on Firm Panel 5460 because of the nature of the limited detail study. The restoration of the channel extends into the non-encroachment limit of Lanes Creek. A no-rise study was submitted to Mr. Lee Jenson Union County Floodplain Manager for Lanes Creek. The proposed project is not within the non encroachment limits of Mill Creek South and no impacts to the floodplain of Mill Creek South will occur due to the proposed project as no fill is proposed within this area.

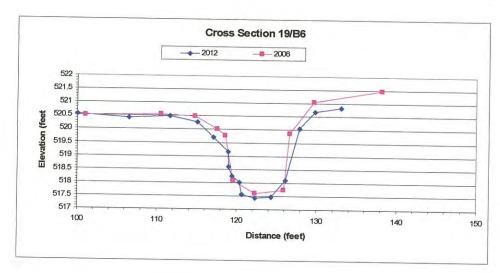


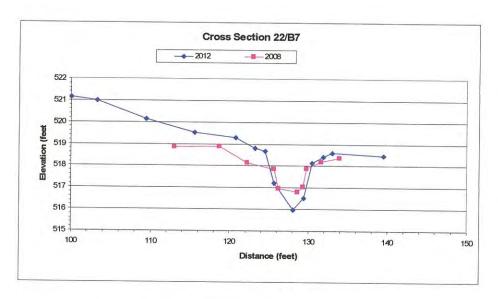


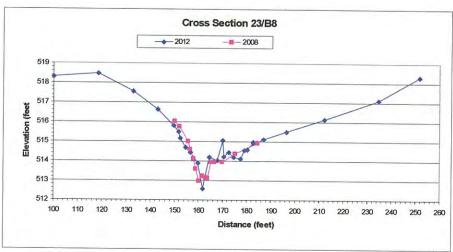












Appendix C. Mitigation Work Plan Data and Analyses

C1. Channel Morphology Tables

Tanyard Branch Reach 1 Union County, North Carolina

Variables	Existing Channel Tanyard Branch Reach 1	Proposed Tanyard Branch Reach 1	Reference Reach UT Richardson Creek
Stream type	G4/B4/C4b	B4/C4b	В4/С4ь
Drainage Area (Sq. Mile)	0.166	0.166	0.144
Bankfull width (Wbkf) feet	21 (7-60)	10	9.88 (7.42-11.61)
Bankfull mean depth (dbkf) feet	0.5 (0.2-0.9)	0.72	0.79 (0.68-0.97)
Width/depth ratio (Wbkf/dbkf)	27 (8-47)	13.9	12.95 (8.14-16.89)
Bankfull Cross Sectional Area (Abkf) (sq ft)	8.3 (4-14.5)	7.2	7.68 (6.02-10.27)
Bankfull Mean Velocity (Vbkf) feet/second	3.2 (2-5)	3.2	3.27 (2.71-3.83)
Bankfull Discharge, cfs (Qbkf) cfs	24	24	27
Bankfull Maximum depth (dmax) feet	1 (0.7-1.4)	1.2	1.39 (0.97-1.82)
Max dmax/dbkf ratio	2.2 (1.5-3.4)	1.67	1.78 (1.28-2.16)
Low Bank Height feet	0.34 (2-0.86)	1.2	1.39 (0.97-1.82)
Ratio of Low bank Height to max dbkf	0.84 (0.4-2)	1.0	1.0 (0.84-1.18)
Width of flood prone area (Wfpa) feet	60 (8-101)	28 (22-35)	26.43 (18.51-33.59)
Entrenchment ratio (Wfpa/Wbkf)	2.4 (1.1-9.5)	2.8 (2.2 – 3.5)	2.4 (2.02-3.24)
Meander length (Lm) feet	96 (36-240)	61 (43-89)	59.67 (43-88)
Ratio of meander length to bankfull width (Lm/Wbkf)	4.6 (1.7-11.5)	6.1 (4.3-8.9)	6.04 (4.35-8.9)
Radius of Curvature (Rc) feet	84 (14.5-118)	33 (16-53)	32.1 (16-52)

Tanyard Branch Reach 1 Union County, North Carolina

		• •	
Ratio of radius of			
curvature to	4	3.3	3.25
bankfull width	(.7-5.6)	(1.6-5.3)	(1.62-5.27)
(Rc/Wbkf)			
Belt width (Wblt)	19.6	18	17.33
feet	(10-35)	(13-21)	(13-20)
Meander width ratio	0.94	1.8	1.76
(Wblt/Wbkf)	(0.5-1.7)	(1.3-2.1)	(1.32-2.03)
Sinuosity (stream	3		
length /valley	1.04	1.17	1.16
distance) (k)			
Valley slope (ft/ft)			
J === F = (==)	0.02	0.02	0.021
Average slope	0.0101		
Savg=(Svalley / k)	0.0196	0.017	0.018
Pool Slope (Spool)	0.005		0.0011
(ft/ft)	(0015)	0.0006	(0.0003-0.0024)
Ratio of pool slope			1
to average slope	0.26	.035	0.06
(Spool/Sbkf)	(0.01-0.76)	.055	(0.02-0.13)
Maximum pool	2.4		1.83
depth (dpool) feet	(1-3.9)	2.2	
Ratio of pool depth			(1.4-2.2)
to average bankfull	4.6	3.0	2.33
depth (dpool/dbkf)	(2-7.8)	5.0	(1.78-2.8)
Pool width (Wpool)	9.2	***************************************	8.75
Feet	(7.1-12.5)	10	1
Ratio of pool width	(7.1-12.3)		(7.46-9.79)
to bankfull width	0.44	1.0	0.89
(Wpool/Wbkf)	(0.24-0.60)	1.0	(0.76-0.99)
Pool Cross		···	
Sectional Area	6.6	14.1	7.77
(sq ft)	(4.3-8.1)	14.1	(5.88-12.10)
1			
Ratio of pool area to bankfull area	0.8	1.0	1.01
1 I	(0.5-0.97)	1.9	(0.77-1.58)
Apool/Abkf		26.5	
Pool to pool spacing	50	36.7	36.2
(p-p) feet	(15.5-128)	(24-58)	(23.5-57.4)
Ratio of p-p spacing	2.4	3.6	3.67
to bankfull width	(0.74-6.1)	(2.4-5.8)	(2.38-5.81)
(p-p/Wbkf)	(a a a a a a a a a a a a a a a a a a a		(2.50 5.01)

Tanyard Branch Reach 2 Union County, North Carolina

Variables	Existing Channel Tanyard Branch Reach 2	Existing Channel Tanyard Branch Reach 2	Reference Reach UT to Underwood Creek
Stream type	C4/E4/DA	C4	C4/E4
Drainage Area	0.212	0.212	0.5
(Sq. Mile)		- -	0.5
Bankfull width	13	12	12.2
(Wbkf)	(7-19)		(10.0-14.3)
Bankfull mean	0.9	0.9	1.12
depth (dbkf)	(0.5-1.33)		(0.92-1.34)
Width/depth ratio	20.4	13.3	11.3
(Wbkf/dbkf)	(6.1-39)		(7.7-15.6)
Bankfull Cross	12	10.7	13
Sectional Area	(6-21)		(12.2-13.4)
(Abkf)			(12.2 15.1)
Bankfull Mean	2.1	2.6	3.0
Velocity (Vbkf)	(1-4)		(2.8-3.2)
Bankfull			
Discharge, cfs	27	27	40
(Qbkf)			
Bankfull	1.4	1.5	1.6
Maximum depth	(0.7-1.9)		(1.2-2.2)
(dmax)			(
Max driff/dbkf	1.8	1.7	1.52
ratio	(1.3-2.8)		(1.0-1.9)
Low Bank Height	1.5	1.5	1.5
	(0.9-1.7)		(1.1-1.7)
Low bank Height	0.9	1.0	1.0
to max dbkf	(.5-1.1)		(0.9-1.2)
Width of flood	107	91.5	77
orone area (Wfpa)	(40-214)	(48-135)	(42-110)
Entrenchment ratio	6	7.6	6.5
(Wfpa/Wbkf)	(2.2-10)	(3.6-10)	(2.9-8.6)
Meander length	70	84	85.5
(Lm)	(46-97)	(61-97)	(62-99)
Ratio of meander			
ength to bankfull	5.3	7.0	7.0
width (Lm/Wbkf)	(3.5-7.4)	(5.1-8.0)	(5.1-8.1)
Radius of	75	47	31
Curvature (Rc)	(68-77)	(38-58)	(20-65)
Ratio of radius of	5.7	3.9	2.55
curvature to pankfull width Rc/Wbkf)	(5.2-5.9)	(3.2-4.8)	(1.6-5.3)

Tanyard Branch Reach 2 Union County, North Carolina

Belt width (Wblt)	32	40	40
(,	(12-42)	(25-65)	(25-65)
Meander width	2.4	3.3	3.3
ratio (Wblt/Wbkf)	(0.9-3.2)	(2.1-5.4)	(2.1-5.4)
Sinuosity (stream			
length /valley	1.01	1.1	1.34
distance) (k)			
Valley slope (ft/ft)	0.0084	0.0084	0.0065
Average slope			
Savg=(Svalley /k)	0.0083	0.0069	0.0048
Pool Slope (Spool)	0.006	0.0009	0.0007
	(0-0.014)		(.00060009)
Ratio of pool slope			
to average slope	0.65	0.125	0.146
(spool/Sbkf)	(0-1.6)		(0.125 -0.188)
Maximum pool	2.8	2.5	2.47
depth (dpool)	(1.9-4.2)		(1.7-3.1)
Ratio of pool depth			
to average bankfull	3,3	2.8	2.20
depth (dpool/dbkf)	(2.3-5)		(1.5-2.8)
Pool width	10	12	15.5
(Wpool)	(7.2-12.4)		(11.8-18.0)
Ratio of pool	0.8	1.0	
width to bankfull	(0.55-0.94)		1.2
width	,		(1.0-1.5)
(Wpool/Wbkf)			(2.0 1.0)
Pool Cross	8	20	21.4
Sectional Area	(4.6-11)	-	(20.6-22.9)
Ratio of pool area	0.68	1.8	1.6
to bankfull area	(0.4-0.9)		(1.54-1.71)
Pool to pool	56	49	48
spacing (p-p)	(20-512)	(38-84)	(29-84)
Ratio of p-p	4.3		
spacing to bankfull	4.3 (1.4-38)	4.1	3.9
width (p-p/Wbkf)	(1.4-30)	(3.2-6.9)	(2.3-6.9)

Tanyard Branch Reach 3 Union County, North Carolina

Variables	Existing Channel Tanyard Branch Reach 3	Proposed Channel Tanyard Branch Reach 3	Reference Reach UT to Underwood Creek
Stream type	C4-G4	C4	E4/C4
Drainage Area	0.52	0.52	0.5
(Sq. Mile)			
Bankfull width	15.7	17	12.2
(Wbkf)	(6.5-29)		(10.0-14.3)
Bankfull mean	0.9	1.18	1.12
depth (dbkf)	(0.5-1.23)		(0.92-1.34)
Width/depth ratio	17.5	14.4	11.3
(Wbkf/dbkf)	(12.8-31)		(7.7-15.6)
Bankfull Cross	14.5	21	13
Sectional Area (Abkf)	(10.5-19.4)		(12.2-13.4)
Bankfull Mean	3.2	2.81	3.0
Velocity (Vbkf)	(2.1-4.3)		(2.8-3.2)
Bankfull	55	55	40
Discharge, cfs			(38-42)
(Qbkf)			
Bankfull	1.7	2.0	1.6
Maximum depth	(1.28-2.1)		(1.2-2.2)
(dmax)			, in the second
Max driff/dbkf	1.89	1.69	1.52
ratio	(1.4-2.3)		(1.0-1.9)
Low Bank Height	2.2	2.0	1.5
	(1.3-4)		(1.1-1.7)
Low bank Height	2.4	1.0	1.0
to max dbkf	(1.4-4.4)		(0.9-1.2)
Width of flood	200	200	77
prone area (Wfpa)	(150-260)	(150-300)	(42-110)
Entrenchment ratio	12.7	11.8	6.5
(Wfpa/Wbkf)	(9.6-16.5)	(8.8-17.6)	(2.9-8.6)
Meander length	57	119	85.5
(Lm)	(32-89)	(87-134)	(62-99)
Ratio of meander	, (7.0	
length to bankfull	3.6	7.0	7.0
width (Lm/Wbkf)	(2-5.7)	(5.1-8.1)	(5.1-8.1)
Radius of	49.7	43	31
Curvature (Rc)	(22.5-78)	(27-63)	(20-122)
Ratio of radius of	3.2	2.5	2.55
curvature to	(1.4-4.9)	(1.6-3.7)	(1.6-3.7)
bankfull width	and the second s		,
(Rc/Wbkf)			

Tanyard Branch Reach 3 Union County, North Carolina

Belt width (Wblt)	41	56	40
Don't Width (Woll)	(13-58)	(35-92)	(25-65)
Meander width	2.6	3.3	3.3
ratio (Wblt/Wbkf)	(1.3-3.7)	(2.1-5.4)	(2.1-5.4)
Sinuosity (stream	(1.5-5.7)	(2,1-3,+)	(2.1-5.4)
length /valley	1.05	1.2	1.20
distance) (k)	1.05	1.2	1.20
Valley slope (ft/ft)	0.0067	0.0067	0.0065
Average slope	0.0064	0.0056	0.0048
Savg= (Svalley /k)	0.0001	0.0050	0.0048
Pool Slope (Spool)	0.0016	0.0007	0.0007
l cor stope (speet)	(0.0004-0.0026)	0.0007	(.00060009)
Ratio of pool slope	0.25	0.125	0.146
to average slope	(0.063-0.41)	0.123	(0.125 -0.188)
(spool/Sbkf)	(0.005 0.11)		(0.123 *0.100)
Maximum pool	2.7	3.4	2.47
depth (dpool)	(1.8-3.4)		(1.7-3.1)
Ratio of pool depth	3	2.8	2.20
to average bankfull	(2-3.8)		(1.5-2.8)
depth (dpool/dbkf)	, ,		
Pool width	16.8	17	15.5
(Wpool)	(11-42)		(11.8-18.0)
	, ,		, , ,
Ratio of pool			
width to bankfull	1.1	1.0	1.2
width	(0.7-2.7)		(1.0-1.5)
(Wpool/Wbkf)			
Pool Cross	16.6	32.3	21.4
Sectional Area	(15.8-17.6)		(20.6-22.9)
Ratio of pool area	1.14	1.53	1.6
to bankfull area	(1.1-1.2)		(1.54-1.71)
Pool to pool	48	66	48
spacing (p-p)	(8-125)	(39-117)	(29-84)
Ratio of p-p	3.06	3.9	3.9
spacing to bankfull	(1.5-7.9)	(2.3-6.9)	(2.3-6.9)
width (p-p/Wbkf)			

Tanyard Branch Reach 4 Union County, North Carolina

Variables	Relic Channel Tanyard Branch Reach 4	Proposed Tanyard Branch Reach 4	Reference Reach UT Richardson Creek
Stream type	G4	B4	B4/C4b
Drainage Area (Sq. Mile)	0.56	0.56	0.144
Bankfull width (Wbkf) feet	11.6 (5.2-20)	16	9.88 (7.42-11.61)
Bankfull mean depth (dbkf) feet	0.9 (0.76-1.1)	0.98	0.79 (0.68-0.97)
Width/depth ratio (Wbkf/dbkf)	12.9 (7-18)	16.3	12.95 (8.14-16.89)
Bankfull Cross Sectional Area (Abkf) (sq ft)	15 (12.3-16)	15.7	7.68 (6.02-10.27)
Bankfull Mean Velocity (Vbkf) feet/second	4 (3.6-4.7)	3.6	3.27 (2.71-3.83)
Bankfull Discharge, cfs (Qbkf) cfs	55	55	27
Bankfull Maximum depth (dmax) feet	1.2 (0.8-1.4)	1.8	1.39 (0.97-1.82)
Max dmax/dbkf ratio	1.2 (1.05-1.33)	1.84	1.78 (1.28-2.16)
Low Bank Height feet	3.5 (3.3-4.2)	1.8	1.39 (0.97-1.82)
Ratio of Low bank Height to max dbkf	3.0 (2.9-3.3)	1.0	1.0 (0.84-1.18)
Width of flood prone area (Wfpa) feet	20 (16-25)	35 (30-40)	26.43 (18.51-33.59)
Entrenchment ratio (Wfpa/Wbkf)	1.7 (1.4-2.2)	2.2 (1.9-2.5)	2.4 (2.02-3.24)
Meander length (Lm) feet	56 (30-113)	97 (69-142)	59.67 (43-88)
Ratio of meander length to bankfull width (Lm/Wbkf)	4.8 (2.6-5.6)	6.04 (4.35-8.9)	6.04 (4.35-8.9)
Radius of Curvature (Rc) feet	34.9 (18-61)	52 (26-84)	32.1 (16-52)

Tanyard Branch Reach 4 Union County, North Carolina

D .: C 1: C	T	J,	·
Ratio of radius of			
curvature to	3	3.25	3.25
bankfull width	(1.6-5.3)	(1.62-5.25)	(1.62-5.27)
(Rc/Wbkf)	· · · · · · · · · · · · · · · · · · ·		
Belt width (Wblt)	32	28	17.33
feet	(12-83)	(21-32)	(13-20)
Meander width ratio	2.8	1.75	1.76
(Wblt/Wbkf)	(1.1-7.2)	(1.31-2.0)	(1.32-2.03)
Sinuosity (stream			
length /valley	1.04	1.13	1.16
distance) (k)			1
Valley slope (ft/ft)			
	0.0125	0.0125	0.021
Average slope			7077.
Savg= (Svalley / k)	0.0144	0.0114	0.018
Pool Slope (Spool)			0.0011
(ft/ft)		0.0009	(0.0003-0.0024)
Ratio of pool slope			(0.0003-0.0024)
to average slope		0.16	0.06
(Spool/Sbkf)		0.10	(0.02—0.13)
Maximum pool	2.5		1.83
depth (dpool) feet	(2-3.2)	3.0	!
Ratio of pool depth		TOTAL TOTAL TOTAL	(1.4-2.2)
to average bankfull	2.1	1.8	2.33
depth (dpool/dbkf)	(1.7-2.7)	1.0	(1.78-2.8)
Pool width (Wpool)	11		
Feet		16	8.75
Ratio of pool width	(10-16)		(7.46-9.79)
	0.95	1.0	0.89
to bankfull width	(0.9-1.4)	1.0	(0.76-0.99)
(Wpool/Wbkf)			(0.70 0.55)
Pool Cross	20		7.77
Sectional Area	(14-33)	26.3	(5.88-12.10)
(sq ft)	()		(3.00-12.10)
Ratio of pool area to	1.3		1.01
bankfull area	(0.9-2.2)	1.6	(0.77-1.58)
Apool/Abkf	(0.7-2.2)		(0.77-1.38)
Pool to pool spacing	29	59	36.2
(p-p) feet	(15-55)	(38-93)	(23.5-57.4)
Ratio of p-p spacing	2.5	2 60	
to bankfull width	(1.3-4.7)	3.68	3.67
(p-p/Wbkf)	(1.3-4.7)	(2.4-5.8)	(2.38-5.81)
			I

C2. Hydraulic Modeling

Upper Design Stream Reach 1 and 2

HEC RAS River	Design Stream	Stream	Comment
Station	CL Station	Feature	Comment
	07.00		
25+59	07+62	er m	
25+42	07+79	ER	
25+31	07+90	CP	
25+19	08+02	HR	
25+00	08+21	ER	
24+92	08+29	CP.	
24+76	08+45	HR	
24+57	08+64	ER	
24+46	08+75	<u>CP</u>	
24+32	08+89	HR	
24+15	09+06	ER	
24+06	09+15	<u>CP</u>	
23+95	09+26	HR	
23+73	09+48	ER	
23+61	09+60	<u>CP</u>	
23+44	09+77	HR	
23+29	09+92	ER	ļ
23+21	10+00	<u>CP</u>	
23+11	10+10	HR	
22+97	10+24	ER	
22+89	10+32	CP	
22+77	10+44	HR	
22+56	10+65	ER	
22+43	10+78	CP	
22+31	10+90	HR	
21+96	11+25	ĘR	
21+83	11+38	CP	
21+71	11+50	HR	
21+49	11+72	ER	
21+38	11+83	<u>CP</u>	
21+25	11+96	HR	
21+10	12+11	ER	
20+99	12+22	CP_	
20+96	12+25	HR	
20+71	12+50	ER	
20+59	12+62	CP_	
20+46	12+75	HR	
20+26	12+95	<u> </u>	
20+17	13+04	<u>CP</u>	
20+01	13+20	HR	
19+68	13+53		Upstream Culvert
19+63	13+58		Farm Crossing Culvert
19+11	14+10	ER	
19+01	14+20	CP	
18+91	14+30	HR	
18+74	14+47	ER	
18+66	14+55	<u>CP</u>	
18+56	14+65	HR.	
18+31	14+90	ER	
18+21	15+00	<u>CP</u>	
18+10	15+11	HR	ļ
1	45.00		
17+84	15+37	ER	
47.70	10.40		i
17+76	15+45	CP_	
47.04	45.57		
17+64	15+57	HR	
17+46	15+75	ER	

	Design		(
HEC RAS	Stream CL	Stream	Comment
River Station	Station	Feature	Comment
47.00			
17+36	15+85	CP	
17+24	15+97	HR	
17+07	16+14	ER	
16+98	16+23	CP_	
16+86	<u>16+35</u>	HR	
16+67	16+54	ER	
16+57	15+64	CP CP	
16+45	16+76	HR	
16+28	16+93	ER	
16+18	17+03	CP	
16+06	17+15	<u> </u>	
15+89	17+32	ER O	
15+78	17+43	CP I	
15+68	17+53	HR	
15+48	17+73	ER	
15+39	17+82	CP	
15+27	17+94	HR HR	
15+11	18+10	ER	
15+03	18+18	CP	
14+93	18+28	HR	
14+76	18+45	ER	
14+66	18+55	CP	
14+55	18+66	HR	
14+39	18+82	ER	
14+30	18+91	CP	
14+18	19+03	HR	
14+02	19+19	ER	
13+93	19+28	CP	
13+81	19+40	HR	
13+68	19+53	ER	
13+58	19+63	CP	
13+51	19+70	HR	
13+26	19+95	ER	
13+18	20+03	CP	
13+06	20+15	HR	
12+91	20+30	ER	
12+81	20+40	CP 1	
12+71	20+50	HR	
12+54	20+67	ER	
12+45	20+76	CP	
12+33	20+88	HR	
12+13	21+08	ER	
12+04	21+17	CP	
11+96	21+25	HR	
11+81	21+40	ER	
11+71	21+50	CP	
11+57	21+64	HR	
11+21	22+00	ER	Begin Reach 2
11+06	22+15	CP	
10+86	22+35	HR	
10+51	22+70	ER	
1 "			
10+31	22+90	CP	
]			
10+06	23+15	HR	
1			
09+66	23+55	ER	
09+48	23+73	CP.	

HEC RAS	Design		
River	Stream CL	Stream	Comment
Station	Station	Feature	
09+26	23+95	HR	Î
08+88	24+33	ER	
08+63	24+58	CP	
08+32	24+69	HR	
08+06	25+15	ER.	
07+81	25+40	CP UB	
07+56 07+29	25+65 25+92	HR ER	
07+13	26+08	CP	
06+93	26+28	HR	
06+79	26+42	ER	
06+70	26+51	CP	
06+59	26+62	HR	
06+46	26+75	ER	
06+32	26+89	<u>CP</u>	
06+16 06+01	27+05 27+20	HR ER	
05+85	27+36	CP	· · · · · · · · · · · · · · · · · · ·
05+66	27+55	HR	
05+46	27+75	ER	
05+29	27+92	CP	
05+09	28+12	HR	
04+93	28+28	ER	
04+82 04+69	28+39 28+52	CP HR	
04+56	28+65	ER	
04+44	28+77	CP	
04+29	28+92	HR	
04+15	29+06	ER	
04+04	29+17	CP	
03+91	29+30	HR	<u> </u>
03+77	29+44	<u> </u>	
03+62 03+43	29+59 29+78	CP HR	
03+26	29+95	ER	-
03+14	30+07	CP	
03+00	30+21	HR	
02+86	30+35	ER	
02+70	30+51	CP	
02+51	30+70	HR	
02+25	30+96	ER CR	
02+08 01+86	31+13 31+35	CP HR	
01+76	31+45	ER	
02+86	30+35	ER	
02+70	30+51	CP	
02+51	30+70	HR	
02+25	30+96	ER	
02+08	31+13	<u>CP</u>	
01+86	31+35	HR	ļ
01+76	31+45	ER	Lansford Road
01+56	31+65		Cuivert
01+30	31+91		Lansford Road Downstream
00+00	33+21		Woods North of Lansford Rd

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper

Reach	Reach River Sta Q Total Min Ch El W.S. Elev	Q Total	Min Ch El	W.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Vellet	Vel Chai	Vel Dieht	Elow Area	Ton Midth
		(cfs)	(ft)	(£)	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(ft/s)	(#/s)	(fVs)	(Sq ft)	(#)
Upper	2815	22.00	551.00	551,86	0.75	0.75	2.59	2.59		3.45)	6.37	10.85
Upper	2815	44.00	551.00	552.17	1.06	0.62	4.59	2.48	0.41	4.35	0.41	10.94	22.62
Upper	2815	30.00	551.00	552.00	0.86	98'0	3.24	3.24		3.77		7.95	11.97
Upper	2815	92.00	551.00	552.31	1.17	75.0	5.47	2.17	0.60	4.69	0.60	14.83	31.59
Upper	2815	81.00	551.00	552.52	1.35	0.59	7.00	2.10	0.82	5.20	0.82	22.67	44.47
Upper	2815	195.00	551.00	553.18	1.63	0.69	10.06	2.05	1.28	6.17	1.36	65.72	85.44
Upper	2767	22:00	920.00	550.77	0.78	0.78	2.67	2.67		3.44		6.40	12.52
Upper	2767	44.00	920.00	551.04	1.13	1.05	4.89	4.54	0.19	4.34	0.19	10.16	16.19
Upper	2767	30.00	550.00	920.90	0.89	0.89	3.33	3.33		3.75		7.99	13.85
Upper	2767	27.00	550.00	551.14	1.38	1.12	6.77	5.39	0.43	4.91	0.43	11.86	18.90
Upper	2767	81.00	550.00	551.36	1.51	1.02	8.10	4.96	0.74	5.36	0.74	16.66	25.02
Upper	2767	195.00	550.00	552.08	1.99	1.06	13.45	4.92	1.28	6.74	1.34	42.10	46.38
Upper	2728	22:00	549.00	549.76	0.83	0.83	2.97	2.97		3.56		6.19	12.33
Upper	2728	44.00	549.00	220.02	1.03	0.82	4.33	3.41	0.24	4.18	0.24	10.65	19.10
Upper	2728	30.00	549.00	549.88	0.93	0.93	3.58	3.58		3.84		7.82	13.71
Оррег	2728	57.00	549.00	550.20	1.13	0.69	5,11	2.86	0.48	4.51	0.48	13.74	27.25
Upper	2728	81.00	549.00	550.38	1.37	0.70	6.98	2.87	0.73	5.11	0.73	19.64	38.24
Upper	2728	195.00	549.00	551.05	1.62	0.74	9.82	2.43	1.20	90'9	1.24	59.17	77.73
Upper	2687	22.00	548.00	548.78	0.70	0.70	2.28	2.28		3.26		6.75	13.34
Upper	2687	44.00	548.00	549.02	1.88	1.02	4.61	4.32	0.13	4.24	0.13	10.39	17.10
Upper	2687	30.00	548.00	548.89	0.81	0.81	2.90	2.90		3.58		8.38	14.74
	2687	57.00	548.00	549,12	1.34	1.03	6.43	4.85	0.38	4.80	0.38	12.15	21.30
	2687	81.00	548.00	549.33	1.42	0.85	7.34	3.85	0.70	5.17	0.70	17.88	31.33
Upper	2687	195.00	548.00	550.03	1.72	0.85	10.71	3.24	1.23	6.23	1.25	50.78	62.96
Upper	2648	22.00	547.00	547.74	06'0	06.0	3.29	3.29		3.67		5.99	12.16
	2648	8.4	547.00	548.08	1.00	0.88	4.10	3.58	0.26	4.12	0.26	10.77	17.21
	2648	30.00	547.00	547.87	96.0	96.0	3.74	3.74		3.89		7.71	13.62
	2648	27.00	547.00	548.25	0.99	0.72	4,23	2.91	0:20	4.26	0.50	14.16	22.04
Upper	2648	81.00	547.00	548.50	1.07	29.0	4.93	2.64	0.73	4.61	0.73	20.54	29.04
	2648	195.00	547.00	549.23	1.56	0.79	9.46	3.13	1.13	6.05	1,22	49.52	52.68
	0000	0											
	5007 5007	22.00	546.00	546,96	0.63	0.63	2.09	2.09		3.31		6.64	9.78
	2003	44.00	546.00	547.29	0.99	0.67	4.36	2.73	0.52	4.42	0.52	10.76	16.29
	2609	30.00	546.00	547.10	0.75	0.62	2.80	2.29	0.26	3.72	0.26	8.17	12.30
	2609	27.00	546.00	547.39	1.28	0.80	6.52	3.61	0.70	5.11	0.70	12.63	18.65
	2609	81.00	546.00	547.61	1.59	0.91	9.37	4.27	0.95	5.88	0.95	17.21	23.44
Upper	2609	195.00	546.00	548.51	1.97	28.0	14.10	3.45	1.43	7.14	1.30	49.35	51.65

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

	EIC HALL	<u> </u>	Keach Kwer Sta Q Total Min Ch El W.S. Elev Shear Chan	W.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Vel Left	Vel Chril	Vel Right	Flow Area	Top Width
		(cfs)	(#)	(£)	(lb/sq ft)	(lb/sd ft)	(lb/ft.s)	(lb/ft s)	(£/s)	(£/k)	(#Vs)	(sd ft)	(£)
Пррег	2561	22.00	544.80	545.75	1.25	1.25	5.62	5.62		4.48		4.91	8.01
Upper	2561	44.00	544.80	546.14	1.47	1.07	7.58	5.30	0.43	5.14	0.43	8.85	14.51
Upper	2561	30.00	544.80	545.92	1.34	1.34	6.31	6.31		4.71		6.37	9.35
Upper	2561	57.00	544.80	546.33	1.48	0.85	7.91	3.98	69.0	5.33	0.69	12.25	20.77
Opper	2561	81.00	544.80	546.61	1.57	0.79	8.97	3.34	0.94	5.71	0.94	19.18	29.69
Upper	2561	195.00	544.80	547.39	2.04	0.95	14.32	3,51	1.57	7.02	1.41	52.69	55.49
Upper	2543	22.00		545.39	0.47	0.43	1.34	1.22	0.14	2.85	0.14	7.74	11.08
Upper	2543	44.00		545.85	65.0	96.0	2.03	1.06	0.54	3.45	0.53	14.97	20.09
Upper	2543	30.00		545.58	0,51	0.37	1.58	1.09	0.35	3.09	0.34	10.24	14.83
Upper	2543	57.00	544.13	546.06	0.65	76.0	2.43	1.08	0.66	3.73	0.58	19.53	24.48
Upper	2543	81.00		546.36	0.76	66.0	3.14	1.10	0.85	4.15	0.64	28.29	32.61
Upper	2543	195.00		547.19	1.26	0.59	7.20	1.79	1.35	5.71	1.06	64.51	54.98
Upper	2533	22.00	543.08	545.42	0.10	60:0	0.15	0.13	0.07	1.46	70.0	15.17	13.05
Оррег	2533	44.00	543.08	545.89	0.20	0,11	0.42	0.21	0.28	2.12	0.28	23.78	23.59
Upper	2533	30.00	543.08	545.62	0.14	0.10	0.24	0.16	0,16	1.73	0.16	18.16	17.44
Upper	2533	67.00	543.08	546.10	0.25	0.13	09.0	0.26	0.37	2.42	0.34	29.17	28.39
Upper	2533	81.00	543.08	546.41	0.34	0.17	76.0	0.34	0.51	2.88	0.44	39.02	35.77
Upper	2533	195.00	543.08	547.23	0.74	0.34	3.33	0.87	1.00	4.50	0.80	76.58	56.38
Upper	2521	22.00	544.12	545.07	1.24	1.24	5.52	5.52		4.46		4.94	8.04
Upper	2521	44.00	544.12	545.45	1.49	1.16	7.72	5.84	0.42	5.17	0.42	8.72	13.37
Upper	2521	30.00	544.12	545,24	1.34	1.34	6.30	6.30		4.71		6.37	9.35
Upper	2521	27.00	544.12	545.64	1.54	0.98	8.33	4.77	69'0	5.42	0.69	11.65	18.02
Upper	2521	81.00	544.12	545.92	1.65	0.91	99.6	4.19	96.0	5.84	96.0	17.59	24.94
Upper	2521	195.00	544.12	546.79	1.94	0.82	13.39	2.94	1.50	68'9	1.23	54.48	60.97
Upper	2502	22.00	543.37	544.64	0.45	0.38	1.27	1.07	0.15	2.80	0.15	7.91	11.93
Upper	2502	00.44	543.37	545.10	0.55	0.31	1.85	0.84	0.56	3.35	0.55	16.42	23.67
Upper	2502	30.00	543.37	544.83	0.49	0.31	1.48	0.88	0.35	3.03	0.35	10.77	17.38
Upper	2502	57.00	543.37	545.29	0,62	0.35	2.27	0.95	0.71	3.64	89.0	21.14	26.67
Upper	2502	81.00	543.37	545.54	0.80	0.45	3.36	1.28	0.92	4.22	98.0	28.13	30.58
Upper	2502	195.00	543.37	546.29	1.51	0.77	9.32	2.65	1.48	6.18	1.32	56.46	46.79
Upper	2490	22.00	542.31	544.67	0.10	70.0	0.14	0.10	0.08	1.44	90.0	15.58	16.93
Upper	2490	44.00	542.31	545.14	0.18	0.07	0.37	0.11	0.29	2.03	0.27	29.54	41.46
Upper	2490	30.00	542.31	544.87	0.13	90:0	0.23	0.10	0.16	1.70	0.16	19,99	27.72
Upper	2490	27.00	542.31	545.33	0.22	0.09	0.50	0.13	0.39	2.28	0.34	38.41	50.34
Upper	2490	81.00	542.31	545.59	0.29	0.12	0.78	0.18	0.52	2.68	0.45	53.15	62.37
Upper	2490	195.00	542.31	546.48	0.44	0.20	1.55	0.31	0.77	3.48	0.82	124.70	95.90

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

2476 (48) (70) <th< th=""><th>Reach</th><th>River Sta</th><th>Reach River Sta O Total Min Ch E1 W S Ek</th><th>Min Ch El</th><th></th><th>Shear Chan</th><th>Shear Total</th><th>Douger Chan</th><th>Douger Total</th><th>Vol Loft</th><th>Vol Chai</th><th>Vol Diaht</th><th>Total Area</th><th>Transferrence</th></th<>	Reach	River Sta	Reach River Sta O Total Min Ch E1 W S Ek	Min Ch El		Shear Chan	Shear Total	Douger Chan	Douger Total	Vol Loft	Vol Chai	Vol Diaht	Total Area	Transferrence
2476 (255) (T) (T)<	lineavi .	The state of the s	3	5	**.C. Liev	1 C C C C C	Olica Total	TOWER CLIGHT	I DAMOL I OPE	Aei Leit	Ne Cilli	vel Right	riow Area	lop wiam
2476 4200 6433 6443 1.35 1.25 657 6.57 6.57 2476 4400 6433 6443 1.43 0.39 7.23 6.31 0.44 2476 4400 6433 6444 1.44 0.74 8.05 6.31 0.69 2476 5100 6433 6448 1.44 0.74 8.05 6.31 0.69 2476 5100 6433 6448 1.49 0.74 8.05 0.61 0.69 2466 5100 6433 64417 1.46 0.74 8.05 0.61 0.69 0.75 0.61 0.69 0.75 0.61 0.69 0.74 0.69 0.74 0.69 0.74 0.69 0.74 0.69 0.74 0.74 0.69 0.74 0.74 0.69 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74			(cts)	Œ	- 1	=	(lp/sd ft)	(lb/ff s)	(ib/ft s	(ft/s)	(£/s)	(£/t)	(sq ft)	(ft)
2476 4400 6433 56448 1,41 6,43 6,448 1,41 6,43 6,448 1,41 6,43 6,448 1,41 1,43 6,43 6,448 1,44 0,68 7,23 6,43 6,64 6,43 6,448 1,44 0,68 7,23 6,58 6,68 6,43 6,44 1,44 0,68 7,23 6,58 6,68 6,43 6,44 1,44 0,68 7,23 6,58 6,68 6,68 7,44 1,45 0,73 1,77 0,78 0,68 2466 2,200 542,56 544,77 0,44 0,58 0,53 0,74 0,58 0,53 0,64 0,64 0,68 0,73 0,74 0,69 0,74 0,68 0,74 0,68 0,74 0,78 0,68 0,74 0,68 0,74 0,74 0,78 0,78 0,74 0,78 0,74 0,78 0,74 0,74 0,74 0,74 0,74 0,74 0,74 0,74	Upper	2476	22.00	543.36	544.31	1.25	1,25				4.47		4.92	8.02
2476 5000 544.38 1544 134 634 651 654 134 634 651 652 654 134 6	Upper	2476	44.00	543.36	544.71	1.43	06:0			0.44	5.06	0.44	9.18	17.13
2478 \$100 \$43.86 \$44.91 \$14.0 0.68 7.29 2.69 0.68 2476 \$15.00 \$43.86 \$46.86 \$14.6 \$1.24 \$1.20 \$2.89 \$1.68	Upper	2476	30.00	543.36	544.48	1.34	1.34				4.71		6.37	9.35
2478 61.00 543.36 546.17 146 0.74 61.07 543.96 546.19 146 0.74 61.07 53.9 1.09 2476 1266 543.96 546.91 0.47 0.43 0.51 1.73 0.59 0.14 2466 40.00 542.66 544.37 0.54 0.31 1.74 0.97 0.43 2466 30.00 542.66 544.37 0.64 0.37 1.46 0.77 0.40 2466 10.00 542.66 544.37 0.64 0.37 1.46 0.77 0.40 2468 11.00 542.66 544.37 0.74 0.66 0.74 0.7	Upper	2476	57.00	543.36		1.40	99.0				5.18	0.68	13.50	26.57
2478 195.00 543.86 546.89 2.18 1.29 16.71 5.33 1.69 2468 2200 542.65 546.37 0.54 0.31 1.77 0.78 0.14 2468 3200 542.65 544.37 0.54 0.31 1.77 0.78 0.14 2468 30.00 542.65 544.37 0.64 0.35 1.74 0.78 0.04 2468 30.00 542.66 544.79 0.78 0.45 0.35 0.17 0.40 2468 51.00 542.66 544.79 0.78 0.36 0.17 0.40 2448 195.00 541.60 544.81 0.10 0.09 0.14 0.00 2448 110.00 541.60 544.81 0.13 0.13 0.14 0.00 2448 110.00 541.60 544.81 0.13 0.13 0.01 0.00 0.00 0.00 0.00 0.00 0.00 0.00 <	Upper	2476	81.00	543.36	545.17	1.46	0.74	8.03				1.05	21.43	32.81
2466 2200 542.66 543.91 0.47 0.36 1.37 0.97 0.14 2466 44.00 562.66 544.13 0.54 0.37 1.77 0.78 0.61 2466 34.00 542.66 544.13 0.64 0.37 1.77 0.78 0.61 2466 57.00 542.66 544.17 0.64 0.37 1.74 0.78 0.61 2466 51.00 542.66 544.79 0.79 0.74 0.79 0.77 2466 181.00 542.66 544.79 0.70 0.74 0.79 0.74 2448 21.00 542.66 544.79 0.70 0.06 0.74 0.70 2448 21.00 542.66 544.86 0.71 0.70 0.71 0.70 2448 21.00 542.64 544.86 0.24 0.74 0.74 0.74 0.74 0.74 0.74 0.75 0.75 0.74 0.75	Upper	2476	195.00	543,36	545.86	2.18	1.29	15.71				1.95	47.09	40.51
2466 2200 64286 54439 0.47 0.58 1.38 0.697 0.614 2466 4400 542.66 544.47 0.64 0.73 1.47 0.71 0.66 2466 30.00 542.66 544.17 0.68 0.75 0.76 0.76 2466 37.00 542.66 544.74 0.62 0.38 0.75 0.76 2466 185.00 542.66 544.74 0.66 0.74 0.74 0.76 2466 185.00 542.66 544.74 0.78 0.74 0.76 0.76 2468 185.00 541.60 544.44 0.78 0.70 0.73 0.77 0.74 2448 240 544.84 0.73 0.73 0.74 0.74 2448 31.00 541.60 544.84 0.74 0.74 0.74 0.75 0.74 0.74 2448 51.00 541.84 0.74 0.74 0.75 0.7														
2466 4400 542.66 544.37 0.64 0.31 1.77 0.78 0.64 2466 30.00 542.66 544.14 0.64 0.27 1.46 0.71 0.40 2466 57.00 542.66 544.74 0.76 0.28 2.74 0.70 0.71 0.70 2466 510.00 542.66 544.74 0.76 0.64 0.71 0.70 0.71 0.70 2448 510.00 541.60 543.66 0.10 0.06 0.16 0.06 0.17 0.03 0.17 0.03 0.17 0.03 0.17 0.03 0.17 0.03 0.17 0.03 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.08 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 <td>Upper</td> <td>2456</td> <td>22.00</td> <td>542.65</td> <td>543.91</td> <td>0.47</td> <td>0.35</td> <td></td> <td></td> <td></td> <td></td> <td>0.14</td> <td>7.84</td> <td>13.85</td>	Upper	2456	22.00	542.65	543.91	0.47	0.35					0.14	7.84	13.85
2466 300 642.66 644.41 0.48 0.27 1.48 0.77 0.40 2466 65.06 642.66 644.64 0.78 0.28 2.26 0.53 0.73 2466 81.00 642.66 645.63 1.29 0.76 0.26 0.76 0.76 2466 18.00 642.66 645.63 1.29 0.76 0.71 0.09 2448 22.00 541.60 544.81 0.71 0.09 0.71 0.09 2448 20.00 541.60 544.81 0.73 0.71 0.09 2448 30.00 541.60 544.84 0.34 0.13 0.07 0.02 2448 51.00 541.60 544.84 0.34 0.13 0.08 0.37 0.43 2448 51.00 541.60 544.84 0.34 0.13 0.89 0.37 0.89 0.37 0.89 0.38 0.71 0.08 0.38 0.31 0.	Upper	2456	44.00	542.65	544.37	0.54	0.31		0.78		3.30	0.64	17.71	25.32
2466 6700 542.66 544.49 0.62 0.38 2.25 0.39 0.76 2466 18100 542.66 544.79 0.76 0.46 7.41 2.03 0.75 2466 18500 542.66 545.66 1.29 0.06 7.41 2.03 1.42 0.03 2448 1800 541.60 544.16 0.19 0.06 0.17 0.09 0.07 2448 4400 541.60 544.16 0.13 0.01 0.03 0.11 0.00 2448 4400 541.60 544.16 0.13 0.01 0.03 0.11 0.00 2448 100 541.60 544.16 0.13 0.01 0.05 0.01 0.05 2448 110 542.64 543.69 0.74 0.24 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05	Upper	2456	30.00	542.65	544.11	0.48	0.27					0.41	11.61	21.54
2456 81 00 542.65 544.79 0.76 0.46 316 1.21 0.93 2468 185.00 542.65 546.83 1.29 0.06 7.41 2.03 1.42 2448 220 541.80 543.85 0.10 0.09 0.01 0.09 0.01 0.09 0.01 0.09 0.01 0.00	Upper	2456	57.00	542.65	544.54	0.62	0.36	2.25				0.77	22.23	27.79
2456 155 00 542.65 545.63 1,29 0.69 7,41 2.00 1,42 2448 22.00 541.60 543.44 0.19 0.00 0.15 0.07 0.05 0.07 0.03 2448 44.00 541.60 544.41 0.13 0.07 0.23 0.11 0.20 2448 50.00 541.60 544.84 0.13 0.07 0.23 0.11 0.20 2448 51.00 541.60 544.84 0.34 0.13 0.07 0.23 0.11 0.07 2448 51.00 541.60 544.84 0.34 0.13 0.07 0.23 0.11 0.02 2448 51.00 541.60 542.84 0.74 0.34 0.31 0.05 0.05 0.04 2448 51.00 542.64 543.69 1.25 0.61 5.80 0.51 1.02 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0	Upper	2456	81.00	542.65	544.79	0.76	0.45	3.16		0.93		0.96	29.85	31.51
2448 2200 54180 54386 0.10 0.06 0.15 0.07 0.08 0.07 0.09 0.07 0.03 0.07 0.03 0.07 0.03 0.07 0.03 0.07 0.03 0.07 0.03 0.07 0.03 0.07 0.03 0.07 0.03 0.04 <	Upper	2456	195.00	542.65	545.63	1.29	99:0	7.41		1.42		1.21	63.72	51.23
2448 22.00 641.60 643.95 0.10 0.06 0.15 0.09 0.07 2448 44.00 641.60 644.81 0.13 0.01 0.03 0.01 0.03 2448 30.00 641.60 644.84 0.24 0.13 0.07 0.03 0.01 0.03 2448 81.00 641.60 644.84 0.24 0.13 0.04 0.05 0.01 0.02 2448 81.00 641.60 644.84 0.24 0.14 0.08 0.03 0.04 2448 195.00 641.60 644.84 0.74 0.34 0.31 0.05 2448 195.00 641.60 643.89 1.25 0.61 0.89 0.37 1.02 2448 195.00 642.64 643.69 1.24 0.34 0.39 0.25 0.61 0.89 0.50 0.50 2443 195.00 642.64 644.40 1.24 1.34 8.64														
2448 44,00 541,60 544,41 0.19 0.10 0.39 0.17 0.20 2448 30.00 541,65 544,15 0.24 0.07 0.23 0.01 0.00 2448 50.00 541,60 544,15 0.24 0.13 0.05 0.01 0.00 2448 51.00 541,60 544,84 0.24 0.13 0.65 0.03 0.01 0.00 2448 61.00 541,60 546,60 0.74 0.34 3.31 0.65 0.01 0.00 2448 195.00 542,64 543,60 0.74 0.34 3.31 0.65 0.51 0.05 2448 195.00 542,64 543,60 1.25 0.51 5.89 2.56 0.51 2434 150.00 542,64 544,10 1.34 1.34 6.87 0.51 0.51 2434 150.00 542,64 544,10 1.34 1.34 6.87 0.52	Upper	2448	22.00	541.60	543.95	0,10	90:0	0,15			1.45	0.07	15.55	18.94
2448 3000 541.60 544.15 0.13 0.07 0.28 0.14 0.20 2448 81.00 541.60 544.58 0.24 0.13 0.68 0.23 0.44 2448 81.00 541.60 544.68 0.74 0.13 0.68 0.23 0.64 2448 81.00 542.64 545.68 0.74 0.13 0.89 0.93 0.69 2448 195.00 542.64 545.68 0.74 0.34 3.31 0.85 0.61 0.68 0.67 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.61 <td>Upper</td> <td>2448</td> <td>44.00</td> <td>541.60</td> <td>544.41</td> <td>0.19</td> <td></td> <td>0.39</td> <td></td> <td></td> <td></td> <td>46.0</td> <td></td> <td>28.67</td>	Upper	2448	44.00	541.60	544.41	0.19		0.39				46.0		28.67
2448 57.00 541.60 544.84 0.24 0.13 0.56 0.23 0.44 2448 181.00 541.60 545.84 0.34 0.19 0.98 0.37 0.58 2448 185.00 541.60 545.64 0.74 0.34 0.19 0.98 0.37 0.58 2448 185.00 541.60 542.64 543.69 1.25 0.61 5.80 5.80 1.02 2434 22.00 542.64 544.00 1.25 0.61 5.80 0.51 0.51 2434 57.00 542.64 544.00 1.25 0.69 6.67 2.60 0.51 0.51 2434 57.00 542.64 544.40 1.54 0.69 6.67 2.60 0.51 0.51 0.51 0.51 0.51 0.51 0.51 0.51 0.51 0.51 0.52 0.51 0.51 0.51 0.51 0.52 0.51 0.52 0.52 0.51 <td< td=""><td>Upper</td><td>2448</td><td>30.00</td><td>541.60</td><td>544.15</td><td>0.13</td><td>70.0</td><td>0.23</td><td></td><td>0.20</td><td>1.70</td><td>0.20</td><td></td><td>25.06</td></td<>	Upper	2448	30.00	541.60	544.15	0.13	70.0	0.23		0.20	1.70	0.20		25.06
2448 61.60 644.68 0.34 0.14 0.09 0.07 0.058 2448 1195.00 641.60 645.68 0.74 0.34 3.31 0.05 1.02 2434 22.00 642.64 643.59 1.25 0.61 6.59 2.65 0.51 2434 22.00 642.64 643.76 1.25 0.61 6.29 2.65 0.51 2434 20.00 642.64 643.76 1.25 0.61 6.29 2.65 0.51 2434 30.00 642.64 643.76 1.25 0.61 6.29 0.55 0.51 2434 61.00 642.64 644.40 1.52 0.61 6.20 0.51 0.51 2434 61.00 642.64 644.40 1.54 1.54 0.68 6.67 0.51 0.51 2434 1.50 642.84 0.43 1.54 0.43 1.34 1.11 0.61 0.58 0.51 0.	Upper	2448	57.00	541.60	544.58	0.24		0.58			2.38	0.43		31.09
2448 195 00 541.60 546.68 0,74 0.34 3.31 0.85 1.02 2434 220 542.64 543.59 1.25 1.25 5.60 5.60 1.02 2434 40.00 542.64 544.09 1.25 0.64 5.89 2.56 0.51 2434 40.00 542.64 543.76 1.34 0.89 6.67 2.67 0.81 2434 30.00 542.64 543.76 1.34 0.89 6.67 2.67 0.81 2434 81.00 542.64 544.40 1.54 0.84 6.67 2.67 0.81 2434 81.00 542.64 545.06 2.51 1.38 19.29 6.05 0.51 2447 43.00 542.01 543.69 0.64 0.39 2.30 1.11 0.68 2417 43.00 542.01 543.89 0.64 0.39 0.30 1.13 0.13 2417 81.	Upper	2448	81.00	541.60	544.84	0.34	0.19	0.98		0.58	2.88	0.58	40.78	34.72
2434 22.00 542.64 543.59 1.25 6.60 5.60	Upper	2448	195.00	541.60	545.68	0.74	0.34	3.31	0.85		4.48	0.83	79.16	58.76
2434 22 00 542 84 543.59 1,25 1,26 560 560 2434 44,00 542 64 543.76 1,25 0,61 5.99 2.56 0,51 2434 30,00 542 64 544.19 1,32 0,64 6.32 6.32 0,51 2434 81,00 542 64 544.19 1,32 0,84 8,64 3.24 1,11 2434 81,00 542 64 544.60 1,54 0,84 8,64 3.24 1,11 2434 81,00 542 64 545.06 2.51 1,38 19.29 6.03 1,84 2447 243 542.01 543.69 0,48 0,43 1,13 1,13 0,13 2417 240 542.01 543.69 0,64 0,39 2.30 1,18 0,13 2417 30,00 542.01 543.89 0,48 0,47 1,13 0,13 0,48 2409 542.01 543.81														
2434 44.00 54264 544.03 1.25 0.61 5.89 2.56 0.51 2434 30.00 542.64 543.76 1.34 1.34 6.32 6.32 0.51 2434 30.00 542.64 543.76 1.34 1.34 6.32 6.32 0.81 2434 81.00 542.64 544.40 1.54 0.69 6.67 2.67 0.81 2434 81.00 542.64 544.40 1.54 0.84 8.64 3.24 1.13 2434 195.00 542.01 543.26 0.48 0.43 1.37 1.13 0.13 2417 240 542.01 543.26 0.64 0.33 2.30 1.13 0.13 2417 30.00 542.01 543.69 0.64 0.35 1.13 0.13 2417 410 542.01 543.69 0.64 0.32 1.16 0.53 2417 810 542.01 543.81	Upper	2434	22.00	542.64	543.59	1.25	1.25	5.60			4.48		4.92	8.02
2434 30,00 542.64 543.76 1.34 1.34 6.32 7.11 7.11 7.11 7.11 7.11 7.11 7.11 7.12 7.13	Upper	2434	44.00	542.64	544.03	1,25	0.61	5.39		0.51	4.78	0.51	10.58	24.49
2434 57.00 542.64 544.19 1.32 0.69 6.67 2.67 0.81 2434 181.00 542.64 544.40 1.54 0.84 8.64 3.24 1.11 2434 181.00 542.64 542.66 542.64 6.45.06 2.51 1.38 18.29 6.03 1.11 247 247 22.00 542.64 545.06 2.51 1.38 1.92 6.03 1.11 2417 22.00 542.01 543.86 0.64 0.39 2.30 1.18 0.63 2417 44.00 542.01 543.81 0.64 0.39 2.30 1.19 0.63 2417 57.00 542.01 543.81 1.66 0.36 1.77 0.68 2417 56.00 542.01 543.81 1.66 0.36 1.73 0.68 2409 52.00 542.01 543.81 0.10 0.09 0.15 0.15 0.15 0.05	Upper	2434	30.00	542.64	543.76	1.34	1.34	6.32			4.71		96.36	9.35
2434 81.00 542.64 544.40 1.54 0.84 8.64 3.24 1.11	Upper	2434	57.00	542.64	544.19	1.32	69.0	6.67	2.67	0.81	5.05	0.82	14.70	27.21
2434 195.00 542.64 545.06 2.51 1.38 19.29 6.03 1.84	Upper	2434	81.00	542.64	544.40	1.54	0.84	8.64	3.24	1.11	5.61	1.13	20.96	30.87
2417 22.00 542.01 543.26 0.48 0.43 1.37 1.23 0.13 2417 44.00 542.01 543.69 0.64 0.39 2.30 1.19 0.53 2417 30.00 542.01 543.46 0.62 0.37 1.60 1.07 0.34 2417 51.00 542.01 543.46 0.65 0.37 1.60 1.07 0.34 2417 81.00 542.01 543.81 1.66 0.96 9.72 4.53 0.96 2417 195.00 542.01 544.88 2.14 1.03 15.46 4.52 1.36 2409 22.00 540.95 543.31 0.10 0.09 0.15 0.15 0.04 0.05 0.05 2409 30.00 540.95 543.50 0.14 0.09 0.15 0.16 0.05 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16	Upper	2434	195.00	542.64	545.06	2.51	1.38	19.29		1.84	7.68	1.82	44.80	43.31
2417 22.00 543.06 0.48 0.43 1.37 1.23 0.13 2417 44,00 542.01 543.69 0.64 0.39 2.30 1.19 0.53 2417 30,00 542.01 543.46 0.62 0.37 1.60 1.07 0.34 2417 51,00 542.01 543.81 1.66 0.96 3.65 1.73 0.68 2417 81,00 542.01 543.81 1.66 0.96 9.72 4.53 0.96 2417 195.00 542.01 544.88 2.14 1.03 15.46 4.52 1.36 2409 22.00 540.95 543.31 0.10 0.09 0.15 0.15 0.07 0.07 2409 30.00 540.95 543.74 0.21 0.10 0.09 0.14 0.09 0.15 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.														
2417 44,00 543.69 0.64 0.39 2.30 1.19 0.63 2417 30.00 542.01 543.6 0.52 0.37 1.60 1.07 0.34 2417 57.00 542.01 543.79 0.87 0.50 3.65 1.73 0.68 2417 81.00 542.01 543.81 1.66 0.96 9.72 4.53 0.96 2417 195.00 542.01 544.68 2.14 1.03 15.46 4.32 1.36 2409 22.00 540.95 543.31 0.10 0.09 0.15 0.12 0.07 2409 30.00 540.95 543.74 0.21 0.12 0.44 0.23 0.15 0.16 2409 57.00 540.95 543.50 0.14 0.09 0.15 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.1	Upper	2417	22.00	542.01	543.26	0.48	0.43	1.37	1.23	0.13		0.13	7.70	11.12
2417 30.00 542.01 543.46 0.52 0.37 1.60 1.07 0.34 2417 57.00 542.01 543.81 1.66 0.96 3.65 1.73 0.68 2417 81.00 542.01 543.81 1.66 0.96 9.72 4.53 0.96 2417 195.00 542.01 544.68 2.14 1.03 15.46 4.32 1.36 2409 22.00 540.95 543.31 0.10 0.09 0.15 0.12 0.07 2409 30.00 540.95 543.74 0.21 0.12 0.44 0.23 0.15 0.16 2409 57.00 540.95 543.50 0.14 0.09 0.23 0.16 0.16 2409 81.00 540.95 543.86 0.23 0.16 0.75 0.75 0.16 2409 195.00 540.95 543.87 0.51 0.56 0.75 0.76 0.76 0.76 <	Upper	2417	44.00	542.01	543.69	0.64	0.39	2.30	1.19	0.53	3.58	0.54	14.36	20.25
2417 57.00 542.01 543.79 0.87 0.50 3.65 1.73 0.68 2417 81.00 542.01 543.81 1.66 0.96 9.72 4.53 0.96 2417 195.00 542.01 544.68 2.14 1.03 15.46 4.32 1.36 2409 22.00 540.95 543.31 0.10 0.09 0.15 0.12 0.07 2409 30.00 540.95 543.74 0.21 0.12 0.44 0.23 0.16 2409 57.00 540.95 543.86 0.24 0.16 0.75 0.75 0.16 2409 81.00 540.95 543.86 0.29 0.16 0.75 0.75 0.76 2409 81.00 540.95 543.87 0.51 0.51 0.77 0.56 2409 195.00 540.95 544.17 2.26 1.08 0.76 0.77 0.96 2409 195.00 <t< td=""><td>Upper</td><td>2417</td><td>30.00</td><td>542.01</td><td>543.46</td><td>0.52</td><td>0.37</td><td>1.60</td><td>1.07</td><td>0.34</td><td>3,10</td><td>0.35</td><td>10.25</td><td>15.28</td></t<>	Upper	2417	30.00	542.01	543.46	0.52	0.37	1.60	1.07	0.34	3,10	0.35	10.25	15.28
2417 81.00 543.81 1.66 0.96 9.72 4.53 0.96 2417 195.00 542.01 544.68 2.14 1.03 15.46 4.32 1.36 2409 22.00 540.95 543.31 0.10 0.09 0.15 0.12 0.07 2409 44.00 540.95 543.74 0.21 0.12 0.44 0.23 0.16 2409 57.00 540.95 543.86 0.14 0.09 0.75 0.16 2409 81.00 540.95 543.86 0.23 0.16 0.75 0.76 2409 81.00 540.95 543.87 0.51 0.75 0.75 0.76 2409 81.00 540.95 543.87 0.51 0.76 0.77 0.51 2409 195.00 540.95 544.17 2.26 1.08 0.77 0.56	Upper	2417	57.00	542.01	543.79	0.87	0:20	3.65		0.68	4.22	0.69	16.53	22.44
2417 195.00 542.01 544.68 2.14 1.03 15.46 4.32 1.36 2409 22.00 540.95 543.31 0.10 0.09 0.15 0.12 0.07 2409 44.00 540.95 543.74 0.21 0.12 0.44 0.23 0.27 2409 57.00 540.95 543.50 0.14 0.09 0.23 0.16 0.16 2409 57.00 540.95 543.86 0.29 0.16 0.75 0.36 0.36 2409 81.00 540.95 543.37 0.51 0.51 0.77 0.51 2409 195.00 540.95 543.97 0.51 0.57 0.56 0.56	Upper	2417	81.00	542.01	543.81	1.66	0.96	9.72		96'0	5.86	76.0	17.10	22.98
2409 22.00 540.95 543.31 0.10 0.09 0.15 0.12 0.07 2409 44.00 540.95 543.74 0.21 0.21 0.44 0.23 0.27 2409 30.00 540.95 543.50 0.14 0.09 0.23 0.15 0.16 2409 57.00 540.95 543.86 0.29 0.16 0.75 0.36 2409 81.00 540.95 543.37 0.51 0.51 0.77 0.51 2409 195.00 540.95 544.17 2.26 1.08 16.71 6.02 0.36	Upper	2417	195.00	542.01		2.14	1.03	15.46		1,36	7.23	1.54	46.52	45.45
2409 22.00 540.95 543.31 0.10 0.09 0.15 0.12 0.07 2409 44.00 540.95 543.74 0.21 0.21 0.04 0.23 0.27 2409 30.00 540.95 543.50 0.14 0.09 0.23 0.15 0.16 2409 57.00 540.95 543.86 0.29 0.16 0.75 0.36 0.36 2409 81.00 540.95 543.87 0.51 0.51 0.77 0.51 0.51 2409 195.00 540.95 544.17 2.26 1.08 16.71 6.02 0.36 0.96														
2409 44.00 540.95 543.74 0.21 0.12 0.14 0.23 0.27 2409 30.00 540.95 543.50 0.14 0.09 0.23 0.16 0.16 2409 57.00 540.95 543.86 0.29 0.16 0.75 0.36 0.36 2409 81.00 540.95 543.97 0.51 0.51 0.77 0.51 2409 195.00 540.96 544.17 2.26 1.08 16.71 6.02 0.36	Upper	2409	22.00	540.95	543.31	0.10	0.09	0.15		0.07	1.44	70.0	15.34	13.24
2409 30.00 540.95 543.50 0.14 0.09 0.23 0.15 0.16 2409 57.00 540.95 543.86 0.29 0.16 0.75 0.36 0.36 2409 81.00 540.95 543.97 0.51 0.51 0.77 0.51 2409 195.00 540.96 544.17 2.26 1.08 16.71 6.02 0.36	Upper	2409	8.4	540.95	543.74	0.21	0.12	0.44			2.15	0.28	23.14	22.51
2409 57.00 540.95 543.86 0.29 0.16 0.75 0.36 0.36 2409 81.00 540.95 543.97 0.51 0.51 0.77 0.51 2409 195.00 540.95 544.17 2.26 1.08 16.71 6.02 0.36	Upper	2409	30.00	540.95	543.50	0.14	0.09	0.23			1.72	0.16	18.35	17.41
2409 81.00 540.95 543.97 0.51 0.27 1.75 0.77 0.51 2409 195.00 540.95 544.17 2.26 1.08 16.71 6.02 0.96	Upper	2409	27.00	540.95	543.86	0.29	0.16	0.75	0.36	0.36	2.59	0.36	25.99	25.06
. 2409 195.00 540.95 544.17 2.26 1.08 16.71 6.02 0.96	Upper	2409	81.00	540.95	543.97	0.51	0.27	1.75	0.77	0.51	3.45	0.52	28.82	27.35
	Upper	2409	195.00	540.95	544.17	2.26	1.08	16.71	6.02	0.96	7.41	1.21	35.00	34.50
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HEC-RAS Plan: UpReachRev7-14 River. Tanyard Branch Reach: Upper (Continued)

Upper Upper Upper Upper Upper Upper	The second secon		i			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	50.5	105 DAS		200		200	
	worden der mer geben der	(cfs)	(tt)	(ft)	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(fl/s)	(th/s)	(LAS)	(sq ft)	(H)
	2396	22.00	542.00	542.95	1.25	1,25	5.61	5.61		4.48		4.91	8.01
	2396	44.00	542.00	543.42	1.12	0.40	5.11	1.39	0.48	4.55	0.48	12.52	39.15
	2396	30.00	542.00	543.12	1.34	1.34	6.33	6.33		4.72		6.36	9.35
	2396	57.00	542.00	543.61	0.99	0.32	4.39	0.80	0.63	4.42	0.63	22.67	65.12
	2396	81.00	542.00	543.80	1.03	0.34	4.78	0.74	0.87	4.62	97.0	36.95	89.83
	2396	195.00	542.00	544.20	1.46	09'0	8.35	1.43	1.55	5.73	1.12	81.78	120.42
	2374	22:00	541.16	542.44	0.44	0.27	1.22	0.73	0.16	2.77	0.16	8.19	17.06
Upper	2374	44.00	541.16	542.94	0.40	0.14	1.13	0.22	0.46	2.85	0.46	28.31	63.26
Upper	2374	30.00	541.16	542.64	0.44	0.17	1.28	0.38	0.35	2.89	0.35	13.60	35.89
Upper	2374	57.00	541.16	543.16	0.34	0.13	0.94	0.17	0.55	2.73	0.49	44.12	79.40
Upper	2374	81.00	541.16	543.47	0:30	0.12	0.78	0.14	0.65	2.62	0.51	71.95	99.89
	2374	195.00	541.16	544.15	0.37	0.17	1.14	0.22	76.0	3.08	0.67	155.28	137.75
Upper	2361	22.00	540.10	542.46	0.10	90:0	0.14	0.08	90.08	1.44	0.08	15.81	20.28
Upper	2361	44.00	540.10	542.94	0.17	90.0	0.33	0.07	0.26	1.96	0.26	34.96	59.94
Upper	2361	30.00	540.10	542.66	0.13	50.0	0.22	70.0	0.16	1.68	0.16	21.48	36.78
Upper	2361	57.00	540.10	543.15	0.19	90.0	0.39	70.0	0.35	2.10	0.25	49.09	76.93
Upper	2361	81.00	540.10	543.45	0.20	20.0	0.46	0.07	0.48	2.25	0.30	76.04	101.68
	2361	195.00	540.10	544.12	0.32	0.12	0.94	0.15	0.82	2.94	0.52	162.44	151.38
Upper	2346	22.00	541.15	542.10	1.24	1.24	5.52	5.52		4.45		4.94	8.04
Upper	2346	44.00	541.15	542.49	1.46	8.1	7.45	4.90	0.43	5.11	0.43	8.97	15.49
Upper	2346	30.00	541.15	542.27	1.34	1.34	6.31	6.31		4.71		6.37	9,35
Upper	2346	57.00	541.15	542.69	1.44	0.78	7.60	3.47	0.69	5.26	69'0	12.75	23.04
Upper	2346	81.00	541.15	542.96	1.54	0.73	8.65	2.91	0.93	5.64	0.93	20.25	33.29
Upper	2346	195.00	541.15	543.74	1.46	0.47	8.70	1.14	1.21	5.95	1.11	80.55	123.34
ï													
Opper	2331	22.00	540.56	541.81	0.48	0.39	1.38	1.12	0.13	2.88	0.13	7.70	12.45
	2331	44.00	540.56	542.29	0.51	0.19	1.66	0.42	0.39	3.23	0.53	20.62	45.42
Upper	2331	30.00	540.56	542.00	0.51	0.27	1.56	0.73	0.33	3.08	0.34	11.08	22.33
	2331	57.00	540.56	542.48	0.51	0.19	1.70	0.34	0.48	3.31	09:0	31.27	61.73
	2331	81.00	540.56	542.76	0,53	0.20	1.84	0.31	0.58	3.46	0.69	50.98	83.92
Upper	2331	195.00	540.56	543.54	0.49	0.21	1.76	0:30	0.89	3,55	0.94	141.74	136.01
	2322	22.00	539.51	541.85	0.10	0.07	0.15	0.10	20.0	1.46	20.0	15.30	16.91
	2322	8.4	539.51	542.32	0.19	0.08	0.38	0.12	0.32	2.05	0.29	28.90	38.06
	2322	30.00	539.51	542.04	0.14	90:0	0.24	0.10	0.17	1.72	0.16	19.86	28.56
	2322	27.00	539.51	542.50	0.23	0.10	0.53	0.16	0.41	2:32	0.37	36.55	44.54
	2322	81.00	539.51	542.75	0.32	0.14	0.88	0.23	0.55	2.77	0.49	48.62	53.19
Upper	2322	195.00	539.51	543.40	0.65	0.23	2.69	0.43	0.62	4.15	96'0	105.26	110.08

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

2231 (46) (70) (46) (70) (46) (47) (46) (47) (48) <th< th=""><th>Reach</th><th>River Sta</th><th>O Total</th><th>Reach River Sta O Total Min Ch El W.S. Elev Shear Chan</th><th>W.S. Flev</th><th>Shear Chan</th><th>Shear Total</th><th>Power Chan</th><th>Power Total</th><th>Vellet</th><th>Vel Chal</th><th>Vel Richt</th><th>Flow Area</th><th>Ton Width</th></th<>	Reach	River Sta	O Total	Reach River Sta O Total Min Ch El W.S. Elev Shear Chan	W.S. Flev	Shear Chan	Shear Total	Power Chan	Power Total	Vellet	Vel Chal	Vel Richt	Flow Area	Ton Width
2221 2200 580 (1) 1,250 1,250 6.60 4.48 0.44 6.60 4.40 0.04 6.60 4.70 0.04 5.00 4.70 0.04 2.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04 6.70 0.04	***************************************	the state of the s	(cfs)	(#)	€	(lb/sq ft)	(lþ/sd ff)	(lb/ft s)	(lb/ft s)	(ft/s)	(s/ti)	(s/tl)	(sq ft)	£
2221 4400 580 9 142 128 7.18 6.18 6.18 6.14 6.04 1.42 0.84 6.12 0.24 6.04 6.03 0.44 0.89 6.04 1.42 0.88 0.89 6.00.31 1.42 0.84 6.13 6.24 0.71 0.68 0.47 0.68 0.47 0.68 0.41 0.69 6.17 0.68 0.41 0.68 0.41 0.68 0.41 0.68 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.41 0.69 0.69 0.61 0.69 0.41 0.69 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61 0.61 <	Upper	2231	22.00		540.14	1.25	1.25	5.60			4.48		4.92	8.02
2221 5100 58919 54074 134 134 6.81 6.81 6.81 6.71 0.88 6.71 138 0.81 7.89 6.87 7.89 6.87 7.89 6.87 7.89 6.87 7.89 6.87 7.89 6.87 7.89 6.87 7.89 6.87 7.89 6.87 6.81 6.82	Upper	2231	44.00		540.54	1.42	0.88	7.18		0.44	5.05	0.44	9.22	17.41
2231 550 58949 54074 1,39 0.67 719 223 0.68 517 0.68 617 0.68 617 0.68 617 0.68	Upper	2231	30.00		540.31	1.34	1.34	6.31	6.31		4.71		6.37	9.35
2221 1650 68618 540.88 1,47 0.64 811 224 6.91 6581 0.91 6581 0.91 6581 0.91 6581 0.91 0.92 1,42 0.98 1,62 0.98 0.91 1,53 0.91 0.93 0.91 0.93 0.91 0.93 0.91 0.93 0.91 0.93 0.91 0.93 0.91 0.93 0.91 0.93 0.93 0.91 0.93 0.91 0.93 0.91 0.93 0.91 0.93 <t< td=""><td>Upper</td><td>2231</td><td>00'29</td><td></td><td>540.74</td><td>1.39</td><td>29.0</td><td>7.19</td><td></td><td>0.68</td><td>5,17</td><td>0.68</td><td>13.60</td><td>27.11</td></t<>	Upper	2231	00'29		540.74	1.39	29.0	7.19		0.68	5,17	0.68	13.60	27.11
2198 155.00 558.14 541.71 1,77 0.08 1122 1,90 1,10	Upper	2231	81.00		540.99	1.47	0.64	8.11	2.34	0.91	5.51	0.91	22.20	39.75
2199 22 00 558 19 558 46 0.46 0.25 1.29 0.66 0.65 0.51 2.89 0.61 2199 3.00 558 19 558 26 0.64 0.25 1.46 0.66 0.57 3.29 0.51 2199 3.00 558 16 540,34 0.67 0.66 0.55 3.45 0.51 2199 57,00 558 16 540,34 0.67 0.25 3.45 0.57 2199 57,00 558 16 540,34 0.67 0.26 0.77 3.46 0.77 2199 750 570 587 13 588 46 540,39 0.71 0.75 0.77 3.46 0.77 2199 750 570 588 47 540,28 0.71 0.78 0.77 1.46 0.77 0.74 0.77 1.46 0.77 0.78 0.77 0.74 0.77 0.74 0.77 0.74 0.77 0.74 0.77 0.74 0.74	Upper	2231	195.00		541.71	1.77	0.68	11.52		1.30	6.51	1.24	69.63	92.68
21999 4200 558419 558-46 0.48 0.035 0.04 0.045 0.05 0.04 0.05 0.05 21999 4200 558419 558-46 0.48 0.05 0.05 0.05 0.05 0.05 21999 5000 528419 558-61 0.48 0.05 0.05 0.05 0.05 0.05 0.05 21999 5100 528419 54041 0.05 0.02 0.05														
2199 4400 598.18 598.89 0.61 0.23 1.65 0.61 0.51 0.51 0.51 0.51 0.51 0.51 0.52 0.51 0.52	Upper	2199	22.00		539.46	0.46	0.35	1.28		0.15	2.81	0.15	7.92	13.25
2199 5300 6381 6386 0.48 0.25 145 0.66 0.65 3.00 0.58 3.00 0.58 3.00 0.58 3.00 0.58 3.00 0.58 3.00 0.58 3.00 0.58 3.00 0.58 3.00 0.57 3.88 0.01 0.02	Upper	2199	44.00		539.93	0.51	0.23	1.65		0.51	3.23	0.51	19.60	36.39
2199 F7,00 SSR 19 54,01 0.56 0.24 1.83 0.52 0.45 0.56 0.57 0.58 0.57 0.58 0.57 0.58 0.57 0.58 0.57 0.58 0.57 0.58 0.57 0.58 0.57 0.58 0.57 0.58 0.14 0.05 0.75 0.05 0.77 0.58 0.77 0.58 0.77 0.58 0.77 0.58 0.77 0.78 0.75 0.75 0.75 0.75 0.75 0.76 0.75	Upper	2199	30.00		539.65	0,48	0.25	1.45		0.35	3.00	0.35	11.50	22.99
2199 81 00 588 19 540.34 0.67 0.30 2 62 0.67 0.75	Upper	2199	22.00		540.11	95'0	0.24	1.93		0.62	3.45	0.61	26.86	44.43
2189 1456.00 580.19 1,14 0,65 61.0 1,27 1,17 6,34 1,17 2186 22.00 587.13 589.48 0.10 0.06 0.05 0.07 1,45 0.07 2186 22.00 587.13 589.68 0.16 0.06 0.23 0.09 0.78 1,70 0.05 2186 57.00 587.13 540.38 0.21 0.06 0.23 0.09 0.78 1,70 0.05 2186 57.00 587.13 540.38 0.21 0.08 0.73 0.10 0.09 0.77 0.10 0.05 0.77 0.00 0.07 0.10 0.05 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 0.06 0.07 <td>Upper</td> <td>2199</td> <td>81.00</td> <td></td> <td>540.34</td> <td>29'0</td> <td>00:00</td> <td>2.62</td> <td>0.63</td> <td>0.77</td> <td>3.88</td> <td>0.75</td> <td>38.29</td> <td>54.18</td>	Upper	2199	81.00		540.34	29'0	00:00	2.62	0.63	0.77	3.88	0.75	38.29	54.18
2186 22 00 58713 58846 0.10 0.06 0.05 0.07 1.46 0.07 2186 44.00 58713 583.66 0.18 0.06 0.23 0.08 0.07 0.09 0.05 1.70 0.06 2186 57.00 58713 563.66 0.13 0.06 0.23 0.08 0.16 1.70 0.06 0.06 0.23 0.09 0.05 0.06 0.07 0.09 0.06 0.07 0.09 0.04 0.09 0.06 0.07 0.06 0.07 0.09 0.04 0.06 0.07 0.09 0.04 0.06 0.07 0.09 0.04 0.09 0.04 0.06 0.04 0.06 0.04 0.06 0.04 0.06 0.04 0.06 0.04 0.06 0.04 0.06 0.04 0.06 0.04 0.06 0.04 0.06 0.06 0.04 0.06 0.04 0.06 0.04 0.06 0.04 0.06	Upper	2199	195.00		540.99	1.14	0.52	6.10		1.21	5.34	1.17	82.91	81.75
2166 2200 637,13 589.46 0.10 0.06 0.15 0.09 0.07 1.46 0.07 2186 34,00 537,13 589.86 0.18 0.06 0.23 0.09 0.18 1.70 0.16 2186 57,00 537,13 540.18 0.13 0.06 0.47 0.10 0.28 2.23 0.36 2186 57,00 537,13 540.13 0.23 0.01 0.08 2.23 0.09 0.18 0.09 0.18 0.09 0.18 0.09 0.04 0.10 0.38 0.23 0.04 0.10 0.38 0.39 0.34 0.38 0.17 0.09 0.43 0.19 0.06 0.43 0.19 0.08 0.43 0.43 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.45 0.43 0.44 0.45 0.44 0.45 0.44 0.45 0.44 0.44 0.44 0.44 0.44 0.44														
2186 44.00 557.13 558.96 0.18 0.06 0.05 0.06 0.05 1.70 0.06 2186 50.00 557.13 559.68 0.13 0.06 0.02 0.01 0.05 1.70 0.06 2186 50.00 557.13 540.38 0.23 0.01	Upper	2186	22.00		539.48		90.0	0.15		70'0	1.45	70.0	15.59	18.78
2186 30.00 537.13 559.68 0.13 0.06 0.23 0.09 0.16 0.10 0.10 0.01 0.01 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.03 0.04	Upper	2186	44.00		539.95		90.0	0.35		0.26	2.00	0.26	32.66	54.22
2166 6700 657713 64013 0.23 0.047 0.10 0.035 2.22 0.036 2186 1860 18100 55713 540.36 0.23 0.01 0.03 0.048 2.86 0.047 2186 18500 55713 540.36 0.028 0.01 0.07 0.05 0.04	Upper	2186	30.00		539.68		90:0	0.23	90.08	0.16	1.70	0.16	20.79	33.79
2186 81 00 587.13 540.36 0.28 0.14 0.75 0.15 0.45 2.61 0.47 2186 1950 587.13 540.22 0.67 0.25 2.23 0.43 0.86 3.89 0.64 2171 2200 588.17 559.12 1.26 1.26 6.50 6.61 4.48 0.64 2171 44.00 558.17 559.24 1.26 1.24 6.31 6.31 4.71 6.45 4.48 0.64 2171 50.00 558.17 559.24 1.26 0.24 6.31 6.31 4.48 0.65 0.45 0.45 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.79 0.74 0.76 0.78 0.78 0.76 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78	Upper	2186	57.00		540,13		80.08	0.47		0.35	2.23	0.35	43.23	62.89
2166 195 OD 537.13 541.02 0.57 0.25 0.26 0.43 0.68 3.68 0.64 2177 22.00 658.17 559.12 1.25 1.25 560 6.04 4.48 0.78 2177 44.00 588.17 539.24 1.38 0.72 6.71 3.26 0.45 4.36 0.45 2177 44.00 588.17 539.24 1.38 0.72 6.71 3.26 0.45 4.36 0.45 2177 81.00 588.17 540.07 1.28 0.54 6.39 0.45 6.73 4.48 0.45 0.45 2177 81.00 588.17 540.06 1.28 0.54 6.19 0.47 4.46 0.45 0.46 1.41 0.74 0.46 0.46 0.49 0.47 0.46 0.46 0.49 0.46 0.46 0.46 0.46 0.46 0.46 0.46 0.46 0.46 0.46 0.46 0.46 </td <td>Upper</td> <td>2186</td> <td>81.00</td> <td></td> <td>540.36</td> <td>0.28</td> <td>0.11</td> <td>0.73</td> <td></td> <td>0.48</td> <td>2.61</td> <td>0.47</td> <td>58.93</td> <td>71.75</td>	Upper	2186	81.00		540.36	0.28	0.11	0.73		0.48	2.61	0.47	58.93	71.75
2171 22.00 588.17 589.24 1.28 1.25 5.60 5.60 5.60 4.48 4.48 2171 44.00 588.17 539.24 1.36 0.72 6.71 3.25 0.45 4.86 0.45 2171 40.00 588.17 539.24 1.36 0.72 6.71 3.25 0.45 4.96 0.67 2171 57.00 538.17 539.74 1.28 0.54 6.39 1.99 0.67 4.96 0.67 2171 185.00 538.17 540.01 1.22 0.48 6.39 1.41 0.87 4.71 6.76 2171 185.00 538.17 540.01 1.22 0.48 6.39 1.44 6.76 0.67 1.45 2171 185.00 538.17 540.01 1.22 0.48 6.19 1.41 0.87 4.86 0.67 2151 217 540.01 1.22 0.48 1.27 0.63 0.1	Upper	2186	195.00		541.02	0.57	0.25	2.23	0.43	0.86	3.89	0.84	114.36	96.83
2171 22.00 558.17 539.12 1.25 1.25 5.60 5.60 6.60 4.48 9.45 0.45 4.40 538.17 539.24 1.28 0.72 6.71 6.31 6.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 0.45 6.31 1.39 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 4.95 0.45 0.45 4.95 0.45														
2171 44.00 538.17 539.54 1.36 0.73 6.71 3.26 0.45 4.59 0.45 0.45 0.45 0.45 0.45 0.45 0.47 0.48 0.43 0.43 0.47 0.47 0.48 0.48 0.49 0.47 0.49 0.48 0.49 0.47 0.48 0.49 0.47 0.48 0.48 0.44 0.47 0.48 0.49 0.47 0.48 0.44 0.47 0.48 0.49 0.47 0.48 0.44 0.48 0.44 0.44 0.48 0.48 0.41 1.10 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48	Upper	2171	22.00	538.17	539.12	1.25	1.25	5.60	5.60		4.48		4.91	8.01
2171 30.00 558.17 559.28 1.34 6.34 6.34 6.34 6.34 6.34 6.34 4.71 4.71 4.71 9.057 4.72 6.34	Upper	2171	44.00		539.54	1.36	0.72	6.71	3.25	0.45	4.95	0.45	9.74	21.29
2171 57.00 539.17 539.74 1.28 0.54 6.39 1.99 0.67 4.98 0.67 2171 81.00 538.17 540.01 1.22 0.48 6.19 1.41 0.87 5.06 0.68 2171 195.00 538.17 540.01 1.22 0.48 6.19 1.41 0.87 5.06 0.68 2151 22.00 537.42 538.89 0.45 0.23 1.27 0.63 0.15 0.14 0.16 0.16 0.16 0.17 0.69 0.60 0.66 0.60 0.66 0.60 0.66 0.60 0.76	Upper	2171	30.00		539.29	1.32	1.34	6.31	6.31		4.71		6.36	9.35
2171 81.00 538.17 540.01 1,12 0,48 6.19 1,41 0,67 5.06 0,86 2171 195.00 538.17 540.56 1,36 0.36 1,74 6.76 1,45 2151 220 537.42 538.69 0.42 0.23 1,27 0.63 0.18 0.16 0.19 0.17 6.63 0.15 1,17 6.76 0.15 1,14 0.19 0.14 0.19 0.14 0.19 0.18 0.16 0.19 0.18 0.14 0.19 0.14 0.19 0.14 0.19 0.14 0.19 0.14 0.19 0.14 0.19 0.14 0.19 0.18 0.14 0.19 0.18 0.19 0.19 0.19 0.19 0.19 0.14 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19 0.19	Upper	2171	57.00		539.74	1.28	0.54	6:30	1.99	0.67	4.98	79.0	15.41	35.04
2171 195.00 538.17 540.56 1.96 0.96 13.22 3.09 1.74 6.76 1.45 2151 22.00 537.42 538.69 0.45 0.23 1.27 0.63 0.14 1.10 0.19 0.15 2.81 0.15 2151 44.00 537.42 538.69 0.42 0.13 1.10 0.19 0.46 2.81 0.50 0.34 0.28 0.34 0.28 0.34 0.39 0.34 0.36 0.36 0.36 0.36 0.36 0.36 0.36 0.36 0.36 0.38 0.34 0.38 0.38 0.38 0.38 0.38 0.38 0.38 0.36 0.46 0.28 0.18 0.76 0.39 0.36 0.38	Upper	2171	81.00		540.01	1.22	0.48	6.19		0.87	5.06	0.86	27.76	53.36
2151 22.00 537.42 538.69 0.45 0.23 1.27 0.63 0.15 2.81 0.15 2151 44.00 537.42 538.13 0.39 0.14 1.10 0.19 0.45 2.81 0.05 2151 44.00 537.42 538.90 0.42 0.13 1.20 0.25 0.34 2.82 0.34 2151 30.00 537.42 538.30 0.46 0.18 1.40 0.26 0.55 3.07 0.63 2151 195.00 537.42 539.36 0.61 0.26 0.26 0.55 3.07 0.63 2140 22.00 537.42 540.34 0.40 0.21 0.24 0.75 3.47 1.03 2140 22.00 536.36 538.72 0.10 0.04 0.14 0.05 0.05 3.47 1.03 2140 22.00 536.36 539.24 0.15 0.06 0.27 0.04 0.27 1	Upper	2171	195.00		540.56	1.96	96.0	13,22		1.74	6.76	1.45	99.09	67.02
2151 22.00 537.42 538.69 0.45 0.23 1.27 0.63 0.15 2.81 0.15 2151 44.00 537.42 538.13 0.39 0.14 1.10 0.19 0.46 2.81 0.50 2151 44.00 537.42 538.13 0.39 0.14 1.10 0.19 0.46 2.81 0.50 2151 30.00 537.42 538.89 0.64 0.13 1.20 0.25 0.34 2.82 0.34 2151 81.00 537.42 539.23 0.46 0.18 1.40 0.26 0.55 3.07 0.63 2151 81.00 537.42 539.34 0.61 0.21 1.25 0.26 0.55 3.07 0.63 2151 81.00 537.42 539.34 0.61 0.21 1.25 0.75 3.76 0.83 2140 220 536.38 539.14 0.15 0.04 0.14 0.05 0.05														
2151 44.00 537.42 538.13 0.39 0.14 1.10 0.19 0.46 2.81 0.50 2151 30.00 537.42 538.90 0.42 0.13 1.20 0.25 0.34 2.82 0.34 2151 30.00 537.42 539.23 0.46 0.13 1.20 0.25 0.34 2.82 0.34 2151 81.00 537.42 539.36 0.61 0.26 0.26 0.55 3.07 0.63 2151 81.00 537.42 539.36 0.61 0.26 2.18 0.70 3.60 0.83 2151 81.00 537.42 540.34 0.40 0.21 0.26 0.75 3.07 0.63 2140 22.00 536.34 0.40 0.10 0.04 0.14 0.05 0.04 0.14 0.05 0.08 0.14 0.03 2140 22.00 536.35 539.14 0.15 0.16 0.04 0.01	Upper	2151	22.00	537.42	538.69	0.45	0.23	1.27	0.63	0.15	2.81	0.15	8.18	20.76
2151 30,00 537.42 538.90 0.42 0.13 1.20 0.25 0.34 2.82 0.34 2151 57,00 537.42 539.23 0.46 0.18 1.40 0.26 0.55 3.07 0.63 2151 81,00 537.42 539.36 0.61 0.26 2.18 0.42 0.70 3.60 0.83 2151 195.00 537.42 540.34 0.61 0.21 1.26 0.72 0.72 0.73 0.73 0.83 2140 22.00 536.36 538.72 0.10 0.04 0.28 0.75 0.74 0.78 0.74 0.78 2140 22.00 536.36 539.14 0.15 0.04 0.27 0.04 0.27 1.44 0.08 0.14 0.05 0.04 0.27 0.04 0.27 0.04 0.27 0.16 0.28 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16 0.16<	Upper	2151	44.00	537.42	539.13	0.39	0.14	1.10	0.19		2.81	0.50	31.85	75.45
2151 57.00 537.42 539.23 0.46 0.18 1.40 0.26 0.55 3.07 0.63 2151 81.00 537.42 539.36 0.61 0.26 2.18 0.42 0.72 3.60 0.83 2151 195.00 537.42 540.34 0.61 0.21 1.25 0.72 0.72 3.47 1.03 1.03 2140 22.00 536.36 538.72 0.10 0.04 0.14 0.05 0.05 0.05 1.44 0.05 0.04 0.27 0.04 0.27 0.04 0.27 0.05	Upper	2151	30.00	537.42	538.90	0.42	0.13	1.20	0.25		2.82	0.34	15.99	54.20
2151 81.00 537.42 539.36 0.61 0.26 2.18 0.42 0.70 3.60 0.83 2151 195.00 537.42 540.34 0.40 0.21 1.25 0.28 0.75 3.17 1.03 1.03 2140 22.00 536.36 538.72 0.10 0.04 0.14 0.05 0.08 1.44 0.08 2140 30.00 536.36 538.72 0.10 0.04 0.27 0.04 0.27 0.08 1.44 0.08 2140 30.00 536.36 538.32 0.12 0.03 0.20 0.04 0.27 1.82 0.27 2140 57.00 536.36 539.24 0.12 0.06 0.39 0.06 0.35 0.06 0.35 0.06 0.35 0.06 0.35 0.06 0.35 0.06 0.35 0.06 0.35 0.06 0.35 0.06 0.35 0.36 0.36 0.36 0.36 0.36<	Upper	2151	92.00	537.42	539.23	0.46	0.18	1.40	0.26		3.07	0.63	39.90	79.09
2151 195.00 537.42 540.34 0.40 0.21 1.25 0.28 0.75 3.17 1.03 0.75 3.17 1.03 0.75 3.17 1.03 0.75	Upper	2151	81.00	537.42	539.36	0.61	0.26	2.18	0.42	0.70	3.60	0.83	50.45	83.63
2140 22.00 536.36 538.72 0.10 0.04 0.14 0.05 0.08 1.44 0.08 2140 44.00 536.36 538.72 0.16 0.04 0.27 0.04 0.27 1.82 0.27 2140 30.00 536.36 538.32 0.12 0.03 0.03 0.16 1.62 0.16 2140 57.00 536.36 539.24 0.19 0.06 0.39 0.06 0.35 2.07 0.36 2140 81.00 536.36 539.36 0.27 0.10 0.68 0.10 0.48 2.51 0.48 2140 195.00 536.36 540.34 0.27 0.10 0.50 0.06 0.35 0.06 0.35 0.06 0.36 0.06 0.36 0.07 0.48 0.48 0.70 0.48 0.70 0.48 0.70 0.48 0.70 0.48 0.70 0.70 0.70 0.70 0.70 0.70 0.70<	Upper	2151	195.00	537.42	540.34	0.40	0.21	1.25	0.28	0.75	3.17	1.03	149.35	119.59
2140 22 00 536.36 538.72 0.10 0.04 0.14 0.05 0.08 1.44 0.08 2140 44.00 536.36 539.14 0.15 0.04 0.27 0.04 0.27 1.82 0.27 2140 30.00 536.36 538.32 0.12 0.03 0.03 0.16 1.62 0.16 2140 81.00 536.36 539.34 0.19 0.06 0.39 0.06 0.35 2.07 0.35 2140 81.00 536.36 539.36 0.27 0.10 0.68 0.10 0.48 2.51 0.48 2140 195.00 536.36 540.34 0.21 0.10 0.50 0.10 0.70 2.38 0.70 1														
2140 44,00 536.36 539.14 0.15 0.04 0.27 0.04 0.27 1.82 0.27 2140 30,00 536.36 538.92 0.12 0.03 0.03 0.06 0.36 0.16 1.62 0.16 2140 57.00 536.36 539.36 0.19 0.06 0.39 0.06 0.35 2.07 0.36 2140 81.00 536.36 539.36 0.27 0.10 0.68 0.10 0.48 2.51 0.48 2140 195.00 536.36 540.34 0.21 0.10 0.50 0.10 0.78 0.70 0.78	Upper	2140	22.00	536.36	538.72	0.10	0.04	0.14	0.05	0.08	4.1	0.08	16.60	35.57
2140 30.00 536.36 538.92 0.12 0.03 0.20 0.03 0.16 1.62 0.16 2140 57.00 536.36 539.24 0.19 0.06 0.39 0.06 0.35 2.07 0.35 2140 81.00 536.36 539.36 0.27 0.10 0.68 0.10 0.48 2.51 0.48 2140 195.00 536.36 540.34 0.21 0.10 0.50 0.10 0.70 2.38 0.70 1	Upper	2140	44.00	536.36	539.14	0.15	0.04	0.27	0.04	0.27	1.82	0.27	49.32	103.63
2140 57.00 536.36 539.24 0.19 0.06 0.39 0.06 0.35 2.07 0.35 2140 81.00 536.36 539.36 0.27 0.10 0.68 0.10 0.48 2.51 0.48 2140 195.00 536.36 540.34 0.21 0.10 0.50 0.10 2.38 0.70 1	Upper	2140	30.00	536.36	538.92	0.12	0.03	0.20	0.03	0.16	1.62	0.16	28.18	80.56
2140 81.00 536.36 539.36 0.27 0.10 0.68 0.10 0.48 2.51 0.48 2140 195.00 536.36 540.34 0.21 0.10 0.50 0.10 0.70 2.38 0.70 1	Upper	2140	57.00	536,36	539.24	0.19	90.0	0.39	90.08	0.35	2.07	0.35	59.93	107.06
2140 195.00 536.36 540.34 0.21 0.10 0.50 0.10 0.70 2.38 0.70	Upper	2140	81.00	536.36	539.36	0.27	0.10	0.68	0.10	0.48	2.51	0.48	73.71	111.35
	Upper	2140	195.00	536.36	540.34	0.21	0.10	0.50	0.10	0.70	2.38	0.70	198.98	144.95
	Manual 2													

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Reach	Reach River Sta O Total Min Ch El W.S. Elav Shear Chan	O Total	Min Ch FI	W.S. Flev	Shear Chan	Shear Total	Power Chan	Power Total	Vol 1 off	Vel Chol	Vel Dight	Flow Area	Ton Midth
		(cfs)	€	€	(lb/sq ft)	(lb/sq ft)	(lb/fts)	(lb/ft s)	(ft/s)	(ft/s)	(Lagran)	(sq ft)	(ft)
Upper	2126	22.00	537.41	538.36	1.25	1.25	5.62	5.62		4.48		4.91	8.01
Upper	2126	44.00	537.41	538.88	0.88	0.23	3.57	0.56	0.48	4.06	0.48	18.24	72.23
Upper	2126	30.00	537.41	538.53	1.35	1.35	6.35	6.35		4.72		6.35	9.34
Пррег	2126	67.00	537.41	539.03	0.80	0.23	3.18	0.41	0.59	3.97	09'0	31.49	101.01
Upper	2126	81.00	537.41	539.18	0.83	0.30	3.43	0.51	0.80	4.13	08.0	47.51	106.41
Пррег	2126	195.00	537.41	540.32	0.24	0.13	09:0	0.14	0.81	2.47	0.80	191.92	147.64
Пррег	2111	22.00	536.82		0.48	0.34	1.38	0.97	0.13	2.88	0.13	7.75	14.51
Upper	2111	44.00	536.82		0.43	0.16	1.28	0.26	0.47	2.97	0.47	26.42	60.33
Upper	2111	30.00	536.82		0.49	0.20	1.47	0.48	0.34	3.02	0.34	12.45	32.77
Upper	2111	57.00	536.82		0.36	0.13	1.02	0.17	0.51	2.81	0.51	43.91	82.78
Upper	2111	81.00	536.82		0.26	0.11	0.64	0.11	0.55	2.46	0.55	81.40	103.40
Upper	2111	195.00	536.82	540.31	0.20	0.11	0.45	0.10	0.71	2.31	0.72	206.74	126.47
Upper	2102	22.00	535.77	538.11	0.10	90.0	0.15	90.0	70.0	1.46	0.16	15.47	20.77
Upper	2102	44.00	535.77	538.60	0.15	0.04	0.27	0.05	0.24	1.82	0.56	38.62	74.39
Upper	2102	30.00	535.77	538.31	0.13	0.05	0.22	90.0	0.16	1.68	0.36	21.71	42.50
Upper	2102	00'29	535.77	538.83	0.14	0.0	0.25	0.04	0.28	1.80	0.64	59.33	100.50
Upper	2102	81.00	535.77	539.21	0.10	0.04	0.16	0.03	0.32	1.61	0.73	103.67	125.98
Upper	2102	195.00	535.77	540.31	0.08	0.04	0.11	0.03	0.42	1.47	0.87	262.32	161.39
Upper	2091	22.00	536.81	537.76	1.25	1.25	5.60	5.60		4.48		4.91	8.01
Upper	2091	44.00	536.81	538.14	1.53	1.36	8.01	7.05	0.41	5.23	0.40	8.50	11.40
Upper	2091	30.00	536.81	537.93	£.	1.34	6.30	6.30		4.71		6.37	9.35
Upper	2091	92.00	536.81	538.31	1.64	1.30	9.14	6.93	0.69	5.57	0.68	10.67	13,35
Upper	2091	81.00	536.81	538.58	1.84	1.30	11.32	7.14	0.99	6.15	0.98	14.71	16.37
Upper	2091	195.00	536.81	539.74	1.64	0.50	10.61	1.57	1.00	6.46	0.95	62.26	86.71
Upper	2071	22.00	536.14	537.40	0.46	0.23	1.29	0.61	0,15	2.82	0.15	8.17	21.53
Upper	2071	44.00	536.14	538.28	0.08	0.03	0.11	0.02	0:30	1.33	0:30	89.50	136.36
Upper	2071	30.00	536.14		0.42	0.12	1.16	0.22	0.33	2.79	0.33	16.77	59.51
Upper	2071	27.00	536.14		0.09	0.04	0.12	0.02	0.35	1.41	0.35	109.41	140.67
Upper	2071	81.00	536.14		0.11	0.05	0.18	0.03	0.43	1.63	0.43	132.91	145.59
Upper	2071	195.00	536.14	539.05	0.25	0.13	0.61	0.13	0.75	2.49	0.75	203.03	159.43
Upper	2059	22.00	535.09	537.43	0,10	0.05	0.15	0.07	0.07	1.46	70.0	15.69	24,41
Upper	2059	44.00	535.09	538.27	90.0	0.02	80.0	0.01	0,24	1.24	0.24	82.66	114.24
Upper	2059	30.00	535.09	537.63	0.13	0.04	0.22	0.05	0.16	1.68	0.16	23.40	53.26
Upper	2059	92.00	535.09	538.41	0.08	0.03	0.11	0.02	0.29	1.38	0.29	99.02	118.04
Upper	2059	81.00	535.09	538.57	0.11	0.05	0.19	0.03	0.38	1.68	0.38	118.03	122.31
Upper	2059	195.00	535.09	539.00	0.29	0.14	0.81	0.16	0.75	2.78	0.75	173.33	133.97

Reach	Kiver Sta	Q Total	Min Ch El	W.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Vel Left	Vel Chri	Vel Right	Flow Area	Top Width
The second secon		(cfs)	(ft)	(#)	(lp/sd ft)	(t) bs/q))	(lb/fts)	(lb/ft s)	(ft/s)	(ft/s)	(ft/s)	(# US)	#
Upper	2047	22.00	536.13	537.08	1.25	1.25	5,60	5.60		4.48	(4 91	804
Upper	2047	44.00	536.13	538.25	0.13	0.05	0.22	0.04	0.38	171	0.32	60 BS	AF 30
Upper	2047	30.00	536.13	537.34	1.02	0.94	4.22	3.88	0.08		900	7.24	40.10
Upper	2047	57.00	536.13	538.38	0.15	0.07	0.28	0.05	0.45		75.0	74.55	10.91
Upper	2047	81.00	536.13	538.54	0.21	0.10		60.0	0.58	222	0.0	8 33	407.70
Upper	2047	195.00	536.13	538.93	0.54	0.26		0.38	1.07	3.66	08.0	135.68	124.59
	0000	000											
Jeddo :	2032	22.00	535.43	536.93	0.20	90.0	0.40	70.0	0.24	1.97	0.24	18.27	63.30
Opper	2032	44.00	535.43	538.26	0.02	0.01	0.01	00:00	0.22	0.69	0.19	158.75	124.97
Upper	2032	30.00	535.43	537.49	0.05	0.02	0.05	0.01	0.25	1.04	0.24	71.09	104.33
Upper	2032	22.00	535.43	538.40	60.03	10.01	0.02	0.00	0.26	0.80	0.00	176.48	128 75
Upper	2032	81.00	535.43	538.55	0.04	0.02	0.04	0.01	0.34	1 02	0.08	198.88	122.02
Upper	2032	195.00	535.43	538.96	0.13	0.08	0.25	90.0	0.66	1.89	0.54	253.03	132.31
									2	3:	5	20:00	145.9
Upper	2017	22.00	534.37	536.94	90.0	0.02	0.07	0.01	0.11	1.18	20 0	00 90	02.40
Upper	2017	44.00	534.37	538.26	0.01	0.01	0.01	000	0.15	0.50	17.0	466.03	04.08
Upper	2017	30.00	534.37	537.49	0.02	0.01	0.02	00.0	0.15	0.75	0.25	78 55	22.03
Jpper	2017	57.00	534.37	538.40	0,01	0.01	0.01	0.00	0.18	0.61	0.35	184.76	104.70
Upper	2017	81.00	534.37	538.55	0.02	0.01	0.02	00.0	0.23	0.78	0.45	205.04	123.00
Jpper	2017	195.00	534.37	538.96	0.07	0.04	0.11	0.03	0.47	1.46	0.85	261 27	144.33
Upper	2001	22.00	535.31	536.88	0.19	60.0	75.0	0.13	0.26	1.93	0.26	14.88	31.87
Upper	2001	44.00	535.31	538.25	0.04	0.02	0.04	0.01	0.23	76.0	0.21	113.45	107.35
Upper	2001	30.00	535.31	537.47	0.08	0.03	0.11	0.02	0.26	1.37	0.26	43.93	88.77
Upper	2001	57.00	535.31	538.39	0.05	0.02	50.05	0.01	0.28	1.12	0.25	128.54	112.35
Upper	2001	81.00	535.31	538.53	0.08	0.04	0.11	0.02	0.38	1.42	0.32	145.62	117 74
Opper	2001	195.00	535.31	538.91	0.25	0.12	29.0	0.13	0.76	2.64	0.62	191.97	131.28
Longia	000	20 00											
Upper	300	22.00	234.72	536.81	0.13	0.04	0.22	0.05	0.18	1.63	0.18	18.72	48.54
10 dd 1	4000	44.00	234.72	228.25	0.02	0.01	0,02	0.00	0.23	0.74	0.20	137.35	99.92
Cpycal 1. page	1800	3 8	534.72	537.46	0.04	0.02	0.9	0.01	0.24	1.01	0.22	65.26	82.53
Porer	1000	30.70	234.72	228.38	0.03	0.02	0.03	0.01	0.28	0.87	0.24	151.16	102.64
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1000	01.00	234.72	538.53	0.05	0.03	0.05	0.01	0.37	1.13	0.31	166.34	105.56
obbei	996	00.081	534.72	238.88	0.17	0.10	0.38	0.10	0.77	2.20	0.63	205.01	112.65
Upper	1963	Culvert											
Opper	1911	22.00	533.46	534.70	0.50	0.47	1.47	1.36	0.11	2.93	0.11	7.52	10.80
Opper	191	44.00	533.46	535,15	0.62	0.37	2.19	1.10	0.54	3.53	0.54	14.76	20.99
Upper	181	30.00	533.46	534.89	0.54	0.39	1.71	1.16	0.34	3.16	0.34	10.00	15.09
Opper	1911	57.00	533.46	535.33	0.71	0.40	2.76	1.20	99.0	3.87	99.0	18.90	25.02
opper	101	51.00	533,45	535.57	0.92	0.49	4.12	1.54	0.85	4.50	0.85	25.48	30.34
												The second secon	

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

(Ib/sqf) (Ib/Rs) <	Reach	River Sta	Q Total	Reach River Sta Q Total Min Ch El W.S. Elev Shear Chan	W.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Velleft	Vel Chal	Vel Picht	Flow Area	Ton Midth
1911 195.00 552.40 556.75 2.42 1.19 116.20 6.54 1.55 7.55 7.55 1.25			(cfs)	(€)	€	(lb/sq ft)	(lb/sd ft)	(lb/ft s)	(lb/ft s)	(ff/s)	(#/s)	(#/e)	(Soft)	(#)
1901 22.00 582.40 583.73 0.10 0.09 0.15 0.07 0.17 0.07 0.17 0.07 0.17 0.07 0.18 0.	Upper	1911	195.00	533.46	536.05	2.42	1.19	18.52	i un	1.55	7.65	1.59	47 77	42.50
1801 22.00 562.40 584.73 0.10 0.06 0.042 0.017 0.07 1.47 1.80 0.02 0.02 0.02 0.02 0.02 0.02 0.018 0.02 0.02 0.018 0.02 0.02 0.018 0.02 0.02 0.018 0.02 0.02 0.018 0.02 0.02 0.018 0.02 0.02 0.018 0.02 0.02 0.018 0.02 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.018 0.02 0.02 0.018 0.02 0.018 0.02 0.02 0.018 0.02 0.02 0.018 0.02 0.02 0.02 0.018 0.02 0.0											3	3	1.77	42.00
1891 350,00 522,40 562,53 0.14 0.05 0.02 0.01 0.01 0.02 0.25 0.14 0.05 0.02 0	Upper	1901	22:00	532.40	534.73	0.10	90'0	0.15		70.0	1.47	0.07	15.13	14.21
1801 57,00 522,40 565,48 0.014 0.024 0.015 0.016 0.0	Upper	1901	44.00	532.40	535.20	0.20	60.0	0.42		0.27	2.11	0.27	25.79	31.73
1901 87,00 8324-0 858,8 0.28 0.15 0.09 0.16 0.05 0.27 0.084 0.18 0.	Upper	1901	30.00	532.40	534.93	0.14	90.0	0.24		0.16	1.74	0.16	18.62	21.57
1907 1900 252.40 556.54 0.94 0.05 0.0	Upper	1901	92.00	532.40	535.39	0.25	0.11	09:0	0.19	0.35	2.41	0.35	32.38	38,79
1861 1950 582-40 586-34 1.28 1.28 1.28 5.60 5.60 6.60 4.65 1.69 1.28 1.28 1.28 1.28 1.28 1.28 1.28 6.34 6.3	Upper	1901	81.00	532.40	535.64	0.34	0.15	0.99	0.27	0.48	2.89	0.48	43.47	48.40
1891 22.00 533.44 534.39 1.25 1.25 5.69 5.69 6.	Upper	1901	195.00	532.40	536.29	0.81	0.34	3.75	0.81	0.94	4.63	0.88	82.67	72.09
1891 42.00 533.44 534.39 1.26 1.26 5.60 5.60 5.60 4.46 1.34 1.34 1.34 6.31 6.														
1891 4400 653.44 684.79 1.43 0.89 7.21 4.57 6.04 1891 30.00 653.44 684.96 1.34 0.64 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.61 6.71 6.62 6.61 6.71 6.61 6.61 6.71 6.61 6.61 6.71 6.61 6.61 6.71 6.61 6.71 6.61 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.61 6.71 6.71 6.72 6.72 6.72 6.72 6.72 6.72 6.72 6.72 6.72 6.72 6.72 6.72	Upper	1891	22.00	533.44	534.39	1.25	1.25	5.60	5.60		4.48		4.92	8.02
1891 30.00 553.44 564.56 1,39 1,39 6.31 6.31 4.71 2.24 0.67 7.77 2.24 0.69 6.17 6.44 1891 51.00 553.44 555.56 1,78 0.67 7.77 2.24 0.69 6.17 1891 61.00 553.44 555.56 1,78 0.77 11.64 2.24 0.69 6.17 1874 22.00 582.86 554.10 0.50 0.41 1,74 1,18 0.11 6.46 1874 22.00 582.86 554.61 0.52 0.25 1,69 0.50 0.51 0.52 <td>Upper</td> <td>1891</td> <td>44.00</td> <td>533.44</td> <td>534.79</td> <td>1.43</td> <td>0.89</td> <td>7.21</td> <td>4.25</td> <td>0.44</td> <td>5.06</td> <td>0.44</td> <td>9.20</td> <td>17.38</td>	Upper	1891	44.00	533.44	534.79	1.43	0.89	7.21	4.25	0.44	5.06	0.44	9.20	17.38
1881 67.00 533.44 584.89 1.39 0.67 717 2.81 0.68 517 1881 1810 67.00 533.44 585.83 1.14 0.62 7.83 2.24 0.91 6.46 1891 1960 533.44 585.83 1.14 0.62 0.73 1.73 6.54 1874 22.00 532.86 584.90 0.65 0.22 1.64 0.70 0.71 0.65 0.74 0.75	Upper	1891	30.00	533.44	534.56	1.34	1.34	6.31	6.31		4.71		6.37	9.35
1891 61.00 533.44 555.56 1.44 0.62 7.89 2.24 0.91 5.46 1891 1891 1800 533.44 555.58 1.78 0.77 11.64 2.20 1.37 6.54 1874 22.00 532.86 554.10 0.50 0.21 1.64 0.45 0.51 0.21 0.52 0.52 1.64 0.75 0.52 0.53 1.64 0.50 0.52 0.50	Upper	1891	57.00	533.44	534.99	1.39	29.0	71.7	2.81	0.68	5.17	0.68	13.63	27.17
1891 1186 0 553.44 555.89 1,78 0,77 1164 2,30 1,37 6,64 1874 2200 532.86 554.10 0,50 0,41 1,44 1,18 0,11 2,37 1874 2200 532.86 554.39 0,51 0,20 0,46 0,46 0,20 0,76 0,50 3,21 1874 50.00 532.86 554.50 0,56 0,46 0,20 1,57 0,09 0,59 3,21 1874 50.00 532.86 556.15 0,46 0,20 1,57 0,39 0,58 3,10 1874 51.00 532.86 556.15 0,46 0,20 1,57 0,39 0,58 0,51 0,46 0,20 1,57 0,39 0,58 0,48 0,48 0,21 0,29 0,58 0,58 0,48 0,48 0,29 0,58 0,58 0,48 0,79 0,78 0,58 0,58 0,48 0,29 1,47 <td>Upper</td> <td>1891</td> <td>81.00</td> <td>533.44</td> <td>535.25</td> <td>1.44</td> <td>0.62</td> <td>7.83</td> <td>2.24</td> <td>0.91</td> <td>5.46</td> <td>0.91</td> <td>22.60</td> <td>40.28</td>	Upper	1891	81.00	533.44	535.25	1.44	0.62	7.83	2.24	0.91	5.46	0.91	22.60	40.28
1874 2200 532.86 534.10 0.55 0.51 1.44 1.14 0.15 0.51 1.20 1874 44.00 532.86 534.30 0.51 0.21 1.64 0.15 0.50 3.21 1874 44.00 532.86 534.30 0.52 0.26 1.60 0.70 0.36 3.21 1874 30.00 532.86 534.30 0.52 0.26 0.26 0.70 0.70 0.38 3.10 1874 81.00 532.86 536.16 0.46 0.16 0.16 0.70 0.36 0.58 3.21 1874 1870 532.86 536.16 0.46 0.10 0.16 0.17 0.20 0.16 0.17 0.20 0.17 0.20 0.16 0.17 0.20 0.16 0.17 0.20 0.16 0.17 0.20 0.16 0.17 0.20 0.16 0.17 0.20 0.16 0.17 0.20 0.16 0.17 <td>Upper</td> <td>1891</td> <td>195.00</td> <td>533.44</td> <td>535.98</td> <td>1.78</td> <td>72.0</td> <td>11.64</td> <td>2.30</td> <td>1.37</td> <td>6.54</td> <td>1.37</td> <td>64.85</td> <td>76.06</td>	Upper	1891	195.00	533.44	535.98	1.78	72.0	11.64	2.30	1.37	6.54	1.37	64.85	76.06
1874 22.00 53.28 6 534.10 0.50 0.41 1.44 1.18 0.11 2.29 1874 4.00 532.86 534.39 0.51 0.21 1.64 0.45 0.60 3.21 1874 50.00 532.86 534.30 0.52 0.62 1.60 0.70 0.34 3.01 1874 57.00 532.86 534.81 0.46 0.20 1.47 0.26 0.68 3.21 1874 150.00 532.86 534.81 0.46 0.20 1.47 0.26 0.68 3.21 1874 150.00 532.86 534.81 0.46 0.20 1.47 0.26 0.61 3.21 1866 22.00 531.80 534.41 0.10 0.09 0.41 0.12 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.45 0.														
1874 44,00 532.86 534,59 0,51 0,21 1,164 0,45 0,50 3,10 3,21 3,10 3,1 3,1 3,1 3,1 <	Upper	1874	22.00	532.86	534.10	0.50	0.41	1.44	1.18	0.11	2.92	0.11	7.59	12.35
1874 30.00 532.66 534.30 0.52 0.26 1.67 0.09 0.39 3.10 1874 31.00 552.86 554.61 0.48 0.46 0.20 1.47 0.56 0.58 3.21 1874 81.00 552.86 554.61 0.46 0.22 1.47 0.56 0.67 3.21 1874 81.00 552.86 556.65 0.44 0.22 1.47 0.32 0.67 0.67 3.21 1866 22.00 531.80 534.61 0.19 0.19 0.12 <td>Upper</td> <td>1874</td> <td>44.00</td> <td>532.86</td> <td>534.59</td> <td>0.51</td> <td>0.21</td> <td>1.64</td> <td>0.45</td> <td>0.50</td> <td>3.21</td> <td>0.50</td> <td>20.62</td> <td>41.29</td>	Upper	1874	44.00	532.86	534.59	0.51	0.21	1.64	0.45	0.50	3.21	0.50	20.62	41.29
1874 57.00 552.86 563.481 0.49 0.20 1.57 0.58 0.58 3.24 1874 81.00 552.86 565.16 0.46 0.26 1.45 0.26 0.61 3.21 1874 185.00 552.86 558.05 0.44 0.10 0.12 0.07 1.48 1866 22.0 551.80 554.41 0.10 0.10 0.15 0.12 0.07 1.48 1866 37.00 551.80 554.61 0.10 0.10 0.16 0.15 0.07 1.48 1866 37.00 551.80 554.81 0.24 0.12 0.07 0.16 0.15 0.07 1.48 1866 87.00 551.80 554.81 0.23 0.10 0.04 0.15 0.15 0.05 0.15 0.16 0.15 0.16 0.15 0.16 0.15 0.16 0.15 0.16 0.15 0.16 0.15 0.16 0.15 0.1	Upper	1874	30.00	532.86	534.30	0.52	0.26	1.60	0.70	0.34	3.10	0.34	11.16	24.04
1874 81 00 552 86 585.15 0.45 0.16 1.45 0.26 0.61 3.21 1874 195.00 552.86 586.05 0.44 0.22 1.47 0.32 0.97 3.38 1866 22.00 531.80 534.14 0.10 0.09 0.15 0.12 0.07 1.46 1866 30.00 531.80 534.61 0.19 0.10 0.40 0.18 0.27 2.08 1866 30.00 531.80 534.61 0.19 0.10 0.40 0.16 0.17 0.16 1.72 1866 30.00 531.80 534.81 0.14 0.10 0.04 0.15 0.16 0.17 0.16 1.72 1866 30.00 531.80 535.89 0.23 0.12 0.13 0.23 0.73 0.16 1.72 1864 0.10 531.80 534.81 1.24 0.20 0.12 0.17 0.18 0.71	Upper	1874	57.00	532.86	534.81	0.49	0.20	1,57	96.0	0.58	3.23	0.58	31.42	54.70
1874 18500 532.86 536.5 0.44 0.22 1.47 0.32 0.97 3.38 1866 22.00 531.80 534.14 0.10 0.09 0.16 0.15 0.07 1.48 1866 44.00 531.80 534.61 0.19 0.10 0.04 0.18 0.27 2.08 1866 30.00 531.80 534.81 0.19 0.10 0.04 0.18 0.27 2.04 1866 30.00 531.80 534.82 0.23 0.12 0.05 0.24 0.15 0.05 2.34 1866 31.00 531.80 534.82 0.23 0.12 0.05 0.21 0.15 0.17 0.15 0.16 0.15 0.16 0.17 0.18 0.17 0.18 0.17 0.18 0.17 0.18 0.17 0.18 0.11 0.11 0.18 0.14 0.18 0.11 0.18 0.14 0.18 0.14 0.18 0.14 <td>Upper</td> <td>1874</td> <td>81.00</td> <td>532.86</td> <td>535.15</td> <td>0.45</td> <td>0.18</td> <td>1.45</td> <td>0.26</td> <td>0.61</td> <td>3.21</td> <td>0.67</td> <td>54.37</td> <td>79.84</td>	Upper	1874	81.00	532.86	535.15	0.45	0.18	1.45	0.26	0.61	3.21	0.67	54.37	79.84
1866 2200 534.80 534.14 0.10 0.09 0.15 0.012 0.07 1.46 1866 44.00 531.80 534.61 0.19 0.19 0.04 0.18 0.07 1.46 1866 44.00 531.80 534.81 0.19 0.09 0.24 0.15 0.07 1.72 1866 81.00 531.80 534.82 0.23 0.10 0.24 0.16 0.16 0.17 0.08 1.72 1866 81.00 531.80 535.83 0.23 0.10 0.24 0.19 0.31 0.71 0.28 2.34 1866 81.00 532.85 533.80 0.48 0.20 1.72 0.38 0.73 3.51 1867 30.00 532.85 533.80 1.24 1.24 5.53 0.73 3.51 1861 30.00 532.85 534.81 1.34 1.34 6.53 6.53 0.74 0.74 0.74 0.	Upper	1874	195.00	532.86	536.05	0.44	0.22	1.47	0.32	76.0	3.38	0.89	137.16	102.88
1866 22.00 531.80 554.14 0.10 0.09 0.15 0.12 0.07 1.46 1866 44.00 531.80 534.61 0.19 0.10 0.40 0.18 0.07 1.06 1866 30.00 531.80 534.81 0.14 0.10 0.04 0.15 0.15 0.16 0.17 0.18 0.17 0.05 0.17 0.05 0.10 0.01														
1866 44,00 531,80 534,61 0.19 0.10 0.40 0.19 0.24 0.15 0.17 2.08 1866 30,00 551,80 534,34 0.14 0.09 0.24 0.15 0.16 0.17 0.16 0.17 0.16 0.17 0.17 0.17 0.17 0.18 0.17 0.18 0.17 0.18 0.19 0.14 0.17 0.18 0.19 0.19 0.19 0.17 0.18 0.17 0.18 0.17 0.14 0.17 0.18 0.18 0.18 0.18 0.18 0.14 0.11 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.19 0.19 0.18 0.18 0.18 0.18 0.18 0.11 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18 0.18	Пррег	1866	22.00	531.80	534.14	0.10	60:0	0.15	0.12	20:0	1.46	0.16	15.22	13.56
1866 30.00 551.80 554.34 0.14 0.09 0.24 0.15 0.16 0.17 0.17 172 1866 57.00 551.80 554.82 0.23 0.10 0.54 0.21 0.36 2.34 1866 81.00 551.80 555.80 0.38 0.48 0.20 0.10 0.81 0.23 2.71 1866 195.00 552.86 533.80 1.24 1.24 5.53 0.73 3.61 1851 22.00 552.86 533.80 1.24 1.24 5.72 5.73 4.46 1851 44.00 552.85 534.85 1.34 1.34 6.30 6.73 4.46 1851 45.00 552.85 534.85 1.53 1.54 6.53 6.53 6.41 1851 57.00 552.85 534.85 1.53 0.88 9.43 3.75 0.65 5.41 1851 52.00 532.85 534.85	Upper	1866	8.4	531.80	534.61	0.19	0.10	0.40	0.18	0.27	2.08	0.63	24.60	26.31
1866 57.00 531.80 534.82 0.23 0.12 0.54 0.21 0.35 2.34 1866 81.00 531.80 535.93 0.36 0.10 0.81 0.03 0.73 2.71 1866 1850 531.80 535.89 0.48 0.20 1.72 0.38 0.73 3.61 1851 22.00 532.85 533.80 1.24 1.24 5.53 0.53 4.46 1851 30.00 532.85 533.87 1.49 1.14 7.72 5.76 0.42 5.17 1851 57.00 532.85 533.87 1.53 0.89 8.23 6.53 0.42 5.17 1851 57.00 532.85 533.87 1.53 0.89 8.23 6.53 0.89 8.23 0.69 5.40 1851 57.00 532.85 534.65 1.53 0.73 1.160 0.75 0.75 0.75 0.75 0.71 0.75 0.	Upper	1866	30.00	531.80	534.34	0.14	60.0	0.24	0.15	0.16	1.72	0.37	18.39	18.85
1866 81.00 531.80 535.13 0.30 0.10 0.01	Upper	1866	57.00	531.80	534.82	0.23	0.12	0.54	0.21	0.35	2.34	0.82	30.69	31.98
1866 195.00 531.80 535.98 0.48 0.20 1,72 0.38 0.73 3.61 1851 22.0 532.86 533.80 1,24 1,24 1,24 5.53 6.53 6.30 4.46 7.72 6.56 0.42 5.17 4.46 7.72 6.30 6.30 4.46 7.72 6.30 0.42 5.17 7.72 6.30 0.42 5.17 7.72 6.30 0.42 5.17 7.72 6.30 0.42 5.17 7.72 6.30 0.42 5.17 7.72 6.30 0.42 5.17 7.72 6.30 0.42 5.17 7.72 6.30 0.42 6.71 7.72 6.30 0.40 6.30	Upper	1866	81.00	531.80	535.13	0.30	0.10	0.81	0.19	0.34	2.71	1.08	44.27	58.24
1851 22.00 532.85 533.80 1.24 1.24 5.63 5.53 4.46 1851 44.00 532.85 534.18 1.48 1.14 7.72 5.76 0.42 5.17 1851 30.00 532.85 533.97 1.34 1.34 6.30 6.30 0.42 5.17 1851 81.00 532.85 533.87 1.53 0.95 8.23 4.59 0.69 5.40 1851 81.00 532.85 534.65 1.63 0.73 11.60 2.35 0.96 5.81 1851 22.00 532.85 535.53 1.76 0.73 11.60 2.35 1.27 6.58 1831 44.00 531.81 533.65 0.45 0.21 1.30 0.75 0.73 0.41 2.86 1831 57.00 531.81 533.45 0.91 0.91 0.71 0.71 0.71 0.71 0.71 0.73 0.71 0.71	Upper	1866	195.00	531.80	535.98	0.48	0.20	1.72	0.38	0.73	3.61	1.72	103.82	83.27
1851 22.00 553.80 1.24 1.24 1.24 5.53 5.63 4.46 1861 44.00 552.86 534.18 1.49 1.14 7.72 5.76 0.42 5.17 1861 30.00 532.86 533.87 1.34 1.34 6.30 6.30 6.30 4.71 1861 81.00 532.86 534.65 1.63 0.86 8.23 4.58 0.69 5.40 1851 81.00 532.85 534.65 1.63 0.73 11.60 2.35 1.27 6.58 1851 22.00 531.81 533.66 0.45 0.73 11.60 2.35 1.27 6.58 1831 44.00 531.81 533.66 0.45 0.21 1.30 0.75 0.19 2.36 1831 57.00 531.81 533.45 0.41 0.41 3.94 1.13 0.73 4.34 1831 81.00 531.81 533.45	11		0											
1851 44,00 532,85 534,18 1,48 1,14 7,72 5,76 0,42 5,17 1851 30,00 532,85 533,97 1,34 1,34 6,30 6,30 6,30 4,71 1851 81,00 532,85 534,65 1,63 0,88 9,49 3,97 0,96 5,81 1851 22,00 532,85 535,53 1,76 0,73 11,60 2,35 1,27 6,58 1831 22,00 531,81 533,06 0,45 0,21 1,36 0,57 0,19 2,86 1831 44,00 531,81 533,37 0,68 0,31 2,50 0,75 0,19 2,86 1831 57,00 531,81 533,45 0,43 0,41 0,41 2,89 1831 81,00 531,81 533,45 0,91 0,41 0,41 2,94 1831 81,00 531,81 533,45 0,91 0,41 0,73 <td< td=""><td>neddo</td><td>1621</td><td>22.00</td><td>237.85</td><td>533.80</td><td>1.24</td><td>1.24</td><td>5.53</td><td>5.53</td><td></td><td>4.46</td><td></td><td>4.94</td><td>8.04</td></td<>	neddo	1621	22.00	237.85	533.80	1.24	1.24	5.53	5.53		4.46		4.94	8.04
1851 30.00 532.85 533.97 1.34 1.34 6.30 6.30 6.30 4.71 1851 57.00 532.85 534.65 1.63 0.95 8.23 4.59 0.69 5.40 1851 81.00 532.85 534.65 1.63 0.88 9.49 3.97 0.96 5.81 1851 22.00 532.85 535.53 1.76 0.73 11.60 2.35 1.27 6.58 1831 22.00 531.81 533.06 0.45 0.21 1.30 0.57 0.19 2.86 1831 30.00 531.81 533.37 0.48 0.31 2.50 0.75 0.73 0.41 2.89 1831 57.00 531.81 533.45 0.91 0.71 1.27 0.59 3.70 1831 81.00 531.81 533.45 0.91 0.71 0.71 0.71 0.73 4.34 1831 81.00 531.81 6	Upper	1851	44.00	532.85	534.18	1.49	1.14	7.72	5.76	0.42	5.17	0.42	8.74	13.58
1851 57.00 532.85 534.37 1.53 0.95 8.23 4.58 0.69 5.40 1851 81.00 532.85 534.65 1.63 0.95 8.23 4.58 0.09 5.81 1851 195.00 532.85 535.53 1.76 0.73 11.60 2.35 1.27 6.58 1831 22.00 531.81 533.65 0.45 0.21 1.30 0.57 0.19 2.86 1831 30.00 531.81 533.37 0.48 0.31 1.23 0.41 0.41 2.86 1831 57.00 531.81 533.45 0.91 0.41 3.94 1.13 0.73 4.34 1831 81.00 531.81 533.45 0.91 0.61 1.13 0.71 0.73 4.34 1831 81.00 531.81 533.56 1.34 0.61 7.18 1.92 0.97 5.36	Upper	1851	30.00	532.85	533.97	1,34	1.34	6.30	6.30		4.71		6.37	9.35
1851 81.00 532.85 534.65 1.63 0.88 9.49 3.97 0.96 5.81 1851 195.00 532.85 535.53 1.76 0.73 11.60 2.35 1.27 6.58 1831 22.00 531.81 533.67 0.45 0.21 1.30 0.57 0.19 2.86 1831 30.00 531.81 533.37 0.68 0.31 2.50 0.76 0.76 0.59 3.70 1831 57.00 531.81 533.45 0.91 0.41 3.94 0.13 0.73 4.34 1831 81.00 531.81 533.45 0.91 0.61 7.18 0.13 0.73 4.34 1831 81.00 531.81 533.56 1.34 0.61 7.18 0.97 0.97 5.36	Upper	1851	27.00	532.85	534.37	1.53	0.95	8.23	4.58	69'0	5.40	0.69	11.77	18.60
1851 195.00 532.85 535.53 1.76 0.73 1160 2.35 1.27 6.58 1831 22.00 531.81 533.06 0.45 0.21 1.30 0.57 0.19 2.86 1831 30.00 531.81 533.37 0.68 0.31 2.50 0.76 0.59 3.70 1831 57.00 531.81 533.27 0.43 0.43 1.25 0.41 0.41 2.89 1831 57.00 531.81 533.45 0.91 0.41 3.94 1.13 0.73 4.34 1831 81.00 531.81 533.56 1.34 0.61 7.18 1.32 0.97 5.36	Upper	1851	81.00	532.85	534.65	1.63	0.88	9.49	3.97	96.0	5.81	96:0	17.94	25.97
1831 22.00 531.81 533.65 0.45 0.21 1.30 0.57 0.19 2.86 1831 44.00 531.81 533.37 0.68 0.31 2.50 0.76 0.59 3.70 1831 30.00 531.81 533.27 0.43 0.19 1.23 0.41 0.41 2.89 1831 57.00 531.81 533.45 0.91 0.41 3.94 1.13 0.73 4.34 1831 81.00 531.81 533.56 1.34 0.61 7.18 1.32 0.97 5.36	Upper	1851	195.00	532.85	535.53	1.76	0.73	11.60	2.35	1.27	6.58	1.40	60.90	69.19
1831 22.00 531.81 533.65 0.45 0.21 1.30 0.67 0.19 2.86 1831 44.00 531.81 533.37 0.68 0.31 2.50 0.76 0.76 0.59 3.70 1831 30.00 531.81 533.45 0.91 1.23 0.41 0.41 2.89 1831 61.00 531.81 533.45 0.91 0.41 3.94 1.13 0.73 4.34 1831 81.00 531.81 533.56 1.34 0.61 7.18 1.92 0.97 5.36														
1831 44,00 531.81 533.37 0.68 0.31 2.50 0.76 0.59 3.70 1831 30.00 531.81 533.27 0.43 0.19 1.23 0.41 0.41 2.89 1831 57.00 531.81 533.45 0.91 0.41 3.94 1.13 0.73 4.34 1831 81.00 531.81 533.56 1.34 0.61 7.18 1.92 0.97 5.36	Upper	1831	22.00	531.81	533.06	0.45	0.21	1.30	25.0	0.19	2.86	0.20	8.31	23.64
1831 30.00 531.81 533.27 0.43 0.19 1.23 0.41 0.41 2.89 1831 57.00 531.81 533.45 0.91 0.41 3.94 1.13 0.73 4.34 1831 81.00 531.81 533.56 1.34 0.61 7.18 1.92 0.97 5.36	Upper	1831	4.00	531.81	533.37	0.68	0.31	2.50	0.76	0.59	3.70	0.62	17.78	37.58
1831 57.00 531.81 533.45 0.91 0.41 3.94 1.13 0.73 4.34 1831 81.00 531.81 533.56 1.34 0.61 7.18 1.92 0.97 5.36	Upper	1831	30.00	531.81	533.27	0.43	0.19	1.23	0.41	0.41	2.89	0.43	14.22	33.03
1831 81.00 531.81 533.56 1.34 0.61 7.18 1.92 0.97 5.36		1831	27.00	531.81	533,45	0.91	0.41	3.94	1.13	0.73	4.34	77.0	20.81	41.04
		1831	81.00	531.81	533.56	1.34	0.61	7.18	1.92	0.97	5.36	1.02	25.81	46.20

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

1821 1855.00 183.01 18	Reach	River Sta	Reach River Sta O Total Min Ch El M.S. Elev. Shorr Chan	Min Ch El	M/S Elev	Shear Chan	Choor Total	and O round	Table T	4-11-71	140,000	1,4-1 0:-1-4	4	110.00
1821 1820 53418 53418 178 1			(sto)	1 €	₩	(lb/saft)	(ib/so ft)	(lhff s)	(h#s)	Ver Leit	(4/4)	Vel rigin	riow Area	l op vvloun
1821 22.00 580.76 583.41 0.010 0.04 0.014 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.15 0.05 0.05 0.15 0.05 0.15 0.05 0.05 0.15 0.05		4007	(610)	(11)	6,100	(1) bean)	(11 heart)	(\$ 11/01)	S H(GI)	(S/II)	(Sul)	(SUI)	(sd tt)	(H)
1821 22.00 580.76 583.10 0.10 0.04 0.14 0.05 1821 3400 580.76 583.41 0.21 0.05 0.02 0.04 0.16 1821 350.00 580.76 583.80 0.01 0.05 0.20 0.07 1821 357.00 580.76 583.80 0.03 0.14 0.79 0.07 1821 357.00 580.76 583.80 0.38 0.14 0.79 0.07 1821 357.00 580.76 583.80 0.38 1.71 0.67 1.72 0.56 1811 44.00 581.80 582.71 1.78 0.73 1.66 0.74 0.76 1811 44.00 581.80 582.21 1.78 0.78 1.78 1.78 1.78 1.78 1.78 1.86 1811 45.00 581.80 582.21 1.78 0.78 1.89 0.89 1.89 1.89 1.89 1.89 <	Opper	1831	35.00	531.81	534.18	1.88	0.89	12.76		1.35	6.78	1,58	63.05	73.21
16271 42200 3007/10 533.10 U.1V U.04 U.14 U.10 U.14 U.10 U.14 U.10 U.14 U.10 U.14 U.10 U.14 U.10 U.14 U.15	1	1007	8	000	0.000	0.40				•	!			
1827 4400 583.46 633.40 0.271 0.70 0.46 0.15 1827 30.00 583.66 583.40 0.12 0.00 0.00 0.00 1827 350.00 580.76 583.80 0.03 0.014 0.73 0.05 1827 367.00 580.76 583.80 0.30 0.014 0.73 0.02 1821 367.00 580.76 583.80 1.73 1.73 7.36 1811 220 581.80 582.76 1.73 1.73 7.36 7.36 1811 30.00 581.80 582.71 1.76 0.65 6.71 0.60 1811 30.00 581.80 582.71 1.76 0.65 6.81 0.60 1811 30.00 581.80 582.31 1.77 0.86 6.81 0.60 6.82 1.77 0.89 6.81 0.60 0.74 1.72 0.86 0.76 0.76 0.76 0.76 <	add.	1021	22.00	220.70	033.10	01.0	0.04	0.14	C).D	0.10	1.45	0.10	16.90	32.81
1821 53.00 583.76 633.30 0.12 0.05 0.02 0.07 1821 57.00 580.76 583.80 0.31 0.44 0.79 0.25 1821 67.00 580.76 583.82 1.71 0.67 1.64 0.57 1811 22.00 581.80 582.76 1.78 1.78 1.28 0.57 1811 22.00 581.80 582.27 1.79 1.79 1.28 1.28 1811 34.00 581.80 582.31 1.65 0.68 6.81 1.68 0.89 6.71 1.28 1.28 1811 34.00 581.80 582.31 1.65 0.68 6.81 1.68 1.71 1.72 1.28 1.78	Лррег	1821	44.00	530.76	533.41	0.21	0.10	0.46	0.15	0.32	2.20	0.36	28.26	38.84
1821 57.00 500.76 633.50 0.04 0.04 0.05 0.05 1821 19.00 500.76 633.82 1.71 0.07 1.12 0.51 1821 19.00 500.76 633.82 1.71 0.07 1.12 3.73 1811 200 551.80 552.91 1.72 0.06 57.44 1.28 1811 4.00 551.80 552.91 1.72 0.06 7.78 1.08 1811 4.00 551.80 552.91 1.68 0.58 5.74 1.28 1811 4.00 551.80 552.91 1.68 0.58 5.74 1.08 1811 4.00 551.80 552.91 1.58 0.58 0.58 0.58 0.68 0.58 0.77 1.08 0.74 1.77 1.08 0.74 1.08 0.74 1.08 0.74 1.08 0.74 1.08 0.74 1.08 0.74 1.08 0.74 1.08 <td>Upper</td> <td>1821</td> <td>30.00</td> <td>530.76</td> <td>533.30</td> <td>0.12</td> <td>0.05</td> <td>0.20</td> <td>0.07</td> <td>0.21</td> <td>1.66</td> <td>0.23</td> <td>23.86</td> <td>36.62</td>	Upper	1821	30.00	530.76	533.30	0.12	0.05	0.20	0.07	0.21	1.66	0.23	23.86	36.62
1821 81.00 530.76 533.82 0.48 0.23 1.67 1.69 0.67 1821 1820 530.76 533.82 1.71 0.67 1.12 3.37 1811 220 531.80 532.31 1.46 0.53 1.73 1.28 7.26 7.28 1811 30.00 531.80 532.31 1.46 0.53 1.00 1.00 1811 30.00 531.80 532.31 1.46 0.53 1.00 1.00 1811 30.00 531.80 532.31 1.65 0.56 631 1.00 1811 30.00 531.80 532.34 1.97 0.56 631 0.74 1.28 1811 44.00 531.80 532.34 0.59 0.23 1.46 0.58 0.58 1814 45.00 531.80 532.34 0.59 0.23 1.42 0.58 184 550 532.84 0.56 0.23 1.46 <td>Jpper</td> <td>1821</td> <td>27.00</td> <td>530.76</td> <td>533.50</td> <td>0.30</td> <td>0.14</td> <td>0.79</td> <td>0.25</td> <td>0.42</td> <td>2.64</td> <td>0.47</td> <td>31.76</td> <td>40.52</td>	Jpper	1821	27.00	530.76	533.50	0.30	0.14	0.79	0.25	0.42	2.64	0.47	31.76	40.52
1871 18500 550,76 553,89 1,71 0.87 11,27 7.96	Jpper	1821	81.00	530.76	533.62	0.48	0.23	1.64	0.51	0.59	3.40	0.67	36.88	42.85
1811 22.00 6591.80 652.76 1,79 1,79 7,36 1,36 0,53 1,47 1,58 0,53 1,47 1,58 0,58 1,57 1,58 0,58 1,58 1,58 0,58 1,58	Jpper	1821	195.00	530.76	533.92	1.71	0.87	11.27	3.37	1.28	6.58	1.47	50.49	48.51
1811 22 00 531.80 532.76 1,78 178 7.98 7.98 7.98 1811 44,00 531.80 532.21 1,48 0.53 5.74 1,28 1811 30.00 531.80 532.31 1,68 2.28 10.80 1.93 1811 30.00 531.80 532.41 1,67 0.68 6.91 1.60 1811 30.00 531.80 532.41 1,67 0.68 6.91 1.60 1811 41.00 531.80 532.41 0.69 0.32 1.77 1.22 1814 41.00 531.80 532.31 0.48 0.77 2.218 0.50 0.22 1.60 0.74 1.03 1774 41.00 530.60 532.31 0.48 0.23 1.77 1.02 1776 42.00 530.60 532.41 0.60 0.23 1.47 1.02 1776 42.00 530.60 532.41 0.50 <														
1811 44 00 551 80 553 21 1.46 0.53 1.46 0.53 1.46 0.53 1.28 1.080	Jpper	1811	22.00	531.80	532.76	1.79	1.79	7.96	7.96		4.45		4.94	8.04
1811 30.00 551.80 552.91 2.26 10.80 10.80 1811 51.00 551.80 552.31 1.58 0.68 6.81 1.60 1811 51.00 551.80 553.43 1.48 0.68 6.81 1.60 1811 51.00 551.80 553.43 1.57 0.89 9.88 2.28 1811 51.00 550.60 550.60 552.31 0.69 0.22 1.42 1.60 1724 22.0 550.60 552.21 0.69 0.22 1.50 0.58 1724 32.00 550.60 552.21 0.69 0.22 1.50 0.58 1774 32.00 550.60 552.41 0.69 0.22 1.50 0.61 1776 350.60 552.41 0.69 0.22 1.50 0.61 1776 350.60 552.50 552.41 0.69 0.22 1.50 0.61 1776 47.70 <	уррег	1811	44.00	531.80	533.21	1.46	0.53	5.74	1.28	0.79	3.94	0.83	18.33	55.83
1811 57.00 \$31.80 533.41 1,650 691 1,69	Jpper	1811	30.00	531.80	532.91	2.26	2.26	10.80	10.80		4.79		6.27	9.27
1811 81.00 \$31.80 \$33.43 1,97 0.89 9.38 2.29 1811 185.00 \$31.80 \$33.83 3.39 1,77 22.18 5.87 1784 22.00 \$30.60 \$32.31 0.49 0.28 1.42 1.09 1784 44.00 \$30.60 \$32.41 0.69 0.23 1.42 0.46 1784 9.00 \$30.60 \$32.44 0.69 0.22 1.50 0.61 1784 \$1.00 \$30.60 \$32.70 0.65 0.29 1.50 0.61 1784 \$1.00 \$30.60 \$32.70 0.66 0.47 4.72 1.02 1776 \$1.00 \$30.60 \$32.34 0.66 0.47 4.72 1.02 1776 \$1.00 \$30.00 \$52.60 \$32.34 0.66 0.77 0.72 0.69 1776 \$1.00 \$30.00 \$32.60 \$32.34 0.60 0.72 4.72 1.02 <	Јррег	1811	92.00	531.80	533.31	1.63	99.0	6.91	1.60	0.99	4.24	1.05	23.60	58.77
(111 196.00 531.80 533.81 1.77 22.18 5.87 1784 22.0 530.60 531.84 0.49 0.38 1.42 1.03 1784 44.00 530.60 532.34 0.50 0.23 1.50 0.63 1784 30.00 530.60 532.47 0.50 0.23 1.50 0.63 1784 30.00 530.60 532.47 0.56 0.22 1.50 0.63 1784 57.00 530.60 532.47 0.56 0.22 1.50 0.63 1784 57.00 530.60 532.47 0.56 0.26 1.91 0.61 1776 1764 57.00 530.60 531.89 0.06 0.47 4.72 1.02 1776 22.00 528.50 531.89 0.06 0.47 4.72 0.06 1776 30.00 528.50 532.44 0.06 0.07 0.03 0.06 1776	Jpper	1811	81.00	531.80	533.43	1.97	0.89	9.38	2.29	1.25	4.76	1.35	31.48	62.91
1784 22.00 531.84 0.49 0.36 1.42 1.08 1784 42.00 530.60 531.84 0.49 0.36 1.42 1.08 1784 40.00 530.60 532.04 0.56 0.23 1.58 0.46 1784 30.00 530.60 532.04 0.56 0.22 1.50 0.58 1784 51.00 530.60 532.47 0.56 0.22 1.50 0.58 1776 520.60 532.47 0.56 0.29 1.42 0.61 1776 22.00 530.60 532.47 0.56 0.47 4.72 1.02 1776 22.00 530.50 531.89 0.06 0.47 4.72 1.02 1776 44.00 528.50 532.94 0.06 0.07 0.05 0.06 1776 41.00 528.50 532.44 0.60 0.07 0.02 0.06 1776 41.00 528.50 5	Jpper	1811	195.00	531.80	533.83	3.39	1.77	22.18	5.87	2.03	6.55	2.24	58.81	75.55
1784 22 00 530 60 531 84 0.49 0.36 1.42 1.03 1784 44,00 530,60 532,41 0.69 0.23 1.58 0.46 1784 30,00 530,60 532,74 0.65 0.26 1.91 0.51 1784 57,00 530,60 532,74 0.65 0.26 1.91 0.61 1784 57,00 530,60 532,74 0.65 0.30 2.49 0.61 1784 51,00 530,60 532,44 0.66 0.47 4.72 0.61 1776 22,00 530,60 532,44 0.66 0.47 4.72 0.02 1776 30,00 523,50 531,84 0.06 0.07 0.73 0.06 1776 44,00 523,50 532,84 0.06 0.07 0.73 0.06 1776 44,00 523,50 532,80 0.12 0.07 0.07 0.06 1776 1														
1784 44.00 550.60 552.31 0.50 0.22 1.56 0.46 1774 30.00 530.60 532.47 0.56 0.22 1.50 0.53 1784 50.00 530.60 532.47 0.56 0.26 1.50 0.53 1784 61.00 550.60 532.40 0.66 0.77 2.49 0.61 1776 22.00 550.60 533.44 0.96 0.47 4.72 1.02 1776 22.00 529.50 531.89 0.09 0.47 4.72 1.02 1776 32.00 529.50 531.89 0.09 0.47 4.72 1.02 1776 32.00 529.50 531.89 0.09 0.47 4.72 1.02 1776 32.00 529.50 532.34 0.16 0.07 0.03 0.09 1776 32.00 529.50 532.50 0.21 0.09 0.47 4.72 1.02 1	lpper	1784	22:00	530.60	531.84	0.49	98'0	1.42	1.03	0.12	2.90	0.12	79.7	13.89
1784 30.00 550.60 552.04 0.48 0.25 1,50 0.58 1784 30.00 552.47 0.58 0.26 1,91 0.51 1784 91.00 550.60 552.70 0.58 0.26 1,91 0.51 1784 196.00 550.60 552.70 0.65 0.73 2.49 0.61 1776 22.00 529.50 531.89 0.09 0.05 0.13 0.06 1776 30.00 529.50 532.89 0.12 0.09 0.04 0.12 0.09 1776 44.00 529.50 532.89 0.12 0.09 0.04 0.05 0.00<	pper	1784	44.00	530.60	532,31	0.50	0.23	1.58	0.46	0.57	3.17	0.53	21.48	40.06
1784 57.00 530.60 582.47 0.56 0.26 1.91 0.51 1784 61.00 530.60 532.70 0.65 0.30 2.49 0.61 1784 196.00 530.60 533.44 0.06 0.47 4.72 1.02 1776 22.00 529.50 531.89 0.09 0.05 0.13 0.06 1776 30.00 529.50 532.34 0.16 0.07 0.22 0.09 1776 30.00 529.50 532.69 0.12 0.06 0.20 0.06 1776 30.00 529.50 532.50 0.21 0.07 0.20 0.06 1776 30.00 529.50 532.50 0.21 0.06 0.74 0.12 1776 41.00 529.50 532.50 0.21 0.09 0.76 0.09 1774 42.00 529.50 531.54 0.29 0.23 0.40 0.76 0.76 0.76 <	ррег	1784	30.00	530.60	532.04	0.49	0.22	1.50	0.53	0.36	3.03	0.35	12.22	29.71
1784 81.00 530.60 532.70 0.65 0.30 249 0.61 1774 1784 196.00 530.60 533.44 0.96 0.47 4.72 1.02 1776 22.00 529.50 531.89 0.09 0.05 0.13 0.06 1776 44.00 529.50 532.34 0.16 0.07 0.32 0.09 1776 30.00 529.50 532.50 0.12 0.05 0.07 0.05 1776 81.00 529.50 532.50 0.21 0.09 0.47 0.12 1776 81.00 529.50 532.73 0.21 0.09 0.47 0.12 1776 81.00 529.50 532.73 0.29 0.31 0.76 0.19 1776 81.00 520.50 533.44 0.60 0.23 0.40 0.75 0.91 1774 44.00 530.59 531.71 1.34 0.53 5.59 0.53 <t< td=""><td>ррег</td><td>1784</td><td>27.00</td><td>530.60</td><td>532.47</td><td>0.56</td><td>0.26</td><td>1.91</td><td>0.51</td><td>0.68</td><td>3.42</td><td>0.63</td><td>28.36</td><td>46.28</td></t<>	ррег	1784	27.00	530.60	532.47	0.56	0.26	1.91	0.51	0.68	3.42	0.63	28.36	46.28
1764 196,00 530.60 533.44 0.96 0.47 4.72 1.02 1776 22.00 529.50 531.89 0.09 0.05 0.013 0.00 1776 30.00 529.50 532.34 0.12 0.07 0.22 0.09 1776 30.00 529.50 532.73 0.12 0.05 0.04 0.00 1776 81.00 529.50 532.73 0.29 0.13 0.01 1776 81.00 529.50 532.73 0.29 0.01 0.07 1776 81.00 529.50 532.73 0.29 0.01 0.01 1776 81.00 529.50 532.73 0.29 0.01 0.01 1776 91.00 529.50 533.44 0.60 0.28 2.40 0.51 1774 44.00 530.59 531.54 1.25 0.28 5.59 1.75 1774 44.00 530.59 532.16 1.24	pper	1784	81.00	530.60	532.70	0.65	0:30	2.49	0.61	0.82	3.80	72.0	40.37	55.49
1776 22.00 529.50 531.89 0.09 0.05 0.13 0.06 1776 44.00 529.50 532.34 0.16 0.07 0.32 0.09 1776 30.00 529.50 532.00 0.12 0.05 0.20 0.07 0.06 1776 57.00 529.50 532.50 0.29 0.13 0.76 0.19 1776 195.00 529.50 532.73 0.29 0.13 0.76 0.19 1776 195.00 529.50 533.74 0.60 0.28 2.40 0.51 1776 22.00 529.50 531.54 1.25 1.25 5.59 5.59 1764 44.00 530.59 531.71 1.34 1.34 6.32 6.59 1764 57.00 530.59 532.16 1.40 0.66 7.49 1.34 1764 44.00 530.59 532.16 1.21 0.23 1.34 1.34 <td< td=""><td>bber</td><td>1784</td><td>195.00</td><td>530.60</td><td>533.44</td><td>96.0</td><td>0.47</td><td>4.72</td><td>1.02</td><td>1.22</td><td>4.91</td><td>1.13</td><td>90.78</td><td>81.38</td></td<>	bber	1784	195.00	530.60	533.44	96.0	0.47	4.72	1.02	1.22	4.91	1.13	90.78	81.38
1776 22.00 529.50 531.89 0.09 0.05 0.05 0.09 1776 44.00 529.50 532.34 0.16 0.07 0.03 0.09 1776 30.00 529.50 532.09 0.12 0.05 0.00 0.00 1776 81.00 529.50 532.50 0.21 0.09 0.47 0.05 1776 81.00 529.50 532.50 0.21 0.09 0.47 0.12 1776 81.00 529.50 533.44 0.60 0.28 0.76 0.19 1776 1776 620 530.50 531.54 1.25 0.28 5.59 5.59 1764 44.00 530.59 531.71 1.34 1.34 6.32 6.59 1764 57.00 530.59 532.16 1.41 0.65 7.49 1.75 1764 44.00 530.59 532.36 1.40 0.65 5.29 5.29 176														
1776 44.00 529.50 532.34 0.16 0.07 0.32 0.09 1776 30.00 529.50 532.09 0.12 0.05 0.02 0.09 1776 30.00 529.50 532.50 0.21 0.03 0.04 0.06 1776 81.00 529.50 532.73 0.29 0.13 0.07 0.12 1776 81.00 529.50 532.73 0.29 0.13 0.76 0.12 1776 156 529.50 533.44 0.60 0.28 0.47 0.12 1764 22.00 530.59 531.54 1.26 0.28 0.76 0.51 1764 22.00 530.59 531.71 1.34 1.34 6.32 6.32 1764 30.00 530.59 532.76 1.21 0.53 5.28 6.32 1764 31.00 530.59 532.76 1.24 0.53 5.28 6.32 1764 22.	pper	1776	22.00	529.50	531.89	0.08	0.05	0.13	90.0	0.09	1.40	60.0	16.56	24.49
1776 30.00 529.50 532.09 0.12 0.05 0.05 0.06 0.07 0.06 0.07 0.06 0.07 0.07 0.06 0.07 0.02 0.07 0.012 0.02 0.04 0.07 0.012 0.02 0.04 0.04 0.012	pper	1776	44.00	529.50	532.34	0.16	70.0	0.32	60.0	0.32	1.94	0.29	33.90	46.72
1776 57.00 529.50 532.50 0.21 0.09 0.47 0.12 1776 81.00 529.50 532.73 0.29 0.13 0.76 0.19 1776 195.00 529.50 533.44 0.60 0.28 2.40 0.51 1764 22.00 530.59 531.54 1.25 1.25 5.59 5.59 1764 22.00 530.59 531.71 1.34 0.47 5.33 1.76 1764 30.00 530.59 532.16 1.21 0.53 5.59 1764 57.00 530.59 532.16 1.21 0.53 5.88 1.80 1764 57.00 530.59 532.16 1.21 0.56 5.28 5.21 1764 81.00 530.59 532.16 1.40 0.66 7.49 2.14 1746 22.00 550.59 533.04 1.86 0.28 1.86 0.73 1746 30.00 <td< td=""><td>pper</td><td>1776</td><td>30.00</td><td>529.50</td><td>532.09</td><td>0.12</td><td>0.05</td><td>0.20</td><td>90.0</td><td>0.19</td><td>1.63</td><td>0.18</td><td>23.05</td><td>38.01</td></td<>	pper	1776	30.00	529.50	532.09	0.12	0.05	0.20	90.0	0.19	1.63	0.18	23.05	38.01
1776 81,00 529.50 532.73 0.29 0.13 0.76 0.19 1776 195,00 529.50 533.44 0.60 0.28 2.40 0.51 1764 22,00 530.59 531.54 1.25 1.25 5.59 5.59 1764 44,00 530.59 531.71 1.34 1.34 6.32 6.32 1764 57.00 530.59 532.16 1.21 0.63 5.88 1.80 1764 57.00 530.59 532.16 1.21 0.63 5.88 1.80 1764 57.00 530.59 532.16 1.40 0.66 7.49 2.14 1764 81.00 530.59 533.04 1.86 0.94 12.28 3.02 1746 22.00 520.59 531.65 0.55 0.54 0.54 0.74 1746 30.00 529.92 531.85 0.54 0.29 0.29 0.29 1746 <td< td=""><td>pper</td><td>1776</td><td>57.00</td><td>529.50</td><td>532.50</td><td>0.21</td><td>60:0</td><td>0.47</td><td>0.12</td><td>0.41</td><td>2.22</td><td>96.0</td><td>41.66</td><td>52.07</td></td<>	pper	1776	57.00	529.50	532.50	0.21	60:0	0.47	0.12	0.41	2.22	96.0	41.66	52.07
1776 195.00 529.50 533.44 0.60 0.28 2.40 0.51 1764 22.00 530.59 531.54 1.25 1.25 5.59 5.59 1764 44.00 530.59 531.71 1.34 6.32 6.32 1764 30.00 530.59 531.71 1.34 6.32 6.32 1764 57.00 530.59 532.16 1.21 0.63 5.88 1.80 1764 57.00 530.59 532.16 1.40 0.66 7.49 2.14 1764 81.00 530.59 533.04 1.86 0.94 12.28 3.02 1746 22.00 520.59 531.65 0.55 0.54 1.40 0.66 7.49 2.14 1746 44.00 529.92 531.65 0.55 0.56 0.58 0.58 0.73 1746 57.00 529.92 531.85 0.56 0.29 0.29 0.59 0.59	pper	1776	81.00	529.50	532.73	0.29	0.13	0.76	0.19	0.54	2.65	0.47	54.61	59.93
1764 22.00 530.59 531.54 1.25 5.59 5.59 5.59 1764 44.00 530.59 531.54 1.25 5.59 5.59 5.59 1764 30.00 530.59 531.71 1.34 6.32 6.32 1764 57.00 530.59 531.71 1.21 0.53 5.88 1.80 1764 81.00 530.59 532.16 1.21 0.66 7.49 2.14 1764 195.00 530.59 532.16 1.86 0.34 12.28 3.02 1746 22.00 530.59 531.18 0.47 0.40 1.34 1.14 1746 30.00 529.92 531.85 0.55 0.28 1.86 0.73 1746 57.00 529.92 531.85 0.56 0.29 0.58 1746 57.00 529.92 531.85 0.59 0.29 0.59 1746 81.00 529.92 531.85	pper	1776	195.00	529.50	533.44	09.0	0.28	2.40	0.51	0.91	4.00	0.86	105.29	83.49
1764 22.00 530.59 551.54 1.25 1.25 5.59 5.59 1764 44.00 530.59 532.00 1.16 0.47 5.33 1.75 1764 30.00 530.59 532.10 1.21 0.53 5.88 1.80 1764 57.00 530.59 532.16 1.21 0.66 7.49 2.14 1764 195.00 530.59 532.36 1.40 0.66 7.49 2.14 1746 22.00 520.92 531.18 0.47 0.40 1.34 1.14 1746 22.00 529.92 531.18 0.47 0.40 1.34 1.14 1746 30.00 529.92 531.65 0.56 0.28 1.34 1.14 1746 57.00 529.92 531.85 0.56 0.29 0.29 0.70 1746 57.00 529.92 531.85 0.56 0.31 2.53 0.71 1746					-				The state of the s					
1764 44,00 530.59 532.00 1.16 0.47 5.33 1.75 1764 30.00 530.59 531.71 1.34 6.32 6.32 6.32 1764 57.00 530.59 532.16 1.21 0.63 5.88 1.80 1764 81.00 530.59 532.36 1.40 0.66 7.49 2.14 1764 195.00 530.59 533.04 1.86 0.94 1.2.28 3.02 1746 22.00 523.92 531.18 0.47 0.40 1.34 1.14 1746 30.00 529.92 531.85 0.55 0.25 0.59 0.73 1746 57.00 529.92 531.85 0.65 0.29 0.29 0.65 0.59 0.29 0.70 0.61 0.29 0.70 0.70 1746 57.00 529.92 531.85 0.66 0.29 0.29 0.70 0.70 0.70 0.70 0.70 <	pper	1764	22.00	530.59	531.54	1.25	1.25	5.59	5.59		4.47		4.92	8.02
1764 30.00 530.59 551.71 1.34 6.32 6.32 6.32 1764 57.00 530.59 532.16 1.21 0.63 5.88 1.80 1764 81.00 530.59 532.36 1.40 0.66 7.49 2.14 1764 1764 195.00 530.59 533.04 1.86 0.94 12.28 3.02 1746 22.00 529.92 531.18 0.47 0.40 1.34 1.14 1746 30.00 529.92 531.58 0.55 0.28 1.85 0.73 1746 57.00 529.92 531.85 0.56 0.29 0.29 0.59 0.59 0.59 0.59 0.70 0.70 1746 57.00 529.92 531.85 0.59 0.29 0.29 0.59 0.59 0.70 0.70 1746 81.00 529.92 531.85 0.66 0.31 2.53 0.71	Jaddi	1764	44.00	530.59	532.00	1.16	0.47	5.33	1.75	0.49	4.61	0.49	11.69	32.12
1764 57.00 530.59 532.16 1.21 0.53 5.88 1.80 1764 81.00 530.59 532.36 1.40 0.66 7.49 2.14 1764 195.00 530.59 533.04 1.86 0.94 1.228 3.02 1746 22.00 523.92 531.18 0.47 0.40 1.34 1.14 1746 30.00 529.92 531.85 0.55 0.28 1.85 0.73 1746 57.00 529.92 531.85 0.51 0.29 0.29 0.51 0.51 0.73 1746 57.00 529.92 531.85 0.56 0.29 0.29 0.51 0.51 0.70 1746 81.00 529.92 531.85 0.69 0.29 0.29 0.70 1746 81.00 529.92 532.16 0.66 0.31 2.53 0.71	Ipper	1764	30.00	530.59	531.71	1.34	1.34	6.32	6.32		4.72		6.36	9.35
1764 81.00 530.59 532.36 1.40 0.66 7.49 2.14 1764 195.00 530.59 533.04 1.86 0.94 12.28 3.02 1746 22.00 529.92 531.18 0.47 0.40 1.34 1.14 1746 30.00 529.92 531.85 0.56 0.28 1.86 0.73 1746 57.00 529.92 531.85 0.69 0.29 0.29 0.70 1746 57.00 529.92 531.85 0.69 0.29 0.29 0.70 1746 81.00 529.92 531.85 0.69 0.29 0.29 0.70	ррет	1764	57.00	530.59	532.16	1.21	0.53	5.88	1.80	62.0	4.85	0.71	16.89	36.66
1764 195.00 530.59 533.04 1.86 0.94 12.28 3.02 1746 22.00 529.92 531.18 0.47 0.40 1.34 1.14 1746 44.00 529.92 531.65 0.55 0.28 1.85 0.73 1746 57.00 529.92 531.85 0.51 0.51 0.31 1.55 0.88 1746 57.00 529.92 531.85 0.69 0.29 2.09 0.70 1746 81.00 529.92 532.16 0.66 0.31 2.53 0.71	pper	1764	81.00	530.59	532.36	1.40	0.66	7.49	2.14	1.09	5.35	0.95	24.83	42.67
1746 22.00 529.92 531.18 0.47 0.40 1.34 1.14 1746 44.00 529.92 531.65 0.55 0.28 1.85 0.73 1746 30.00 529.92 531.87 0.51 0.31 1.55 0.88 1746 57.00 529.92 531.85 0.59 0.29 2.09 0.70 1746 81.00 529.92 532.16 0.66 0.31 2.53 0.71	pper	1764	195.00	530.59	533.04	1.86	0.94	12.28	3.02	1.68	6.62	1.46	60.79	63.17
1746 44.00 529.92 531.37 0.51 0.23 1.55 0.73 1746 30.00 529.92 531.37 0.51 0.31 1.55 0.88 1746 57.00 529.92 531.85 0.59 0.29 2.09 0.70 1746 81.00 529.92 532.16 0.66 0.31 2.53 0.71	nner	1746	22.00	529 92	534 4R	77.0	070	1 24	* * *	7 + 0	20.0	7,70	1	0.47
1746 30.00 529.92 531.85 0.54 0.29 0.29 0.29 0.51 0.51 0.64 0.70 0.70 1746 57.00 529.92 531.85 0.59 0.59 0.29 0.29 0.70 1746 81.00 529.92 532.16 0.66 0.31 2.53 0.71	nner	1746	44.00	520 02	534 BE	5.0 5.0	ac c	5 8	0.720	i c	20.2	2 0	17.00	11.00
1746 57.00 529.92 531.85 0.59 0.59 0.59 0.70 1746 81.00 529.92 532.16 0.66 0.31 2.53 0.71	PP0	4746	3	253.92	201.00	000	0.20	00.1	0.73	0.03	C. 50	0.03	1,00	27.37
1746 81.00 529.92 532.16 0.66 0.31 2.53 0.71	pha h	1746	3.60	28.820	351.57	0.51	10.0	00.1	0.88	0.35	3.07	0.35	10.69	18.26
17.40 81.00 323.92 332.16 0.66 0.31 2.53 0.71	ia D	17.40	00.70	28.870	021.80	SC C	87.0	2.02 2.03	0.70	0.63	3.55	0.63	23.37	34.19
	ladd	11/40	01.00	סלמימל	937. ID	00.0	0.31	7,33	1U.0	0.78	3.86	0.74	35.18	44.13

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

10000	District Offi	Total C	Adia Or El	יאל פי בוייי	10,000	Chara Take			2-11-7	1.101.73		i	
Leach	NIVEL OLD	Z .		vy.3. ⊏lev	Olfedi Citalii	oriear lotal	rower chan	rower rotal	vei Len	Vel Curi	vei Kignt	Flow Area	Lob Width
		(cts)	Œ	(£)	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/fts)	(s,t,j)	(tt/s)	(£/k)	(sd ft)	(¥)
Opper	1746	195.00	529.92	533.01	0.95	0.44	4.69	1.01	1.18	4.96	1.07	85.10	72.55
Upper	1736	22:00	528.87	531.21	0.10	90.08	0.15	0.12		1.46	0.07	15.21	13.93
Upper	1736	44.00	528.87	531.68	0.20	0.10	0.41	0.17	0.27	2.11	0,27	25.26	28.87
Upper	1736	30.00	528.87	531.41	0.14	90.08	0.24	0.14	0.16	1.73	0.16		20.16
Upper	1736	57.00	528.87	531.88	0.24	0.11	0.58	0.20	0.36	2.39	0.36		35.31
Upper	1736	81.00	528.87	532.18	0.32	0.14	0.91	0.27	0.49	2.82	0.46	43.45	44.82
Upper	1736	195.00	528.87	533.00	0.65	0.28	2.74	09.0	0.91	4.21	0.81	91.64	72.05
Upper	1724	22.00	529.91	530.86	1.25	1.25	5.58	5.58		4.47		4.92	8.02
Upper	1724	44.00	529.91	531.25	1.47	1.07	7.58		0.43	5.14	0.43	8.85	14.53
Upper	1724	30.00	529.91	531.03	1,34	1.34	6.31	6.31		4.71		6.37	9.35
Upper	1724	00'29	529.91	531.44	1.48	0.85	7.91	3.97	69'0	5.33	0.69	12.25	20.80
Upper	1724	81.00	529.91	531.72	1.57	0.79	8.96	3.32	0.94	5.70	0.94	19.20	29.76
Upper	1724	195.00	529.91	532.50	2.04	0.95	14.37			7.03	1.42	52.66	55.55
Upper	1707	22.00	529.28	530.52	0.49	0.43	1.44	1.23	0.12	2.91	0.12	7.59	11.71
Upper	1707	44.00	529.28	530.99	0.56	0.26	1.87	0.65	0.52	3.35	0.52	17.79	31.63
Upper	1707	30.00	529.28	530.72	0.52	0:30	1.63	0.84	0.34	3.11	0,34	10.68	19.96
Upper	1707	57.00	529.28	531.19	0.59	0.27	2.11	0.61	0.62	3.55	0.62	24.79	40.03
Upper	1707	81.00	529.28	531.45	89'0	0:30	2.67	0.66	0.76	3.91	0.75	36.88	51.40
Upper	1707	195.00	529.28		0.95	0.43	4.71	0.92	1.09	4.94	1.10	91.04	84,98
Upper	1698	22.00	528.22	530.56	0.10	90.08	0.15	0.11	20.0	1.46	70.0	15.25	14.83
Upper	1698	44.00	528.22	531.03	0.19	0.09	0.40	0.14	0.27	2.09	0.27	26.70	34.33
Upper	1698	30.00	528.22	530.76	0.14	0.08	0.24	0.12	0.16	1.72	0.16	18.96	22.96
Upper	1698	67.00	528.22	531.22	0.24	0.10	0.57	0.17	0.35	2.37	0.35	34.04	43.06
Upper	1698	81.00	528.22	531.47	0.33	0.13	0.93	0.23	0.46	2.83	0.46	46.57	54.84
Upper	1698	195.00	528.22	532.24	0.64	0.26	2.64	05.0	0.81	4.14	0.84	101.49	88.22
Upper	1686	22.00	529.26	530.21	1.25	1.25	5.60	5.60		4.48		4.91	8.01
Upper	1686	44.00	529.26	530.61	1.42	0.89	7.21	4.28	0.44	5.06	0.44	9.19	17.22
Upper	1686	30.00	529.26	530.38	1.34	1.34	6.31	6.31		4.71		6.37	9.35
Upper	1686	57.00	529.26	530.81	1.40	0.68	7.23		0.68	5.18	0.68	13.51	26.70
Upper	1686	81.00	529.26	531.08	1.42	0.65	7.71	2.33	0.93	5.43	0.94	22.50	38.21
Upper	1686	195.00	529.26	531.76	2.04	1.01	14.25	3.58	1.55	6.97	1.61	54.81	57.18
Upper	1667	22.00	528.58	529.84	0.47	0.35	1.35	0.99	0.14	2.85	0.14	7.81	13.77
Upper	1667	44.00	528.58	530.31	0.49	0.22	1.55	0.47	0.56	3.16	0.52	20.95	38.22
Upper	1667	30.00	528.58	530.03	0.49	0.23	1.47	0.59	0.36	3.02	0.35	11.86	26.40
Upper	1667	27.00	528.58	530,50	0.52	0.23	1.74	0.46	0.65	3.33	0.61	28.83	46.08
Upper	1667	81.00	528.58	530.75	0.61	0.27	2.24	0.53	0.78	3.69	0.74	41.68	56.59

HEC-RAS Plan: UpReachRey7-14 River: Tanyard Branch Reach: Upper (Continued)

(cfs) (ff) (ff) (78.50 198.00 198.00 528.58 198.00 527.52 198.00 527.52 198.00 527.52 198.00 527.52 198.00 527.52 198.00 527.52 198.00 528.57 198.00 528.57 198.00 528.57 198.00 528.57 198.00 527.92 195.00 525.52 195.00 525.52 195.00 525.52 195.00 525.52 195.00 525.52 195.00 527.90 195.00 527.90 195.00 527.90 195.00 527.90 195.00 527.90 195.00 527.90 195.00 527.90 195.00 527.27 195.00 195.27.27 195.00 195.27.27 195.00 195.27.27 195.00 195.27.27 195.00 195.27.27 195.00 195.27.27 195.00 195.27.27 195.00 195.27.27 195.00 195.27.27 195.00 195.27.27 195.00 195.27.27 195.00 195.00		v shear chan	Shear lotal	Power Chan	Power Total	Velleft	Vel Chul	Vel Right	Flow Area	Top Width
1667 195.00 528.58 1657 22.00 527.52 1657 44.00 527.52 1657 30.00 527.52 1657 30.00 527.52 1657 30.00 527.52 1657 81.00 527.52 1657 81.00 527.52 1657 81.00 527.52 1645 22.00 528.57 1645 30.00 528.57 1645 30.00 528.57 1645 81.00 528.57 1628 30.00 527.92 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.90 1618 81.00 527.90 1618 81.00 527.90 1606 81.00 527.90 <t< th=""><th>(ft) (ft)</th><th>(lb/sq ft)</th><th>(lb/sq ft)</th><th>(lb/ff s)</th><th>(lb/ft s)</th><th>(ft/s)</th><th>(ft/s)</th><th>(£/t)</th><th>(sq ft)</th><th>(£)</th></t<>	(ft) (ft)	(lb/sq ft)	(lb/sq ft)	(lb/ff s)	(lb/ft s)	(ft/s)	(ft/s)	(£/t)	(sq ft)	(£)
1657 22.00 527.52 1657 44.00 527.52 1657 30.00 527.52 1657 57.00 527.52 1657 57.00 527.52 1657 57.00 527.52 1657 195.00 527.52 1657 195.00 527.52 1645 22.00 528.57 1645 30.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 81.00 527.92 1618 81.00 527.90 1618 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 <		1.04	0.50	5.34	1.12	1.22	5.11	1.18	86.70	80.68
1657 22.00 527.52 1657 44.00 527.52 1657 30.00 527.52 1657 57.00 527.52 1657 81.00 527.52 1657 81.00 527.52 1645 22.00 528.57 1645 30.00 528.57 1645 81.00 528.57 1645 81.00 527.92 1645 81.00 528.57 1645 81.00 527.92 1645 81.00 527.92 1658 81.00 527.92 1658 81.00 527.92 1658 81.00 527.92 1618 81.00 527.92 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 527.90 1618 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 <td< th=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>										
1657 44.00 527.52 1657 30.00 527.52 1657 81.00 527.52 1657 81.00 527.52 1657 81.00 527.52 1645 22.00 528.57 1645 30.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1658 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 30.00 527.92 1618 30.00 527.92 1618 57.00 525.52 1618 57.00 527.90 1606 30.00 527.90 1606 30.00 527.90 <td< th=""><th>527.52</th><th></th><th></th><th>0.15</th><th>0.08</th><th>0.07</th><th>1.45</th><th>20.0</th><th>15.63</th><th>19.86</th></td<>	527.52			0.15	0.08	0.07	1.45	20.0	15.63	19.86
1657 30.00 527.52 1657 57.00 527.52 1657 195.00 527.52 1657 195.00 527.52 1645 22.00 528.57 1645 30.00 528.57 1645 30.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1658 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 22.00 527.92 1618 57.00 525.52 1618 57.00 525.52 1618 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 <	527.52			0.35	60'0	0.28	1.99	0.29	32.53	48.78
1657 57.00 527.52 1657 81.00 527.52 1657 195.00 527.52 1645 22.00 528.57 1645 22.00 528.57 1645 30.00 528.57 1645 30.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 81.00 527.92 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 <t< th=""><th>527.52</th><th>.07 0.13</th><th>90.02</th><th>0.22</th><th>90.08</th><th>0.17</th><th>1.69</th><th>0.17</th><th>21.15</th><th>34.57</th></t<>	527.52	.07 0.13	90.02	0.22	90.08	0.17	1.69	0.17	21.15	34.57
1657 81.00 527.52 1657 195.00 527.52 1645 22.00 528.57 1645 44.00 528.57 1645 30.00 528.57 1645 30.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1628 30.00 527.92 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 81.00 527.92 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 <t< th=""><th>527.52</th><th></th><th></th><th>0.47</th><th>0.11</th><th>0.36</th><th>2.23</th><th>96.0</th><th>42.34</th><th>58.30</th></t<>	527.52			0.47	0.11	0.36	2.23	96.0	42.34	58.30
1657 195,00 527,52 1645 22,00 528,57 1645 22,00 528,57 1645 30,00 528,57 1645 30,00 528,57 1645 30,00 528,57 1645 81,00 528,57 1645 81,00 528,57 1628 30,00 527,92 1628 30,00 527,92 1628 81,00 527,92 1628 81,00 527,92 1628 81,00 527,92 1618 30,00 527,92 1618 30,00 527,92 1618 57,00 525,52 1618 57,00 525,52 1618 57,00 525,52 1618 57,00 525,52 1606 57,00 527,90 1606 57,00 527,90 1606 57,00 527,90 1606 57,00 527,90 <t< th=""><th>527.52</th><th>.77 0.28</th><th>0.11</th><th>0.73</th><th>0.15</th><th>0.46</th><th>2.61</th><th>0.47</th><th>58.32</th><th>71.14</th></t<>	527.52	.77 0.28	0.11	0.73	0.15	0.46	2.61	0.47	58.32	71.14
1645 22.00 528.57 1645 44.00 528.57 1645 30.00 528.57 1645 30.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1628 22.00 527.92 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 81.00 527.92 1618 81.00 527.92 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 87.00 527.90 <td< th=""><th>527.52</th><th>.43 0.55</th><th>0.24</th><th>2.11</th><th>0.41</th><th>0.84</th><th>3.83</th><th>0.90</th><th>114.68</th><th>97.61</th></td<>	527.52	.43 0.55	0.24	2.11	0.41	0.84	3.83	0.90	114.68	97.61
1645 22.00 528.57 1645 44.00 528.57 1645 30.00 528.57 1645 30.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1628 22.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 81.00 527.92 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 87.00 527.90 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></td<>										
1645 44,00 528.57 1645 30.00 528.57 1645 57.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1628 22.00 527.92 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 22.00 527.92 1618 30.00 527.92 1618 30.00 527.92 1618 57.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 <td< th=""><th>528.57</th><th>.52 1.25</th><th>1.25</th><th>5.61</th><th>5.61</th><th></th><th>4.48</th><th></th><th>4.91</th><th>8.01</th></td<>	528.57	.52 1.25	1.25	5.61	5.61		4.48		4.91	8.01
1645 30.00 528.57 1645 57.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1628 22.00 528.57 1628 22.00 527.92 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 22.00 527.92 1618 81.00 527.92 1618 81.00 527.92 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 87.00 527.90 1606 87.00 527.90 <td< th=""><th>528.57</th><th>.92 1.41</th><th>68.0</th><th>7.11</th><th>3.91</th><th>0.43</th><th>5.04</th><th>0.44</th><th>9.33</th><th>18.63</th></td<>	528.57	.92 1.41	68.0	7.11	3.91	0.43	5.04	0.44	9.33	18.63
1645 57.00 528.57 1645 81.00 528.57 1645 81.00 528.57 1628 22.00 527.92 1628 30.00 527.92 1628 30.00 527.92 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 22.00 527.92 1618 30.00 527.92 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 44.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 <td< th=""><th>528.57</th><th></th><th></th><th>6.31</th><th>6.31</th><th></th><th>4.71</th><th></th><th>96.36</th><th>9.35</th></td<>	528.57			6.31	6.31		4.71		96.36	9.35
1645 81.00 528.57 1645 195.00 528.57 1628 22.00 527.92 1628 30.00 527.92 1628 30.00 527.92 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 22.00 527.92 1618 30.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 22.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 87.00 527.90 1606 87.00 527.90 1606 57.00 527.90 1606 87.00 527.90 <t< th=""><th>528.57</th><th>.13 1.32</th><th>0.58</th><th>29'9</th><th>2.29</th><th>0.44</th><th>5.05</th><th>0.75</th><th>14.52</th><th>31.41</th></t<>	528.57	.13 1.32	0.58	29'9	2.29	0.44	5.05	0.75	14.52	31.41
1645 195.00 528.57 1628 22.00 527.92 1628 44.00 527.92 1628 30.00 527.92 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 22.00 527.92 1618 30.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 22.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 <t< th=""><th>528.57</th><th>.39 1.36</th><th>0.54</th><th>7.23</th><th>1.79</th><th>0.69</th><th>5.31</th><th>1.00</th><th>24.65</th><th>47.78</th></t<>	528.57	.39 1.36	0.54	7.23	1.79	0.69	5.31	1.00	24.65	47.78
1628 22.00 527.92 1628 44.00 527.92 1628 30.00 527.92 1628 57.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 22.00 527.92 1618 30.00 527.92 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 30.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.27 <td< th=""><th>528.57</th><th>1.75</th><th>0.72</th><th>11.29</th><th>2.02</th><th>1.21</th><th>6.45</th><th>1.46</th><th>69.61</th><th>88.46</th></td<>	528.57	1.75	0.72	11.29	2.02	1.21	6.45	1.46	69.61	88.46
1628 22.00 527.92 1628 44.00 527.92 1628 30.00 527.92 1628 30.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 195.00 527.92 1618 22.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 22.00 525.52 1606 30.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></t<>										
1628 44,00 527.92 1628 30.00 527.92 1628 57.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1628 195.00 527.92 1618 22.00 527.92 1618 30.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 30.00 525.52 1606 30.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.27 1689 30.00 527.27 1689 57.07 527.27 <t< th=""><th>527.92</th><th></th><th>0.51</th><th>1.61</th><th>1.54</th><th>20.0</th><th>3.01</th><th>20.07</th><th>7.31</th><th>10.47</th></t<>	527.92		0.51	1.61	1.54	20.0	3.01	20.07	7.31	10.47
1628 30.00 \$27.92 1628 57.00 \$27.92 1628 81.00 \$27.92 1628 81.00 \$27.92 1618 22.00 \$27.92 1618 22.00 \$25.52 1618 30.00 \$25.52 1618 81.00 \$25.52 1618 81.00 \$25.52 1618 81.00 \$25.52 1618 81.00 \$25.52 1618 81.00 \$25.52 1606 30.00 \$27.90 1606 81.00 \$27.90 1606 57.00 \$27.90 1606 57.00 \$27.90 1606 57.00 \$27.90 1606 57.00 \$27.90 1606 57.00 \$27.90 1606 57.00 \$27.90 1606 57.00 \$27.90 1606 57.00 \$27.27 1689 30.00 \$27.27 <td< th=""><th>527.92</th><th>.52 0.76</th><th>0.43</th><th>2.91</th><th>1.41</th><th>0.54</th><th>3.84</th><th>0.54</th><th>13.44</th><th>21.72</th></td<>	527.92	.52 0.76	0.43	2.91	1.41	0.54	3.84	0.54	13.44	21.72
1628 57.00 527.92 1628 81.00 527.92 1628 81.00 527.92 1618 22.00 525.52 1618 30.00 525.52 1618 30.00 525.52 1618 57.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 22.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.27 1689 57.07 527.27 1689 57.00 527.27 <td< th=""><th>527.92</th><th>.33 0.58</th><th>0.37</th><th>1.79</th><th>1.13</th><th>0.33</th><th>3,21</th><th>0.33</th><th>9.95</th><th>16.30</th></td<>	527.92	.33 0.58	0.37	1.79	1.13	0.33	3,21	0.33	9.95	16.30
1628 81.00 527.92 1628 195.00 527.92 1618 22.00 525.52 1618 44.00 525.52 1618 30.00 525.52 1618 57.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 22.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.27 1689 57.07 527.27 1689 57.00 527.27 1689 57.07 527.27	527.92	.66 0.92	0.49	3.99	1.67	0.68	4.33	0.68	16.73	25.81
1628 195.00 527.92 1618 22.00 525.52 1618 44.00 525.52 1618 30.00 525.52 1618 30.00 525.52 1618 57.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 22.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.27 1689 30.00 527.27 1689 57.07 527.27	527.92	.85 1.23	0.62	6.28	2.24	0.90	5.12	0.90	22.31	31.55
1618 22.00 525.52 1618 44.00 525.52 1618 30.00 525.52 1618 30.00 525.52 1618 57.00 525.52 1618 57.00 525.52 1618 81.00 525.52 1606 22.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.27 1589 44.00 527.27 1589 57.00 527.27 1589 57.00 527.27	527.92	54 2.03	0.92	14.25	3.46	1.61	7.02	1.26	52.09	55.45
1618 22.00 525.52 1618 44.00 525.52 1618 30.00 525.52 1618 57.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 22.00 527.90 1606 30.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.27 1689 30.00 527.27 1689 57.00 527.27		***************************************								
f618 44.00 525.52 1618 30.00 525.52 1618 57.00 525.52 1618 81.00 525.52 1618 81.00 525.52 1606 22.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1659 22.00 527.27 1589 44.00 527.27 1589 57.00 527.27	525.52	20 0.07	90.0	90.08	0.07	0.05	1.20	90.0	18.50	13.67
1618 30.00 525.52 1618 57.00 525.52 1618 81.00 525.52 1618 195.00 525.52 1606 22.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1659 22.00 527.27 1659 30.00 527.27 1659 57.27 527.27	525.52	60 0.16	60.0	0:30	0.14	0.22	1.89	0.22	26.50	25.92
1618 57.00 525.52 1618 81.00 525.52 1618 195.00 525.52 1606 22.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 57.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 22.00 527.90 1659 30.00 527.27 1659 30.00 527.27 1659 57.27	525.52	40 0.10	90.0	0.14	0.08	0.13	1.45	0.13	21.84	19.72
1618 81.00 525.52 1618 195.00 525.52 1606 22.00 527.90 1606 44.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 44.00 527.90 1689 30.00 527.27 1589 57.00 527.27 1589 57.00 527.27	525.52	75 0.22	0.11	0.49	0.21	0:30	2.25	0.30	30.73	30.45
1618 195.00 525.52 1606 22.00 527.90 1606 44.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 44.00 527.90 1589 44.00 527.27 1589 30.00 527.27 1589 57.00 527.27	525.52		0.16	0.94	0.34	0.44	2.83	0.44	38.14	37.10
1606 22.00 527.90 1606 44.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 81.00 527.90 1606 81.00 527.90 1606 195.00 527.90 1639 22.00 527.27 1589 44.00 527.27 1589 57.00 527.27 1589 57.00 527.27	525.52	57 0.93	0.38	4.55	1.09	0.93	4.91	08.0	68.41	63.81
1606 22 00 527.90 1606 44.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 81.00 527.90 1606 195.00 527.90 1589 22.00 527.27 1589 44.00 527.27 1589 30.00 527.27 1589 57.00 527.27										
1606 44.00 527.90 1606 30.00 527.90 1606 57.00 527.90 1606 81.00 527.90 1606 195.00 527.90 1606 195.00 527.27 1589 44.00 527.27 1589 30.00 527.27 1589 57.00 527.27	527.90		1.24	5.55	5.55		4.46		4.93	8.03
1606 30.00 527.90 1606 57.00 527.90 1606 81.00 527.90 1606 195.00 527.90 1589 22.00 527.27 1589 44.00 527.27 1589 30.00 527.27 1589 57.00 527.27	527.90		0.64	4.08	2.61	0.57	4.44	0.38	10.78	23.93
1606 57.00 527.90 1606 81.00 527.90 1606 195.00 527.90 1589 22.00 527.27 1589 44.00 527.27 1589 30.00 527.27 1589 57.00 527.27	527.90	01 1.36	1.36	6,46	6.46		4.75		6.32	9.31
1606 81.00 527.90 1606 195.00 527.90 1589 22.00 527.27 1589 44.00 527.27 1589 30.00 527.27 1589 57.00 527.27	527.90	41 1.11	0.71	5.22	2.86	62.0	4.71	0.59	14.14	28.60
1606 195.00 527.90 1589 22.00 527.27 1589 44.00 527.27 1589 30.00 527.27 1589 57.00 527.27	527.90		0.82	7.07	3.23	1.06	5.12	0.85	20.52	35.82
1589 22.00 527.27 1589 44.00 527.27 1589 30.00 527.27 1589 30.00 527.27 1589 57.00 527.27	527.90	25 2.14	1.13	13.52	4.30	1.83	6.32	1,43	51.21	61.10
1589 22.00 527.27 1589 44.00 527.27 1589 30.00 527.27 1589 57.00 527.27				••••						
1589 44.00 527.27 1589 30.00 527.27 1589 30.00 527.27 1589 57.00 527.27	527.27		0.41	1.38	1.16	0.13	2.87	0.13	7.70	11.90
1589 30.00 527.27 1589 57.00 527.27	527.27		0.28	1.90	0.71	0.52	3.37	0.52	17.23	29.33
1589 57.27	527.27		0.30	1.58	0.85	0.34	3.09	0.35	10.72	19.21
_	527.27		0.29	2.30	0.72	0.65	3.65	0.61	23.13	36.77
1589 81.00 527.27	527.27	40 0.78	0.34	3.22	0.85	0.81	4.15	92.0	32.94	46.65

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Reach	River Sta	O Total	Min Ch El	Reach River Sta O Total Min Ch El M/ S Elev Sheer Chan	Shear Chan	Shoot Total	- Chan	Dough Total	4-11-71	1/21 0421	17.00	Ī	
		(cfs)	a		(lb/sa ft)	(lb/sa ft)	(lb/ff s)	(lh/ft e)	(#/e)	(#fe)	(Afri)	THOW MAIN	현
Upper	1589	195.00	527.27	530.03	1.41	0.63	8.37	1 73	1 30	502	1 25	(34.17)	77.50
							2	2	8.	70.0	37.	70.00	
Upper	1578	22:00	526.21	528.55	01.10	20.0	0.15	0.10	20.0	1.46	0.07	15,35	16.25
Upper	1578	44.00	526.21	529.02	0.19	90.08	68.0	0.11	0.27	2.06	0.27	28.85	41.92
Пррег	1578	30.00	526.21	528.75	0.14	20.0	0.23	0.10	0.16	1.72	0.16	19.59	27.11
Upper	1578	27.00	526.21	529.20	0.23	60.0	0.54	0.14	0.36	2.33	0.33	37.23	51,11
Upper	1578	81.00	526.21	529.44	0.32	0.12	0.88	0.19	0.49	2.77	0.43	50.89	63.29
Opper	1578	195.00	526.21	530.09	0.67	0.27	2.79	0.52	0.89	4.20	0.82	103.02	93.72
Upper	1568	22.00	527.26	528.21	1.24	1.24	5.55	5.55		4.46		4.93	8.03
Upper	1568	44.00	527.26	528.62	1.38	0.78	6.91	3.60	0.45	4.99	0.45	9.52	19.73
Upper	1568	30.00	527.26	528.38	1.34	1.34	6.31	6.31		4.71		6.36	9.35
Upper	1568	22.00	527.26	528.82	1.32	0.58	29'9	2.25	0.68	5.05	0.68	14.72	32.01
Upper	1568	81.00	527.26	529.08	1.35	0.56	7.18	1.81	0.91	5.30	0.87	24.93	47.01
Upper	1568	195.00	527.26	529.71	1.88	0.81	12.55	2.43	1.50	6.67	1.32	64.90	79.79
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Upper	1548	22.00	526.57	527.82	0.47	0.39	1.36	1.	0.13	2.86	0.13	7.74	12.30
Upper	1548	44.00	526.57	528.23	0.63	0:30	2.21	0.82	0.53	3.53	0.54	16.34	29.31
Upper	1548	30.00	526.57	528.02	0.51	0.28	1.55	0.78	0.35	3.07	0.35	10.96	20.71
Upper	1548	57.00	526.57	528.33	0.83	66.0	3.42	1.15	0.67	4.12	0.68	19.40	33.22
Upper	1548	81.00	526.57	528.46	1.25	0.58	6.46	1.96	0.90	5,15	16.0	23.88	38.24
Upper	1548	195.00	526.57	529.11	1.97	0.87	13.59	2.96	1.48	6.88	1.34	57.66	65.51
Upper	1539	22.00	525.52	527.86	0.10	70.0	0.15	60.0	0.07	1.46	0.07	15.41	18.21
Upper	1539	44.00	525.52	528.28	0.20	0.08	0.42	0.13	0:30	2.11	0.30	28.15	38.55
Upper	1539	30.00	525.52	528.06	0.14	90:0	0,23	60.0	0.17	1.71	0.17	20.43	31.00
Upper	1539	67.00	525.52	528.40	0.27	0.12	0.68	0.20	0.39	2.50	0.39	32.86	42.50
Upper	1539	81.00	525.52	528.56	0.42	0.18	1.33	0.37	0.54	3.15	0.54	40.13	47.97
Upper	1539	195.00	525.52	529.20	0.94	0.41	4.66	1.02	1.03	4.94	0.92	77.99	72.08

Upper	1527	22.00	526.56	527.51	1.25	1.25	5.60	5.60		4.48		4.92	8.02
Upper	1527	44.00	526.56	528.03	0.92	0.29	3.85	0.81	0:20	4.16	0.51	15.97	52.97
Upper	1527	30.00	526.56	527.68	1.34	1.34	6.34	6.34		4.72		6.36	9.34
Upper	1527	27.00	526.56	528.14	1.03	0.38	4.62	0.98	0.67	4.48	0.74	22.13	57.11
Upper	1527	81.00	526.56	528.30	1.23	0.51	6.14	1.31	0.87	9.00	1.01	31.58	62.94
Upper	1527	195.00	526.56	529.21	0.82	0.44	3.66	0.82	40.1	4.47	1.29	104.13	93.18
Opper	1511	22.00	525.99	527.23	0.49	0.44	1.43	1.26	0.11	2.91	0.12	7.59	11.42
Upper	1511	44.00	525.99	527.70	0.58	0.29	1.96	0.77	0.52	3.41	0.53	16.68	27.55
Upper	1511	30.00	525.99	527.42	0.53	0.33	1.65	0.94	0.34	3.13	0.34	10.43	18.07
Upper	1511	27.00	525.99	527.90	0.61	0.29	2.22	0.73	0.62	3.61	0.63	22.98	34.56
Upper	1511	81.00	525.99	528.19	0.69	0.31	2.74	0.72	0.57	3.95	0.79	34.61	46.71

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Keach			i	i (::			-	1					
	Kiver Sta	C lotal	5 5	W.S. Efev	Shear Chan	Shear Iotal	Power Chan	Power lotal	VelLeft	Vel Chri	Vel Right	Flow Area	Top Width
		(cts)	£	£	(lb/sq ft)	(lb/sd ft)	(lb/ft s)	(lb/ft s)	(£Ns)	(£/s)	(£Qs)	(sq ft)	(£)
Upper	1511	195.00	525.99	629.00	0.98	0.42	4.91	0.93	0.87	5.02	1.18	87.73	84.06
Upper	1503	22:00	524.94	527.27	0.10	0.09	0.15	0.13		1.47	0.07	15.11	13.73
Upper	1503	44.00	524.94	527.74	0.20	0.10	0.42	0.18	0.27	2.12	0.27	25.00	28.69
Upper	1503	30.00	524.94	527.47	0.14	60:0	0.24	0.14		1.74	0.16	18.39	19.97
Upper	1503	57.00	524.94	527.94	0.25	0.12	09.0		0.35	2.41	0.36	31.31	35.05
Upper	1503	81.00	524.94	528.22	0.34	0.14	96.0	0.27	0.32	2.87	0.50	42.75	47.31
Upper	1503	195.00	524,94	528.99	89'0	0.27	2:92	0.56	0.65	4.29	0.91	93.44	83.68
Upper	1493	22.00	525.98	526.93	1.25	1.25	5.61	5.61		4.48		4.91	8.01
Upper	1493	44.00	525.98	527.32	1.46	1.02	7.47	5.00	0.43	5.12	0.43	8.94	15,20
Upper	1493	30.00	525.98	527.10	1.34	1.34	6.31	6.31		4.71		6.37	9.35
Upper	1493	92.00	525.98	527.51	1.47	0.81	7.81	3,69	0.68	5.31	0.69	12.50	22.17
Upper	1493	81.00	525.98	527.79	1.53	0.74	8.65	2.99	0.93	5.64	0.94	20.04	32.29
Upper	1493	195.00	525.98	528.56	1.96	0.85	13.45		1.16	6.87	1.52	56.79	64.53
Upper	1476	22.00	525.32	526.57	0.48	0.43	1.39	1.24	0.13	2.88	0.13	7.66	11.29
Upper	1476	44.00	525.32	527.03	0.58	0.32	2.00	0.90	0.54	3.43	0.52	15.82	23.90
Upper	1476	30.00	525.32	526.76	0.52	0.34	1.61	1.00	0.35	3.11	0.35	10.37	16.56
Upper	1476	57.00	525.32	527.22	0.65	0.34	2.44	66.0	02.0	3.72	0.59	20.81	29.16
Upper	1476	81.00	525.32	527.46	0.82	0.41	3.51	1.14	06:0	4.28	0.74	28.77	36.00
Upper	1476	195.00	525.32	528.20	1.45	99.0	8.80	2.02	1.31	90.9	1.23	63.32	60.49
Upper	1466	22.00	524.26		0.10	60.0	0.15	0.13	0.07	1.46	20.0	15.22	13.34
Upper	1466	44.00	524.26	527.07	0.20	0.11	0.42	0.20	0.28	2.12	0.26	24.11	25.01
Upper	1466	30.00	524.26	526.80	0.14	60.0	0.24	0.15	0.16	1.73	0.16	18.32	18.15
Upper	1466	57.00	524.26	527.26	0.25	0.13	0.62	0.25	0.38	2.44	0.32	29.27	30.24
Upper	1466	81.00	524.26	527.50	0.37	0.17	1.11	0.38	0.53	3.00	0.45	37.47	37.06
Upper	1466	195.00	524.26	528.22	68'0	0.37	4.32	1.02	0.92	4.87	68.0	71.66	61.27
Upper	1453	22.00	525.30	526.25	1.24	1.24	5:52	5.55		4.46		4.93	8.03
Upper	1453	44.00	525.30	526.65	1.43	0.90	7.22	4.30	0.44	90.5	0.44	9.18	17.18
Upper	1453	30.00	525.30	526.42	1.34	1.34	6.31	6.31		4.71		6.37	9.35
Upper	1453	67.00	525.30	526.85	1.40	69.0	7.26	2,90	0.68	5.19	0.68	13.48	26.60
Upper	1453	81.00	525.30	527.12	1.43	0.68	7.76	2.49	0.95	5.44	96:0	22.19	35.96
Upper	1453	195.00	525.30	527.80	2.11	1.15	14.98	4.44	1.61	7.09	1.78	50.62	47.54
Upper	1439	22.00	524.72	525.97	0.48	0:30	1.37	0.85	0.13	2.87	0.13	7.83	16.44
Upper	1439	44.00	524.72	526.30	0.72	0.34	2.69	0.92	0.62	3.74	0.57	16.16	32.26
Upper	1439	30.00	524.72	526.17	0.48	0.23	1.44	0.57	0.41	3.00	0.39	12.35	26.98
Upper	1439	92.00	524.72	526.37	1.01	0.47	4.49	1.45	0.78	4.46	67.0	18.45	35.04
Upper	1439	81.00	524.72	526.50	1.44	29:0	7.85	2.30	1.04	5.44	76.0	23.48	40.50

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

(cfs)	(ff) 524.72	(#)	(Breat)						,		
1439 195.00 1430 22.00 1430 44.00 1430 30.00 1430 81.00 1430 195.00 1430 195.00 1418 22.00 1418 44.00 1418 81.00 1418 81.00 1418 81.00 1402 22.00 1402 22.00 1402 44.00 1403 81.00 1402 44.00 1403 81.00 1383 44.00 1381 44.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 44.00 1383 44.00 1384 44.00 1388 44.00 1388 44.00 1388 30.00 1388 44.00 1388 44.00	524.72		(in being)	(lb/sq ft)	(lb/fts)	(lb/ft s)	(£/\cdot)	(ths)	(th/s)	(sq ft)	€
1430 22.00 1430 30.00 1430 30.00 1430 57.00 1430 195.00 1430 195.00 1418 22.00 1418 44.00 1418 81.00 1418 81.00 1402 22.00 1402 44.00 1402 44.00 1402 44.00 1402 44.00 1403 81.00 1404 44.00 1383 44.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 44.00 1383 30.00 1384 44.00 1388 44.00 1388 44.00 1388 44.00 1388 44.00		527.17	1.93	0.95	13.03	3.10	1.53	6.75	1.58	59.58	63.75
1430 22 00 1430 44 00 1430 57 00 1430 81 00 1430 195 00 1430 195 00 1418 22 00 1418 30 00 1418 81 00 1418 81 00 1402 22 00 1402 22 00 1402 81 00 1402 195 00 1402 195 00 1403 81 00 1404 195 00 1405 195 00 1406 195 00 1383 44 00 1381 44 00 1381 81 00 1381 195 00 1381 81 00 1381 81 00 1381 81 00 1388 44 00 1389 44 00 1388 44 00 1389 44 00 1388 44 00 1388 44 00 <td></td>											
1430 44.00 1430 30.00 1430 30.00 1430 195.00 1430 195.00 1418 22.00 1418 44.00 1418 81.00 1418 81.00 1418 81.00 1402 22.00 1402 22.00 1402 44.00 1402 44.00 1402 44.00 1403 81.00 1383 44.00 1381 44.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 22.00 1383 44.00 1384 44.00 1388 44.00 1388 44.00 1388 30.00 1388 44.00	523.66	526.01	0.10	0.03	0.14	0.04	90.08	1.44	0.08	17.24	47.29
1430 30.00 1430 57.00 1430 195.00 1430 195.00 1418 22.00 1418 44.00 1418 57.00 1418 81.00 1418 81.00 1402 22.00 1402 44.00 1402 44.00 1402 44.00 1403 81.00 1404 44.00 1383 44.00 1381 44.00 1381 44.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 22.00 1383 44.00 1384 81.00 1388 44.00 1388 44.00 1388 30.00 1388 44.00 1388 30.00 1388 30.00 1388 30.00	523.66	526.37	0.18	0.07	0.37	0.09	0.32	2.02	0.33	35.57	55.82
1430 57.00 1430 57.00 1430 195.00 1418 22.00 1418 22.00 1418 44.00 1418 195.00 1402 22.00 1402 30.00 1402 30.00 1402 44.00 1402 30.00 1383 44.00 1381 22.00 1381 22.00 1381 30.00 1381 30.00 1381 30.00 1381 57.00 1381 81.00 1381 81.00 1381 81.00 1381 30.00 1381 81.00 1384 44.00 1386 22.00 1388 44.00 1389 30.00 1388 44.00	523.66	526.21	0.12	0.04	0.19	0.05	0.21	1.61	0,21	27.19	52.09
1430 81.00 1430 195.00 1418 22.00 1418 22.00 1418 44.00 1418 81.00 1402 22.00 1402 30.00 1402 30.00 1402 44.00 1402 30.00 1383 44.00 1381 22.00 1381 22.00 1381 30.00 1381 30.00 1381 30.00 1381 57.00 1381 57.00 1381 81.00 1381 81.00 1381 81.00 1381 44.00 1381 81.00 1381 81.00 1384 44.00 1386 22.00 1388 30.00 1388 30.00 1388 30.00	523.66	526.47	0.25	0.10	0.59	0.14	0.41	2.38	0.43	41.28	58.23
1430 195.00 1418 22.00 1418 22.00 1418 44.00 1418 81.00 1402 22.00 1402 30.00 1402 30.00 1402 44.00 1402 81.00 1333 44.00 1383 44.00 1381 22.00 1381 22.00 1381 30.00 1381 30.00 1381 30.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1384 44.00 1389 30.00 1389 44.00 1388 44.00 1388 44.00 1388 44.00 1388 44.00 1388 30.00 1388 30.00	523.66	526.61	0.38	0.17	1.13	0.27	0.57	2.97	0.59	49.86	61.66
1418 22.00 1418 44.00 1418 30.00 1418 57.00 1418 100 1418 100 1402 22.00 1402 22.00 1402 30.00 1402 44.00 1402 1400 1402 1400 1402 1400 1403 81.00 1381 22.00 1381 44.00 1381 30.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1384 44.00 1386 44.00 1388 44.00 1389 44.00 1388 44.00 1388 44.00 1388 44.00 1388 44.00	523.66	527.29	0.71	0.36	3.05	0.73	1.00	4.28	1.06	97.00	77.60
1418 22.00 1418 44.00 1418 30.00 1418 81.00 1418 100 1402 22.00 1402 22.00 1402 30.00 1402 30.00 1402 44.00 1333 44.00 1383 81.00 1381 22.00 1381 44.00 1381 30.00 1381 44.00 1381 30.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 44.00 1383 44.00 1384 81.00 1386 22.00 1388 44.00 1388 44.00 1388 30.00 1388 30.00 1388 30.00 1388 30.00											
1418 44.00 1418 30.00 1418 57.00 1418 81.00 1402 22.00 1402 44.00 1402 30.00 1402 44.00 1402 30.00 1402 1400 1402 1400 1333 44.00 1381 22.00 1381 22.00 1381 30.00 1381 57.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 44.00 1383 44.00 1384 81.00 1386 44.00 1388 44.00 1388 44.00 1388 44.00 1388 44.00 1388 44.00 1388 44.00 1388 44.00	524.71	525.66	1.25	1.25	5.61	5.61		4.48		4.91	8.01
1418 30.00 1418 57.00 1418 81.00 1418 100 1402 22.00 1402 44.00 1402 30.00 1402 44.00 1402 30.00 1333 44.00 1381 22.00 1381 44.00 1381 44.00 1381 57.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1384 81.00 1386 44.00 1388 44.00 1389 44.00 1389 44.00 1388 44.00 1388 44.00 1388 44.00 1388 44.00 1388 30.00 1388 30.00	524.71	526.15	98.0	0.28	3.41	0.61	0.58	3.98	0.59	19.94	67.23
1418 57.00 1418 81.00 1418 1402 1402 22.00 1402 44.00 1402 30.00 1402 1402 1402 1400 1402 1400 1402 1400 1403 81.00 1383 44.00 1381 22.00 1381 44.00 1381 30.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1384 81.00 1388 44.00 1389 30.00 1388 44.00 1389 30.00 1388 30.00 1388 30.00 1388 30.00	524.71	525.82	1.36	1.36	6.46	6,46		4.75		6.32	9.31
1418 81.00 1418 180.00 1402 22.00 1402 44.00 1402 30.00 1402 1402 1402 14.00 1402 14.00 1403 81.00 1383 44.00 1381 22.00 1381 22.00 1381 44.00 1381 30.00 1381 57.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 30.00 1383 44.00 1384 81.00 1386 44.00 1388 44.00 1388 30.00 1388 44.00	524.71	526.24	96.0	0.36	4.23	0.90	0.76	4.33	0.77	26.10	69.84
1418 195.00 1402 22.00 1402 44.00 1402 30.00 1402 1402 1402 14.00 1402 14.00 1402 14.00 1333 44.00 1381 22.00 1381 22.00 1381 44.00 1381 30.00 1381 57.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 30.00 1383 44.00 1384 81.00 1388 44.00 1389 44.00 1388 44.00 1388 44.00 1388 44.00 1388 30.00 1388 30.00 1388 30.00	524.71	526.38	1.14	0.49	5.47	1.10	0.99	4.78	1.01	36.37	73.98
1402 22.00 1402 22.00 1402 44.00 1402 30.00 1402 57.00 1402 61.00 1402 105.00 1333 22.00 1381 22.00 1381 22.00 1381 44.00 1381 44.00 1381 44.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 44.00 1383 44.00 1384 81.00 1388 44.00 1388 30.00 1388 30.00 1388 30.00 1388 30.00 1388 30.00	524.71	527.27	0.70	0.41	2.89	0.70	1.18	4.11	1.19	113.31	97.36
1402 22.00 1402 44.00 1402 44.00 1402 57.00 1402 61.00 1402 61.00 1402 105.00 1333 44.00 1381 22.00 1381 22.00 1381 44.00 1381 44.00 1381 44.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1384 81.00 1386 22.00 1368 44.00 1368 30.00 1368 30.00 1368 30.00 1368 30.00											
1402 44.00 1402 30.00 1402 30.00 1402 81.00 1402 105.00 1383 22.00 1383 44.00 1381 22.00 1381 44.00 1381 22.00 1381 44.00 1381 44.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1382 22.00 1383 44.00 1384 81.00 1388 30.00 1368 30.00 1368 30.00 1368 30.00 1368 30.00	524.09	525.34	0.48	0.40	1.36	1.15	0.13	2.87	0.13	7.73	11.99
1402 30.00 1402 57.00 1402 57.00 1402 81.00 1383 22.00 1383 44.00 1383 81.00 1381 22.00 1381 22.00 1381 44.00 1381 30.00 1381 44.00 1381 81.00 1381 81.00 1381 81.00 1382 30.00 1383 44.00 1384 81.00 1388 30.00 1368 30.00 1368 30.00 1368 30.00 1368 30.00 1368 30.00	524.09	525.81	0.56	0.27	1.87	0.69	0.52	3.35	0.52	17.42	29.68
1402 57.00 1402 81.00 1402 195.00 1383 22.00 1383 44.00 1383 81.00 1381 22.00 1381 44.00 1381 22.00 1381 44.00 1381 81.00 1381 81.00 1381 81.00 1382 22.00 1383 44.00 1384 81.00 1388 44.00 1368 44.00 1368 30.00 1368 30.00 1368 30.00	524.09	525.54	0.51	0:30	1.56	0.83	0.35	3.07	0.35	10.80	19.43
1402 81.00 1402 195.00 1393 22.00 1393 44.00 1393 81.00 1393 81.00 1393 195.00 1381 22.00 1381 30.00 1381 30.00 1381 81.00 1381 81.00 1381 81.00 1382 44.00 1383 44.00 1384 81.00 1388 44.00 1368 30.00 1368 30.00 1368 30.00 1368 30.00	524.09	525.99	0.62	0.29	2.26	0.71	0.63	3.63	0.63	23.32	36.46
1402 195.00 1393 22.00 1393 44.00 1393 81.00 1393 81.00 1393 195.00 1381 22.00 1381 44.00 1381 30.00 1381 81.00 1381 81.00 1381 81.00 1382 22.00 1368 22.00 1368 30.00 1368 30.00 1368 30.00	524.09	526.22	0.76	0.36	3.14	06:0	0.81	4.12	0.82	32.65	42.75
1393 22.00 1393 44.00 1393 44.00 1393 57.00 1393 81.00 1391 22.00 1381 30.00 1381 57.00 1381 81.00 1381 44.00 1381 44.00 1381 44.00 1382 22.00 1368 22.00 1368 30.00 1368 30.00 1368 30.00	524.09	526.77	1.67	0.83	10.64	2.69	1.44	6:39	1.47	59.85	56.93
1393 22.00 1393 44.00 1393 30.00 1393 57.00 1393 81.00 1393 195.00 1381 22.00 1381 57.00 1381 57.00 1381 81.00 1381 44.00 1381 44.00 1381 44.00 1388 44.00 1368 22.00 1368 30.00 1368 30.00 1368 30.00											
1393 44.00 1393 30.00 1393 57.00 1393 81.00 1393 195.00 1381 22.00 1381 57.00 1381 57.00 1381 81.00 1381 57.00 1381 44.00 1381 44.00 1382 22.00 1368 22.00 1368 30.00 1368 30.00 1368 30.00	523.04	525.38	0.10	0.09	0.15	0.12	0.07	1,46	70.0	15.20	13.71
1393 30.00 1393 57.00 1393 81.00 1393 195.00 1381 22.00 1381 57.00 1381 57.00 1381 81.00 1381 57.00 1381 44.00 1381 44.00 1388 44.00 1368 22.00 1368 30.00 1368 30.00 1368 30.00	523.04	525.84	0.20	0.10	0.42	0.18	0.28	2.12	0.27	24.68	27.37
1393 57.00 1393 81.00 1383 195.00 1381 22.00 1381 44.00 1381 57.00 1381 81.00 1381 81.00 1381 44.00 1382 22.00 1388 44.00 1388 30.00 1388 30.00	523.04	525.58	0.14	0.09	0.24	0.14	0.16	1.73	0.16	18.46	19.52
1393 81.00 1393 195.00 1381 22.00 1381 44.00 1381 57.00 1381 81.00 1381 81.00 1381 81.00 1381 44.00 1368 22.00 1368 30.00 1368 30.00	523.04	526.02	0.26	0.13	0.63	0.24	0.36	2.46	0.36	29.88	32.57
1393 195.00 1381 22.00 1381 44.00 1381 81.00 1381 81.00 1381 81.00 1381 81.00 1381 44.00 1388 30.00 1388 30.00 1388 30.00	523.04	526.24	0.38	0.17	1.15	0.37	0.48	3.03	0.51	38.03	39,98
1381 22.00 1381 44.00 1381 30.00 1381 57.00 1381 81.00 1381 136 1388 22.00 1368 44.00 1368 30.00	523.04	526.73	1.15	05.0	6.27	1.58	0.99	5.46	1.06	61.47	56.08
1381 22.00 1381 44.00 1381 57.00 1381 67.00 1381 81.00 1381 44.00 1368 22.00 1368 44.00 1368 30.00											
1381 44.00 1381 30.00 1381 57.00 1381 81.00 1381 81.00 1381 44.00 1368 22.00 1368 44.00 1368 30.00	524.08	525.04	1.24	1.24	5.49	5.49		4.45		4.95	8.05
1381 30.00 1381 57.00 1381 81.00 1381 1.00 1388 22.00 1368 44.00 1368 30.00	524.08	525.44	1.38	77.0	6.85	3.52	0.45	4.98	0.45	9.57	20.05
1381 57.00 1381 81.00 1381 105.00 1368 22.00 1368 44.00 1368 30.00	524.08	525.20	1.34	1.34	6.31	6.31		4.71		6.36	9.35
1381 81.00 1381 195.00 1368 22.00 1368 44.00 1368 30.00	524.08	525.64	1.31	0.57	6.60	2.19	0.68	5.04	0.68	14.86	32.62
1381 195.00 1368 22.00 1368 44.00 1368 30.00	524.08	525.90	1.35	0.54	7.15	1.75	0.88	5.29	0.88	25.21	48.56
1368 22.00 1368 44.00 1368 30.00	524.08	526.49	1.94	0.94	13.11	3.02	1.45	6.75	1.66	80.78	67.36
1368 22.00 1368 44.00 1368 30.00											
1368 44.00	523.58	524.81	0.50	0.40	1.47	1.16	0.11	2.93	0.11	7.55	12.83
1368 30.00	523.58	525.26	0.54	0.25	1.77	0.56	0.44	3.29	0.65	19.78	36.40
0007	523.58	525.01	0.52	0.23	1.60	0.59	0.32	3.09	0.35	11.65	28.36
DD:/c	523.58	525.40	0.63	0:30	2.30	0.68	0.54	3.63	0.82	25.08	40.79
	523.58	525.60	08.0	0.39	3.34	0.92	0.70	4.17	1.05	33.89	47.20

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Reach	River Sta	Reach River Sta O Total Min Ch El W.S. Fley Shear Chan	Zin Ch	W.S. Flev	Shear Chan	Shear Total	Power Chan	Power Total	Vallaft	Vel Chul	Vel Right	Flow Area	Top Width
		(cfs)	(ft)	(H)	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(s/µ)	(ths)	(ftVs)	(sq ft)	(£)
Upper	1368	195.00	523.58	526.23	1.40	0.71	8.17	2.01	1.25	5.84	1.66	69.40	64.96
Upper	1358	22.00	522.52	524.85	0.10	90.0	0.15	0.03	70.0	1.47	0.07	15.35	19.74
Upper	1358	44.00	522.52	525.29	0.19	0.08	0.38	0.11	0.29	2.05	0.33	30.73	43.16
Upper	1358	30.00	522.52	525.05	0.14	90'0	0.23	0.08	0.17	1.71	0.17	21.08	36.36
Upper	1358	00'29	522.52	525.43	0.25	0.11	0.58	0,16	0.38	2.38	0.44	36.87	46.97
Upper	1358	81.00	522.52	525.62	0.35	0.16	1.03	0.28	0.51	2.91	0.60	46.68	52.49
Upper	1358	195.00	522.52	526.23	0.81	0.38	3.73	0.88	1.02	4.59	1.10	83.91	70,90
Upper	1351	22.00	523.57	524.52	1.25	1.25	5.61	5.61		4.48		4.91	8.01
Upper	1351	44.00	523.57	525.01	1.04	0.37	4.59	1.23	0.50	4.40	0.50	13.36	40.31
Upper	1351	30.00	523.57	524.69	1.34	1.34	6.33	6:33		4.72		6.36	9.35
Upper	1351	67.00	523.57	525.14	1.14	0.46	5.33	1.40	0.75	4.69	0.76	18.85	43.83
Upper	1351	81.00	523.57	525.32	1.33	0.61	6.97	1.81	1.02	5.22	1.04	27.18	48.69
Upper	1351	195.00	523.57	525.88	2.09	1.09	14.47	3.62	1.67	6.93	1.74	58.61	63.78
Upper	1326	22.00	522.40	523.65	0.48	0.39	1.38	1.12	0.13	2.88	0.13	7.70	12.47
Upper	1326	44.00	522.40	524.12	0.54	0.25	1.76	0.58	0.53	3.29	0.53	18.85	33.93
Upper	1326	30.00	522.40	523.85	0.51	0.27	1.56	0.73	0.34	3.07	0.34	11.10	22.26
Upper	1326	57.00	522.40	524.29	0.60	0.28	2.13	0.63	0.65	3.56	0.64	25.09	39.70
Upper	1326	81.00	522.40	524.51	0.75	0.35	3.04	0.82	0.82	4.07	0.81	34.67	47.20
Upper	1326	195.00	522.40	525.19	1.24	0.61	6.88	1.59	1.29	5.56	1.31	74.69	68.36
Upper	1318	22.00	521.35	523.69	0.10	0.07	0.15	0.10	20.0	1.46	70.0	15.33	16.52
Upper	1318	44.00	521.35	524.15	0.19	80.0	0.38	0.12	0.29	2.06	0.29	28.95	38.85
Upper	1318	30.00	521.35	523.89	0.14	90:0	0.24	0.10	0.16	1.72	0.16	19.73	28.31
Upper	1318	57.00	521.35	524.32	0.24	0.10	0.55	0.17	0.39	2.35	0.39	35.82	43.04
Upper	1318	81.00	521.35	524.54	0.34	0.15	96'0	0.27	0.53	2.85	0.53	45.87	48.53
Upper	1318	195.00	521.35	525.19	0.79	0.37	3.61	0.88	1.00	4.57	96'0	82.89	65.60
U pper	1306	22:00	522.39	523.34	1.25	1.25	5.56	5.56		4.47		4.93	8.03
Upper	1306	44.00	522.39	523.76	1.34	0.68	6.59	3.05	0.46	4.92	0.46	9.89	22.38
Upper	1306	30.00	522.39	523.51	1.34	1.34	6.31	6.31		4.71		6.36	9.35
Upper	1306	27.00	522.39	523.98	1.20	0.48	5.82	1.68	0.67	4.84	29.0	16.49	38.30
Jpper	1306	81.00	522.39	524.19	1.35	0.60	7.12	1.90	76.0	5.28	0.94	25.36	45.23
Upper	1306	195.00	522.39	524.79	2.04	1.03	14.11	3.46	1.65	6.91	1.56	57.73	62.12
Upper	1231	22.00	521.77	523.03	0.47	0.33	1.33	0.92	0.16	2.85	0.17	7.89	14.73
Upper	1291	44.00	521.77	523.43	0.63	0.34	2.21	0.93	0.56	3.53	0.60	16.05	25.80
	1291	30.00	521.77	523.22	0.49	0.29	1.49	22.0	0.38	3.03	0.42	11.31	20.13
	1291	57.00	521.77	523.57	0.77	0.40	3.06	1.16	69.0	3.98	0.73	19.81	29.54
Upper	1291	81.00	521.77	523.76	1.02	0.52	4.79	1,61	0.89	4.70	0.93	26.18	34.97

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Reach													
		╁	 	€	(lhfea ft)	(libles #)	10 mm C mm C	TOWER TOTAL	אפו רפונ	Vel Cillis	Vel Right	FIOW Area	unplan do i
Ilanor	1001	(600)	(11)	61.7		(1) hearn)	(10)11 5)	(15 11/01)	(ROS)	(108)	(TUS)	(sq ft)	(H)
eddo	1831	195,00	27.17	524.40	1.89	0.98	12.81	3.58	1.48	6.78	1.61	53,33	49.63
	7007	00	1			1							
Opper	1281	22.00	520.72	523.06	0.10	0.05	0.15	0.07	0.09	1.45	0.10	16.16	25.67
Upper	1281	44.00	520.72	523.48	0.19	0.10	0.40	0.15	0.33	2.09	0,35	28.36	33.41
Upper	1281	30.00	520.72	523.26	0.13	70.0	0.22	60:0	0.21	1.68	0.22	21.61	29.38
Оррег	1281	27.00	520.72	523.62	0.26	0.13	0.62	0.22	0.43	2.43	0.45	33.40	36.13
Upper	1281	81,00	520.72	523.84	0.37	0.19	1.11	0.37	0.57	2.98	0.61	41.63	40.17
Upper	1281	195.00	520.72	524.49	0.90	0.47	4.38	1 29	1.07	4 86	1 14	71.81	52 40
												2	ST.:30
Upper	1269	22.00	521.76	522.71	1.26	1.26	5.63	583		4 48		7 04	100
Upper	1269	8,44	521.76	523.17	1.10	0.48	4 96	161	0.64	4 50	A C	19.00	22 22
Upper	1269	30.00	521.76	522 88	136	38	R 42	CPS	5	A 7.4	3	00.0	5 5
Upper	1269	57 00	521.78	523.20	133	92.0	25.00	3,00	90	† 6	000	0.33	9.32
Innar	1260	84.00	A7 10A	523.40	777	3,000	1 6	00	0.00	50.4	0.00	17.74	30.02
200	0007	00.10	02.10	023.40	\$ 1. T	0.70	11'1	ES.2	EL.1	5.40	1.15	24.93	40.80
obbei	6071	195.00	97.126	524.10	2.15	1.19	15.20	4.28	1.77	7.06	1.81	54.44	54.70
Inner	1254	22.00	A24 4E	522 44	27.0	700	60.4				4		
Langer L	7367	26.25	021.10	322.41	74.0	0.37	05.7	3	U.13	2.86	0.13	7.77	13.01
Chrei	+021	3.4	07.170	577.69	LC.D	0.22	1.85	0.47	0.51	3.22	0.51	20.28	39.71
Upper	1254	30,00	521.16	522.61	0,50	0.25	1.52	0.66	0.34	3.05	0.34	11.41	24.07
Upper	1254	27.00	521.16	523.08	0.53	0.23	1.78	0.45	0.62	3.36	09:0	28.79	47.90
Upper	1254	81.00	521.16	523.33	09'0	0.28	2.19	0.55	62'0	3.66	0.75	41.59	53.94
Upper	1254	195.00	521.16	524.12	0.86	0.45	4.00	0.95	1.21	4.67	1.11	91.96	73.11
Upper	1245	22.00	520.11	522.45	0,10	0.07	0.15	0.11	70.0	1.46	0.07	15.31	16.06
Upper	1245	44.00	520.11	522.92	0.19	0.08	0.39	0.12	0.27	2.07	0.27	28.68	41.47
Upper	1245	30.00	520.11	522.65	0.14	0.07	0.24	0,10	0.16	1.72	0.16	19.51	26.77
Upper	1245	57.00	520.11	523.10	0.23	60.0	0.54	0.15	0.36	2.33	0.35	36.97	48.37
Upper	1245	81.00	520.11	523.34	0.31	0.14	78.0	0.22	0.51	2.77	0.48	49.26	54.13
Upper	1245	195.00	520.11	524.10	0.62	0:30	2.54	0.60	0.94	4.08	0.87	97.58	72.55
Upper	1233	22.00	521.15	522.10	1.25	1.25	5.61	5.61		4.48		4.91	8.01
Upper	1233	44.00	521.15	522.51	1.39	0.79	6.92	3.65	0.45	9.00	0.45	9.49	19.52
Upper	1233	30.00	521.15	522.27	1.34	1.34	6.32	6.32		4.71		6.36	9.35
Upper	1233	57.00	521.15	522.71	1.33	0.59	6.71	2.29	0.68	5.06	0.68	14.61	31.55
Upper	1233	81.00	521.15	522.99	1.28	0.52	9.60	1.62	0.87	5.17	0.87	25.98	48.58
Upper	1233	195.00	521.15	523.97	1.01	0.54	5.08	1.28	1.28	5.03	1.28	84.00	69.45
Upper	1213	24.00	520,20	521.51	1.21	1.06	3.53	3.05	0.33	2.91	0.33	8.33	11.63
Upper	1213	48.00	520.20	522.00	1.47	0.95	5.11	2.88	06.0	3.47	16.0	15.83	18.99
Upper	1213	38.00	520.20	521.81	1.39	0.96	4.55	2.91	0.74	3.28	0.74	12.58	16.22
Upper	1213	72.00	520.20	522.37	1.60	0.83	6.02	2.40	0.88	3.77	1.21	24.80	29.05
Joner	17.5	102 001	520 20	A22 78	101	-							The second secon

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

1 047-700	an: upreacing	TEC-RAS FIRM: Upreacritice/-14 Kiver; Lariyard Dianch Reach; Upper (Conditional)	allyaid Diane.	יייייי ביייי	, , , , , , , , , ,								
Keacu	KIVET STA	E 0	MID CD EI	W.S. ERW	snear Chan	Shear lotai	Power Chan	Power lotal	Vei Left	Vel Chnl	Vel Kight	Flow Area	lop Width
		(cts)	(£)	(£)	(lb/sd ft)	(lb/sd ft)	(lb/ft s)	(lb/ft s	(LIAS)	(£/£)	(£/\s)	(sq ft)	(£)
Upper	1213	242.00	520.20	523.84	1.79	0.93	7.94	2,45	1.66	4.43	1.72	92.11	57.80
Upper	1204	24.00	519.15			0.10	0.17		60.0	1.54	60'0	15.74	12.77
Upper	1204	48.00	519.15		0.22	0.15	0.50	06.0		2.26	0.31	23.42	19.24
Upper	1204	38.00	519.15		0.18	0.13	0.35		0.23	1.99	0.23	20.22	16.58
Upper	1204	72.00	519.15		0.32	0.16	0.88	0.37	0.35	2.78	0.46	32.01	29.03
Оррег	1204	102.00	519.15	522.74	0.42	0.19	1.35	0.44	0.48	3.26	09.0	44.11	38.84
Upper	1204	242.00	519.15	523.69	0.83	0.40	4.00		1.02	4.84	1.04	90.01	55.60
Upper	1193	24.00	520.19	521.19	1.27	1.27	5.76	5.76		4.53		5.30	8.39
Upper	1193	48.00	520.19	521.57	1.55	1.24	8.26	6.42	0.51	5.32	0.51	9.28	13.01
Upper	1193	38.00	520.19	521.44	1.43	1.34	7.13	6.62	0.22	4.97	0.22	7.66	10.80
Оррег	1193	72.00	520.19	521.88	1.70	1,12	9.92	5.75	0.89	5.84	0.89	13.98	17.95
Оррег	1193	102.00	520.19	522.19	1.85	1.02	11.72	5.01	1.00	6.33	1.15	20.65	25.35
Upper	1193	242.00	520.19	523.20	2,12	1.03	15.66	4.15		7.38	1.65	60.13	50.41
Upper	1181	24.00	519.61	520.92	0.47	0.32	1.38	0.88	0.21	2.90	0.21	8.58	15.83
Upper	1181	48.00	519.61	521.42		0.26	1.68	0.61	0.57	3.27	0.64	20.92	31.46
Upper	1181	38.00	519.61	521.23	0.51	0.27	1.60	0.66	0.48	3.16	0.54	15.40	26.30
Upper	1181	72.00	519.61	521.81	0.53	0.26	1.81	0.54	69'0	3.44	0.77	35.04	41.86
Upper	1181	102.00	519.61	522.20	0.54	0.27	1.94		0.81	3.60	0.83	53.20	51.72
Upper	1181	242.00	519.61	523.38		0.33	2.64		1.08	4.20	1.02	131.44	79.83
Оррег	1169	24.00	518.55	520.95	0.11	70.0	0.17	0.11	0.10	1.52	0,10	16.24	17.81
Upper	1169	48.00	518.55	521.44	0.20	0.10	0.43	0.17	06.0	2.15	0.35	28.68	31.97
U ррег	1169	38.00	518.55	521.26	0.17	60:0	0.32	0.14	0.23	1.93	0.27	23.23	26.98
Upper	1169	72.00	518.55	521.82	0.26	0.12	0.67	0.21	0.43	2.54	0.49	42.49	42.04
Upper	1169	102.00	518.55	522.19	0.32	0.15	0.92	0.26	95.0	2.88	0.59	60.18	51.63
Upper	1169	242.00	518.55	523.36	0.49	0.24	1.85	0.42		3.77	0.85	136.83	79.31
Upper	1158	24.00	519.60	520.60		1.27	5.78	5.78		4.54		5.29	8.38
Upper	1158	48.00	519.60	520.98	1.56	1.26	8.30	6.57	0.51	5.33	0.51	9.24	12.76
Upper	1158	38.00	519.60	520.85	1.44	1.34	7.14	6.67	0.22	4.97	0.22	7.66	10.73
Upper	1158	72.00	519.60	521.28	1.73	1.17	10.19		0.89	5.89	0.88	13.71	17.22
Upper	1158	102.00	519.60	521.59	1.90	1.16	12.20	6.00	1.16	6.41	1.15	19.75	21.87
Upper	1158	242.00	519.60	522.68	2.19	06.0	16.53	3.67	1.44	7.54	1.30	59.14	57.40
Upper	1121	26.00	518.01	519.48		0.32	0.98	0.82	0.31	2.64	0.26	10.09	12.02
Upper	1121	52.00	518.01	519.97		0.40	1.90	1.23	0.61	3.44	0.52	16.91	15.75
Upper	1121	45.00	518.01	519.86		0.37	1.62	1.10	0.55	3.24	0.47	15.24	14.93
Upper	1121	84.00	518.01	520.38	0.76	0.47	3.23	1.60	0.82	4.22	0.59	24.53	21.34
Upper	1121	120.00	518.01	520.74	76.0	0.55	4.78	2.00	1.01	4.90	0.78	33.02	26.32
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HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Reach River Sta O Total Mr.O. Ello W.S. Ello Stract Chan Stract Chan Clade (Phine Chan Pomer Chan Clade (Phine Chan Pomer Chan P	HEC-KAS F	HEC-KAS Plan: Upreachrev/-14 River: Tanyard Branch Reach: Upper (Continued)	W/-14 Kiver.	anyard branch	אלכן יוספטן	(Common)								
1121 Carbo (R) (R) (R) (Bolenty (Bolenty) (Bolenty) (Bolenty (Reach	River Sta	Q Total	Min Ch Ei		Shear Chan	Shear Total	Power Chan	Power Total	Vel Left	Vel Chri	Vel Right	Flow Area	Top Width
1106 282.00 518.04 521.82 164 0.05 11.10 11.06 282.00 517.26 519.46 0.13 0.13 0.13 0.15 0.20 11.10 11.06 45.00 517.26 519.89 0.23 0.14 0.042 11.06 45.00 517.26 519.89 0.23 0.14 0.042 11.06 45.00 517.26 520.43 0.31 0.17 0.83 11.06 11.06 45.00 517.26 520.43 0.33 0.22 0.14 0.042 11.06 11.06 45.00 517.26 520.43 0.33 0.23 0.17 0.83 11.06 11.06 45.00 518.00 519.27 0.23 0.23 0.23 0.23 11.06 11.06 45.00 518.00 519.27 0.23 0.23 0.23 0.23 11.06 11.06 45.00 518.00 519.27 0.23 0.23 0.23 0.23 11.06 1			(cfs)	Œ	€	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(£/L)	(£/L)	(£/L)	(sd ft)	Œ
1106 25.00 517.26 519.46 0.13 0.13 0.12 0.14 0.15 0.14 0.15 0.14 0.15 0.14 0.15 0.15 0.14 0.15 0.	Upper	1121	282.00	518.01	521.82	1.64	0.65	11.10	2.36	1.45	6.79	1.03	77.53	60.38
1106 52.00 517.28 519.48 0.13 0.13 0.20 1106 45.00 517.28 519.99 0.23 0.11 0.45 1106 45.00 517.28 520.43 0.21 0.14 0.42 1106 45.00 517.28 520.43 0.21 0.14 0.42 1106 282.00 517.28 520.43 0.21 0.14 0.42 1106 282.00 517.28 520.43 0.23 0.13 0.13 1086 52.00 518.00 519.57 0.89 0.65 0.73 0.13 1086 52.00 518.00 519.57 0.89 0.68 3.61 1086 46.00 518.00 519.57 0.89 0.68 3.61 1086 46.00 518.00 520.05 1.15 0.54 1086 52.00 518.00 520.05 1.15 0.54 1086 52.00 518.00 520.05 1.15 0.54 1081 46.00 517.43 518.39 0.65 0.41 1.10 1081 46.00 517.43 518.39 0.65 0.40 1.50 1081 46.00 517.43 518.39 0.65 0.40 0.12 1081 46.00 518.42 518.30 0.69 0.60 1081 46.00 518.42 518.30 0.69 0.60 1081 46.00 518.42 518.30 0.60 0.60 1081 46.00 518.42 518.30 0.60 0.60 1081 46.00 518.42 518.30 0.60 0.60 1081 46.00 518.42 518.30 0.60 0.60 1081 46.00 518.42 518.30 0.60 0.60 1081 46.00 518.42 518.30 0.60 0.60 1081 46.00 518.42 518.30 0.60 0.60 1081 46.00 518.42 518.30 0.60 0.60 1081 52.00 518.42 518.30 0.60 0.60 1080 45.00 517.40 518.85 0.71 0.71 0.71 1080 52.00 517.40 518.85 0.71 0.71 0.71 1080 52.00 517.40 518.80 0.50 0.60 1080 52.00 517.40 518.80 0.50 0.60 0.60 1080 52.00 517.40 518.80 0.50 0.60 0.60 1080 52.00 517.40 518.80 0.50 0.60 0.60 1080 52.00 517.40 518.80 0.50 0.60 0.60 1080 52.00 517.40 518.80 0.60 0.60 0.60 1080 52.00 517.40 518.80 0.50 0.60 0.60 1080 52.00 517.40 518.80 0.50 0.60 0.60 1080 52.00 517.40 518.80 0.50 0.60 0.60 1080 52.00 518.80 0.60 0.60 0.60 0.60 1080 52.00														
1106 45.00 517.26 518.99 0.23 0.12 0.42 1.106 45.00 517.26 550.43 0.31 0.14 0.42 1.106 45.00 517.26 520.82 0.34 0.31 0.17 0.63 1.10 1.106 45.00 517.26 520.82 0.38 0.12 0.13 0.15 1.10 0.15 1.10 0.15 1.10 0.15 0.10 0.15 0.10 0.15 0.10 0.15 0.10 0.15 0.10 0.15 0.10 0.15 0.10 0.15 0.10 0.15 0.10 0.15	Upper	1106	26.00	517.26	519.48	0.13	0.13	0.20	0.20		1.60		16.27	12.66
1106 45.00 517.26 519.87 0.20 0.14 0.42 1.106 1.106 1.20.00 517.26 520.24 0.21 0.17 0.023 1.108 1.106 1.20.00 517.26 520.24 0.23 0.21 1.118 1.100.00 517.26 520.24 0.23 0.22 1.118 1.106 1.20.00 518.00 520.04 1.12 0.73 5.24 1.108 1.008 520.00 518.00 520.04 1.12 0	Upper	1106	52.00	517.26	519.99	0.23	0.12	0.50	0.25	0.17	2.23	0.17	24.84	29.01
1106 64 00 517.26 520.43 0.31 0.17 0.08 1106 22,000 517.26 520.82 0.38 0.02 1.18 1106 22,000 516.00	Upper	1106	45.00	517.26	519.87	0.20	0.14	0.42	0.28	0.10	2.09	0.10	21.96	21.40
1106 120.00 517.26 520.82 0.38 0.22 1.19 1106 282.00 517.26 521.89 0.67 0.33 2.91 1106 282.00 516.00 519.67 0.73 0.73 2.60 1086 46.00 518.00 519.67 0.04 0.73 3.61 1086 46.00 518.00 520.06 1.12 0.73 3.61 1086 46.00 518.00 520.04 1.12 0.73 3.61 1086 46.00 518.00 520.04 1.12 0.73 3.61 1086 282.00 518.00 521.75 1.15 0.54 6.47 1086 282.00 517.43 518.89 0.41 1.10 0.41 1.10 1081 45.00 517.43 518.89 0.41 1.10 0.41 1.10 1081 45.00 517.43 518.89 0.41 1.10 0.41 1.10	Пррег	1106	84.00	517.26	520.43	0.31	0.17	0.83	0.37	0.42	2.71	0.47	39.24	34.74
1106 282.00 517.26 521.39 0.67 0.23 251 1086 25.00 518.00 518.07 518.07 518.07 523 2.60 1086 45.00 518.00 518.07 518.07 518.07 523 2.60 1086 45.00 518.00 578.67 0.84 0.73 2.60 1086 45.00 518.00 578.67 0.89 0.83 3.61 1086 282.00 518.00 571.74 518.89 0.41 1.10 1086 282.00 517.43 518.89 0.41 0.41 1.10 1081 282.00 517.43 518.89 0.41 0.41 1.10 1051 45.00 517.43 518.89 0.41 0.41 1.10 1051 45.00 517.43 518.89 0.41 0.41 1.10 1051 45.00 517.43 518.89 0.41 0.41 1.10 1051	Upper	1106	120.00	517.26	520.82	0.38	0.22	1.18	0.49	0.58	3.10	29'0	53.61	39.03
1086 28.00 518.00 518.23 0.73 2.80 1086 52.00 518.00 518.67 0.83 0.73 2.80 1086 45.00 518.00 518.67 0.83 0.73 3.85 1086 46.00 518.00 520.06 1.12 0.73 3.81 1086 282.00 518.00 520.06 1.12 0.73 3.81 1086 282.00 518.00 520.04 1.12 0.73 5.42 1086 282.00 517.43 518.88 0.41 0.41 1.10 1051 45.00 517.43 518.88 0.41 0.41 1.10 1051 45.00 517.43 518.80 0.62 0.41 1.10 1051 45.00 517.43 520.12 0.94 0.50 0.72 1051 45.00 517.43 520.87 0.14 0.41 1.10 1051 45.00 516.42 518.20	Upper	1106	282.00	517.26	521.98	29.0	0.33	2.91	0.81	0.95	4.38	0.91	113.74	66.59
1086 26.00 518.00 518.07 518.07 0.73 0.73 2.60 1086 52.00 518.00 518.07 0.84 0.73 3.95 1086 84.00 518.00 520.06 1.12 0.73 5.42 1086 84.00 518.00 520.40 1.12 0.58 5.42 1086 282.00 518.00 520.40 1.22 0.58 5.47 1081 28.00 517.43 518.39 0.41 0.41 1.10 1081 28.00 517.43 518.39 0.52 0.41 1.10 1051 45.00 517.43 518.28 0.42 0.41 1.10 1051 45.00 517.43 518.28 0.42 0.41 1.10 1051 45.00 517.43 518.28 0.42 0.41 1.10 1051 22.00 517.43 520.12 0.41 0.41 1.10 1051 22.00														
1086 52.00 518.00 518.67 0.94 0.79 3.95 1086 45.00 518.00 518.67 0.83 3.61 1086 64.00 518.00 520.06 1.12 0.53 5.62 1086 120.00 518.00 520.06 1.12 0.53 5.42 1086 282.00 517.43 518.89 0.41 1.10 5.47 1051 26.00 517.43 518.89 0.41 1.10 1.10 1051 45.00 517.43 518.89 0.41 1.10 1.10 1051 45.00 517.43 518.80 0.52 0.41 1.10 1051 45.00 517.43 518.80 0.52 0.41 1.10 1051 45.00 517.43 518.80 0.52 0.41 1.10 1051 45.00 517.43 520.12 0.94 0.40 1.50 1051 50.00 517.43 520.12	Upper	1086	26.00	518.00	519.23	0.73	0.73	2.60	2.60		3.54		7.35	9:90
1086 45.00 518.00 518.07 0.89 0.89 3.61 1086 84.00 518.00 520.04 1.12 0.73 54.2 1086 120.00 518.00 520.40 1.12 0.64 6.70 1086 222.00 518.00 521.75 1.15 0.54 6.70 1051 222.00 517.43 518.38 0.41 1.10 1.10 1051 220 517.43 518.39 0.62 0.41 1.10 1051 45.00 517.43 518.39 0.69 0.50 1.70 1051 45.00 517.43 518.30 0.69 0.04 1.50 1051 45.00 517.43 518.30 0.69 0.04 1.50 1051 45.00 517.43 518.30 0.69 0.04 1.50 1051 45.00 517.43 518.37 0.91 0.02 0.71 1051 520.01 518.37	Upper	1086	52.00	518.00	519.67	0.94	62.0	3.95	3,28	0.35	4.22	0.35	12.52	14.54
1086 64.00 518.00 520.06 1.12 0.73 5.42 1086 120.00 518.00 520.40 1.29 0.68 7.00 1086 120.00 518.00 527.76 1.15 0.54 6.47 1081 282.00 517.43 518.88 0.41 1.10 1.10 1051 52.00 517.43 518.28 0.41 1.10 1.10 1051 45.00 517.43 519.28 0.41 1.10 1.50 1051 45.00 517.43 519.28 0.44 1.10 1.50 1051 45.00 517.43 520.12 0.91 0.40 1.50 1051 282.00 517.43 520.12 0.14 0.12 0.25 1051 282.00 516.42 519.30 0.26 0.20 0.12 1051 46.00 516.42 519.30 0.26 0.20 0.12 1031 46.00 516.42	Upper	1086	45.00	518.00	519.57	0.89	0.83	3.61	3,33	0.20	4.05	0,20	11.15	13.05
1086 120.00 518.00 520.40 1.28 0.68 7.00 1086 282.00 518.00 521.75 1.15 0.54 8.47 1051 26.00 517.43 518.88 0.41 1.10 1.10 1051 45.00 517.43 519.89 0.52 0.41 1.69 1051 45.00 517.43 519.80 0.52 0.41 1.60 1051 45.00 517.43 519.80 0.69 0.40 1.50 1051 282.00 517.43 519.80 0.69 0.62 2.73 1051 282.00 517.43 519.80 0.69 0.62 2.73 1051 282.00 516.42 518.87 0.09 0.02 0.12 1031 45.00 516.42 519.30 0.76 0.03 0.12 1031 45.00 516.42 520.97 0.16 0.13 0.28 1031 45.00 516.42	Upper	1086	84.00	518.00	520.06	1.12	0.73	5.42	3.18	99.0	4.86	0.73	19.31	21.18
1086 282.00 518.00 521.75 1.15 0.54 6.47 1051 28.00 517.43 518.88 0.41 1.10 1.10 1051 52.00 517.43 518.38 0.52 0.41 1.10 1051 45.00 517.43 519.39 0.59 0.40 1.50 1051 45.00 517.43 520.12 0.91 0.62 4.27 1051 120.00 517.43 520.12 0.91 0.62 4.27 1051 282.00 517.43 520.12 0.91 0.62 4.27 1051 282.00 516.42 518.87 0.09 0.09 0.12 1031 84.00 516.42 519.80 0.76 0.02 0.02 1031 84.00 516.42 520.12 0.39 0.25 0.42 1031 45.00 516.42 520.12 0.29 0.09 0.05 1031 45.00 516.42	Upper	1086	120.00	518.00	520.40	1.29	89.0	7.00	2.90	0.81	5.42	1.80	28.16	31.16
1051 26.00 517.43 518.88 0.41 0.41 1.10 1051 52.00 517.43 518.38 0.62 0.41 1.16 1051 45.00 517.43 519.28 0.48 0.40 1.50 1051 46.00 517.43 519.80 0.69 0.50 2.73 1051 120.00 517.43 520.87 2.18 1.33 16.64 1051 282.00 516.42 518.87 0.09 0.09 0.12 1031 282.00 516.42 519.87 0.16 0.13 0.25 1031 45.00 516.42 519.87 0.16 0.13 0.25 1031 45.00 516.42 519.87 0.14 0.12 0.26 1031 45.00 516.42 519.87 0.14 0.12 0.26 1031 45.00 516.42 519.27 0.14 0.12 0.27 1031 282.00 516.42	Upper	1086	282.00	518.00	521.75	1.15	0.54	6.47	1.56	1.27	5,63	1.01	96.75	68.93
1051 26.00 517.43 518.88 0.41 0.41 1.10 1051 52.00 517.43 518.39 0.52 0.41 1.69 1051 45.00 517.43 518.20 0.68 0.40 1.50 1051 120.00 517.43 520.12 0.91 0.62 4.27 1051 282.00 517.43 520.87 2.18 1.33 16.64 1051 282.00 516.42 518.87 0.09 0.05 4.27 1031 282.00 516.42 518.87 0.09 0.02 0.02 1031 282.00 516.42 519.27 0.13 0.02 0.02 1031 46.00 516.42 519.27 0.04 0.02 0.02 1031 282.00 516.42 520.92 1.06 0.02 0.02 1031 282.00 516.42 520.90 1.06 0.04 0.02 1006 25.00 517.40														
1051 52.00 517.43 519.39 0.52 0.41 1.69 1051 45.00 517.43 519.28 0.48 0.40 1.50 1051 1051 26.00 517.43 519.80 0.69 0.50 2.73 1051 282.00 517.43 520.12 0.91 0.62 4.27 1051 282.00 516.42 518.87 0.09 0.09 0.012 1031 45.00 516.42 519.39 0.16 0.13 0.22 1031 45.00 516.42 519.80 0.16 0.13 0.22 1031 45.00 516.42 519.80 0.16 0.13 0.22 1031 45.00 516.42 519.80 0.26 0.20 0.67 1031 45.00 516.42 519.80 0.16 0.13 0.23 1031 120.00 516.42 520.80 1.06 0.20 0.67 1006 52.00	Upper	1051	26.00	517.43	518.88	0.41	0.41	1.10	1.10		2,69		9.67	11.59
1051 45.00 517.43 519.28 0.48 0.40 1.50 1051 84.00 517.43 519.80 0.69 0.50 273 1051 282.00 517.43 520.12 0.91 0.62 4.27 1051 282.00 516.42 518.87 0.09 0.09 0.012 1031 28.00 516.42 519.38 0.16 0.13 0.02 1031 45.00 516.42 519.37 0.14 0.12 0.26 1031 45.00 516.42 519.27 0.14 0.12 0.26 1031 84.00 516.42 520.20 0.26 0.26 0.26 1031 282.00 516.42 520.92 0.26 0.26 0.27 1031 282.00 516.42 520.92 0.26 0.26 0.26 1006 52.00 516.42 520.92 0.76 0.26 0.26 1006 52.00 517.40	Upper	1051	52.00	517.43	519.39	0.52	0.41	1.69	1.29	0.45	3.27	0.42	16.70	15.90
1051 84,00 517,43 519,80 0.69 0.69 0.50 2.73 1051 120,00 517,43 520,12 0.91 0.62 4.27 1051 282,00 517,43 520,687 2.18 1.33 16.64 1031 28,00 516,42 518,87 0.09 0.09 0.12 1031 45,00 516,42 519,29 0.14 0.13 0.32 1031 45,00 516,42 519,27 0.14 0.13 0.32 1031 45,00 516,42 519,27 0.14 0.13 0.32 1031 45,00 516,42 519,27 0.14 0.12 0.28 1031 282,00 516,42 519,29 0.26 0.20 0.28 1006 52,00 517,40 518,65 0.71 0.71 2.46 1006 45,00 517,40 519,48 0.06 0.59 0.58 1006 282,00	Upper	1051	45.00	517.43	519.28	0.48	0.40	1.50	1.21	0.38	3.11	0.35	14.93	14.93
1051 120,00 517,43 520,12 0.91 0.62 4.27 1051 282,00 517,43 520,87 2.18 1.33 16.64 1031 28,00 516,42 518,87 0.09 0.09 0.012 1031 45,00 516,42 519,39 0.14 0.13 0.32 1031 45,00 516,42 519,27 0.14 0.13 0.05 1031 45,00 516,42 519,27 0.14 0.12 0.26 1031 45,00 516,42 519,27 0.14 0.12 0.26 1031 282,00 516,42 520,80 1.06 0.26 0.05 1036 26,00 517,40 519,80 0.26 0.26 0.05 1006 52,00 517,40 519,49 1.00 0.56 3.24 1006 45,00 517,40 519,49 1.00 0.56 4.62 1006 282,00 517,40	Upper	1051	84.00	517.43	519.80	0.69	0:50	2.73	1.75	0.70	3.95	0.64	23.89	19.31
1051 282.00 517.43 520.87 2.18 1.33 16.64 1031 26.00 516.42 518.87 0.09 0.09 0.12 1031 45.00 516.42 519.39 0.16 0.13 0.32 1031 46.00 516.42 519.87 0.04 0.05 0.02 1031 46.00 516.42 519.80 0.26 0.20 0.05 1031 46.00 516.42 520.12 0.39 0.25 1.24 1031 120.00 516.42 520.90 1.06 0.25 1.24 1034 282.00 517.40 518.65 0.71 0.71 2.46 1006 52.00 517.40 519.49 1.00 0.55 3.24 1006 52.00 517.40 519.49 1.00 0.56 3.24 1006 282.00 517.40 520.80 0.56 0.57 3.24 1006 282.00 516.99	Upper	1051	120.00	517.43	520.12	0.91	0.62	4.27	2.42	0.92	4.67	0.76	30.51	22.19
1031 26.00 516.42 518.87 0.09 0.09 0.02 0.12 1031 52.00 516.42 519.39 0.16 0.13 0.25 1031 45.00 516.42 519.27 0.14 0.12 0.26 1031 45.00 516.42 519.80 0.26 0.25 0.67 1031 120.00 516.42 520.12 0.39 0.25 0.67 1031 120.00 516.42 520.90 1.06 0.26 0.67 1031 282.00 516.42 520.90 1.06 0.46 5.80 1006 28.00 517.40 518.65 0.71 0.71 2.46 1006 28.00 517.40 519.49 1.00 0.56 3.24 1006 282.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 520.80 1.35 0.65 8.06 566 52.00	Upper	1051	282.00	517.43	520.87	2.18	1.33	16.64	7.49	1.77	7.62	1.30	49.93	29.67
1031 26.00 516.42 518.87 0.09 0.09 0.12 1031 62.00 516.42 519.39 0.16 0.13 0.32 1031 46.00 516.42 519.27 0.14 0.12 0.26 1031 84.00 516.42 519.80 0.26 0.20 0.67 1031 120.00 516.42 520.12 0.39 0.26 0.67 1031 282.00 516.42 520.90 1.06 0.46 5.80 1006 26.00 517.40 518.65 0.71 0.71 2.46 1006 52.00 517.40 519.11 0.86 0.58 3.49 1006 84.00 517.40 519.49 1.00 0.51 5.49 1006 282.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 519.82 1.36 0.52 8.06 966 28.00 516.39														
1031 52.00 516.42 519.39 0.16 0.13 0.32 1031 45.00 516.42 519.27 0.14 0.12 0.26 1031 84.00 516.42 519.27 0.26 0.20 0.67 1031 120.00 516.42 520.12 0.39 0.25 1.24 1031 282.00 516.42 520.90 1.06 0.46 5.80 1006 28.00 517.40 518.65 0.71 0.71 2.46 1006 45.00 517.40 519.11 0.86 0.58 3.49 1006 45.00 517.40 519.49 1.00 0.56 4.62 1006 84.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 519.82 1.36 0.49 1.45 566 28.00 516.89	Upper	1031	26.00	516.42	518.87	60'0	60:0	0.12	0.12		1.34		19.37	13.78
1031 45.00 518.42 519.27 0.14 0.12 0.26 1031 84.00 516.42 519.80 0.26 0.20 0.67 1031 120.00 516.42 520.12 0.39 0.25 1.24 1031 282.00 516.42 520.90 1.06 0.46 5.80 1006 26.00 517.40 518.65 0.71 0.71 2.46 1006 52.00 517.40 519.11 0.86 0.58 3.49 1006 45.00 517.40 519.49 1.00 0.56 4.62 1006 84.00 517.40 519.49 1.00 0.50 4.62 1006 120.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 519.82 1.10 0.51 5.49 966 26.00 516.99 518.89 0.58 0.52 8.06 966 26.00 516.99	Upper	1031	52.00	516.42	519.39	0.16	0.13	0.32	0.25	0.21	1.94	0.28	27.92	18.29
1031 84.00 516.42 519.80 0.26 0.26 0.26 0.67 1031 120.00 516.42 520.12 0.39 0.25 1.24 1031 282.00 516.42 520.90 1.06 0.46 5.80 1006 28.00 517.40 518.65 0.71 0.71 2.46 1006 52.00 517.40 519.11 0.86 0.58 3.49 1006 45.00 517.40 519.49 1.00 0.57 3.21 1006 84.00 517.40 519.49 1.00 0.50 4.62 1006 120.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 520.80 1.35 0.62 8.06 966 28.00 516.59 518.37 0.49 0.49 1.42 966 45.00 516.59 518.77 0.55 0.55 1.79 966 120.00	Upper	1031	45.00	516.42	519.27	0.14	0.12	0.26	0.21	0.17	1.80	0.23	25.84	17.69
1031 120.00 516.42 520.12 0.39 0.25 1.24 1031 282.00 516.42 520.90 1.06 0.46 5.80 1006 28.00 517.40 518.65 0.71 0.71 2.46 1006 52.00 517.40 519.11 0.86 0.58 3.49 1006 45.00 517.40 519.49 1.00 0.57 3.21 1006 84.00 517.40 519.49 1.00 0.50 4.62 1006 120.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 520.80 1.35 0.62 8.06 966 282.00 516.39 518.37 0.49 0.49 1.42 966 52.00 516.39 518.37 0.49 0.55 1.79 966 45.00 516.39 518.31 0.65 0.55 1.79 966 120.00 516.59	Upper	1031	84.00	516.42	519.80	0.26	0.20	0.67	0.47	0.37	2.55	0.47	35.91	20.46
1031 282.00 516.42 520.90 1.06 0.46 5.80 1006 28.00 517.40 518.65 0.71 0.71 2.46 1006 52.00 517.40 519.11 0.86 0.53 3.49 1006 45.00 517.40 519.49 1.00 0.67 3.21 1006 84.00 517.40 519.82 1.10 0.50 4.62 1006 120.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 520.80 1.35 0.62 8.06 966 282.00 517.40 520.80 1.35 0.49 1.42 966 52.00 516.39 518.37 0.49 0.49 1.42 966 45.00 516.39 518.37 0.65 0.55 1.79 966 84.00 516.99 518.31 0.65 0.49 1.79 966 120.00 516.99	Upper	1031	120.00	516.42	520.12	0.39	0.25	1.24	0.71	0.41	3.17	0.56	43.00	25.52
1006 26.00 517.40 518.65 0.71 0.71 2.46 1006 52.00 517.40 519.11 0.86 0.58 3.49 1006 45.00 517.40 519.00 0.82 0.67 3.21 1006 84.00 517.40 519.49 1.00 0.50 4.62 1006 120.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 520.80 1.35 0.62 8.06 966 28.00 516.39 518.37 0.49 0.49 1.42 966 52.00 516.39 518.89 0.58 0.58 1.79 966 45.00 516.39 518.77 0.65 0.65 1.79 966 84.00 516.99 519.86 0.75 2.60 966 120.00 516.99 519.86 0.75 2.60	Upper	1031	282.00	516.42	520.90	1.06	0.46	5.80	1.80	0.78	5.46	0.91	72.78	50.87
1006 26.00 517.40 518.65 0.71 0.71 2.46 1006 52.00 517.40 519.11 0.86 0.58 3.49 1006 45.00 517.40 519.00 0.82 0.67 3.21 1006 84.00 517.40 519.82 1.10 0.50 4.62 1006 120.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 520.80 1.35 0.62 8.06 966 26.00 516.39 518.37 0.49 0.49 1.42 966 52.00 516.39 518.83 0.58 0.58 1.34 966 45.00 516.99 518.77 0.65 0.55 1.79 966 84.00 516.99 519.81 0.65 0.55 1.79 966 120.00 516.99 519.81 0.75 0.45 0.75 966 120.00 516.99 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>														
1006 52.00 517.40 519.11 0.86 0.58 3.49 1006 45.00 517.40 519.00 0.82 0.67 3.21 1006 84.00 517.40 519.49 1.00 0.50 4.62 1006 120.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 520.80 1.35 0.62 8.06 966 26.00 516.39 518.37 0.49 0.49 1.42 966 52.00 516.39 518.37 0.65 0.58 1.34 966 45.00 516.39 518.37 0.65 0.55 1.79 966 84.00 516.39 518.37 0.65 0.55 1.79 966 120.00 516.99 519.86 0.75 0.45 1.79 966 120.00 516.99 519.86 0.75 0.42 2.60 966 120.00 516.99 <t< td=""><td>Upper</td><td>1006</td><td>26.00</td><td>517.40</td><td>518.65</td><td>0.71</td><td>0.71</td><td>2.46</td><td>2.46</td><td></td><td>3.48</td><td></td><td>7.47</td><td>10.00</td></t<>	Upper	1006	26.00	517.40	518.65	0.71	0.71	2.46	2.46		3.48		7.47	10.00
1006 45.00 517.40 519.00 0.82 0.67 3.21 1006 84.00 517.40 519.49 1.00 0.50 4.62 1006 120.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 520.80 1.35 0.62 8.06 966 26.00 516.39 518.37 0.49 0.49 1.42 966 45.00 516.39 518.37 0.58 0.58 1.94 966 84.00 516.39 518.77 0.65 0.55 1.79 966 120.00 516.99 518.37 0.65 0.58 1.79 966 120.00 516.99 519.86 0.75 0.42 2.60 966 120.00 516.99 519.86 0.79 0.42 2.60	Upper	1006	52.00	517.40	519.11	0.86	0.58	3.49	2.26	0.46	4.06	0.31	13.40	18.88
1006 84,00 517,40 519,49 1.00 0.50 4.62 1006 120,00 517,40 519,82 1.10 0.51 5.49 1006 282,00 517,40 520.80 1.35 0.62 8.06 966 26,00 516,99 518.37 0.49 0.49 1.42 966 52,00 516,99 518.89 0.58 0.58 1.34 966 45,00 516,99 518,77 0.65 0.55 1.79 966 84,00 516,99 518,31 0.68 0.42 2.60 966 120,00 516,99 519,66 0.79 0.40 339	Upper	1006	45.00	517.40	519.00	0.82	0.67	3.21	2.58	0.25	3.91	0.24	11.66	15.09
1006 120.00 517.40 519.82 1.10 0.51 5.49 1006 282.00 517.40 520.80 1.35 0.62 8.06 966 26.00 516.99 518.37 0.49 1.42 966 52.00 516.99 518.89 0.58 0.58 1.34 966 45.00 516.99 518.77 0.65 0.55 1.79 966 84.00 516.99 519.31 0.68 0.42 2.60 966 120.00 516.99 519.66 0.79 0.40 3.39	Upper	1006	84.00	517.40	519.49	1.00	0.50	4.62	1.81	0.85	4.62	0.65	23.25	32.95
1006 282.00 517.40 520.80 1.36 0.62 8.06 966 26.00 516.99 518.37 0.49 0.49 1.42 966 52.00 516.99 518.89 0.58 0.58 1.34 966 45.00 516.99 518.77 0.65 0.55 1.79 966 84.00 516.99 519.31 0.68 0.42 2.60 966 120.00 516.99 519.66 0.79 0.40 3.39	Upper	1006	120.00	517.40	519.82	1.10	0.51	5.49	1.69	1.04	5.00	0.85	36.31	45.29
966 28.00 516.99 518.37 0.49 0.49 1.42 966 52.00 516.99 518.89 0.58 0.58 1.94 966 45.00 516.99 518.77 0.65 0.55 1.79 966 84.00 516.99 519.31 0.68 0.42 2.60 966 120.00 516.99 519.66 0.79 0.40 3.39	Upper	1006	282.00	517.40	520.80	1.35	0.62	8.06	1.81	1.11	5.97	1.37	97.34	79.09
966 26.00 516.99 518.37 0.49 0.49 1.42 966 52.00 516.99 518.89 0.58 0.58 1.94 966 45.00 516.99 518.77 0.65 0.55 1.79 966 84.00 516.99 519.31 0.68 0.42 2.60 966 120.00 516.99 519.66 0.79 0.40 3.39														
966 52.00 516.99 518.89 0.58 0.58 1.94 966 45.00 516.99 518.77 0.65 1.79 966 84.00 516.99 519.31 0.68 0.42 2.60 966 120.00 516.99 519.66 0.79 0.40 3.39	Upper	996	26.00	516.99	518.37	0.49	0.49	1.42	1.42		2:92		8.91	11.07
966 45.00 516.99 518.77 0.55 0.55 1.79 966 84.00 516.99 519.31 0.68 0.42 2.60 966 120.00 516.99 519.66 0.79 0.40 3.39	Upper	996	52.00	516.99	518.89	0.58	0.58	1.94	1.94		3.35		15.53	14.35
966 84.00 516.99 519.31 0.68 0.42 2.60 966 120.00 516.99 519.66 0.79 0.40 3.39	Upper	996	45.00	516.99	518.77	0,55	0.55	1.79	1.79		3.24		13.90	13.66
966 120,00 516,99 519,66 0.79 0.40 3.39	Upper	996	84.00	516.99	519.31	0.68	0.42	2.60	1.51	0.37	3.81	0.38	23.64	26.54
	Upper	996	120.00	516.99	519.66	0.79	0.40	3.39	1.38	09:0	4.26	0.61	34.97	39.28

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Chickeg 10 Chi	Reach	River Sta	O Total	Min Co	W.S. Fley	Shear Chan	Shoor Total	10,000		2 11 21				
948 282.00 516.39 550.90 -1.19 Code 0.12 1.19 (40.8)			(cfs)	##	₩	(lb/ea ft)	(h/ca 4)	Line of Mall	rower rotal	Vei Leit	Vel Chri	Vel Right	Flow Area	Top Width
Secondary Seco	Upper	996	282 OU	548.00	520 60	(Incort It)	(in beam)	(ST/CI)		(ff/s)	(tt/s)	(£/s)	(sq ft)	£
946 5200 516.97 518.04 0.08 0.09 0.01 0.17 0.17 0.18 0.19 0.11 0.19 0.11 0.10 0.11 0.10 0.11 0.10 0.11 0.10 0.11 0.10 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.10 0.11	0240	8	Z0Z.UU	88.010	970.60	1.18	0.54	6.60	1.74	0.84	5.58	1.17	87.87	72.35
946 \$20.0 \$15.87 \$15.82 \$10.0 \$10.0 \$10.1 \$10.1 \$13.7 \$15.90 \$10.10	Upper	948	26.00	515.97	518 40	000	000	0						
5.60 45.00 51.52 m. 51	liner	978	2000	10.00	2 0	60.0	60.03	0.12			1.37		19.01	13.66
9.95 9.00 9.15 0.15 0.12 0.27 0.14 0.16 0.17 0.18 0.17 0.28 0.14 0.19 0.14 0.19 0.14 0.14 0.17 0.28 0.14 0.12 0.14 0.17 0.28 0.14 <th< td=""><td>Upper.</td><td>240</td><td>32.00</td><td>19.97</td><td>28.910</td><td>0.16</td><td>0.09</td><td>0.32</td><td>0.15</td><td></td><td>1.95</td><td>0.21</td><td>30.34</td><td>32.47</td></th<>	Upper.	240	32.00	19.97	28.910	0.16	0.09	0.32	0.15		1.95	0.21	30.34	32.47
948 64.00 916.57 917.50 0.24 0.12 0.04 0.07 0.02 0.04 0.01 0.02 0.01 0.02 0.04 0.04 0.02 0.04 0.04 0.02 0.04 0.04 0.02 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.04	10ddo	040	45.UC	78.616	518.80	0.15	0.08	0.27	0.14	0.16	1.82	0.17	26.81	27.60
818 12000 515.87 519.87 619.71 0.04 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.05 0.04 0.05 0.05 0.04 0.05 0.05 0.04 0.05	Opper	948	84.00	515.97	519.35	0.24	0.12	0.57	0.21	0.30	2.41	0.41	47.25	43.73
948 282.00 915.87 50.04 0.04 0.29 27.7 0.67 0.73 4.7 0.50 1.20.2 9289 28.00 516.00 516.00 516.00 1.30 1.35 6.27 0.27 0.50 0.50 9289 52.00 516.00 516.00 518.20 1.40 1.40 7.80 6.27 0.50 6.70 0.50 6.50 9.50 1.50 0.50 6.50 9.50 1.50 0.50 6.50 9.50 1.50 0.50 6.50 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.50 6.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 0.70 <td>Opper</td> <td>948</td> <td>120.00</td> <td>515,97</td> <td>519.71</td> <td>0.31</td> <td>0.15</td> <td>0.87</td> <td>0.28</td> <td>0.41</td> <td>2.83</td> <td>950</td> <td>84.18</td> <td>74 FA</td>	Opper	948	120.00	515,97	519.71	0.31	0.15	0.87	0.28	0.41	2.83	950	84.18	74 FA
996 2200 616.88 517.99 1.35 6.13	Upper	948	282.00	515.97	520.64	0.64	0.29	2.72	0.67	0.74	4 27	800	124.20	2 2 2
1 200 55.00 51.50 1.53 6.21 6.21 4.67 4.67 6.56 9.50 1 200 45.00 516.62 1.52 1.55 1.55 6.57 6.57 6.56 9.50 1 200 46.00 516.85 516.42 1.56 1.56 7.56 6.57 6.57 9.50 1 200 46.00 516.85 516.85 1.67 1.67 1.09 4.02 1.59 0.06 1.51 9.50 1 200 516.80 516.85 516.80 2.22 1.03 1.72 4.02 1.05 1.72 0.06 5.73 0.07 1.02 1.72 0.06 5.73 0.05 1.72 0.06 0.06 1.72 0.06 0.06 0.07 1.03 1.72 0.06 0.06 0.07 1.06 0.07 1.06 0.07 0.06 0.07 0.06 0.07 0.07 0.06 0.07 0.07 0.06 0.07 0.07 0.07 <td></td> <td>B</td> <td>24.40</td> <td>79.10</td>												B	24.40	79.10
900 52.00 516.86 516.42 1.56 6.13	Upper	926	26.00	516.95	517.99	1.33	1 33	R 24	10.0		157			
988 28.00 516.56 516.32 1.40 7.53 7.54 0.60 5.70 0.89 988 28.00 516.56 518.72 1.40 1.00 7.56 0.60 5.70 0.08 16.14 988 28.00 516.56 518.72 1.67 1.07 1.72 4.18 1.76 1.73 0.08 16.14 988 28.00 516.50 516.50 0.37 0.37 0.38 1.48 0.49 3.77 0.48 0.37 1.72 0.48 0.57 0.08 1.73 0.08 1.73 0.08 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 1.73 0.09 0.09 0.09	Upper	926	52.00	516.95	518.42	1.55	7.7	0 40	17.0		4.07		5.56	8.36
988 52.00 51.00 51.00 51.00 61.00 51.00 61.00 51.00 61.00 51.00 61.00 51.00 61.00 51.00 6	Joner	926	A5.00	518.05	140 00	2 4	3.5	27.0	8.13		5.25		9:30	11.75
7 30.00 136.24 136.74	- Labor	222	20.00	010.30	26.910	84.	1.48	7.55	7.55		5.10		8.83	11.01
7 32.20 516.80 518.12 1,73 0.87 10.60 4,72 10.6 61.30 0.78 25.64 9.50 228.20 516.80 516.80 0.58 1.03 1.78 1.78 0.78 1.59 1.01 68.37 1.01	addo	920	25.55 1.00	516.95	518.79	1.67	1.01	9.69	5.24	0.69	5.79	0.69	16.14	22.98
7 92.80 28.00 516.50 517.50 0.48 0.37 0.35 1.13 0.44 3.17 0.45 1.13 0.44 3.17 0.45 1.13 0.44 3.17 0.45 1.13 0.44 3.17 0.45 1.13 0.44 3.17 0.45 1.13 0.44 3.17 0.45 1.13 0.44 3.17 0.44 3.17 0.44 3.17 0.44 3.17 0.44 3.17 0.44 3.12 0.44 3.17 0.44 3.12 0.44 3.12 0.44 0.44 0.44 0.44 0.45 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.44 0.	Jpper	926	120.00	516.95	519.12	1.73	0.87	10.60	4.02	1.05	6.13	0.76	25 84	34.60
888 26.00 516.50 516.89 0.37 0.38 1.53 1.13 0.44 3.17 0.46 1.53 1.13 0.44 3.17 0.45 1.01 1.53 1.13 0.44 3.17 0.45 1.53 1.13 0.44 3.17 0.45 1.53 1.13 0.44 3.17 0.45 1.53 1.13 0.44 3.17 0.45 1.53 1.13 0.44 3.17 0.45 1.53 1.13 0.44 3.17 0.45 1.53 1.13 0.44 3.17 0.45 1.53 1.13 0.44 3.17 0.45 1.53 1.13 0.44 3.17 0.45 1.53 1.14 0.44 3.17 0.45 1.53 1.14 0.49 0.55 0.44 3.17 0.49 0.55 0.44 3.17 0.49 0.55 0.44 0.40 0.40 0.40 0.40 0.41 0.40 0.40 0.41 0.40 0.41 0.40 0.44	Jpper	926	282.00	516.95	519.99	2.28	1.03	17.28	4.18	1.76	7.58	1.30	69.37	66.47
7 888 26,00 515,50 516,50 516,50 516,50 516,50 516,50 516,50 516,50 517,50 0.48 0.37 1,53 1,13 0.44 3,17 0.45 17,33 1 888 45,00 516,50 517,50 0.48 0.37 1,13 0.44 3,17 0.45 17,33 1 888 45,00 516,50 517,50 0.78 0.78 0.49 1,25 0.48 0.79 0.48 1,25 0.48 0.45 0.49 <td></td>														
7 889 52.00 515.50 517.50 0.48 0.38 1.53 1.13 0.44 3.17 0.46 1.73 889 45.00 515.50 517.38 0.44 0.37 1.35 1.06 0.37 3.01 0.68 15.50 1 889 120.00 515.50 517.38 0.44 0.45 0.49 1.35 0.06 0.37 1.06 0.37 3.01 0.88 15.50 1.06 0.78 0.07 0.49 0.48 0.35 0.06 0.08 0.44 0.37 0.09 0.09 0.44 0.37 0.09 0.09 0.09 0.09 0.09 0.01 0.01 0.01 0.04 0.09 0.09 0.01 0.01 0.01 0.01 0.01 0.01 0.09 0.02 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01	Joper	888	26.00	515.50	516.99	0.37	0.37	0.95	0.95		2.57		10 13	11 90
(450) 515.50 517.38 0.45 0.37 1.36 1.06 0.37 3.01 0.38 1.55 888 4500 516.50 517.33 0.683 0.44 2.39 1.46 0.66 3.79 0.68 25.35 888 120.00 516.50 519.42 1.04 0.04 5.89 1.07 0.08 26.20 0.08 0.08 0.08 25.20 0.08	Jpper	888	52.00	515.50	517.50	0.48	0.38	1.53	1.13	0.44	3.17	0.45	17.33	18.46
1 888 84.00 515.50 517.39 0.68 0.44 2.39 1.46 0.68 3.79 0.68 5.55 1 889 220.00 515.50 518.30 0.79 0.37 3.48 1.55 0.49 4.39 0.68 5.55 1 889 220.00 518.50 519.42 0.79 0.37 3.48 1.55 0.49 4.39 0.68 5.55 1 883 220.00 518.50 518.50 0.18 0.08 0.01 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.11 0.12 0.12 0.12 0.18 0.89 3.50 1.18 1.08 0.50 0.11 0.11 0.11 0.11 0.12 0.11 0.11 0.12 0.18 0.28 0.28 0.18 0.28 0.50 0.18 0.50 0.11 0.11 0.12 0.18 0.28 0.28 0.18 0.18 0.18 0.28 0.28 0.18 0.1	pper	888	45.00	515.50	517.38	0.45	0.37	1.35	1.06	0.37	304	82.0	, th	4 A
F BBB 120.00 515.50 518.20 0.78 0.37 3.48 1.25 0.49 4.39 0.26 3.50 0.50 3.50 0.50 <	pper	888	84.00	515.50	517.93	0.63	0.44	2.39	1.46	0.66	3 79	0.68	25.27 75.37	26.00
7 888 282.00 515.50 519.42 1.04 6.62 1.07 1.06 6.40 1.04 1.07 1.06 6.40 1.04 1.04 1.04 1.05 1.04 1.04 1.05 1.04 1.05 1.04 1.05 1.04 1.05 1.04 1.05 1.04 1.05 1.04 1.05 1.04 1.05 1.04 1.05 1.04 1.05 1.04 1.05 1.04 1.05 1.05 1.04 1.05 <	ррег	888	120.00	515.50	518.30	0.79	0.37	3.48	1.25	0.49	4 39	0.82	35.20	35.05 35.05
863 26.00 514.50 516.89 0.08 0.01 0.11 0.11 1.31 1.31 1.32 863 \$2.00 514.50 517.80 0.04 0.01 0.01 0.13 0.13 0.22 28.65 863 \$2.00 514.50 517.80 0.14 0.11 0.24 0.18 0.19 0.24 0.18 0.19 0.18 0.19 0.24 0.18 0.19 0.18 0.19 0.18 0.19 0.18 0.19 0.24 0.18 0.19 0.18 0.19 0.24 0.18 0.19 0.18 0.19 0.19 0.18 0.19 0.18 0.18 0.19 0.18	pper	888	282.00	515.50	519.42	4.5	0.40	5.62	1.07	1.08	5.40	1 04	105.70	00.00
883 26.00 514.50 516.89 0.08 0.01 0.11 0.11 0.11 0.11 0.12 1.983 883 52.00 514.50 517.50 0.16 0.12 0.20 0.21 0.22 28.65 883 52.00 514.50 517.34 0.14 0.14 0.11 0.11 0.12 0.22 1.91 0.22 28.65 883 84.00 514.50 517.94 0.24 0.16 0.03 0.24 0.26 0.18 0.24 0.16 0.03 0.24 0.16 0.03 0.24 0.07 0.18 0.24 0.07 0.28 0.26 0.28 0.29 0.24 0.16 0.00 0.38 0.24 0.16 0.00 0.39 0.39 0.34 0.16 0.00 0.38 0.39 0.39 0.37 0.37 0.37 0.38 0.39 0.34 0.14 0.11 0.11 0.11 0.11 0.31 0.39 0.34														20.00
863 52.00 514.50 517.50 0.16 0.12 0.30 0.21 0.22 1.91 0.22 2.863 863 45.00 514.50 517.36 0.14 0.11 0.24 0.18 0.18 1.77 0.18 2.85 863 12.00 514.50 517.34 0.24 0.16 0.03 2.46 0.37 2.90 863 12.00 514.50 517.34 0.24 0.16 0.03 2.46 0.37 2.90 863 12.00 514.50 516.30 0.24 0.16 0.38 0.28 0.29 0.29 0.76 118.77 863 2.80 2.80 0.60 0.38 0.24 0.76 0.89 0.76 0.76 0.71 118.77 863 2.80 515.00 517.41 0.79 0.78 2.88 0.89 2.44 0.71 118.77 822 52.00 515.50 517.74 0.78 0.78	pper	863	26.00	514.50	516.99	0.08	0.08	0.11	0.11		134		40.03	10.04
863 45.00 514.50 517.38 0.14 0.11 0.24 0.16	pper	863	52.00	514.50	517.50	0.16	0.12	0.30	0.21	0.0	19	0.00	28.65	20.04
863 84,00 514,50 517,94 0.24 0.16 0.60 0.34 0.38 2.46 0.57 30,50 863 120,00 514,50 518,20 618,32 0.34 0.16 0.03 2.47 0.50 513,80 863 280 280 2.69 0.60 0.38 0.39 2.97 0.50 513,80 832 280 2.60 616,50 516,71 0.79 0.79 2.88 0.60 0.82 4.28 0.71 118,77 832 52.00 516,50 516,71 0.73 0.78 2.88 0.60 0.88 0.71 1.18 832 45.00 516,50 517,13 0.78 0.28 2.41 0.71 4.40 0.71 1.88 832 84.00 516,50 517,82 1.42 0.89 7.97 3.86 0.71 1.18 832 120,00 516,50 517,82 1.42 0.89 7.97 <td>ррег</td> <td>863</td> <td>45.00</td> <td>514.50</td> <td>517.38</td> <td>0.14</td> <td>0.11</td> <td>0.24</td> <td>0.18</td> <td>0 18</td> <td>121</td> <td>0.48</td> <td>20.02</td> <td>40.02</td>	ррег	863	45.00	514.50	517.38	0.14	0.11	0.24	0.18	0 18	121	0.48	20.02	40.02
863 120.00 514.50 518.32 0.34 0.16 1.00 0.38 0.29 2.97 0.50 51.38 863 282.00 514.50 519.40 0.63 0.25 2.68 0.69 0.69 0.70 0.71	pper	863	84.00	514.50	517.94	0.24	0.16	09:0	0.34	0.38	2.4E	0.00	20.02	90.00
863 282.00 514.50 519.40 0.65 0.25 2.68 0.60 0.82 4.28 0.70 118.77 832 26.00 515.50 516.71 0.79 0.79 2.88 2.88 3.66 0.71 11.08 832 45.00 515.50 517.13 1.03 0.86 4.54 3.74 0.31 4.40 0.31 11.08 832 45.00 515.50 517.04 0.98 0.92 4.10 3.87 0.14 4.21 0.14 10.71 832 45.00 515.50 517.04 0.98 0.92 4.10 3.87 0.14 4.21 0.14 10.71 832 120.00 515.50 517.64 1.23 0.78 5.29 0.97 5.63 0.97 27.15 832 120.00 515.50 517.82 1.42 0.74 1.24 0.74 1.24 0.74 1.24 0.74 1.25 0.80 1.28 3	pper	863	120.00	514.50	518.32	0.34	0.16	1.00	0.38	0.39	266	20.0	20.00	07.07
832 26.00 515.50 516.71 0.79 0.79 2.88 2.88 2.88 3.66 7.11 832 26.00 515.50 517.13 1.03 0.79 2.88 2.88 3.74 0.31 4.40 0.31 11.98 832 45.00 515.50 517.44 0.98 0.92 4.10 3.74 0.14 4.21 0.14 11.98 832 84.00 515.50 517.82 1.42 0.80 7.97 3.55 0.97 5.63 0.71 11.88 832 282.00 515.50 517.82 1.42 0.80 7.97 3.55 0.97 5.63 0.71 11.88 832 282.00 515.02 516.48 0.40 0.40 1.06 7.97 3.47 1.24 7.43 1.50 69.65 806 28.00 52.00 516.98 0.40 0.40 1.06 0.74 1.24 1.77 1.77 806	pper	863	282.00	514.50	519.40	0.63	0.25	268	US C	CBO	0C F	200	2	50.03
832 26.00 515.50 516.71 0.79 0.79 2.88 2.88 2.88 3.66 7.11 832 52.00 515.50 517.13 1.03 0.86 4.54 3.74 0.31 4.40 0.31 11.98 832 45.00 515.50 517.04 0.98 0.92 4.10 3.87 0.14 4.21 0.14 10.71 832 45.00 515.50 517.60 1.23 0.78 6.23 3.47 0.72 5.08 0.72 18.80 832 120.00 515.50 517.82 1.42 0.80 7.97 3.55 0.97 5.09 0.72 18.80 832 286.00 515.02 518.72 2.13 0.86 1.58 3.47 1.24 7.43 1.50 69.65 806 28.00 52.00 515.02 516.48 0.40 0.40 1.06 1.06 0.97 2.66 0.74 17.72 3.71 0.									800	70.07	4.20	0.70	118.77	81.84
832 52.00 515.50 517.13 1.03 0.86 4.54 3.74 0.31 4.40 0.31 7.11 832 45.00 516.50 517.04 0.98 0.92 4.10 3.87 0.14 4.21 0.14 10.71 832 84.00 516.50 517.62 1.23 0.78 6.23 3.47 0.72 5.06 0.72 18.80 832 120.00 516.50 517.82 1.42 0.80 7.97 3.55 0.97 5.03 0.97 18.80 832 282.00 516.50 518.72 2.13 0.86 15.86 3.47 1.24 7.43 1.50 8.96 806 28.00 516.03 516.48 0.40 0.40 1.06 1.06 0.97 1.24 1.50 8.78 806 52.00 516.03 516.98 0.53 0.33 1.76 0.97 3.16 0.97 4.17 806 52.00 <td></td> <td>832</td> <td>26.00</td> <td>515.50</td> <td>516.71</td> <td>0.79</td> <td>0.79</td> <td>2.88</td> <td>2.88</td> <td></td> <td>88</td> <td></td> <td>7.44</td> <td>25.0</td>		832	26.00	515.50	516.71	0.79	0.79	2.88	2.88		88		7.44	25.0
832 45.00 515.50 517.04 0.98 0.92 4.10 3.87 0.14 4.21 0.13 11.38 832 84.00 515.50 517.50 1.23 0.78 6.23 3.47 0.72 5.06 0.72 18.80 832 120.00 515.50 517.82 1.42 0.80 7.97 3.55 0.97 5.63 0.97 1.80 832 282.00 515.50 518.72 2.13 0.86 1.58 3.47 1.24 7.43 1.50 69.65 806 28.00 515.02 516.48 0.40 0.40 1.06 1.06 2.66 9.78 9.78 806 52.00 515.02 516.95 0.53 0.33 1.76 0.97 0.94 17.72 806 45.00 515.02 517.34 0.50 0.33 1.56 0.97 0.97 0.91 1.53 806 45.00 515.02 517.74 0.75		832	92.00	515.50	517.13	1.03	0.86	4 54	17.6	200	2 2	200	11.7	17.6
832 84.00 515.50 517.50 1.23 0.78 6.23 3.47 0.12 4.21 10.71 832 120.00 515.50 517.82 1.42 0.80 7.97 3.55 0.97 5.63 0.97 27.15 832 282.00 515.50 518.72 2.13 0.86 15.86 3.47 1.24 7.43 1.50 68.65 806 26.00 515.02 516.48 0.40 0.40 1.06 1.06 1.06 2.66 9.78 806 45.00 515.02 516.84 0.53 0.33 1.76 0.97 0.44 17.72 806 45.00 515.02 515.03 517.74 0.75 0.44 17.72 29.28 806 120.00 515.02 517.74 0.75 0.44 3.76 0.71 3.76 0.72 29.28		832	45.00	515.50	517.04	0.98	260	4 10	3.87	200	2 2	0.31	28.1.	14.68
832 120.00 515.50 517.82 1.42 0.86 7.97 3.56 0.97 5.63 0.97 18.0 832 282.00 515.50 518.72 2.13 0.86 15.86 3.47 1.24 7.43 1.50 68.65 806 28.00 515.02 516.48 0.40 0.40 1.06 1.06 0.97 2.66 9.78 806 45.00 515.02 516.84 0.63 0.33 1.76 0.97 0.37 3.16 0.71 3.26 806 45.00 515.02 515.84 0.63 0.33 1.56 0.97 0.37 3.16 0.71 3.26 806 45.00 515.02 517.24 0.74 3.76 0.71 3.76 0.72 29.28 806 120.00 515.02 517.74 0.75 0.74 3.76 0.72 29.28		832	84.00	515,50	517.50	1 23	87.0	6.73	2 47	5 0	13.4	7 0	1.701	12.74
832 282 00 515.50 518.72 2.13 0.36 15.86 3.47 1.24 7.43 1.50 68.65 806 28.00 515.02 516.48 0.40 0.40 0.40 1.06 1.06 1.06 2.66 9.78 9.78 806 45.00 515.02 516.84 0.63 0.33 1.76 0.97 0.44 3.31 0.44 17.72 806 45.00 515.02 515.02 517.39 0.63 0.37 2.56 0.71 3.76 0.72 29.28 806 120.00 515.02 517.74 0.75 0.44 3.76 0.77 3.76 0.72 29.28 806 120.00 515.02 517.74 0.75 0.44 3.76 0.71 3.76 0.72 29.28		832	120,00	515.50	517.82	1 42	080	70.7	3000	27.0	8.0	0.72	18.80	22.41
806 26.00 515.02 516.48 0.40 0.40 1.06 1.06 1.24 7.43 1.50 69.65 806 26.00 515.02 516.48 0.40 0.40 1.06 1.06 2.66 9.78 806 45.00 515.02 516.84 0.50 0.33 1.76 0.97 0.94 3.31 0.44 17.72 806 85.00 515.02 517.39 0.63 0.37 2.36 1.06 0.71 3.76 0.72 29.28 806 120.00 515.02 517.74 0.75 0.44 3.76 0.77 29.28		832	282 00	515.50	518 72	2 43	90 0	200	3 1	76.0	20.03)Bio	27.15	29.20
806 26.00 515.02 516.48 0.40 0.40 1.06 1.06 1.06 2.68 9.78 806 52.00 515.02 516.96 0.63 0.33 1.76 0.97 0.44 3.31 0.44 17.72 806 45.00 515.02 516.84 0.60 0.33 1.58 0.97 0.37 3.16 0.37 15.38 806 44.00 515.02 517.73 0.63 1.06 0.71 3.76 0.72 29.28 806 120.00 515.02 517.74 0.75 0.44 3.76 0.71 3.76 0.72 29.28						5	3	00.00	3.47	1.24	7.43	1.50	69.65	69.64
806 52.00 515.02 516.95 0.53 0.33 1.76 0.97 0.44 2.70 0.44 17.72 806 45.00 515.02 516.84 0.50 0.33 1.58 0.97 0.37 3.16 0.37 15.38 806 84.00 515.02 517.74 0.75 0.44 3.76 0.72 29.28 806 120.00 515.02 517.74 0.75 0.44 3.76 0.72 29.28		808	26.00	515.02	516.48	0.40	0.40	1.06	9		28.0		07.0	
806 45.00 515.02 516.84 0.50 0.33 1.58 0.97 0.37 3.16 0.37 15.38 806 84.00 515.02 517.39 0.63 0.37 2.35 1.06 0.71 3.76 0.72 29.28 806 120.00 515.02 517.74 0.75 0.44 3.20 1.06 0.71 3.76 0.72 29.28		806	52.00	515.02	516.95	0.53	0.33	1.76	26.0	0.44	3 34	77.0	47.70	11.07
806 84.00 515.02 517.39 0.63 0.37 2.36 1.06 0.71 3.76 0.72 29.28 806 120.00 515.02 517.74 0.75 0.44 3.70 1.20 0.01 3.76 0.02 29.28		908	45.00	515.02	516.84	0.50	0.33	1.58	79.0	0.37	0.00	1 0	11.12	77.77
806 120.00 515.02 517.74 0.75 0.444 3.30 1.30 0.30 0.30 0.30 0.30 0.30 0.30		808	84.00	515.02	517.39	0.63	0.37	2.35	106	0.74	3.70	0.37	00.00	20.30
		806	120.00	515.02	517.74	0.75	0.44	222	7 20	000	2 5	21.0	23.20	3.63

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Reach	River Sta O Total Min Ob E 1/4/8 Elect Obser Obes	LefoT O	Min Ch E	14/ C Elea:	Chon Chon	Total Target							
		177	3 3	VV.C. EIEV	Green Crear	Orical Total	Lower Chan	Power lotal	Vei Left	Vel Chri	Vel Right	Flow Area	Top Width
		(cis)		(E)	(lb/sq ft)	(Ib/sq ft)	(lb/ff.s)	(lb/ft s)	(fVs)	(ft/s)	(fVs)	(sq ft)	€
Opper	808	282.00	515.02	518.54	1.61	0.75	10.60	2.77	1.20	6.58	1.40	75.99	58.98
11	700	0000		4									
opper.	781	26.00		516.48		0.08	0.11	0.11		1.32		19.75	13.91
Opper	781	52.00	514.00	516.95		0.11	0.32	0.20	0.21	1.96	0.21	28.40	23.07
jedd C	781	45.00		516.84	0.14	0.10	0.26	0.18	0.17	1.81	0.17	26.00	20.88
Пррег	781	84.00		517.39		0.14	0.63	0.29	0.34	2.50	0.39	40.42	32.33
Upper	781	120.00		517.73	0.35	0.18	1.05	0.41	0.47	3.01	0,53	52.88	39.77
Upper	781	282.00	514.00	518.54	0.87	0.40	4.33	1.20	0.94	4.96	0.91	93.14	62.37
Upper	756	26.00		516.26	0.64	0.64	2.12	2.12		3.32		7.83	10.28
Upper	756	52.00		516.55	1.19	1.00	5.56	4.65	0.23	4.67	0.23	11.21	14.44
Upper	756	45.00		516.50	1.02	76.0	4.38	4.17	0.09	4.29	60'0	10.50	12.63
Upper	756	84.00		516.82	1.66	0.98	9.59	5.04	0.69	5.77	690	16.31	23.70
Upper	756	120.00	514.98	517.15	1.72	0.82	10.51	3.73	06.0	6.11	10,1	26.39	37.13
Upper	756	282.00		518.07	1.99	0.86	14.11	3.03	1.41	7.10	1.56	79.72	78 15
Upper	729	26.00	514.57	516.02	0.41	0.16	1.10	0.41	0.08	2.69		9.97	31.84
Upper	729	52.00	514.57	516.49	0.36	0.18	76.0	0.27	0.59	2.71	0.36	33,63	55.51
Upper	729	45.00	514.57	516.40	0.35	0.16	0.92	0.25	0.53	2.64	0.31	28.67	53.83
Upper	729	84.00	514.57	516.81	0.42	0.23	1.28	0.37	0.79	3.05	0.51	52.48	61.48
Upper	729	120.00	514.57	517.11	0.47	0.27	1.54	0.45	0.94	3.30	0.60	72.09	68.31
Upper	729	282.00	514.57	517.99	99.0	0.37	2.73	0.74	1.37	4.17	0.86	143.12	93.73
Upper	713	26.00	513.56	516.04	0.08	0.03	0.11	40.0	0.05	1.31		20.63	41.84
Upper	713	52.00	513.56	516.48	0.14	90.06	0.25	0.07	0.31	1.80	0.19	43.52	56.38
Upper	713	45.00	513.56	516.40	0.12	0.05	0.21	90.0	0.26	1.67	0.16	38.72	54.61
Upper	713	84.00	513.56	516.79	0.22	0.10	0.49	0.14	0.48	2.28	0.31	61.94	62.75
Upper	713	120.00	513.56	517.09	0.28	0.14	0.74	0.21	0.63	2.65	0.42	81.40	69.57
Opper	713	282.00	513.56	517.95	0.50	0.26	1.87	0.48	1.10	3.73	0.72	151.62	94.41
	000												
Opper	589	26.00	514.54	515.85	0.60	0.60	1.91	1.91		3.21		8.10	10.48
Upper	693	52.00	514.54	516.31	0.57	0.24	1.89	0.51	09:0	3.34	0.36	25.03	53.02
Opper	693	45.00	514.54	516.21	0.59	0.23	1.99	0.53	0.49	3.36	0.28	19.70	50.93
Upper	693	84.00	514.54	516.64	0.59	0.31	2.11	69'0	0.85	3.56	0.55	43.57	59.72
Upper	693	120.00	514.54	516.96	0.61	0.34	2.26	0.64	1.00	3.72	79'0	63.38	66.13
Upper	693	282.00	514.54	517.88	99'0	0.36	2.74	99'0	1.35	4.16	0.92	152.01	108.11
Cpper	6/9	26.00	514.32	515.71	0.47	0.47	1.37	1.37		2.88		9.02	11.14
Upper	679	52.00	514.32	516.24	0.43	0.16	1.28	0.28	0.45	2.97	0.52	29.21	64.85
Upper	629	45.00	514.32	516.11	0.48	0.14	1.47	0.31	0.31	3.07	0.42	21.14	62.83
Upper	629	84.00	514.32	516.60	0.42	0.20	1.30	0.32	0.71	3.07	0.71	53.33	70.55
Upper	679	120.00	514.32	516.93	0.42	0.23	1.32	0.35	0.86	3.14	0.81	77.62	75.86

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Reach	River Sta O Total Min Ch E! W.S. Flev Shear Chan	O Total	Min Ch El	W.S. Flev	Shear Chan	Shear Total	Dough Chan	Down Total	40.100	1.40 1.41	14.10	Ī	
		(cfs)	€	(#)	(lh/en#)	(fries 4)	Capal	rower rotal	vei Leit	Vet Con	Vel Kight	Flow Area	ch Width
Unner	679	282 00	514 32	547.07	CA CO		(10)(19)	(10/11/8)	(sal)		(E/L)	(sd ft)	(¥)
2120	2	202,00	20.4.02	10.110	0.40	0.21	1,49	OE'O	1.14	3.42	0.82	198,20	146.69
Innar	670	5	513 30	24 27 20	8	000	0.0			1			
Ilpher	670	2002	40.00	2 000		0.09	0.1z	0.12		1.36		19.15	13.70
Cypel Lpage	070	32.00	515.52	210.27		0.05	0.27	20.0	0.23	1.85	0.26	40.80	65.27
200	O,O	45.00	213.32	510.15	0.14	0.04	0.24	90.0	0.16	1.76	0.21	33.46	63.44
Opper	670	84.00	513.32	516.60	0.21	0.09	0.48	0.12	0.41	2.27	0.43	63.52	70.62
Пррег	670	120.00	513.32	516.92	0.26	0.13	0.68	0.17	0.55	2.58	0.56	86.86	75.72
Upper	670	282.00	513.32	517.84	0.37	0.16	1.21	0.22	06.0	3.24	0.69	203.83	145.70
Upper	629	26.00	514.31	515.55	0.72	0.72	2.52	2.52		3.51		7.42	6 63
Оррег	629	52.00	514.31	516.01	98'0	0.20	3.52	0.72	0,11	4.07	0.38	14.64	64 11
Upper	629	45.00	514.31	515.90	0.84	0.51	3.30	1.94	0.22	3.94	0.24	11.80	20.82
Upper	629	84.00	514.31	516.48	0.58	0.26	2.04	0.48	0.70	3.53	0.77	45 19	68 64
Upper	659	120.00	514.31	516.84	0,52	0.27	1.81	0.46	0.84	3.48	0.88	71.04	74.42
Upper	629	282.00	514.31	517.81	0.51	0.24	1.87	0.36	1.13	3.68	0.86	189.08	144.52
Upper	646	26.00	514.04	515.43	0.47	0.47	1.36	1.36		2.88		9.03	11.16
Upper	646	52.00	514.04	515.93	0.58	96.0	1.99	1.12	0.44	3.43	0.44	16.87	22.09
Upper	646	45.00	514.04	515.82	0.54	76.0	1.78	1.14	0.36	3.27	0.36	14.65	1930
Upper	646	84.00	514.04	516.28	7.70	0.34	3.18	1.03	0.52	4.12	0.74	27.53	40.65
Upper	646	120.00	514.04	516.59	0.30	0.35	4.11	66°O	69'0	4.58	0.94	43.00	59.24
Upper	646	282.00	514.04	517.67	0.75	0:30	3.40	0.54	1.10	4.52	0.84	154.92	136.10
Upper	632	26.00	513.02	515.47	0.09	0.09	0.12	0.12		1.35		19.29	13.75
Upper	632	52.00	513,02	515.97	0.16	90.08	0.30	60.0	0.21	1.91	0.21	34.30	49.00
Upper	632	45.00	513.02	515.86	0.14	90.08	0.25	60.0	0.17	1.78	0.17	28.32	40.41
Upper	632	84.00	513.02	516.35	0.23	0.09	0.54	0.14	0.39	2.37	0.34	56.03	65.70
Upper	632	120.00	513.02	516.67	0.29	0.12	0.80	0.18	0.51	2.73	0.45	79.12	79.10
Upper	632	282.00	513.02	517.68	0.42	0.18	1.47	0.28	0.89	3.48	0.64	181.36	124.83
	0,50												
indical :	010	79°.00	514.01	515.24	0.74	0.74	2.61	2.61		3.54		7.34	9.83
Upper	616	52.00	514.01	515.69	06'0	0.46	3.72	1.75	0.36	4.14	0.36	13.74	26.37
Opper	616	45.00	514.01	515.59	0.86	0.58	3.43	2.25	0.22	3.99	0.22	11.55	18.61
Upper	616	84.00	514.01		0.87	0.35	3.76	0.95	0.70	4.31	0.66	30.84	55.06
Upper	616	120.00	514.01	516.50	0.74	0.32	3.05	0.69	0.86	4.13	0.75	56.25	71.88
Upper	616	282.00	514.01	517.61	0.63	0.30	2.59	0.51	1.15	4.12	0.84	162.94	121.57
Upper	601	26.00	513.70	515.11	0.45	0.45	1.28	1.28		2.82		9.21	11.28
Upper	601	52.00	513.70	515.61	0.53	0.27	1.76	0.72	0.44	3.30	0.43	19.20	31.15
Upper	601	45.00	513.70	515.50	0.51	0.28	1.62	0.78	0.36	3.18	96.0	16.03	26.01
Upper	601	84.00	513.70	516.04	0.58	0.26	2.10	0.59	0.64	3.61	0.63	36.71	50.31
Upper	601	120.00	513.70	516.44	0.58	0.27	2.15	0.54	0.77	3.73	0.75	59.24	63.03

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach; Upper (Continued)

Reach	River Sta	River Sta Q Total Min Ch El W.S. Elev Shear Chan	Min Ch El	W.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Valleff	Vel Chri	Vel Binht	Flow Area	Ton Midth
		(cfs)	€	(£)	(lb/sq ft)	(Ib/sq ft)	(lb/ft s)	(fb/ft s)	(ft/s)	(ft/s)	(ft/s)	(soff)	(#)
Upper	601	282.00	513.70	517.53	0.65	0.32	2.78	0.62	1.13	4.26	0.91	146.75	97.36
Upper	585	26.00	512.68	515.14	60.0	60:0	0.11	0.11		1.34		19.41	13.80
Upper	585	52.00	512.68	515.64	0.16	60:08	0.31	0.16	0.22	1.94	0.21	29.75	28.12
Upper	585	45.00	512.68	515.53	0.14	60.0	0.25	0.15	0.17	1.79	0.17	26.85	24.77
Upper	585	84.00	512.68	516.05	0.25	0.12	0.61	0.23	0.36	2.48	0.35	43.89	41.26
Upper	585	120.00	512.68	516.43	0.32	0.14	0.93	0.27	0.47	2.89	0.46	62.26	56.97
Upper	585	282.00	512.68	517.48	0.53	0.23	2.08	0.44	0.87	3.92	0.70	143.74	95.74
Upper	566	26.00	513.66	514.92	0.68	99.0	2.32	2.32		3.42		7.61	10.11
Upper	566	52.00	513.66	515.36	0.88	0.66	3.62	2.64	0.37	4.11	0.37	13.07	16.65
Upper	566	45.00	513.66	515.27	08.0	79.0	3.11	2.57	0.28	3.87	0.25	11.76	14.66
Upper	566	84.00	513.66	515.63	1.29	0.79	6.65	3.59	0.72	5.16	0.71	18.52	23.17
Upper	266	120.00	513.66	515.85	1.73	86.0	10.67	4,83	1.80	6.15	0.99	24.28	28.48
Upper	566	282.00	513.66	516.84	2.09	0.85	15.35	3.28	1.33	7.34	1.58	73.05	73.25
Upper	546	26.00	513.30	514.75	0,40	0.40	1.08	1.08		2.68		9.70	11.62
Upper	546	52.00	513.30	515.29	0.41	0.20	1.19	0.40	0.51	2:92	0.50	25.55	40.24
Upper	546	45.00	513.30	515.19	0.40	0.18	1.12	0.38	0.41	2.83	0.43	21.38	39.08
Upper	546	84.00	513.30	515.64	0.51	0.28	1.71	0.58	0.78	3.37	0.70	40.31	44.09
Upper	546	120.00	513.30	515.94	0.61	0.36	2.34	0.80	0.98	3.81	0.86	53.92	47.36
Upper	546	282.00	513.30	516.88	1.02	0.57	5.34	1.48	1.39	5.24	1.21	107.70	68.20
Upper	529	26.00	512.29	514.77	0.08	90.08	0.11	0.11		1.32		19.76	13.92
Upper	629	52.00	512.29	515.31	0.14	0.07	0.26	0,10	0.25	1.83	0.26	35.68	40.35
Upper	529	45.00	512.29	515.20	0.13	0.06	0.22	90.0	0.19	1.70	0.21	31.63	39.24
Upper	529	84.00	512.29	515.64	0.23	0.12	0.55	0.20	0.45	2.38	0.42	50.01	44.09
Upper	529	120.00	512.29	515.93	0.32	0.18	0.93	0.33	0.62	2.88	0.56	63.18	47.26
Upper	529	282.00	512.29	516.84	69.0	0.36	3.06	0.88	1.03	4.43	0.92	114.89	67.34
, m., c., m.	-												
Upper	508	26.00	513.27	514.58	0.59	0.59	1.89	1.89		3.20		8.13	10.50
Upper	509	92.00	513.27	515.09	0.64	0.26	2.28	92.0	0.36	3.57	0.47	17.84	38.04
Upper	509	45.00	513.27	515.00	0.61	0.22	2.08	0.70	0.17	3.43	0.34	14.33	37.01
Upper	509	84.00	513.27	515.40	0.81	0.41	3.38	1.14	0.79	4.18	0.78	29.97	41.40
Upper	509	120.00	513.27	515.66	0.98	0.53	4.60	1.56	1.07	4.71	66'0	41.18	44.28
Upper	509	282.00	513.27	516.47	1.83	06.0	10.60	3.09	1.68	6.49	1.40	82.15	60.18
Upper	493	26.00	513.02	514.43	0.45	0.45	1.26	1.26		2.81		9.26	11.32
Upper	493	52.00	513.02	515.01	0.48	0.17	1.50	0.45	0.16	3.15	0.45	19.51	42.21
Upper	493	45.00	513.02	514.92	0.42	0.26	1.23	0.67	0.38	2:92	0.38	17.32	22.92
Upper	493	84.00	513.02	515.30	0.68	0.28	2.61	0.73	0.56	3.87	0.71	32.68	49.40
Upper	493	120.00	513.02	515.55	0.84	0.38	3.68	0.98	0.81	4.41	0:30	46.24	55.84

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Program Color <		STATE AND A	2		1	OF				2				
462 282.00 516.00 10.44 (10.44) (10.44		5	(90)		VY.O. Elev	oriear Crian	Shear Iotal	Power Chan	Power Total	Vel Left	Vel Chul	Vel Right	Flow Area	Top Width
462 262,00 515,40 1123 0.58 7.00 161 1.13 5.70 1.12 10,44 462 262,00 515,00 <td>- Const</td> <td>100</td> <td>(CIS)</td> <td>(11)</td> <td>(III)</td> <td>(lb/sq ft)</td> <td>(lp/sd ft)</td> <td>(ib/fts)</td> <td>(lb/ft s)</td> <td>(ft/s)</td> <td>(ft/s)</td> <td>(£/s)</td> <td>(sq ft)</td> <td>(£)</td>	- Const	100	(CIS)	(11)	(III)	(lb/sq ft)	(lp/sd ft)	(ib/fts)	(lb/ft s)	(ft/s)	(ft/s)	(£/s)	(sq ft)	(£)
482 28.00 512.01 514.47 0.08 0.08 0.11 0.01 1.33 1.32 0.22 0.38 1.34 1.34 0.14 0.08 0.01 0.03 0.03 1.32 0.02 0.03 0.03 1.34 0.03	jaddo	483	282.00	513.02	516.42	1.23	0.59	7.00	1.61	1.37	5.70	1.21	104.41	81.12
1879 1870	Loner	782	00	70 070	1, 11,									
442 50.00 51.50 515.00 61.46 0.04 0.05 0.03	10 T	707	70.07	512.01	514.47	0.08	0.08	0.11	0.11		1.33		19.49	13.82
482 4500 61201 0.05 <th< td=""><td>Upper</td><td>482</td><td>92.00</td><td>512.01</td><td>515.05</td><td>0.14</td><td>90.0</td><td>0.26</td><td>0.00</td><td>0.23</td><td>1.82</td><td>0.22</td><td>35.99</td><td>43.44</td></th<>	Upper	482	92.00	512.01	515.05	0.14	90.0	0.26	0.00	0.23	1.82	0.22	35.99	43.44
Mail	Opper	482	45.00	512.01	514.96	0.12	0.05	0.20	0.08	0.18	1.67	0.18	37 14	30.70
4482 1200 51200 51201 51640 0.34 0.16 1.02 0.55 0.56 0.57 0.58 0.16 0.78 0.16 0.78 0.16 0.78 0.16 0.28 0.58	Upper	482	84.00	512.01	515.35	0.24	0.11	0.58	0.18	0.40	2.42	0.37	50.00	54 44
Marco Marc	Upper	482	120.00	512.01	515.60	0.34	0.16	1.02	0.30	0.55	200	0.54	20.00	1000
469 2600 61300 61430 61430 61643 6169 6180 61430 61431 61843 6	Upper	482	282.00	512.01	516.44	0.71	0.33	3.15	0.78	4 03	2 48	5 6	4.02	00.00
489 2200 51420 51420 0.68 0.68 2.10 2.10 2.10 2.10 2.10 2.10 2.10 2.10 2.10 2.10 2.10 2.10 2.10 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.20 0.28 0.20 0.28 0.20 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 0.28 0.29 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>2</td><td>3</td><td>ř</td><td>0,02</td><td>122.40</td><td>60.29</td></t<>									2	3	ř	0,02	122.40	60.29
489 52.00 513.00 514.81 0.56 0.76 1.69 0.24 0.70 3.00 0.70 1.70 489 52.00 513.00 514.82 0.47 0.70 1.40 0.70 3.00 0.70	Upper	469	26.00	513.00	514.28	0.63	0.63	210	2.40		8			
489 4600 61300 61489 0.47 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.48 0.70 0.38 0.70 0.70 0.70 0.70 0.70 0.70 0.70 <t< td=""><td>Upper</td><td>469</td><td>52.00</td><td>513.00</td><td>514.91</td><td>0.50</td><td>0,0</td><td>4 60</td><td>2 5</td><td>0,0</td><td>0.0</td><td></td><td>7.86</td><td>10.30</td></t<>	Upper	469	52.00	513.00	514.91	0.50	0,0	4 60	2 5	0,0	0.0		7.86	10.30
469 64.00 61.00 6	Unper	469	45.00	20.00	2077	300	0.13	8.	0.43	0.42	3.20	0.42	23.04	49.94
1,000 1,00	2012	3	3 6	013.00	014.03	0.47	0.18	1.42	0.43	0.36	3.05	0.36	19.09	42.03
469 17000 515.49 0.69 0.33 273 0.69 0.77 3.89 0.77 98.38 469 280 17300 516.40 0.69 0.45 4.09 0.39 1.39 0.77 0.59 1.38 0 469 280 280 512.74 516.40 0.41 0.41 0.43 0.43 0.43 0.43 0.49 1.39 4.75 0.59 0.77 0.59 0.59 0.54 0.59 0.54 0.59 0.54 <th< td=""><td>leddo :</td><td>468</td><td>84.00</td><td>513.00</td><td>515.21</td><td>0.62</td><td>0.27</td><td>2.30</td><td>0.56</td><td>0.70</td><td>3.69</td><td>0.63</td><td>40,17</td><td>62.13</td></th<>	leddo :	468	84.00	513.00	515.21	0.62	0.27	2.30	0.56	0.70	3.69	0.63	40,17	62.13
469 282.00 613.00 518.40 0.86 0.46 0.96 1.39 4.79 0.99 1.29 4.79 0.99 1.29 4.79 0.99 1.29 4.79 0.99 1.29 4.79 0.99 1.29 4.79 0.99 1.29 4.79 0.99 0.21 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.42 2.69 0.42 2.69 0.42 2.69 0.42 2.69 0.42 2.69 0.42 2.69 0.42 2.69 0.42 0.49 0.78 0.49	Cpper	469	120.00	513.00	515,49	69.0	0.33	2.73	0.68	0.91	3,98	0.77	58.35	67.73
466 25.00 512.74 514.19 0.41 0.41 1.11 1.11 0.43 2.70 0.84 456 52.00 512.74 514.89 0.34 0.46 0.17 0.24 0.28 2.51 0.43 2.60 456 6.20 512.74 516.48 0.34 0.14 0.73 0.74 0.24 0.68 0.63 2.51 0.97 2.50 0.43 2.50 456 6.400 512.74 516.34 0.74 0.24 0.24 0.68 0.79 0.80 2.51 0.79 0.80 446 5.20 512.74 516.34 0.74 0.24 0.78 0.79 0.80 0.71 0.79 0.80 0.71 0.79 0.80 0.71 0.79 0.80 0.71 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78	Upper	469	282.00	513.00	516.40	0.85	0.45	4.06	0.98	1.39	4.75	06	129 90	97.00
456 250 51274 51419 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.41 0.42 0.25 0.42 0.26 0.42 0.26 0.42 0.26 0.42 0.56 0.42 0.56 0.42 0.56 0.42 0.56 0.42 0.56 0.42 0.56 0.42 0.56 0.42 0.62 0.56 0.42 0.56 0.43 0.49 0.64 0.64 0.64 0.74 0.78 0.62 0.62 0.62 0.78 0.62 0.78 0.62 0.78 0.62 0.78 0.62 0.78 <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>2</td><td>21.70</td></th<>													2	21.70
456 52.00 512.74 514.88 0.34 0.16 0.09 0.031 0.44 2.66 0.42 2.66 0.42 2.66 0.45 2.66 2.66 2.46 2.66 2.	Upper	456	26.00	512.74	514.19	0.41	0.41	1.1	1.1		2.70		0 64	14 50
456 4500 61274 61480 0.34 0.14 0.74 0.27 0.38 2.61 0.37 2.62 456 4500 61274 616.14 0.54 0.24 1.88 0.54 0.63 3.49 0.67 0.78 3.49 0.67 37.82 456 120.00 612.74 516.24 1.06 0.48 5.59 1.17 1.28 0.67 1.69 3.49 0.62 37.82 7 466 282.00 511.73 514.81 0.12 0.09 0.14 0.05 0.19 0.07 0.09 1.18 0.12 0.09 1.18 0.12 0.09 1.18 0.12 0.09 1.18 0.14 0.05 0.14 0.17 0.09 0.14 0.17 0.09 0.14 0.14 0.09 0.14 0.17 0.09 0.11 0.11 0.12 0.09 0.19 0.14 0.14 0.12 0.09 0.19 0.14 0.14	Upper	456	52.00	512.74	514.88	0.34	0.16	0.90	0.31	0.43	2 69 C	0.42	5 5	70.00
458 64.00 512.74 515.14 0.54 0.24 1.88 0.54 0.58 3.48 0.52 3.49 0.52 3.49 0.52 3.49 0.52 3.49 0.52 3.50 0.54 0.58 3.09 0.74 0.59 0.74 0.59 0.74 0.59 0.74 0.59 0.74 0.59 0.74 0.59 0.74 0.78 0.78 0.09 4.18 0.79 4.93 444 282.00 511.73 514.22 0.08 0.09 0.71 0.71 1.26 0.24 1.08 1.17 1.28 0.72 1.68 0.72 1.68 0.72 1.68 0.72 1.68 0.72 1.68 0.72 1.68 0.72 1.68 0.72 1.68 0.72 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78	Upper	456	45.00	512.74	514.80	06.0	0.14	0.74	0.27	0.38	251	0.37	32.53	20.00
466 120.00 512.74 516.36 0.74 0.36 0.79 0.79 0.80 4.18 0.79 4.02 4.18 0.79	Upper	456	84.00	512.74	515.14	0.54	0.24	1.88	0.54	0.63	3.49	0.0	37.02	40 50
f 456 522.00 512.74 516.24 1.05 0.48 5.59 1.17 1.28 5.31 1.08 1.15 (1.08) 444 26.00 511.73 514.22 0.08 0.01 0.01 1.31 1.08 0.15 (1.08) 7 444 52.00 511.73 514.81 0.12 0.05 0.15 0.06 0.22 1.33 1.08 0.24 0.38 2.24 0.33 6.92 7 444 45.00 511.73 514.82 0.10 0.04 0.15 0.06 0.22 1.36 0.24 0.33 6.92 7 444 45.00 511.73 515.41 0.20 0.06 0.12 0.05 0.12 0.05 0.12 0.06 0.12 0.03 0.14 0.05 0.14 0.05 0.14 0.05 0.14 0.05 0.14 0.05 0.14 0.05 0.14 0.10 0.10 0.14 0.10 0.12 0.14	Upper	456	120.00	512.74	515.36	0.74	0.33	3.09	62.0	C	4.18	20.0	20.10	42.00
444 28.00 511.73 514.22 0.08 0.01 0.01 0.01 0.13 0.10 1.08 144 52.00 511.73 514.32 0.08 0.01 0.01 0.02 1.98 0.01 0.05 0.19 0.06 0.02 1.98 0.01 0.08 0.01 1.52 0.19 0.08 0.01 1.52 0.19 0.08 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.05 0.01 0.05	Upper	456	282.00	512.74	516.24	1.05	0.48	5.59	1 17	1.08	2 7	6.19	46.93	70.07
444 26.00 511.73 514.22 0.08 0.08 0.11 0.11 0.11 0.11 0.12 1.38 19.86 444 52.00 511.73 514.81 0.12 0.05 0.13 0.05 0.12 0.18 0.02 4.306 444 52.00 511.73 514.82 0.10 0.04 0.12 0.05 0.12 0.03 2.24 0.33 58.73 444 84.00 511.73 516.74 0.20 0.13 0.05 0.12 0.05 0.12 0.05 0.12 0.05 0.12 0.05 0.04 0.05 0.05 0.04 0.05										2	200	3	10.04	82.33
444 52.00 511.73 514.91 0.12 0.05 0.19 0.06 0.02 1.66 0.02 1.69 0.06 0.05 1.69 0.06 0.02 1.69 0.06 0.05 0.19 1.00 0.00 0.04 0.15 0.05 0.19 1.62 0.19 38.67 0.00 0.00 0.01 0.05 0.19 1.62 0.01 0.05 0.19 0.15 0.19 0.15 0.05 0.19 0.15 0.01 0.05 0.01 0.05 0.10 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.01 0.05 0.02 0.05	Upper	444	26.00	511.73	514.22	0.08	0.08	0.11	0.11		1 34		40.06	40.00
r 444 45.00 511.73 514.82 0.10 0.04 0.15 0.05 0.12 1.05 0.12 1.05 0.02 43.06 1 444 84.00 511.73 516.17 0.20 0.09 0.05 0.12 0.05 0.19 3.67 0.03 59.23 1 444 120.00 511.73 516.17 0.20 0.09 0.01 0.01 0.03 2.24 0.03 59.23 69.23 444 282.00 511.73 516.27 0.56 0.25 0.25 0.05 0.05 0.16 0.17 0.53 0.04 0.18 0.14 0.53 0.04 0.15 0.27 0.05 0.05 0.05 0.05 0.16 0.16 0.05 0.05 0.16 0.05 0.05 0.16 0.05 0.05 0.05 0.05 0.05 0.16 0.05 0.05 0.16 0.05 0.05 0.05 0.05 0.05 0.05	Upper	444	52.00	511.73	514.91	0.12	0.05	0 10	900	500	0.00	000	00.00	0.00
444 84.00 511.72 515.74 0.00 0.04 0.15 0.19 1.52 0.19 3.867 444 282.00 511.73 515.41 0.20 0.03 0.45 0.12 0.38 2.24 0.33 592.33 444 282.00 511.73 516.41 0.29 0.13 0.25 0.05 1.01 0.39 2.24 0.33 592.33 444 282.00 511.73 516.27 0.56 0.13 0.25 0.05 1.01 3.89 0.69 140.83 429 28.00 512.72 514.05 0.56 0.76 1.76 0.77 2.59 0.62 140.83 429 52.00 512.72 514.73 0.32 0.76 0.27 0.27 0.27 0.28 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.50 0.37 2.50 0.62 2.78 0.71 0.71 0.71	Upper	444	45.00	511 73	514 82	0 10	20.0	2 0	B	0.22	00.1	0.22	43.06	54.33
444 120.0 511.73 515.14 0.29 0.13 0.45 0.12 0.23 2.24 0.33 59.23 444 120.0 511.73 516.41 0.29 0.13 0.25 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.77 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76 0.76	Inner	444	00.55	644 70	2014:02	0.10	40.0	CL.U	O.05	0.19	1.52	0.19	38.67	49.26
444 282.00 511.73 515.41 0.58 0.13 0.81 0.21 0.53 2.75 0.43 7461 444 282.00 511.73 516.27 0.56 0.28 0.28 0.25 0.55 1.01 3.39 0.69 140.33 429 26.00 512.72 514.05 0.56 0.16 1.01 0.83 0.42 2.78 0.42 2.78 0.42 2.80 429 45.00 512.72 514.80 0.36 0.16 1.01 0.83 0.42 2.78 0.42 2.80 429 45.00 512.72 515.01 0.62 0.26 0.28 0.58 0.58 0.58 0.63 0.78 0.58 0.78	Long.	777	20.00	011.70	210.17	0.20	0.08	0.45	0.12	0.38	2,24	0.33	59.23	63.48
444 282.00 511.73 516.27 0.56 0.28 2.25 0.55 1.01 3.99 0.69 140.83 429 226.00 512.72 514.05 0.56 0.56 1.76 1.76 1.76 0.42 2.78 0.62 1.76 429 52.00 512.72 514.05 0.36 0.16 1.01 0.30 0.42 2.78 0.42 2.69 0.37	ביייים ביייים	***	120.00	571.73	515.41	0.29	0.13	0.81	0.21	0.53	2.75	0.43	74.61	68.15
429 26.00 512.72 514.05 0.56 0.56 1.76 1.76 3.13 3.13 8.31 429 52.00 512.72 514.80 0.36 0.16 1.71 0.37 2.59 0.42 2.78 0.42 2.68 429 45.00 512.72 514.73 0.32 0.14 0.83 0.27 0.37 2.59 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.37 2.69 0.77 1.02 2.69 0.77 1.02 2.69 0.78 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74 0.74	iaddo	#	787.00	511.73	516.27	0.56	0.28	2.25	0.55	1.01	3.99	0.69	140.93	88.01
429 55.00 512.72 514.80 0.56 1.76 1.76 1.76 3.13 8.31 8.31 429 52.00 512.72 514.80 0.36 0.16 1.01 0.39 0.42 2.78 0.42 2.68 0 429 45.00 512.72 514.73 0.32 0.14 0.83 0.27 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.59 0.78 3.71 4.74	Long	\$	00.00	010										
4.28 55.00 512.72 514.80 0.36 0.16 1.01 0.30 0.42 2.78 0.42 2.68 0 429 45.00 512.72 514.73 0.32 0.14 0.83 0.27 0.37 2.59 0.37 2.59 0.37 2.59 0.37 2.68 0 0.37 2.59 0.37 2.68 0 0.37 2.59 0.37 2.50 0.37 2.59 0.37 2.59 0.37 2.58 0.37 2.59 0.37 2.59 0.37 2.58 0.37 0.59 37.13 0.69 37.13 0.78 47.41 1.07 110.29 0.78 0.78 47.41 1.07 110.29 0.78 0	P. C.	423	Z0.02	2177.12	514.05	0,56	0.56	1.76	1.76		3.13		8.31	10.64
429 45.00 512.72 514.73 0.32 0.14 0.83 0.27 0.37 2.59 0.37 2.362 8.20 2.28 0.58 0.68 0.63 3.70 0.53 3.713 2.362 9.713 4.28 0.78 0.58 0.58 0.68 4.48 0.78 0.713 4.741 <	eddo.	878	22.00	512.72	514.80	0.36	0.16	1.01	06.0	0.42	2.78	0.42	26.80	44.81
429 84,00 512.72 515.01 0.62 0.26 0.58 0.68 0.68 3.70 0.63 37.13 7.10 429 120.00 512.72 515.18 0.87 0.39 3.90 0.98 0.88 4.48 0.78 47.41 7.11 7.11 7.11 0.58 6.13 1.48 1.48 0.78 47.41 7.11	Cpper	428	45.00	512.72	514.73	0.32	0.14	0.83	0.27	0.37	2.59	0.37	23.62	40.61
429 120,00 512,72 516,18 0.87 0.39 3.90 0.96 0.98 4.48 0.78 47.41 47.41 4.81 6.78 47.41 4.81 6.78 47.41 4.81 6.78 47.41	Opper	429	84.00	512.72	515.01	0.62	0.26	2.28	0.58	0.63	3.70	0.63	37.13	56.14
429 282.00 512.72 516.07 1.13 0.58 6.13 1.48 1.41 5.44 1.07 110.29 415 26.00 512.48 513.94 0.39 0.39 1.04 1.04 2.65 0.40 9.82 415 52.00 512.48 514.79 0.22 0.10 0.48 0.13 0.41 2.21 0.40 39.08 415 45.00 512.48 514.72 0.19 0.08 0.39 0.11 0.37 2.05 0.36 51.11 415 84.00 512.48 514.79 0.39 0.17 1.17 0.28 0.59 3.00 0.58 51.02 415 10.00 512.48 515.16 0.58 0.29 0.71 0.50 0.79 3.72 0.69 57.38	Upper	429	120.00	512.72	515.18	0.87	0.39	3.90	96'0	0.88	4.48	0.78	47.41	80.38
415 26.00 512.48 513.94 0.39 0.39 1.04 1.04 2.65 9.62 9.82 415 52.00 512.48 514.79 0.22 0.10 0.48 0.13 0.41 2.21 0.40 39.08 415 45.00 512.48 514.72 0.19 0.08 0.39 0.11 0.37 2.05 0.36 35.11 415 84.00 512.48 514.99 0.39 0.17 1.17 0.28 0.59 3.00 0.58 51.02 415 10.00 512.48 515.16 0.58 0.21 0.50 0.79 3.79 0.69 67.38	Upper	429	282.00	512.72	516.07	1.13	0.58	6.13	1.48	1,41	5,44	1.07	110 29	82.03
415 26.00 512.48 513.94 0.39 0.39 1.04 1.04 1.04 2.65 9.82 9.82 415 52.00 512.48 514.79 0.22 0.10 0.48 0.13 0.41 2.21 0.40 39.08 415 45.00 512.48 514.72 0.19 0.08 0.39 0.11 0.37 2.05 0.36 35.11 415 84.00 512.48 514.99 0.39 0.17 1.17 0.28 0.59 3.00 0.58 51.02 415 10.00 512.48 515.16 0.58 0.215 0.50 0.79 3.77 0.69 67.38														
415 52.00 512.48 514.79 0.22 0.10 0.48 0.13 0.41 2.21 0.40 39.08 415 45.00 512.48 514.72 0.19 0.08 0.39 0.11 0.37 2.05 0.36 35.11 415 84.00 512.48 514.99 0.39 0.17 1.17 0.28 0.59 3.00 0.58 51.02 415 120.00 512.48 515.16 0.59 2.15 0.50 0.79 3.79 0.69 67.38	Jpper	415	26.00	512.48	513.94	0.39	0.39	1.04	1.04		2.65		9.82	11 70
415 45.00 512.48 514.72 0.19 0.08 0.39 0.11 0.37 2.05 0.36 35.11 415 84.00 512.48 514.99 0.39 0.17 1.17 0.28 0.59 3.00 0.58 51.02 415 1.20.00 512.48 515.16 0.58 0.26 2.15 0.50 0.79 3.72 0.69 62.38	Jpper	415	52.00	512.48	514.79	0.22	0.10	0.48	0.13	0.41	2.21	0.40	39.08	55.04
415 84.00 512.48 514.39 0.39 0.17 1.17 0.28 0.59 3.00 0.58 51.02 415 1.20.00 512.48 515.16 0.58 0.26 2.15 0.50 0.79 3.72 0.69 62.38	Jpper	415	45.00	512.48	514.72	0.19	0.08	0.39	0.11	0.37	2.05	0.36	35 11	51 43
415 120.00 512.48 515.16 0.58 0.26 2.15 0.50 0.79 3.72 0.69 62.38	Jpper	415	84.00	512.48		0.39	0.17	1.17	0.28	0.59	3.00	0.58	51.02	64 50
	Лррег	415	120.00	512.48	515.16	0.58	0.26	2.15	0.50	62.0	370	08.0	20.00	30 00

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

THE TAIL OF THE TOTAL TRANSPORT TOTAL TRANSPORT TOTAL		1		745 : CP2	opper (conninea)								
reach	Kiver ota	C Otal	Mm Ch El	W.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Vel Left	Vel Chnl	Vel Right	Flow Area	Top Width
		(cts)	((£)	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(£/s)	(fVs)	(fVs)	(saft)	
Upper	415	282.00	512.48	516.06	0.79	0.38	3.66	92.0	1.23	4.62	0.92	141.05	104.09
l lance	707	000											
opper	ţ.	79.00	74.11.5	513.98	0.08	20.0	0.10		10.01	1.29	0.01	20.09	16.07
copper Copper	404	52.00	511.47	514.80	0.09	9.0	0.13	0.04	0.24	1.48	0.27	53.10	56.95
Upper	404	45.00	511.47	514.73	20.0	0.03	0.10	0.03	0.21	1.34	0.23	48.93	53.87
Upper	404	84.00	511.47	515.01	0.17	70.0	0.37	0.10		2.10	0.40	65 59	65.29
Upper	404	120.00	511.47	515.18	0.28	0.12	77.0	0.19		2.70	0.47	77 15	74 54
Opper	404	282.00	511.47	516.05	0.54	0.24	2.09	0.44	0.94	3.90	0.71	153,30	103.65
Inner	304	90	070	000		1							
Jenos.	204	3 8	512.46	513.82	0.51	0.51	1.52	1.52		2.99		8.74	10.92
Opper	283	52.00	512.46	514.75	0.21	0.10	0.47	0.13	0.44	2.19	0.39	40.28	54.68
Upper	391	45.00	512.46	514.68	0.19	60:0	78.0	0.11	0.39	2.02	0.35	36.57	51.76
Upper	391	84.80	512.46	514.92	0.40	0.19	1.23	0.31	0.64	3.05	0.57	49.93	61.65
Upper	391	120.00	512.46	515.04	0.67	0.31	2.64	0.65	0.85	3.96	0.75	57.28	00 S
Upper	391	282.00	512.46	515.93	06:0	0.43	4.37	0.93	1.30	4.88	0.95	131 40	00.00 40
													21.00
	377	26.00	512.16	513.77	0.27	0.18	09:0	0.38	0.15	2.24	0.15	12.00	19 16
	377	52.00	512.16	514.76	0,10	40.04	0.15	0.03	0.41	1.52	0.34	64.63	88 12
	377	45.00	512.16	514.69	0.09	0.03	0.12	0.03	0.37	1.42	0.31	58.48	83.01
	377	84.00	512.16	514.94	0.17	0.07	0.35	0.07	0.59	2.03	0.47	81.65	100.90
	3//	120.00	512.16	515.08	0.25	0.10	0.64	0.13	0.79	2.51	0.56	96.16	108.05
nbber	377	282.00	512.16	516.02	0.26	0.13	0.71	0.17	1.14	2.70	0.54	213.92	143.82
	000	0000											
	362	26.00	511.14	513.79	90.0	0.04	20.0	0.05	0.07	1.18	70.0	22.65	21.82
	205	92.00	511.14	514.76	0.05	0.02	90'0	0.01	0.27	1.18	0.23	73.44	85.42
	700	45.00	511.14	514.69	0.05	0.02	0.05	0.01	0.24	1.08	0.21	67.55	80.52
	200	84.00	511.14	514.93	0.11	0.04	0.17	0.04	0.42	1.66	0.35	89.46	97.51
	362	120.00	511.14	515.07	0.17	90:0	0.37	0.07	0.58	2.13	0.42	102.76	104.70
Jaddo	302	282.00	511.14	515.99	0.23	0.10	0.59	0.13	9.	2.58	0.43	217.54	142.74
Upper	343	26.00	512.13	513.69	0.31	0.25	0.73	at C	0 40	26.0	9	1	
Upper	343	52.00	512.13	514.74	60.0	000	0 14	000	2 6	20.7	0.00	CO.1 -	15.23
Upper	343	45.00	512.13	514.67	0.08	0.03	0.12	20.0	0000	0 t	0.20	17.30	113.2/
Upper	343	84.00	512.13	514.91	0.16	90.0	0.32	0.05	0.57	20.0	0.23	42.50	103.00
	343	120.00	512.13	515.04	0.24	0.09	0.59	60.0	0.74	2.45	0.00	110 02	151.51
Upper	343	282.00	512.13	515,99	0.20	0.10	0.47	0.10	0.99	2.36	0.64	262 44	178 58
	326	26.00	511.85	513.66	0.16	0.05	0.28	90:0	0.20	1.76	0.20	20.79	56.15
	326	52.00	511.85	514.75	0.03	0.02	0.03	0.01	0.24	0.91	0.24	140.89	142.42
	320	45.00	511.85		0.03	0.01	0.02	0.00	0.22	0.84	0.22	130.93	138.88
opper	320	84.00	511.85	514.92	90.0	0.03	0.08	0.01	0.35	1.24	0.35	165.98	150.97
	070	120.00	511.85		0.10	0.05	0.16	0.03	0.46	1.59	0.46	185.49	156.71

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Peach	Divor Ch	THE C			Commission (Southlead)								
	5	(ofe)		VV.O. Elev	Shear Chan	Shear lotal	Power Chan	Power Total	Vel Left	Vel Chnl	Vel Right	Flow Area	Top Width
Imper	308	282,00	(16)	(II)	(Ib/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(ft/s)	(fVs)	(£/s)	(sq ft)	(#)
2420	220	707'707		515.89	0.13	0.07	0.24	90.08	0.65	1.91	0.67	349.00	191.46
Upper	314	26.00	510.84	513.67	500	200	900	200	0,0				
Upper	314	52.00	510.84	514 75	200	20.0	200	0.0	0.70	1.03	0.10	32.06	59.34
Upper	314	45.00	510.84	514.68	200	0.00	20.0	00.0	0.18	0.79	0.18	151.59	142.33
Upper	314	84.00	510.84	514.92	50.0	600	200	0.00	71.0	C.C3	0.16	141.68	138.80
Upper	314	120 00	540 84	515.04	90.0	2000	0.00	10.0	0.28	1.11	0.28	176.36	150.78
Upper	374	282 00	510 BA	212,01	0.00	0.03	rr.u	0.02	0.37	1.45	0.37	195.40	156.46
		202.00	0.00	0.30	11.0	90.0	0.21	0.04	0.58	1.85	0.59	358.22	191.12
Upper	300	26.00	511.83	51362	0.18	3	000	100					
Upper	300	52.00		514 74	0.03	300	00.00	0.07	0.23	1.79	0.20	20.54	58.25
	300	45.00	511.83	514.67	8.0	500	20.0	Onin	0.22	0.84	0.22	158.90	164.17
Upper	300	848		54 4 04	20.0	10.0	20:0	0.00	0.20	0.78	0.20	147.49	159.81
	300	420.00		0.4.0	CO.O	0.02	90:0	0.01	0.32	114	0.32	187.39	174.60
Inper	200	00.021	011.83	515.04	90.08	0.04	0.12	0.02	0.42	1.46	0.42	209.27	182.38
ipdido	200	787.00		515.98	0.10	0.05	0.17	0.03	0.56	1.69	0.59	410.19	245.33
linor	900	0000											
	790	78.00	511.53	513.62	0.08	0.03	0.10	0.02	0.20	1.27	0.20	37.36	79.65
Opper	987	22:00	511.53	514.74	0.02	0.01	0.02	00:0	0.19	0.73	0.19	182.93	165.37
	220	45.00	511.53	514.67	0.02	0.01	0.01	00.0	0.18	0.67	0.17	171 45	161 37
	786	84.00	511.53	514.91	0.04	0.02	0.04	0.04	0.28	1.02	0.28	21132	174 88
Upper	286	120.00	511.53	515.03	0.07	0.03	60'0	0.02	0.38	132	0.38	23.02	100.00
	286	282.00	511.53	515.97	60.0	0.04	0.15	0.03	0.53	1.63	0.54	433.27	244.06
												17:001	00.44
	270	26.00	510.52	513.63	0.02	0.04	0.04	00.00	0.15	690	77.0	79.04	450 70
	270	52.00	510.52	514.74	00'0	0.00	0.00	0.00	0.12	0.37	0.14	340.70	244.47
	270	45.00	510.52	514.67	0.00	0.00	0.00	00.00	0.11	0.33	210	20.57	14.4.7
	270	84.00	510.52	514.91	0.01	00:00	0.01	00:00	0.18	0.53	0.23	247.44	200.74
	270	120.00	510.52	515.03	0.02	10.01	0.01	0.00	0.24	69 0	0.28	375.00	200.00
Upper	270	282.00	510.52	515.97	0.03	0.02	0.03	0.01	0.36	0.97	0.43	619 25	200.28
													220.00
	251	26.00	511.50	513.61	90.0	0.03	90.0	0.01	0.23	1.09	0.25	46 43	137 43
	162	52.00	511.50	514.74	0.01	0.01	0.01	00.00	0.15	0.51	0.14	288 09	225.67
	- FS	45.00	511.50	514.67	0.01	0.00	00:0	00'0	0.14	0.47	0.12	27.2 30	223 53
- obbei	251	84.00	511.50	514.91	0.02	0.01	0.01	00.0	0.22	0.72	0.20	326 11	220.22
	291	120.00	511.50	515.03	0.03	0.02	0.03	0.01	0.29	0.94	0.26	354 11	234 33
	251	282.00	511.50	515.97	90.0	0.03	20.0	0.02	0.44	128	0.40	585.60	00000
											2	7	40000
	225	26.00	510.50	513.61	0.02	0.01	0.01	0.00	0.08	29'0	0.17	72 18	77 32
	525	52.00	510.50	514.74	0.02	00:0	0.01	00.0	0.15	0.68	0.11	221 44	200 55
	225	45.00	510.50	514.67	0.01	00.0	0.01	0.00	0.13	0.62	0.10	207.22	100 33
Upper	225	84.00	510.50	514.90	0.03	0.01	0.03	0.00	0.22	66 0	0.16	257 33	20.000
	225	120.00	510.50	515.01	90.0	0.02	0.07	0.01	0.31	130	0.24	284 94	233.30
										22::	1.4.7	10.402	640.23

HEC-RAS Plan: UpReachRev7-14 River: Tanyard Branch Reach: Upper (Continued)

Lower Design Stream

Reach 3 and 4

HEC RAS	D	C4	
River	Design Stream CL Station	Stream Feature	Comment
Station	CL Station	reature	
15+54	43+06	Tie in	
15+30	43+30	ER	
15+05	43+55	CP	
14+80	43+80	HR	
14+60	44+00	ER	
14+40	44+20	CP	
14+15	44+45	<u>HR</u>	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
13+95	44+65	ER	
13+78 13+55	44+82 45+05	CP HR	
13+38	45+22	ER	
13+25	45+35	CP	
13+05	45+55	HR	
12+90	45+70	ER	
12+75	45+85	CP.	
12+55	46+05	HR	
12+40	46+20	ER	
12+27	46+33	CP	
12+10	46+50	HR	
11+93	45+67		Upstream Culvert
11+53	47+07		Culvert
11+39	47+21		Downstream Culvert
11+07	47+53	ER	
10+90	47+70	CP	
10+70	47+90	HR	
10+55	48+05	ĘR	
10+40	48+20	CP	
10+20	48+40	<u>HR</u>	
10+00	48+60	ER	
09+85 09+60	48+75	CP .	
09+35	49+00 49+25	HR ER	
09+15	49+45	CP	
08+90	49+70	HR	
08+75	49+85	ER	***************************************
08+65	49+95	CP	
08+50	50+10	HR	
08+35	50+25	. ER	
08+20	50+40	CP	
08+00	50+60	HR	
07+80	50+80	ER	
07+68	50+92	ÇP	
07+50	51+10	HR	
07+30	51+30	ER	
07+15	51+45	Cb	
D6+95	51+65	HR	
06+73	51+87	ER	
06+58	52+02	CP	
06+37	52+23	HR	
06+20	52+40	ER	
06+05	52+55	CP	
05+85	52+75	HR	
05+70 05+58	52+90	ER CD	
05+42	53+02	CP HR	
05+25	53+18 53+35	ER	
05+25	53+52	CP	
04+90	53+70	HR	End of Reach 3
	30.10	1117	City of Descrip

HEC RAS River Station	Design Stream CL Station	Stream Feature	Comment
04+65	53+95	ER	
04+50	54+10	CP CP	
04+35	54+25	HR	
04+15	54+45	ER	
04+00	54+60	CP CP	
03+85	54+75	HR	
03+65	54+95	ER	
03+47	55+13	CP CP	
03+30	55+30	HR	· · ·
03+10	55+50	ER	
02+95	55+65	ČP	***************************************
02+80	55+80	HR	
02+60	56+00	ER	
02+45	56+15	CP	
02+30	56+30	HR	
02+00	56+60	ER	
07+80	50+80	ĒR	
07+68	50+92	CP	
07+50	51+10	HR	
07+30	51+30	ER I	•
07+15	51+45	ÇP	
06+95	51+65	HR	
06+73	51+87	ER	
06+58	52+02	CP	
06+37	52+23	HR	
06+20	52+40	ER	
06+05	52+55	CP CP	
05+85	52+75	HR	
05+70	52+90	ER	
05+58	53+02		
05+42	53+18	CP HR	
05+25	53+35	ER	
05+08	53+52	CP.	
04+90	53+70	HR	
04+65	53+95	ER	
04+50	54+10	CP	***************************************
04+35	54+25	HR	
04+15	54+45	ER	
04+00	54+60	CP	
03+85	54+75	HR	
03+65	54+95	ER	
03+47	55+13	CP CP	
03+30	55+30	HR	
03+10	55+50	ER	
02+95	55+65	CP	·
02+80	55+80	HR	
02+60	56+00	ER	
02+45	56+15	CP	*****
02+30	56+30	HR	
02+00	56+60	ER	
01+85	56+75	ČP	
01+70	56+90	HR	
01+45	57+15	ER	
01+30	57+30	CP	
01+10	57+50	HR	
00+80	57+80	EK 1	
00+80	57+80 58+00	ER CP	
		CP HR	

HEC-RAS Plan: Prop lower ineff River: Tanyard Branch Reach: Lower

	River Sta	OTotal	Min Ch El	W.S. Flav	Shear Chan	Chear Total	Design Chan	Dought Total	40 1 104	led Oby	17710101	,	Town 14 Cale
		(#) (#) (#)	. €	₩	(lb/sq ft)	(Holen fit)	(lb/ff s)	(h/ft e)	VGI LGIL (#/c)	(#/e)	(#/c)	(# CO)	IRDIA do I
Lower	1554	55.00	497.10	498 73	0.72	62.0	2.60		(60)	386	(601)	15.05	15.54
Lower	1554	110.00	497.10	498.90	1.98	1.98	12.30			6.2		17.72	16.21
Lower	1554	90.00	497.10	498.78	1.74	1.74	10.00			5.74		15.69	15.70
Lower	1554	163.00	497.10	499.39	1.03	0.36	4.87		1.18		0.43	61.43	119.27
Lower	1554	227.00	497.10	489.54	1.26	0.49	6.68	1.40			0.61	80.04	126.85
Lower	1554	518.00	497.10	500.01	2.06	76'0	14.59		2.60	7.08	1.12	144.98	150.16
And the first first free flower or was an annual second													
Lower	1530	55.00	496.72	498.57	0.45	0.45	1.34	1.34		2.97		18.51	115.92
Lower	1530	110.00	496.72	498.96	0.16	20'0	0.29	0.07	0.75	1.84	0.15	110.82	167.84
Lower	1530	90.00	496.72	498.97	01.0	90'0	0.15	0.04	0.61	1.49	0.13	112.47	169.18
Lower	1530	163.00	496.72	499.19	0.18	60.0	0.35	01.0	0.89	1.99	0.27	150.18	178,25
Lower	1530	227.00	496.72	499.40	0.20	0.11	0.43	0.13	1.04	2.16	0.35	189.30	184.29
Lower	1530	518.00	496.72	500.07	0.31	0.20	0.88	0.32	1.53		0.59	318.00	202.63
Lower	1505	55.00	495.30	498.58	0.12	0.12	0.20	0.20		1.65		33.38	117.54
Lower	1505	110.00	495.30	498.93	0.12	0.05	0.20		0.55	1.67	0.11	118.87	157.27
Lower	1505	00.06	495.30	498.95	20.0	0.03	0.10	0.02	0.44	1.33	60.0	122.47	159.72
Lower	1505	163.00	495.30	499.15	0.15	90.0	0.29	0.07	0.71	1.93	0.20	154.98	168.40
Lower	1505	227.00	495.30	499.36	0.19	60.0	0.40	0.10	0.87	2.17	0.28	191.12	173.26
Lower	1505	518.00	495.30	500.01	0.32	0.18	76'0	0:30	1.41	2.98	0.51	308.42	188.19
Lower	1480	55.00	496.69	498.33	0.70	0.70	2.52			3.62		15.21	55.16
Lower	1480	110.00	496.69	498.69	0.79	0.33	3.14		0.92	3.99		49.31	98.77
Lower	1480	90:00	496.69	498.43	1.51	1.51	8.10	8,10		5.37		16.75	67.05
Lower	1480	163.00	496.69	498.88	0.95	0.40	4.24	0.94	1.21	4.48	0.33	70.20	119.97
Lower	1480	227.00	496.69	499.08	1.07	0.47	5.17	1.12	1.43		0.58	95.94	138.62
Lower	1480	518.00	496.69	499.72	1.33	99'0	7.61	1.72	1.96	5.73	1.22	199,21	183.50
Lower	1460	22.00	496.35	498.21	0.44	0.44	1.30	1.30		2.95		18.66	80.22
Lower	1460	110,00	496.35	498.66	0.33	0.13	06.0	0,18	0.78	2.69	92.0	78.86	140.04
Lower	1460	90:00	496.35	498.53	0.34	0.12	0.90	0.18	0.71	2.67	0.19	61.48	125.78
Lower	1460	163.00	496.35	498.84	0.43	0.17	1.35	0.27	0.99	3.13	0.38	106.38	160.04
Lower	1460	227.00	496.35	499.04	0.50	0.21	1.73	0.35	1.17	3.44	0.50	140.14	179.29
Lower	1460	518.00	496.35	499.68	0.70	0.36	2.97	0.70	1.65	4.25	1.00	264.61	209.69
10,14	4440	00 40	70,00	00000	0,0			0					
Lower	1440	00.00	494.94	498.23	21.0	0.12	0.19	0.19		1.64		33.58	88.56
Lower	1440	J10.00	484.84	488.63	U.1/	90.0	0.36	0.07	0.52	2.05	0.15	91.65	137.35
Lower	1440	00.06	494.94	498.51	0.15	0.05	0.29	90.0	0.44	1.91	0.10	75.43	123.85
Lower	1440	163.00	494.94	498.80	0.27	0.03	0.69	0.13	0.73	2.58	0.25	115.74	155.25
Lower	1440	227.00	494.94	498.98	0.36	0.13	1.09	0.20	0.92	3.02	0.35	145.63	174.94
Lower	1440	518.00	494.94	499.57	0.65	0.28	2.72	0.57	1.50	4.20	0.79	258.58	204.55

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Reach River Sta O Total Min Ch El	River Sta	O Total		W.S. Flow	-lov Shear Chan	Shear Total	Douger Chan	Downer Total	Vel Left	John Chal	Ved Olimba	Class Area	Ton Midth
		(cfs)	€	₩	(lb/saft)	(llb/saff)	(lb/ff s)	(lh/ff s)	(#/8)	(#/6)	(#/e)	(# US)	(#)
Lower	1415	55.00	496.32	498.01	0.64	0.64	221	2.21	,	3.47	/22/	15.85	80.16
Lower	1415	110.00	496.32	498.51	0.45	0.18	1.39	0.29		3.09	0.23	67.51	125.75
Lower	1415	90.00	496.32	498.35	0.51	0.19	1.66	0.35	0.74	3.23	0.08	49.08	109.13
Lower	1415	163.00	496.32	498.61	0.72	0.29	2.86	0.59		3.96	0.37	80.66	136.37
Lower	1415	227.00	496.32	498.76	06.0	0.38	4.07	0.83	14.1	4.50	0.52	102.71	152.53
Lower	1415	518.00	496.32	499.37	1.16	0.57	6.19	1.40		5:35	1.05	210.13	194.97

Lower	1395	22:00	496.01	497.88	0.43	0.43	1.25	1.25		2.91		18.89	16.50
Lower	1395	110.00	496.01	498.07	1.15	0.21	5.58	0.79	0.43	4.85	0.17	29.46	127.86
Lower	1395	90.00	496.01	498.26	0.40	0.11	1.18	0.18	0.57	2.93	0.25	54.50	140.80
Lower	1395	163.00	496.01	498.38	0.87	0.27	3.79	0.62	1.03	4.37	0.46	71.85	149.12
Lower	1395	227.00	496.01	498.59	0.85	0.31	3.74	0.67	1.28	4.41	0.58	106.04	164.28
Lower	1395	518.00	496.01	499.25	96.0	0.45	4.66	1.03	1.86	4.91	0.95	226.70	200.47
Lower	1378	55.00	494.60	497.91	0.12	0.12	0.19	0.19		1.62		33.97	19.02
Lower	1378	110.00	494.60	498.15	0.31	90.0	0.84	0.12	0.31	2.70	0.21	58.30	152.88
Lower	1378	90.00	494.60	498.26	0.16	0.04	0.32	0.05	0,31	1.97	0.21	74.50	156.29
Lower	1378	163.00	494.60	498.34	0.43	0.12	1.40	0.22	09.0	3.24	0.41	88.35	159.14
Lower	1378	227.00	494.60	498.52	0.55	0.18	2.05	0.34	0.85	3.71	0.57	117.38	164.97
Lower	1378	518.00	494.60	499.09	0.93	0.40	4.65	0.96	1.58	4.99	1,04	215.95	183.36
Lower	1355	55.00	495.99	497.70	0.60	09:0	2.02	2.02		3.38		16.28	73.60
Lower	1355	110.00	495.99	498.08	0.42	0.16	1.25	0.24	0.21	2.96	0.89	74.64	154.76
Lower	1355	90.00	495.99	497.81	1.27	1.27	6.35	6.35		4.98		18.05	82.91
Lower	1355	163.00	495.99	498.27	0.50	0.22	1.67	0.34	0.48	3.31	1.10	105.50	166.30
Lower	1355	227.00	495.99	498.45	0.60	0.28	2.18	0.47	69'0	3.66	1.30	135.66	176.85
Lower	1355	518.00	495.99	499.01	0.88	0.47	4.11	1.01	1.27	4.67	1.88	243.79	210.36
												,	
Lower	1338	55.00	495.73	497.60	0.43	0.43	1.26	1.26		2.91		18.87	76.39
Lower	1338	110.00	495.73	498.02	0.32	60:0	0.85	0.11	0.32	2.64	0.72	92.50	215.82
Lower	1338	90.00	495.73	497.91	0.32	0.10	0.82	0.12	0.21	2.59	99.0	70.37	171.31
Lower	1338	163.00	495.73	498.22	0.34	0.13	96'0	0.15	0.56	2.79	0.86	137.40	225.09
Lower	1338	227.00	495.73	498.40	0.38	0.16	1.13	0.20	0.75	2.98	66.0	179.03	233,35
Lower	1338	518.00	495.73	498.97	0.52	0.27	1.87	0.43	1.24	3.63	1.38	319.43	259.29
	2007	i i	00.707	10.107	3,0								
Lower	1320	25.00	494.32	497.64	LL.O	0.11	0.18	0.18		1.61		34.12	83.19
Lower	1325	110.00	494.32	498.00	0.18	0.04	0.36	0.05	0.20	2.06	0.45	105.34	215.13
Lower	1325	90.00	494.32	497.90	0.15	0.04	0.28	0.04	0.12	1.89	0.38	85.08	170.42
Lower	1325	163.00	494.32	498.19	0.24	20.0	0.57	80.0	0.39	2.42	0.61	147.02	223.77
Lower	1325	227.00	494.32	498.36	0:30	0.10	0.84	0.13	0.57	2.77	0.76	185.36	231.43
Lower	1325	518.00	494.32	498.91	0.50	0.22	1.86	0.36	1.09	3.70	1.21	318.78	256.32

HEC-RAS Plan: Prop lower ineff River. Tanyard Branch Reach: Lower (Continued)

Lower 1305 Lower 1305 Lower 1305 Lower 1305 Lower 1305 Lower 1305 Lower 1200 Lower 1290 Lower 1290 Lower 1290 Lower 1290 Lower 1275 Lower 1255 Lower 1250 Lower 1240	(cfs) (55.00 110.00 90.00 227.00	<u> </u>	W.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Vel Left	Vel Chril	Vel Right	Flow Area	Top Width
	(cfs) 55.00 110.00 90.00 163.00				-							
	55.00 110.00 90.00 163.00	(£)	£	(lp/sd ft)	(lþ/sd ft)	(lb/ft.s)	(lb/ft s)	(HVs)	(ft/s)	(#/s)	(# vs)	(#)
	90.00 163.00 227.00	495.71	497.45	0.57	0.57	1.86			3.20	(San)	18 74	(11)
	90.00	495.71	497.88		0.16	166		VC O	70.50	8	1/01	98.09
	163.00	495.71	497.77		0.17	1 46	02.0	t C.	3.40	0.82	66.79	160,53
	227.00	495.71	498.07		0.18	1 00	00.00	0.12	3.10	0.72	52.66	115.75
		495.71	498.26		0.30	200	07.0		3.03	0.99	105.65	218.25
	518 00	405 71	708 02		7 7 7	2.07	25.0		3.61	1.13	148.04	226.91
	2		60.02		0.34	2.84	0.62	1.34	4.14	1.53	283,73	252.66
	55.00	495.45	497.48	0.17	20.0	0.80	000	700	00,			
	110.00	495 45	497 88	200	000	20.00		#O.O.	1.86	0.49	52.46	100.67
	00 06	495 45	497 78	0.21	0000	0.40		0.25	2.16	0.71	104.68	167.25
	163.00	405.45	90 907	2 0	00.00	75.0	0.03	0.20	2.01	0.83	89.26	145.70
	227.00	40E 4E	456.00	0.28	OL.O	0.71	0.12	0.40	2.54	0.89	140.84	217.67
	20,000	24.004	430.24	45.0	0.14	76.0	0.18	0.58	2.85	1.04	180.04	225.71
	00.010	450.45	498.78	0.54	0.27	2.03	0.46	1,13	3.74	1.48	309.53	250.46
	55.00	494 04	497 AR	200	000	6						
	110.00	70707	00 707	0.0	0.00	SO'S	0.02	0.25	1.26	0.27	70.48	107.16
	8	10,101	457.00	/n'n	0.02	0.10	0.02	1.37	1.36	0.38	130.03	189.13
	90.00	434.04	497.78	0.07	0.02	0.10	0.02	1.19	1.34	0.36	111.81	168.52
	103.00	494.04	488.06	90.08	0.03	0.12	0.03	1.58	1.46	0.44	167.91	216.83
	227.05	494.04	498.24	60.0	0.03	0.14	0.04	1.80	1.55	0.49	206.79	225.01
	218.00	484.04	498.77	0.13	90:0	0.25	60.0	2.57	1.90	0.67	333.29	249.79
	00	4. 10.										
	00.00	485.43	497.33	0.41	0.41	1.16	1.16		2.84		19.35	16.61
	110.00	495.43	497.66	0.66	0.15	2.51	0.33	0.31	3.77	0.66	52.04	558.83
	90.00	495.43	497.54	29'0	0.13	2.53	0.36	0.20	3.75	0.41	34.01	378.54
	163.00	495.43	497.89	0.65	0.18	2.46	0.31	0.56	3.81	0.96	93.76	607.19
	227.00	495.43	498.12	0.57	0.19	2.10	0:30	0.76	3.66	1.11	145.03	631 RD
	518.00	495.43	498.70	0.65	0.32	2.68	0.59	1.32	4.09	1.56	281.97	640.50
	00 11	100										
	00.00	490.19	497.30	0.25	0.05	0.57	0.09	0.12	2.29	0.25	33.79	321.45
	00.01	495.19	497.68	0.28	0.09	0.72	0.11	0.35	2.54	0.66	91.63	579.31
	80.00	455.18	497.56	0.28	0.08	0.71	0.10	0.27	2.50	0.56	71.02	561.86
	163.00	495.19	497.89	0.34	0.11	0.94	0.14	0:20	2.80	0.85	130.73	608.44
	227.00	495.19	498.10	0.36	0.14	1.05	0.17	0.64	2.94	0.99	177.68	626 71
LOWER 124U	218.00	495.19	498.66	0.53	0.26	1.97	0.45	1.16	3.72	1.49	307.20	636.50
Lower 1227	25.	A03 78	207.00	900	000	1						
	3 5	400.40	437.32	90.0	70.0	0.11	0.05	0.07	1.38	0.14	52.10	368.26
	8 8	450.70	497.00	cr.o	0.04	0.29	0.04	0.22	1.93	0.41	107.17	578.47
	30.00 30.00	493.78	497.36	0.13	0.03	0.23	0.03	0.16	1.78	0.33	87.81	562.05
	103.00	493.78	497.87	0.21	0.06	0.50	20:0	0.34	2.34	0.59	143.58	605.84
	227.00	493.78	498.07	0.27	0.08	0.70	0.10	0.47	2.64	0.76	188.96	640.70
LOWER 122/	218.00	493.78	498.61	0.47	0.20	1.69	0.32	0.99	3.61	1.26	319.97	646.08

HEC-RAS Plan: Prop lower ineff River: Tanyard Branch Reach: Lower (Continued)

1210 (155) (11)	Reach	River Sta	O Total	Min Ch El	W.S. Flav	ley Shear Chan	Shear Total	Codo como	Danie Teach	27.11.71				
1210 55.00 495.17 447.22 0.30 1210 110.00 495.17 497.60 0.35 1210 1220 1227.00 495.17 497.60 0.35 1210 1227.00 495.17 497.61 0.44 1210 227.00 495.17 497.61 0.44 1210 227.00 495.17 498.64 0.64 1210 227.00 495.17 497.91 0.67 1183 10.00 495.17 497.92 0.46 1183 10.00 495.17 497.92 0.46 1183 227.00 495.17 497.92 0.46 1183 227.00 496.17 497.92 0.46 1183 227.00 496.17 497.92 0.46 1183 227.00 496.17 497.92 0.46 1139 227.00 496.17 497.92 0.25 1139 227.00 496.32 496.75 0.25 1139 227.00 494.32 496.76 0.26 1107 227.00 494.32 496.76 0.44 1107 227.00 494.32 496.76 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 1107 227.00 494.32 496.60 0.44 11080 250.00 494.32 496.60 0.47 11090 110.00 492.91 496.61 0.16 11090 110.00 492.91 496.61 0.16 11090 518.00 492.91 496.61 0.16 11090 518.00 492.91 496.61 0.16 1107 249.20 492.91 496.61 0.16 1107 249.20 492.91 496.61 0.16 11080 518.00 492.91 496.61 0.16 11090 518.00 494.30 0.90 11070 65.00 494.30 0.90 11070 65.00 494.30 0.90 11070 65.00 494.30 0.90 11070 65.00 494.30 0.90 11070 65.00 494.30 0.90 11070 65.00 494.30 0.90 11070 69.00 69.00 11070 69.00 69.00 11070 69.00 69.00 11070 69.00 69.00 11070 69.00 69.00 11070 69.00 11070 69.00 11070 69.00 11070 69.00			(cfs)	(£)	(#)	(lb/saft)	(lb/sq ft)	(lh/ft s)	(lb/ft s)	Yei Leit	Vel Chril	Vel Kight	Flow Area	Top Width
1210	Lower	1210	55.00	495.17	497.22	0.30	0.08	0.74	(mile)	(801)	(10'S)	(TVS)	(sq ft)	(¥)
1210 90.00 495.17 497.47 497.74 497.74 497.74 497.74 497.74 497.74 497.74 497.74 497.74 497.74 497.74 497.74 497.74 497.74 497.74 497.75 497.	Lower	1210	110.00	495.17	497.60	0.35	20.00	7 00 0	. c	0.00	2.48	0.16	28.65	179.29
1210 163.00 495.17 497.79 1210 227.00 495.17 498.01 1210 227.00 495.17 498.01 1210 227.00 495.17 498.01 1210 227.00 495.17 497.19 1210 227.00 495.17 497.72 123.00 495.17 497.72 123.00 495.17 498.42 497.72 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 494.32 496.36 123.00 492.31 496.31 123.00 492.31 496.31 123.00 492.31 496.31 123.00 492.31 496.31 123.00 492.31 496.31 123.00 492.31 496.31 123.00 492.31 496.31 123.00 492.31 496.31 123.00 494.30 496.31 123.00 494.30 496.31 123.00 494.30 496.30 123.00 123.00 494.30 496.30 123.00 123.00 494.30 496.30 123.00 123.00 494.30 496.30 123.00 123.00 494.30 496.30 123.00 123.00 494.30 496.81 123.	Lower	1210	00.06	495 17	497.47	0000 0000	- 6	600	0.13	40.0	2.81	99.0	79.65	567.11
1210 227.00 495.17 498.01	_ower	1210	163.00	495 17	497 79	5,0	2.5	1.02	0.10	0.20	2.81	0.56	59.21	549.14
1210 518.00 496.17 498.54	.ower	1210	227 00	495 17	498.04	0.44	1 0 0	3.5	0.20	0.51	3.13	06.0	114.41	594.86
1193 55.00 495.17 495.34 495.34 495.34 495.34 497.19 495.34 497.19 497.19 497.19 497.19 497.19 497.19 497.19 497.19 497.19 497.19 497.10 495.17 497.22 496.35 496.	Ottoor	1210	649 00	106.12	2000	F 3	0 0	24.	0.22	0.65	3.25	1.06	159.97	625.12
1193 55.00 495.17 497.19 1193 110.00 495.17 497.47 497.39 1193 518.00 495.17 497.32 497.72 1193 518.00 495.17 497.32 496.34 497.32 497.33 4		200	3	430.17	45.54	0.64	0.31	2.63	0.57	1.22	4.09	1.60	282.32	633.13
1193 110.00 495.17 497.47 1193 90.00 495.17 497.39 1193 163.00 495.17 497.32 1193 227.00 495.17 497.32 1193 227.00 495.17 498.42 1193 518.00 494.32 496.36 1139 55.00 494.32 496.86 1139 518.00 494.32 496.86 1107 110.00 494.32 496.86 1107 110.00 494.32 496.86 1107 110.00 494.32 496.86 1107 518.00 494.32 496.81 1108 55.00 494.32 496.81 1109 55.00 494.32 496.81 1107 518.00 494.32 496.81 1109 55.00 494.32 496.81 1090 55.00 492.91 496.81 1090 518.00 492.91 496.81 1090 518.00 492.91 496.81 1090 518.00 492.91 496.32 1070 56.00 494.30 496.33 1070 56.00 494.30 496.33 1070 56.00 494.30 496.31 1070 56.00 494.30 496.31 1070 56.00 494.30 496.31 1070 518.00 494.30 496.31 1070 518.00 494.30 496.31 1070 518.00 494.30 496.31 1070 56.00 494.30 496.31 1070 56.00 494.30 496.83 1070 56.00 494.30 496.83 1070 56.00 494.30 496.83 1070 56.00 494.30 496.83 1070 56.00 494.30 496.83 1070 66.80 494.30 496.83 1070 67.00 494.30 496.83	ower	1193	55.00	495.17	497 19	0.24	700	77.0	000		0		-	
1193 90.00 495.17 497.39 1193 153.00 495.17 497.32 1193 227.00 495.17 498.42 1193 518.00 495.17 498.42 1193 55.00 494.32 496.86 1139 55.00 494.32 496.86 1139 518.00 494.32 496.76 1139 518.00 494.32 496.76 1139 518.00 494.32 496.76 1107 518.00 494.32 496.76 1107 518.00 494.32 496.76 1107 518.00 494.32 496.76 1107 518.00 494.32 496.76 1107 518.00 494.32 496.76 1107 518.00 494.32 496.76 1107 518.00 494.32 496.76 1109 55.00 494.32 496.76 1109 55.00 494.32 496.76 1109 55.00 494.32 496.76 1109 55.00 492.91 496.71 1109 55.00 492.91 496.81 1109 55.00 492.91 496.81 1109 55.00 492.91 496.81 1107 518.00 492.91 496.81 1107 518.00 492.91 496.81 1107 518.00 492.91 496.81 1107 518.00 492.91 496.81 1107 518.00 494.30 496.83 1107 518.00 496.83 1107 518.00 496.83 1107 518.00 496.83 1107 518.00 496.83 1107 518.00 496.83 1107 518.00 496.83 1107 518.00 496.83 1107 518.00 496.83 1107 518.00 496.83 1107 518.00 496.83 1107 518.00 1107 518.00 1108 518.00 1108 518.00 1108 518.00 11	ower	1193	110.00	495 17	77 707	11.0	5 6	1	0.00		2.20	0.04	25.92	96.60
1135 1500 495.17 497.72 1193 227.00 496.17 497.72 1193 227.00 496.17 497.72 1193 227.00 496.17 497.72 1139 55.00 494.32 496.30 496.72 1139 518.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 494.32 496.90 110.00 492.91 496.90 110.00 492.91 496.90 110.00 492.91 496.90 110.00 492.91 496.90 110.00 518.00 492.91 496.90 110.00 518.00 494.30 496.30 100.00 494.30 496.90 110.00 494.30 496.90 110.00 492.91 496.90 110.00 518.00 492.91 496.90 110.00 518.00 492.91 496.90 110.00 650.00 494.30 496.90 110.00 494.30 496.90 110.00 492.91 496.90 110.00 650.00 494.30 496.90 110.00 650.00 494.30 496.90 110.00 650.00 494.30 496.90 110.00 650.00 494.30 496.90 110.00 650.00 494.30 496.90 110.00 650.00 494.30 496.90 110.00 650.00 494.30 496.90 110.00 650.00 494.30 496.90 110.00 650.00 494.30 496.90 110.00 650.00 494.30 496.90 110.00 496.90	Otto	4400	200	130.17	431.41	C+.0	ZL'O	1,4/	0.24		3.27	0.57	55.50	548,68
1183 163.00 495.17 497.72 1183 227.00 495.17 497.92 1183 227.00 495.17 498.42 497.92 496.36 497.12 1139 55.00 494.32 496.30 494.32 496.50 494.32 496.50 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 494.32 496.60 4	-ower	282	30.00	495.17	497.39	0.37	0.03	1.08	0.17		2.94	0.42	46.96	537.79
(1193 227.00 495.17 497.92 (1193 518.00 495.17 498.42 (1173 Culvert 494.32 496.36 (1139 55.00 494.32 496.36 (1139 110.00 494.32 496.36 (1139 163.00 494.32 496.36 (1139 163.00 494.32 496.77 (1139 163.00 494.32 496.16 (1139 518.00 494.32 496.16 (1107 518.00 494.32 496.16 (1107 518.00 494.32 496.16 (1107 518.00 494.32 496.16 (1107 518.00 494.32 496.16 (1107 518.00 494.32 496.19 (1080 55.00 494.32 496.90 (1090 55.00 492.91 496.90 (1090 55.00 492.91 496.90 (1090 518.00 492.91 496.90 <	-ower	1193	163.00	495.17	497.72	0.41	0.12	1.27	0.18	0.42	3.13	0.81	106.29	584 16
r 1193 518.00 495.17 498.42 r 1153 Cul/vert 494.32 496.36 r 1139 55.00 494.32 496.36 r 1139 55.00 494.32 496.36 r 1139 110.00 494.32 496.36 r 1139 163.00 494.32 496.77 r 1139 163.00 494.32 496.76 r 1139 518.00 494.32 496.16 r 1107 55.00 494.32 496.16 r 1107 518.00 494.32 496.81 r 1107 518.00 494.32 496.81 r 1090 55.00 492.91 496.91 r 1090 55.0	.ower	1193	227.00	495.17	497.92	0.46	0.14	1.54	0.22	0.57	3.37	1.02	147 10	613 79
r 1153 Culvert r 1139 55.00 494.32 496.35 r 1139 55.00 494.32 496.36 r 1139 110.00 494.32 496.36 r 1139 163.00 494.32 496.77 r 1139 163.00 494.32 497.12 r 1139 518.00 494.32 497.12 r 1107 55.00 494.32 496.66 r 1107 56.00 494.32 496.16 r 1107 56.00 494.32 496.16 r 1107 518.00 494.32 496.60 r 1107 518.00 494.32 496.90 r 1107 518.00 494.32 496.90 r 1107 518.00 494.32 496.90 r 1090 55.00 492.91 496.90 r 1090 518.00 492.91 496.93<	-ower	1193	518.00	495.17	498.42	0.74	0.31	3.26	0.62	1.15	4.42	1,66	260.78	631.35
r 1153 Cullvert r 1139 55.00 494.32 496.36 r 1139 55.00 494.32 496.36 r 1139 110.00 494.32 496.30 r 1139 163.00 494.32 496.71 r 1139 163.00 494.32 497.12 r 1139 227.00 494.32 497.12 r 1139 55.00 494.32 497.88 r 1107 518.00 494.32 496.60 r 1107 518.00 494.32 496.60 r 1107 518.00 494.32 496.91 r 1107 518.00 494.32 496.91 r 1107 518.00 494.32 496.91 r 1107 518.00 492.91 496.91 r 1090 55.00 492.91 496.93 r 1090 518.00 492.91 496.												3	2.00	3
r 1139 55.00 494.32 496.35 r 1139 110.00 494.32 496.36 r 1139 10.00 494.32 496.36 r 1139 163.00 494.32 497.12 r 1139 163.00 494.32 497.12 r 1139 518.00 494.32 497.88 r 1107 55.00 494.32 496.66 r 1107 56.00 494.32 496.16 r 1107 56.00 494.32 496.16 r 1107 518.00 494.32 496.76 r 1107 518.00 494.32 496.96 r 1107 518.00 494.32 496.96 r 1107 518.00 492.91 496.96 r 1090 55.00 492.91 496.93 r 1090 518.00 492.91 496.93 r 1090 518.00 </td <td>-ower</td> <td>1153</td> <td>Culvert</td> <td></td>	-ower	1153	Culvert											
r 1139 55.00 494.32 496.36 r 1139 110.00 494.32 496.30 r 1139 90.00 494.32 496.30 r 1139 163.00 494.32 497.12 r 1139 227.00 494.32 497.32 r 1139 518.00 494.32 497.88 r 1107 55.00 494.32 497.88 r 1107 55.00 494.32 496.66 r 1107 56.00 494.32 496.66 r 1107 518.00 494.32 496.66 r 1107 518.00 494.32 496.66 r 1107 518.00 494.32 496.91 r 1107 518.00 492.91 496.91 r 1090 55.00 492.21 496.93 r 1090 518.00 492.91 496.93 r 1090 518.00 </td <td></td>														
r 1139 110.00 494.32 496.90 r 1139 90.00 494.32 496.77 r 1139 163.00 494.32 497.12 r 1139 227.00 494.32 497.88 r 1139 55.00 494.32 497.88 r 1107 55.00 494.32 496.16 r 1107 56.00 494.32 496.16 r 1107 56.00 494.32 496.16 r 1107 518.00 494.32 496.16 r 1107 518.00 494.32 496.16 r 1107 518.00 494.32 496.19 r 1090 55.00 492.91 496.61 r 1090 55.00 492.91 496.93 r 1090 518.00 492.91 496.93 r 1070 55.00 494.30 496.30 r 1070 494.30 <td>.ower</td> <td>1139</td> <td>55.00</td> <td>494.32</td> <td>496.35</td> <td>0.23</td> <td>0.03</td> <td>0.53</td> <td>0.07</td> <td></td> <td>2.29</td> <td>800</td> <td>28 10</td> <td>420.20</td>	.ower	1139	55.00	494.32	496.35	0.23	0.03	0.53	0.07		2.29	800	28 10	420.20
r 1139 90.00 494,32 496.77 r 1139 163.00 494,32 497.12 r 1139 227.00 494,32 497.88 r 1139 518.00 494,32 497.88 r 1139 518.00 494,32 497.88 r 1107 55.00 494,32 496.16 r 1107 50.00 494,32 496.16 r 1107 110.00 494,32 496.60 r 1107 518.00 494.32 496.91 r 1107 518.00 494.32 496.91 r 1107 518.00 492.91 496.61 r 1090 55.00 492.91 496.61 r 1090 518.00 492.91 496.63 r 1090 518.00 492.91 496.93 r 1070 55.00 492.91 496.93 r 1070 494.30<	ower.	1139	110.00	494.32	496.90	0.24	60.0	0.60	0,12		2.46	800	83.72	26.63
1139 163.00 494.32 497.12 1139 227.00 494.32 497.32 1139 518.00 494.32 497.88 1107 55.00 494.32 496.16 1107 110.00 494.32 496.16 1107 90.00 494.32 496.60 1107 227.00 494.32 496.60 1107 227.00 494.32 496.81 1107 227.00 494.32 496.81 1090 55.00 492.91 496.19 1090 110.00 492.91 496.81 1090 163.00 492.91 496.81 1090 163.00 492.91 496.83 1090 55.00 492.91 496.83 1070 55.00 492.91 496.83 1070 55.00 494.30 496.93 1070 65.00 494.30 496.43 1070 66.00 496.30 496.83 <	ower	1139	90.00	494.32	496.77	0.22	0.07	0.52	60.0		2.54	0.54	20.00	30.00
r 1139 227.00 494.32 497.32 r 1139 518.00 494.32 497.88 r 1107 55.00 494.32 496.16 r 1107 110.00 494.32 496.16 r 1107 110.00 494.32 496.16 r 1107 110.00 494.32 496.50 r 1107 227.00 494.32 496.50 r 1107 518.00 494.32 496.91 r 1107 518.00 492.91 496.19 r 1090 55.00 492.91 496.61 r 1090 518.00 492.91 496.93 r 1090 518.00 492.91 496.93 r 1090 518.00 492.91 496.93 r 1070 55.00 492.91 496.93 r 1070 494.30 496.43 496.43 r 1070 494.3	ower	1139	163.00	494.32	497.12	0.23	0.08	0.55	0.09	0.36	239	0.75	142.70	738.02
1139 518.00 494.32 497.88 1107 55.00 494.32 496.16 1107 110.00 494.32 496.60 1107 90.00 494.32 496.60 1107 163.00 494.32 496.84 1107 227.00 494.32 496.94 1107 227.00 494.32 497.57 1090 55.00 492.91 496.19 1090 110.00 492.91 496.19 1090 110.00 492.91 496.81 1090 163.00 492.91 496.81 1090 163.00 492.91 496.83 1090 518.00 492.91 496.83 1070 55.00 492.91 496.83 1070 55.00 492.91 496.43 1070 494.30 496.43 1070 494.30 496.83 1070 494.30 496.83	ower	1139	227.00	494.32	497.32	0.29	0.12	080	0.15	0.00	20.2 77.0	2.0	477.00	3/0.20
1107 55.00 494.32 496.16 1107 110.00 494.32 496.16 1107 90.00 494.32 496.60 1107 163.00 494.32 496.94 1107 227.00 494.32 496.94 1107 227.00 494.32 497.10 1090 55.00 492.91 496.19 1090 55.00 492.91 496.61 1090 163.00 492.91 496.61 1090 163.00 492.91 496.89 1090 518.00 492.91 496.89 1070 55.00 492.91 496.89 1070 55.00 494.30 496.43 1070 494.30 496.43	ower	1139	518.00	494.32	497 AR	0.54	30.0	800	2.5	0.43	2.74	45.0	1/7.32	285.77
1107 55.00 494.32 496.16 1107 110.00 494.32 496.76 1107 90.00 494.32 496.60 1107 163.00 494.32 496.94 1107 227.00 494.32 497.10 1107 518.00 494.32 497.10 1090 55.00 492.91 496.19 1090 110.00 492.91 496.19 1090 163.00 492.91 496.80 1090 163.00 492.91 496.93 1090 518.00 492.91 496.93 1070 55.00 492.91 496.93 1070 55.00 494.30 496.43 1070 494.30 496.43				2	25: 15:	1	67.0	50.2	2.44	18.0	3.8	1.57	291.09	614.21
1107 110.00 494.32 496.76 1107 90.00 494.32 496.60 1107 227.00 494.32 496.94 1107 227.00 494.32 497.10 1107 227.00 494.32 497.10 1090 55.00 492.91 496.19 1090 110.00 492.91 496.19 1090 163.00 492.91 496.61 1090 163.00 492.91 496.93 1090 518.00 492.91 496.93 1070 55.00 492.91 496.93 1070 55.00 494.30 496.43 1070 494.30 496.43 1070 494.30 496.43		1107	55.00	494.32	496 16	0.48	970	1 20	00.4					
1107 90.00 494.32 496.60 1107 227.00 494.32 496.94 1107 227.00 494.32 497.10 1107 227.00 494.32 497.10 1090 55.00 492.91 496.19 1090 110.00 492.91 496.19 1090 163.00 492.91 496.61 1090 163.00 492.91 496.61 1090 227.00 492.91 496.93 1070 55.00 492.91 496.93 1070 55.00 494.30 496.43 1070 56.00 494.30 496.43 1070 110.00 494.30 496.83 1070 496.83 496.83		1107	110.00	494 37	AC 76	2 77	2 5	3 8	00.7		30.5		18.31	16.35
1107 163.00 494.32 496.94 1107 227.00 494.32 496.94 1107 227.00 494.32 497.10 1090 55.00 492.91 496.19 1090 55.00 492.91 496.19 1090 90.00 492.91 496.61 1090 103.00 492.91 496.93 1090 227.00 492.91 496.93 1090 518.00 492.91 497.08 1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 163.00 494.30 496.83		1107	00 00	20,1707	2000	14.0	0.12	1.23	0.18	0.35	3.02	0.53	77.74	283.14
1107 103.00 494.32 496.34 1107 227.00 494.32 497.10 1090 55.00 492.91 496.19 1090 55.00 492.91 496.19 1090 100.00 492.91 496.19 1090 100.00 492.91 496.61 1090 163.00 492.91 496.93 1090 227.00 492.91 496.93 1090 518.00 492.91 497.08 1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 163.00 494.30 496.83		1407	35.65	454.32	490.00	0.44	0.11	1.34	0.19	0.28	3.07	0.42	53.61	204.58
1107 227.00 494.32 497.10 1107 518.00 494.32 497.57 1090 55.00 492.91 496.19 1090 110.00 492.91 496.19 1090 1000 492.91 496.76 1090 163.00 492.91 496.93 1090 227.00 492.91 496.93 1090 518.00 492.91 497.08 1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 163.00 494.30 496.88		1107	103,00	494.32	486.94	0.54	0.18	1.90	0.28	0.54	3.53	0.73	107.80	369.03
1107 518.00 494.32 497.57 1090 55.00 492.91 496.19 1090 110.00 492.91 496.19 1090 1000 492.91 496.76 1090 163.00 492.91 496.61 1090 227.00 492.91 496.93 1090 518.00 492.91 497.08 1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 163.00 494.30 496.88		/011	227.00	494.32	497.10	29.0	0.25	2.67	0.42	0.74	3.99	0.92	138.47	441.19
1090 55.00 492.91 496.19 1090 110.00 492.91 496.76 1090 90.00 492.91 496.61 1090 163.00 492.91 496.93 1090 227.00 492.91 497.08 1090 518.00 492.91 497.51 1070 55.00 494.30 495.97 1070 110.00 494.30 496.30 1070 163.00 494.30 496.88	awei	110/	518.00	494.32	497.57	1.23	0.58	6.93	1.31	1.43	5.61	1.55	229.21	604.80
1090 110,00 492,91 496,76 1090 110,00 492,91 496,76 1090 90,00 492,91 496,63 1090 227,00 492,91 497,08 1090 518,00 492,91 497,08 1070 55,00 494,30 495,97 1070 110,00 494,30 496,43 1070 163,00 494,30 496,88		1090	25.00	100 001	408 408	C, C	OF C	0						
1030 110,00 492,31 496,10 1090 90,00 492,91 496,61 1090 163,00 492,91 496,83 1090 227,00 492,91 497,08 1090 518,00 492,91 497,51 1070 55,00 494,30 495,97 1070 90,00 494,30 496,43 1070 163,00 494,30 496,88		1000	440.00	20.00	2 200	21.0	21.0	270	0.25		1.85		33.34	18.85
1030 492.91 496.81 1080 163.00 492.91 496.83 1080 227.00 492.91 497.08 1080 518.00 492.91 497.51 1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 163.00 494.30 496.88		1000	3 8	492,91	430.75	0.17	0.05	0.36	90.0	0.20	2.07	0.40	94.65	286.12
1090 163.00 492.91 496.93 1080 227.00 492.91 497.08 1080 518.00 492.91 497.51 1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 163.00 494.30 496.88		200	30.00	+92.91	450.01	0.16	0.04	0.32	0.05	0.15	1.97	0.29	71.83	214.38
1090 227,00 492.91 497.08 1090 518.00 492.91 497.51 1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 163.00 494.30 496.88		OSO!	163.00	492.91	496.93	0.27	0.07	69'0	0.10	0.32	2.59	09.0	123.46	378.70
1090 518.00 492.91 497.51 1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 90.00 494.30 496.30 1070 163.00 494.30 496.88		1030	227.00	492.91	497.08	0.37	0.10	1.12	0.15	0.45	3.07	0.80	156.15	475.11
1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 90.00 494.30 496.30 1070 163.00 494.30 496.88		1090	518.00	492.91		0.75	0.28	3.36	0.57	1.06	4.50	1.44	257.46	635.14
1070 55.00 494.30 495.97 1070 110.00 494.30 496.43 1070 90.00 494.30 496.30 1070 163.00 494.30 496.68														
1070 110.00 494.30 496.43 1070 90.00 494.30 496.30 1070 163.00 494.30 496.88		1070	55.00	494.30		0.66	99.0	2.34	2.34		3.53		15.56	15.67
1070 90.00 494.30 496.30 1070 163.00 494.30 496.68		0/01	110.00	494.30	496.43	0.98	0.20	4.45	0.65	0.48	4.53	0.45	33,99	133.81
1070 163.00 494.30 496.68		0/01	90.00	494.30	496.30	0.91	0.91	3.93	3.93		4.30		20.94	16.99
		10/0	163.00	494.30	496.68	0.91	0.25	4.05	0.59	0.87	4.48	0.95	70.37	261.55
Lower 1070 227.00 494.30 496.83 1.06		1070	227.00	494.30	496.83	1.06	0.33	5.20	0.78	1.12	4.91	1.25	95.68	335.73

HEC-RAS Plan: Prop lower ineff River: Tanyard Branch Reach: Lower (Continued)

DO SAICE CONTRACTOR			- 201	Creat Creat	-						-	
	\vdash	15 (4)	W.O. ERW	Olical Crian	Shear lotai	Power Chan	Power Total	Vel Left	Vel Chri	Vel Right	Flow Area	Top Width
1000 1000	(CIS)	(H)	(H)	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(£/s)	(ff/s)	(ft/s)	(sq ft)	€
	00.8100	494.30	497.40	1.00	0.42	5.00	66'0	1.74	5.00	1.11	221.45	597.23
Lower 1055	55.00	494 04	70 AOA	17.0	į							
	110.00	404.04	20.00	0.47	0.47	1.41	1.41		3.02		18.22	16.33
	00.00	10,101	430,43	45.0	0.11	0.93	0.15	0.32	2.75	0.68	79.97	554.08
	20.00	3	450.01	0.40	0.11	1.17	0.18	0.26	2.93	0.56	54.15	536.11
	87.8	484.04	450.63	0.49	0.17	1.62	0.27	0.47	3.34	0.94	102.55	568.15
	227.00	484.04	486.80	0.59	0.22	2.21	0.38	0.64	3.74	1.18	132.11	584.90
	00,810	494.04	497.31	0.91	0,40	4.42	0.85	1.19	4.83	1.84	241.96	633.05
10Mpr	93	00 007	1 47									
	25.00	492.63	495.91	0.12	0.12	0.20	0.20		1.65		33,34	18.85
	110.00	492.63	496,49	0.15	0.04	0.29	0.04	0.28	1.93	0.40	111 59	588 64
	00.06	492.63	496.32	0.15	0.04	0.29	0.04	0.20	1.91	0.31	08.08	574 04
	163.00	492.63	496.62	0.24	20.0	0.60	60.0	0.41	247	03.0	20.00	0,4.8
	227.00	492.63	496.78	0.33	0.11	0.95	0.14	920	7 00 0	0.00	137.17	599.34
Lower 1040	518.00	492.63	497.25	0.64	0.26	2.66	070	5 5	2,4	7.7.0	CC.50	612.15
							P S	-	4.17	1.3/	2/6.94	632.55
Lower 1020	55.00	494.02	495.69	0.66	990	2.35	200		i			
Lower 1020	110.00	494.02	496.06	1.24	0.19	8.33	07.0	700	40.0	0	15.55	15.67
	00'06	494.02	495.99	0.95	0.95	4 18	2.5	#2.0	20.00	07.70	26.26	394.05
	163.00	494.02	496.37	0.92	0.26	4 12	0.57	33.0	9,4	0	20.54	16.89
	227.00	494.02	496.52	1.08	0.35	534	0.79	78.0	24.4	0.30	12.67	572.14
Lower 1020	518.00	494.02	496.91	1.77	07.0	11.81	000	5 5	† C	97.1	3.5	586.75
						5	20.1	6.	0.00	2.23	183.10	626.27
	55.00	493.71	495.55	0.46	0.46	1 36	4.00		000			
Lower 1000	110.00	493.71	496.17	0.29	200	74 0	000	000	2.33		18.39	16.37
Lower 1000	90.00	493.71	495.97	0.42	0 11	1 90	0,00	0.38	2.55	0.63	97.78	653.32
Lower 1000	163.00	493.71	496.32	0.35		3 6	0.00	0.20	3.00	0.55	51.83	532.18
Lower 1000	227.00	493 71	496.43	0.00	- 4	3.	0.13	0.59	2.84	0.81	135.96	656,32
Lower 1000	518.00	493.71	408.00	740	0.00	44.	0.21	0.79	3.24	1.00	166.32	658.68
		1,000	200.000	\$ i	0.0	2.56	0.53	1.36	4.02	1.50	289.33	668.02
Lower 985	55.00	492.30	495.59	0.12	010	0.10	0,0					
Lower 985	110.00	492.30	406.18	1 2 2	2 00	500	2		1.64		33.52	18.90
	0006	492 30	405.00	2 4	0.03	0.24	0.03	0.30	1.81	0.37	131.09	653.27
	163.00	702 30	00.004	0.13	0.03	0.23	0.03	0.20	1.90	0:30	86,55	643.88
	20.00	400.00	450.30	8.0	co.o	0.43	0.05	0.46	2.21	0.52	166.03	656.02
	22.00	492.30	496.41	0.28	0.09	92.0	0.10	0.63	2.69	69.0	192.84	658.10
	210.00	492.30	496.84	0.54	0.22	2.07	0.38	1.18	3.82	1.22	305.99	666.73
Lower 960	- 25 m	403 EB	36 304	1000	L							
	410.00	20.00	490.30	co.n	0.65	2.25	2.25		3.49		15.75	15.72
	3 6	493.00	450.03	1.48	1.48	8.08	8.08		5.45		20.19	16.81
	30.00	493.00	490.62	1.01	1.01	4.52	4.52		4.49		20.05	16.78
Ower Oct	103.00	493.58	496.12	0,65	0.12	2.49	0.19	0.50	3.82	0.93	102.37	752.44
	CO. 777	483.68	496.22	0.78	0.18	3.28	0.29	0.77	424	1 16	136.08	6,

HEC-RAS Plan: Prop lower ineff River. Tanyard Branch Reach: Lower (Continued)

W.S. Elva (Near Chan) Shear Total (Infrag) (Infrag th) (Infrag th) (Infrag th)		ċ				1								
1900 1915	i como	go pan	E COL		VV.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Vel Left	Vel Chril	Vel Right	Flow Area	Top Width
124 124 125 124 125 124 125 124 125 124 125 124 125 124 125		000	(cis)	(E)	£	(lb/sq ft)	(lp/sd ft)	(lb/fft s)	(lb/fts	(ft/s)	(£/\dagger)	(\$/JJ)	(sq ft)	(£)
935 55.00 493.32 495.50 0.42 0.42 1.23 1.23 1.23 935 110.00 483.32 485.50 0.28 0.07 0.62 0.07 0.62 0.07 935 110.00 483.32 486.50 0.28 0.10 0.12 0.10 0.15 935 158.00 483.22 486.51 0.28 0.10 0.07 0.06 0.07 935 518.00 483.32 486.71 0.23 0.11 0.02 0.12 0.07 0.05 0.07 915 518.00 481.31 486.72 0.15 0.02 0.04 0.02 916 518.00 481.31 486.50 0.15 0.02 0.04 0.05 0.07 0.05<	Lower	200	518.00	493.68	496.78	0.52	0.21	1.87		1.24	3.60	1.30	337.15	765,52
915 150 453,22 465,28 0.02 0.07 0.08 0.09 0.04 915 150 453,22 465,38 0.02 0.07 0.08 0.07 0.08 0.07 915 150 453,22 465,38 0.23 0.13 0.10 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.08 0.07 0.09 0.07 0.09 0.07 0.09 0.07 0.09 0.07 0.09 0.07 0.09 0.07 0.09 0.07 0.09 <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>														
1,000 1,00	Lower	935	25.00	493.32	495.20	0.42	0.42	1.23			2.89		19.01	16.53
1835 183 000 4893 22 445 655 0.29 0.07 0.69 0.09 0.037 1835 183 000 4893 22 445 614 0.28 0.13 0.105 0.16	Lower	935	110.00	493.32	495.78	0.26	20.0	0.62		0.45	2.41	0.60	105.52	624 85
1836 183.00 483.22 485.84 0.23 0.10 0.66 0.12 0.06 0.12 0.06 0.12 0.06 0.12 0.06 0.12 0.06 0.12 0	Lower	935	90.00	493.32	495.65	0.28	20.0	0.69		0.37	2.47	0.50	78 97	644.04
1955 127.00 463.22 466.11 0.05 0.13 1.100 0.16 0.78 1956 1950 461.91 466.22 0.15 0.012 0.022 1.46 0.034 1.21 1915 1950 461.91 466.24 0.14 0.024 0.025 0.04 0.025 1915 1910 461.91 466.54 0.14 0.024 0.025 0.024 0.02 1915 1910 461.91 466.54 0.14 0.024 0.025 0.024 0.02 1915 1910 461.91 466.54 0.14 0.024 0.025 0.024 0.07 0.024 1915 1910 461.91 466.54 0.024 0.025 0.024 0.02 0.024 0.02 1915 1910 461.91 466.54 0.024 0.02 0.024 0.02 0.024 0.02 1915 1910 461.91 466.54 0.024 0.02 0.024 0.02 0.024 0.02 1915 1910 463.22 466.54 0.02 0.02 0.02 0.02 0.02 0.02 0.02 1915 1910 463.22 466.54 0.02 0.02 0.02 0.02 0.02 0.02 1915 1910 463.22 466.54 0.02 0.02 0.02 0.02 0.02 0.02 1915 1910 463.22 466.54 0.02 0.02 0.02 0.02 0.02 0.02 0.02 1915 1910 463.22 466.54 0.02 0.02 0.02 0.02 0.02 0.02 0.02 1916 1910 463.20 466.54 0.02 0.	Lower	935	163.00	493.32	495.94	0.32	0.10	0.85		0.61	270	0.78	10.07	17.110
915 518.00 483.20 486.70 0.46 0.22 1.48 0.34 1.21 915 165.00 481.91 486.72 0.15 0.01 0.02 0.03 0.02 0.03 0.03 0.03 0.04 0.03 0.04 0.03 0.04 0.03 0.04 0.03 0.04 0.03 0.04 0.04 0.03 0.04	Lower	935	227.00	493.32	496.11	0.35	0.13	100		92.0	0.4	0.70	145.00	043.2
1 1 4	Lower	935	518.00	493.32	498 70	0.43	2 2	20.		00	2.00	0.92	186.89	652.24
916 \$5.00 491.91 496.22 0.12 0.12 0.19 0.19 0.19 1 915 \$10.00 491.91 496.75 0.14 0.14 0.02 0.05 0.05 0.05 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.03 0.02 0.03 0.02 0.03 0.03 0.04 0.03 0.04 0.04 0.03 0.04 0.04 0.05 0.04 0.04 0.04 0.04 0.05				10000	2	P o	0.22	1.40		1.21	3.35	1.33	338.63	663.99
915 110.00 481.51 485.52 0.14 0.12 0.15 0.14 0.29 0.04 0.29 1915 90.00 481.91 485.84 0.14 0.03 0.05 0.04 0.29 0.04 0.29 0.04 0.29 0.04 0.29 0.04 0.29 0.04 0.29 0.04 0.29 0.04 0.29 0.04 0.05 0.04 0.02 0.04 0.05 0.04 0.05 0.04 0.02 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.05 0.04 0.05	Lower	915	55.00	491 91	405 22	0.4.0	6	9						
915 9100 491131 455.75 0.14 0.03	, out of	945	200	10.104	77.054	0.12	0.12	0.19			1.62		33.96	19.02
17 915 9100 461 ST 0,14 0,03 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,02 0,00 0,02	Owel	910	J10.001	491.91	495.75	0.15	0.04	0.29	0.04	0.29	1.93	0.39	115.48	620.18
71 515 163.00 491.51 465.60 0.028 0.08 0.64 0.07 0.043 915 227.00 491.51 466.65 0.23 0.04 0.19 0.58 0.07 0.08 0.04 0.01 0.08 0.04 0.08 0.06 0.08 0.07 0.09 0.08 0.07 0.09 0.08 0.07 0.09 0.08 0.07 0.09 0.08 0.07 0.09 0.08 0.06 0.09	-ower	915	80.00	491.91	495.64	0.14	0.03	0.25	0.03	0.21	1.82	0.31	91.20	606 53
1 5 5 5 5 0 0 49 1.51 496 05 0.29 0.09 0.01 0.05 0.09 0.01 0.05 0.09 0.01 0.05 0.	ower	915	163.00	491.91	495.90	0.23	90'0	0.54	20.0	0.43	2.38	0.56	148 93	637 74
915 518.00 491.91 496.63 0.44 0.19 1.52 0.29 1.07 880 55.00 493.29 495.44 0.58 0.59 1.57 1.57 1.07 890 110.00 493.29 495.44 0.88 0.73 0.45 0.78 0.71 3.13 0.49 0.78 890 110.00 493.29 495.67 0.79 0.73 3.13 0.49 0.76 890 518.00 493.29 495.67 0.79 0.22 2.20 0.49 0.78 890 518.00 493.29 496.54 0.69 0.29 0.29 0.78 0.79 0.73 0.86 0.89 0.72 0.89 0.78 <td>-ower</td> <td>915</td> <td>227.00</td> <td>491.91</td> <td>496.05</td> <td>0.29</td> <td>0.09</td> <td>0.81</td> <td>0.11</td> <td>0.58</td> <td>3.75</td> <td>0.73</td> <td>20.04</td> <td>200.00</td>	-ower	915	227.00	491.91	496.05	0.29	0.09	0.81	0.11	0.58	3.75	0.73	20.04	200.00
890 55.00 483.29 495.01 0.59 0.59 1.87 1.87 1.87 890 110.00 483.29 495.01 0.59 0.17 3.88 0.46 0.28 890 110.00 483.29 495.67 0.78 0.17 3.31 0.45 0.58 890 163.00 483.29 495.67 0.79 0.73 3.31 0.46 0.16 890 227.00 483.29 495.67 0.79 0.21 2.21 0.36 0.86 890 55.00 483.29 495.67 0.79 0.21 2.21 0.36 0.86 875 55.00 483.29 496.54 0.56 0.74 1.72 0.39 0.26 875 55.00 483.09 496.54 0.51 0.16 1.72 0.39 0.28 875 518.00 483.09 496.54 0.75 0.75 0.75 0.75 0.76 0.17 0.39 0.28	ower.	915	518.00	491.91	496.63	0.44	0.19	1.52	0.00	1 07	2.47	2 0	100.04	001.00
890 55.00 493.29 495.01 0.59 0.59 1.97 1.97 1.97 880 110.00 483.29 495.61 0.68 0.13 3.13 0.45 0.28 880 110.00 483.29 495.67 0.78 0.13 3.13 0.45 0.15 890 158.00 483.29 495.80 0.67 0.22 2.61 0.39 0.06 890 55.00 483.29 496.50 0.67 0.29 2.28 0.49 0.66 890 55.00 483.29 496.54 0.59 0.29 2.28 0.49 1.30 875 110.00 483.09 496.54 0.65 0.73 0.28 0.73 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>3</td> <td>5</td> <td>ř</td> <td>0</td> <td>004.10</td> <td>LC:700</td>									3	5	ř	0	004.10	LC:700
890 110 tool 483.28 485.44 0.089 0.17 3.88 0.46 0.28 890 180.00 493.29 485.45 0.78 0.13 3.31 0.43 0.16 890 163.00 493.29 486.67 0.59 0.28 0.28 0.08 890 227.00 493.29 486.67 0.59 0.28 0.28 0.69 0.89 875 518.00 493.29 486.54 0.59 0.28 0.28 0.49 1.30 875 518.00 493.09 484.31 0.68 0.73 0.28 0.28 0.73 0.73 875 10.00 493.09 485.33 0.46 0.12 1.39 0.23 0.28 875 10.00 493.09 485.68 0.73 0.29 0.29 0.24 0.73 875 518.00 483.09 485.69 0.72 0.29 0.20 0.27 0.24 885 56.	ower	890	55.00	493.29	495.01	0.59	0.59	197	1 97		3 25		40.44	40 LT
890 90.00 493.28 495.35 0.78 0.13 3.13 0.48 0.15 890 163.00 493.29 495.67 0.79 0.21 3.31 0.39 0.05 890 227.00 493.29 495.50 0.67 0.29 2.28 0.49 1.30 890 518.00 493.29 496.54 0.59 0.28 0.28 0.84 890 518.00 493.09 494.91 0.48 0.48 1.48 1.48 1.30 0.65 875 55.00 493.09 495.33 0.45 0.12 2.28 0.48 1.30 875 165.00 493.09 495.61 1.00 0.38 4.80 0.61 0.12 0.23 0.26 875 518.00 493.09 495.61 1.01 0.38 4.80 0.61 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78 0.78	ower	890	110.00	493.29	495.44	0.89	0.17	3.88	0.45	0.08	5.33	22.0	10.41	15.88
890 163.00 493.29 495.67 0,79 0,27 3.31 0.39 0.06 890 277.00 493.29 495.90 0,67 0,29 2.61 0.38 0.08 890 277.00 493.29 496.54 0,59 0,29 2.28 0,49 1.30 875 55.00 483.09 494.91 0,48 0,48 1.48 1.48 1.30 875 110.00 493.09 495.33 0,45 0,73 0,28 0,28 0,28 875 163.00 493.09 495.53 0,45 0,12 1.39 0,28 0,28 875 163.00 493.09 495.53 0,45 0,12 0,12 0,13 0,18 0,48 875 163.00 493.09 495.60 0,19 0,28 2,97 0,54 0,48 875 160.00 491.68 495.60 0,19 0,12 0,12 0,12 0,14 0,18 0	ower	980	90.00	493.29	495.35	0.78	0.13	3.13	0.43	0.15	4.03	200	40.13	429.01
890 227,00 495,29 495,46 0.67 0.22 2.61 0.36 0.84 890 518.00 495,29 496,54 0.59 0.26 2.28 0.49 1.30 875 55.00 493,09 494,91 0.48 0.46 0.14 1.72 0.30 0.53 875 100,00 493,09 495,41 0.51 0.16 1.72 0.30 0.53 875 163,00 493,09 495,54 0.73 0.12 1.72 0.20 0.53 0.58 875 163,00 493,09 495,54 0.73 0.73 0.54 0.78 0.54 0.78 0.54 0.54 0.78 0.50 0.58 0.59 0.51 <td>эжег</td> <td>068</td> <td>163.00</td> <td>493.29</td> <td>495.67</td> <td>0.79</td> <td>0.21</td> <td>3.31</td> <td>0.39</td> <td>0.65</td> <td>1.0.4</td> <td>0.00</td> <td>27.10</td> <td>212.83</td>	эжег	068	163.00	493.29	495.67	0.79	0.21	3.31	0.39	0.65	1.0.4	0.00	27.10	212.83
890 518.00 499.29 496.54 0.59 0.28 2.28 0.49 1.30 875 55.00 483.09 494.41 0.48 0.44 1.48 1.30 875 110.00 483.09 495.31 0.45 0.12 1.72 0.30 0.33 875 163.00 483.09 495.53 0.45 0.12 1.39 0.26 0.26 875 163.00 483.09 495.56 0.73 0.26	JAM6E	890	227.00	493.29	495.90	0.67	0.22	2.61	98.0	0.84	300	4 000	407.00	010.09
875 55.00 483.09 494.91 0.48 0.48 1.48 0.33 0.33 0.33 0.33 0.33 0.28	wer	890	518.00	493.29	496.54	65'0	0.28	2.28	0.49	130	20.0	1 70	05.700	036.37
875 55.00 493.09 494.91 0.48 0.48 1.48 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.38 0.38 0.38 0.38 0.38 0.38 0.38 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.39 0.38 0.38 0.39									2	3	8	64.1	733.78	997,99
975 110.00 493.09 495.41 0.5f 0.15 1.72 0.03 0.33 875 90.00 493.09 495.53 0.45 0.12 1.39 0.23 0.26 875 90.00 493.09 495.56 0.73 0.26 2.97 0.54 0.48 875 227.00 493.09 495.66 1.00 0.38 4.80 0.91 0.63 875 227.00 493.09 495.66 1.00 0.38 4.80 0.91 0.63 875 518.00 491.68 496.10 1.91 0.84 1.21 2.74 1.21 865 55.00 491.68 494.95 0.12 0.05 0.06 0.07 0.19 865 160.00 491.68 495.44 0.21 0.05 0.06 0.16 0.07 0.19 865 163.00 491.68 495.46 0.21 0.05 0.06 0.05 0.05 0.06 0.0	wer	875	55.00	493.09	494.91	0.48	0.48	1.48	1 48		90,0		10.54	
875 90.00 493.09 496.33 0.45 0.12 1.02 0.20 20.00 496.30 496.55 0.73 0.26 2.97 0.26 0.73 0.26 2.97 0.26 0.78 0.26 0.78 0.26 0.78 0.26 0.78 0.26 0.78 0.26 0.78 0.26 0.78 0.26 0.78	wer	875	110.00	493.09	495.41	0.51	0.16	170	0.30	66.0	200	000	CS. 7-1	19.2/
875 163.00 493.09 495.56 0.73 0.15 0.15 0.150 875 227.00 493.09 495.68 1.00 0.38 4.80 0.54 0.64 875 227.00 493.09 495.68 1.00 0.38 4.80 0.91 0.63 885 55.00 491.68 496.74 0.21 0.05 0.46 0.07 0.19 885 90.00 491.68 496.74 0.21 0.06 0.05 0.05 0.15 885 90.00 491.68 496.78 0.15 0.05 0.05 0.05 885 227.00 491.68 496.79 0.34 0.13 0.05 0.05 885 55.00 491.68 496.70 0.47 0.13 0.67 1.09 850 55.00 491.68 496.14 0.89 0.34 0.32 0.67 0.49 850 55.00 493.07 495.70 0.89 0.1	wer	875	90.06	493.09	495.33	0.45	0.10	1 30	8 8	200	0.00	0.59 1.59	. Se. 73	527.61
875 227.00 493.09 495.68 1,00 0.38 4.80 0,03 0,03 875 518.00 493.09 495.68 1,00 0.38 4.80 0,09 0,03 865 55.00 491.68 495.49 0,12 0,12 0,02 0,07 0,19 865 90.00 491.68 495.49 0,12 0,04 0,32 0,07 0,19 865 163.00 491.68 495.59 0,16 0,04 0,32 0,05 0,15 865 227.00 491.68 495.59 0,33 0,08 0,33 0,15 0,05 865 227.00 491.68 496.14 0,89 0,31 4,33 0,67 1,09 865 518.00 491.68 496.14 0,89 0,31 4,33 0,67 1,09 860 550.00 493.07 496.47 0,68 0,16 2,20 0,21 0,05 860 163.00)Wer	875	163.00	493 09	495.55	0.73	21.20	2000	0.23	0.20	3.10	0.54	48.38	522.72
875 518.00 493.09 496.10 1.30 0.84 4.80 0.91 0.63 865 55.00 491.68 494.95 0.12 0.12 0.20 0.20 0.12 0.13 0.12 0.13 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12 0.12	wer	875	227.00	493.00	405.60	2 5	0.20	78.3	40.0	0.48	4.06	1.02	77.35	535.97
865 55.00 491.68 495.6 0.12 0.12 0.02 0.20 0.19 1.21 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.22 1.23	wer	875	278.00	00.004	450.00	3. 5	D . C	08.4	0.91	0.63	4.80	1,35	94.59	543.28
865 55.00 491.68 494.95 0.12 0.12 0.20 0.20 0.09 865 110.00 491.68 495.44 0.21 0.05 0.04 0.07 0.19 865 90.00 491.68 495.36 0.16 0.04 0.03 0.05 0.15 865 163.00 491.68 495.70 0.47 0.13 1.62 0.22 0.49 865 5718.00 491.68 496.14 0.89 0.31 4.33 0.67 1.09 850 55.00 493.07 494.76 0.63 0.63 0.22 0.49 850 110.00 493.07 495.73 0.63 0.16 2.29 0.34 0.54 850 163.00 493.07 495.56 0.89 0.14 3.76 0.51 0.79 850 163.00 493.07 495.46 0.89 0.74 3.53 0.46 0.79 850 163.00 493.		2	3000	190,03	430.10	1.81	0.84	13.11	2.74	1.21	6.86	2.41	159.55	567.94
865 110.00 491.68 495.44 0.21 0.05 0.05 0.020 865 90.00 491.68 495.44 0.121 0.05 0.04 0.07 0.01 865 163.00 491.68 495.50 0.16 0.04 0.03 0.05 0.05 865 227.00 491.68 495.70 0.47 0.13 1.62 0.22 0.49 865 518.00 491.68 496.74 0.89 0.31 4.33 0.67 1.09 850 55.00 493.07 494.76 0.63 2.20 2.20 2.20 850 90.00 493.07 495.47 0.89 0.14 3.76 0.54 850 163.00 493.07 495.40 0.89 0.14 3.76 0.51 850 163.00 493.07 495.40 0.89 0.74 3.53 0.46 0.79 850 163.00 493.07 495.40 0.89 <td< td=""><td>ower</td><td>865</td><td>55.00</td><td>491 68</td><td>404 95</td><td>0 13</td><td>2,70</td><td>8</td><td>000</td><td></td><td></td><td></td><td></td><td></td></td<>	ower	865	55.00	491 68	404 95	0 13	2,70	8	000					
865 90.00 491.08 495.44 0.21 0.05 0.05 0.05 0.05 865 90.00 491.68 495.58 0.16 0.04 0.03 0.05 0.05 0.15 865 163.00 491.68 495.70 0.47 0.13 1.62 0.22 0.49 865 55.00 491.68 496.14 0.89 0.31 4.33 0.67 1.09 850 491.60 493.07 494.76 0.63 2.20 2.20 2.20 850 90.00 493.07 495.23 0.75 0.16 2.99 0.34 0.54 850 163.00 493.07 495.07 0.89 0.14 3.76 0.51 0.20 850 163.00 493.07 495.07 0.89 0.14 3.76 0.51 0.79 850 163.00 493.07 495.40 0.89 0.14 3.69 0.76 0.79 850 163.00 </td <td>hwar</td> <td>865</td> <td>140.00</td> <td>404 60</td> <td>200</td> <td>30.76</td> <td>0.12</td> <td>0.20</td> <td>O.ZU</td> <td></td> <td>1.65</td> <td></td> <td>33.29</td> <td>18.84</td>	hwar	865	140.00	404 60	200	30.76	0.12	0.20	O.ZU		1.65		33.29	18.84
655 90,00 491,08 495,36 0,16 0.04 0.32 0.05 0,15 865 163,00 491,68 495,58 0,33 0.08 0,93 0,12 0,33 865 227,00 491,68 495,70 0,47 0,13 1,62 0,22 0,49 865 55,00 491,68 496,14 0,89 0,63 2,20 0,67 1,09 850 110,00 493,07 495,73 0,63 0,75 0,16 2,99 0,34 0,54 850 163,00 493,07 495,73 0,89 0,14 3,76 0,51 0,26 850 163,00 493,07 495,40 0,89 0,14 3,76 0,61 0,79 850 163,00 493,07 495,56 0,89 0,74 3,76 0,79 0,79 850 163,00 493,07 495,56 0,89 0,74 3,70 0,69 0,79 850 </td <td>1000</td> <td>200</td> <td>20.02</td> <td>431.00</td> <td>495.44</td> <td>0.21</td> <td>0.05</td> <td>0.46</td> <td>20.0</td> <td>0.19</td> <td>2.23</td> <td>0.40</td> <td>84.05</td> <td>563.28</td>	1000	200	20.02	431.00	495.44	0.21	0.05	0.46	20.0	0.19	2.23	0.40	84.05	563.28
865 277.00 491.68 495.58 0.33 0.08 0.93 0.12 0.33 865 277.00 491.68 495.70 0.47 0.13 1.62 0.22 0.49 865 55.00 493.07 496.14 0.89 0.63 2.20 2.20 0.67 1.03 850 110.00 493.07 495.23 0.75 0.16 2.99 0.34 0.54 0.54 850 163.00 493.07 495.47 0.89 0.14 3.76 0.51 0.26 0.79 850 163.00 493.07 495.47 0.89 0.14 3.76 0.51 0.26 0.79 850 163.00 493.07 495.40 0.89 0.74 3.53 0.46 0.79 850 227.00 493.07 495.56 0.89 0.74 0.70 0.79 0.79	5	3 6	20.00	481.08	480.36	0.16	0.04	0.32	0.05	0.15	1.98	0.31	71.79	550.15
855 55.00 491.68 495.70 0.47 0.13 1.62 0.22 0.49 865 55.00 491.68 496.14 0.89 0.31 4.33 0.67 1.09 850 55.00 493.07 494.76 0.63 2.20 2.20 2.20 850 110.00 493.07 495.23 0.75 0.16 2.99 0.34 0.54 850 163.00 493.07 495.40 0.83 0.24 3.53 0.46 0.79 850 227.00 493.07 495.56 0.89 0.74 3.53 0.46 0.79	wei	200	163.00	491.68	495.58	0.33	0.08	0.93	0.12	0.33	2.85	0.61	109.85	599.12
855 518.00 491.68 496.14 0.89 0.31 4.33 0.67 1.09 850 55.00 493.07 494.76 0.63 2.20 2.20 2.20 850 110.00 493.07 495.23 0.75 0.16 2.99 0.34 0.54 850 163.00 493.07 495.40 0.83 0.24 3.53 0.46 0.79 850 227.00 493.07 495.56 0.89 0.34 3.53 0.46 0.79)wer	865	227.00	491.68	495.70	0.47	0.13	1.62	0.22	0.49	3,45	0.83	135.36	613.94
850 55.00 493.07 494.76 0.63 0.63 2.20 2.20 850 110.00 493.07 495.23 0.75 0.16 2.99 0.34 0.54 850 90.00 493.07 495.07 0.89 0.14 3.76 0.51 0.26 850 163.00 493.07 495.46 0.83 0.24 3.53 0.46 0.79 850 227.00 493.07 495.56 0.89 0.30 4.00 6.00	wer	865	518.00	491.68	496.14	68'0	0.31	4.33	0.67	1.09	4.87	1.51	241.25	652.88
850 55.00 493.07 494.76 0.63 0.63 2.20 2.20 2.20 850 110.00 493.07 495.23 0.75 0.16 2.99 0.34 0.54 850 90.00 493.07 495.40 0.83 0.14 3.76 0.51 0.26 850 163.00 493.07 495.46 0.83 0.24 3.53 0.46 0.79 850 227.00 493.07 495.56 0.89 0.90 4.00 0.90 0.00														
850 110.00 493.07 495.23 0.75 0.16 2.99 0.34 0.54 850 90.00 493.07 495.07 0.89 0.14 3.76 0.51 0.26 850 163.00 493.07 495.40 0.83 0.24 3.53 0.46 0.79 850 227.00 493.07 495.56 0.89 0.90 4.00 0.90 0.79	wer	850	55.00	493.07	494.76	0.63	0.63	2.20	2.20		3.47		15.87	15.75
850 90.00 493.07 495.07 0.89 0.14 3.76 0.51 0.26 650 163.00 493.07 495.40 0.83 0.24 3.53 0.46 0.79 850 227.00 493.07 495.56 0.89 0.90 0.90 0.90 0.79		820	110.00	493.07	495.23	0.75	0.16	2.99	0.34	0.54	3.98	0.56	. 52.22	580 84
850 163.00 493.07 495.40 0.83 0.24 3.53 0.46 0.79 850 227.00 493.07 495.56 0.89 0.30 4.03 6.60 6.70		820	80.00	493.07	495.07	0.89	0.14	3.76	0.51	0.26	4.23	20.0	24 66	132 GR
850 227.00 493.07 495.56 0.8a 0.3a 4.02 0.5a		850	163.00	493.07	495.40	0.83	0.24	3.53	0.46	0.79	4.26	0.91	84.85	596 41
4.02 4.02 4.02 0.38		850	227.00	493.07	495.56	0.89	0:30	4.02	0.58	0.98	4.50	117	117 34	640.77

HEC-RAS Plan: Prop lower ineff River: Tanyard Branch Reach: Lower (Continued)

Reach	Reach River Sta Q Total Min Ch El W.S.	Q Total	Min Ch El	W.S. Elev	Elev Shear Chan	Shear Total	Power Chan	Power Total	Velleft	Val Chal	Vel Bioht	Flow Area	Ton 1864th
-		(cts)	æ	(#)	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(£/s)	(Lt/s)	(fl/s)	(sq ft)	(E)
Lower	850	518.00	493.07	496.07	1.07	0.47	5.47	1.03	1.51	5.13	1.80	234.79	651.36
- Annual Control of the Party o													
Lower	835	92.00	492.81	494.67	0.44	0.44	1.30	1.30		2.95		18.67	16.44
Lower	835	110.00	492.81	495.27	0.26	0.07	0.64	0.08	0.45	2.43	0.61	102.57	632.14
Lower	835	90.00	492.81	495.11	0.33	20.0	0.90	0.10	0.33	2.70	0.55	67.62	613,31
Lower	835	163.00	492.81	495.42	0.33	0.10	0.30	0.12	0.63	2.75	0.79	138.89	650.21
Lower	835	227.00	492.81	495.57	0.38	0.13	1.12	0.17	0.78	2.99	0.95	179.48	668.97
Lower	835	518.00	492.81	496.06	0.53	0.22	1.95	96.0	1.21	3.68	1.41	323.22	721.16
Lower	820	55.00	491.40	494.70	0.12	0.12	0.19	0.19		1.83		33.81	18.98
Lower	820	110.00	491.40	495.25	0.15	0.04	06.0	0.03	0.29	1.94	0.36	115.30	630.23
Lower	820	30.00	491.40	495.11	0.15	0.03	0.29	0.03	0.19	1.91	0.28	83.21	612.85
Lower	820	163.00	491.40	495.38	0.24	90.0	0.57	0.07	0.45	2.43	0.52	146.91	646.16
Lower	820	227.00	491.40	495.52	0.32	60'0	0.92	0.12	0.61	2.87	0.67	181.25	662.37
Lower	820	518.00	491.40	495.95	0.61	0.21	2.45	0.36	1.11	40,4	1.18	306.77	714 58
Lower	800	55.00	492.79	494.50	0.60	09:0	2.03	2.03		3.38		16.27	15.85
Lower	800	110.00	492.79	494.88	1.07	0.21	5.06	0.75	0.22	4.71	0.45	31.18	274.45
Lower	800	90:00	492.79	494.80	06:0	0.20	3.84	0.84	0.03	4.27	0.05	21.40	80.62
Lower	800	163.00	492.79	495.17	08:0	0.20	3.37	0.38	0.64	4.21	0.96	83.95	620.93
Lower	800	227.00	492.79	495.29	0.98	0.28	4.61	0.57	0.91	4.71	1.22	110,56	634.94
Lower	800	518,00	492.79	495.84	0.89	0.35	4.21	0.70	1.41	4.71	1.68	258.25	701.07
Lower	780	25.00	492.53	494.36	0.47	0.47	1.41	1.41		3.02		18.22	16.33
Lower	780	110.00	492.53	494.95	0.23	0.09	0.74	0.10	0.47	2.54	0.61	98.01	602:39
Lower	780	90.00	492.53	494.81	0.34	0.09	0.92	0.11	0.40	2.71	0.52	69.18	590.14
Lower	780	163.00	492.53	495.10	0.39	0.13	1.14	0.16	0.64	2.97	0.82	128.60	621.56
Lower	780	227.00	492.53	495.25	0.45	0.17	1.48	0.23	0.79	3.27	1.01	164.86	638.71
Lower	780	518.00	492.53	495.77	0.63	0.27	2.51	0.47	1.21	4.00	1.51	302.63	694.92
	100	1											
Lower	80	00.00	481.12	494.40	0.12	0.12	0.20	0.29		1.64		33.48	18.89
Lower	768	110.00	491.12	494.95	0.16	0.04	0.30	0.04	0:30	1.95	0.39	113.15	605.95
Lower	768	90.00	491.12	494.81	0.15	0.03	0.28	0.03	0.23	1.88	0:30	86.44	591.42
Lower	768	163.00	491.12	495.07	0.25	0.07	0.61	0.08	0.44	2.48	0.56	140.54	619.86
Lower	768	227.00	491.12	495.21	0.34	0.10	0.98	0.14	0.59	2.93	0.75	172.64	635.12
Lower	768	518.00	491.12	495.69	0.62	0.23	2.52	0.40	1.06	4.09	1.32	295.96	686.26
	750	55.00	492.51	494.20	0.63	0.63	2.18	2.18		3.45		15.92	15.76
***************************************	750	110.00	492.51	494.61	8.	0.17	4.57	0.50	0.37	4.56	0.47	37.48	366.47
	750	80.00	492.51	494.49	0.95	0.95	4.14	4.14		4.37		20.61	16.91
_	750	163.00	492.51	494.85	98.0	0.24	3.75	0.47	0.72	4.35	0.93	81.84	596.82
Lower	750	227.00	492.51	494.99	1.01	0.32	4.83	0.66	0.95	4.78	1.22	109.51	611.38

HEC-RAS Plan: Prop lower ineff River: Tanyard Branch Reach: Lower (Continued)

Reach	Reach River Sta O Total Min Ch El M.S.	O Tofat	Min Ch El		Flav Shear Chan	Chear Total	Double Chan	Los Tours	4-11-4	1-101-11	7.7.0	-	
		(cfs)	1 €	(#)	(lb/scr#)	(B)(e) (B)	(h#a)	TOWER TOTAL	16/4/	Vel Crim	vel Right	riow Area	nob width
Losson	750	(2)	2007	(4)	(31 75 (31)	(Integral	(8.1161)	(IDUL S)	(sna)	(S/L)	(ff/s)	(sd ft)	Œ
FOME	8	010.00	492.51	450.08	48.0	0.39	4.56	0.81	1.38	4.84	1.74	252.01	674.39
7	730	o u	00 007	10,101	L								
Jamor.	730	00.00	492.22	484.07	0.45	0.45	1.35	1.35		2.98		18.46	16.39
Lower	730	110.00	492.22	494.69	0.25	0.08	09:0	0.08	0.46	2.38	09'0	105.32	602.03
Lower	730	90.00	492.22	494.52	0.31	0.08	0.82	0.10	0.40	2.61	0.52	72.75	586.98
Lower	730	163.00	492.22	494.80	0.38	0.13	1.11	0.17	0.64	2.94	0.82	128.73	612.19
Lower	730	227.00	492.22	494.96	0.44	0.17	1.43	0.23	62'0	3.24	1.01	164.42	626.81
Lower	730	518.00	492.22	495.51	09.0	0.27	2.38	0.47	1.20	3.94	1.51	302.68	676.22
Lower	715	55.00	490.81	494.10	0.12	0.12	0.19	0.19		1.64		33.59	18.92
Lower	7115	110.00	490.81	494.67	0.14	0.04	0.26	0.04	0.30	1.87	0.39	119.72	601.54
Lower	715	00.06	490.81	494.52	0.14	0.03	0.26	0.03	0.23	1.84	0.31	88.91	587.38
Lower	715	163.00	490.81	494.77	0.24	20.0	09.0	0.08	0.44	2.47	0.57	139.65	610.20
Lower	715	227.00	490.81	494.92	0.33	0.11	0.97	0.14	0.59	2:92	0.76	171.12	673.18
Lower	715	518.00	490.81	495.43	0.59	0.23	2.38	0.40	1.05	4.01	1.32	296,33	69899
Lower	695	55.00	492.20	493.89	0.63	0.63	2.17	2.17		3.45		15.95	15.77
Lower	695	110.00	492.20	494.22	1.28	0.16	6.53	0.72	0.16	5.10	0.22	24.96	255.18
Lower	695	30.00	492.20	494.20	0.91	0.91	3.91	3,91		4.29		20.97	16.99
Lower	695	163.00	492.20	494.54	0.87	0.24	3.78	0.49	0.72	4.36	0.95	80.90	590.39
Lower	695	227.00	492.20	494.74	0.82	0.28	3.57	0.53	0.91	4.33	1.18	120.85	608.21
Lower	695	518.00	492.20	495.31	06.0	0.39	4.30	0.81	1.37	4.75	1.74	252.65	658.42
Lower	673	55.00	491.90	493.74	0.46	0.46	1.38	1.38		3.00		18.32	16.36
Lower	673	110.00	491.90	494.31	0.32	60:0	0.87	0.11	0.44	2.68	0.64	90.56	611.03
Lower	673	90:00	491.90	494.21	0.31	0.08	0.82	0.10	0.35	2.62	0.54	70.79	592.71
Lower	673	163.00	491.90	494.53	0.32	0.10	0.89	0.12	0.58	2.74	08.0	141.18	651.92
Lower	673	227.00	491.90	494.73	0.33	0.11	0.93	0.13	69'0	2.81	0.92	195.51	689.46
Lower	673	518.00	491.90	495.29	0.38	0.16	1.22	0.22	1.04	3.16	1.25	381.47	754.53
	0.0	1											
Lower	88	00.00	490.49	493.77	0.12	0.12	0.20	0.2 8		1.64		33.45	18.88
Lower	658	110.00	490.49	494.30	0.16	0.04	0.32	0.04	0.28	1.98	0.39	112.23	628.28
Lower	658	86.00	490.49	494.21	0.14	0.03	0.25	0.03	0.22	1.82	0.31	92.27	613.83
Lower	658	163.00	490.49	494.51	0.20	0.05	0.45	0.05	0.42	2.25	0.55	162.79	661.32
Lower	859	227.00	490.49	494.70	0.24	20.0	0.58	20.0	0.54	2.47	0.68	216.49	692.36
Lower	658	518.00	490.49	495.25	0.35	0.13	1.09	0.17	0.91	3.11	1.07	396.85	752.45
	637	\$5.00	491.88	493.55	0.65	0.65	2.30	2.30		3.51		15.65	15.69
	637	110.00	491.88	494.12	0.60	0.13	2.18	0.24	0.41	3.60	0.65	60.11	599.40
	637	80.06	491.88	493.93	0.79	0.13	3.21	0.44	0.14	4.04	0.29	27.49	339.24
	637	163.00	491.88	494.43	0.40	0.12	1.19	0.15	0.62	3.01	0.83	129.46	648.90
Lower	637	227.00	491.88	494.64	0.37	0.13	1.11	0.16	0.73	2.97	0.94	186.35	683.12

HEC-RAS Plan: Prop lower ineff River: Tanyard Branch Reach: Lower (Continued)

2	Ċ												
Nego.	NIVE OLA	E C IOES	3 C E	W.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Vel Left	Vel Chnl	Vel Right	Flow Area	Top Width
	100	(cfs)	(¥)	(£)	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(ff/s)	(ft/s)	(ft/s)	(sq ft)	£
Lower	63/	518.00	491.88	495.20	0.43	0.18	1.41	0.26	1.08	3.31	1.29	367.25	750.16
Lower	620	22.00	491.61	493.44		0.47	1.42	1.42		3.03		18.16	16.32
Lower	620	110.00	491.61	494.03		0.14	1.71	0.26	0.38	3.37	09'0	57.94	584 93
Lower	620	80.00	491.61	493.87	0.50	0.15	1.65	0.34	62.0	3 29	0.48	CRUP	549.04
Lower	620	163.00	491.61	494.29		0.17	2.01	Augant Angelin	0.63	3.64	080	20.0t	045.04 825.84
Lower	620	227.00	491.61	494.49	0.62	0.20	2.39	0.33	0.82	386	900	137.03	020.030
Lower	620	518,00	491.61	495.04	0.83	0.31	3.88	0.58	1.32	4.66	1.36	275.70	741 08
											3	03:00 tm	25.14.
Lower	605	55.00	490.20	493.47	0.12	0.12	0.20	0.20		1.85		33 30	10 00
Lower	605	110.00	490.20	494.06	0.19	0.05	0.40		0.30	2.15	0 33	92,200	10.03
Lower	605	90.00	490.20	493.90	0.17	0.04	0.35		0.20	2.13	20.0	67.15	07.600
Lower	909	163.00	490.20	494.29	0.25	0.07	0.64	600	0.46	2.54	0.50	190 74	362.87
Lower	605	227.00	490.20	494.48	0.33	0.10	0.98	0.15	0.61	15.2 10.0	0+0	169.71	038.20
Lower	605	518.00	490.20	494.98	0.64	0.20	2,69	0.38	2 7	5.5	8 6	100.00	79.690
							22	25.0	-	4.21	97.	34.55	737.20
Lower	585	22.00	491.58	493.26	0.65	0.65	225	225		3.40		70 20	AL 14
Lower	585	110.00	491.58	493.72	1.00	0.24	4.59	0.82	72.0	4.58	0.43	34.05	13.72
Lower	585	90.00	491.58	493.61	0.86	0.24	3.61	0.95	600	4 19	21.0	201.92	410.48
Lower	585	163.00	491.58	493.99	1.03	0.30	4.95	0.74	0.72	4 79	0.84	65.94	400.47
Lower	585	227.00	491.58	494.18	1.15	0.37	5.94	0.86	060	5 15	80.5	40.00	23.050
Lower	585	518.00	491.58	494.64	1.71	0.62	11.15	1.68	1.71	6.52	173	192.25	689 12
												2	71.700
Lower	570	65.00	491.36	493,15	0.51	0.51	1.62	1.62		3.15		17.45	16.14
Lower	570	110.00	491.36	493.80	0.32	0.08	0.86	0.10	0.52	2.67	0.48	94.72	677.29
Lower	570	90:00	491.36	493.59	0.45	0.10	1.41	0.17	0.43	3.11	0.41	1 2 5 E	622 73
Lower	570	163.00	491.36	493.96	0.38	0.11	1.13	0.13	0.68	2.96	0.63	136.49	722.15
Lower	570	227.00	491.36	494.12	0.43	0.13	1.36	0.16	0.81	3.18	0.74	182.82	764 53
Lower	9/0	518.00	491.36	494.58	0.57	0.20	2.16	0.29	1.17	3.80	1.06	353,21	886.30
Lower	558	00	10000	07.007									
louis.	000	33.00	408.80 C	483.18	0.13	0.13	0.21	0.21		1.68		32.68	18.66
Lower	558	20.00	489.95	493.79	0.16	0.04	0.33	0.04	0.33	2.00	0.30	110.50	678.03
1000	000	80.00	409,90	493.02	0.17	0.03	0.34	0.0	0.24	2.01	0.23	74.44	631.00
Cowe	2000	103.00	489.95	493.94	0.24	0.06	0.60	90.0	0.47	2.47	0.43	147.90	718.21
, Act	93 1	227.00	489.30	494.08	0.32	0.08	0.93	0.10	0.61	2.88	0.56	187.99	755.48
rowei	358	518.00	489.95	494.49	09'0	0.17	2.39	0.27	1.05	4.01	0.95	334.27	863.93
Cower	542	£5.00	70107	90 007	1								
lower	542	44000	10.101	452.30	0.74	47.0	7.75	2.75		3.71		14.82	15.48
Camer	543	30.00	431.34	493.28	7.0.1	1.52	8.36	8.36		5.51		19.97	16.76
Lower	277	30.00	401.04	493.28	1.01	1.01	4.51	4.51		4.49		20.06	16.78
CWA	242	00.00	401.04	493.72	0.86	0.22	3.74	0.42	0.79	4.36	0.74	82.87	661.89
	-	00:127	40.104	490.07	RS:O	0.27	4.67	0.53	1.02	4.74	0.94	115.43	699.32

HEC-RAS Plan: Prop lower ineff River. Tanyard Branch Reach: Lower (Continued)

Beach Diversity O Total Mit Of Fire	Disp Ct	Total	Mi- Of F	Seach.	rower (Continued)				£				
Innov	90	(1)-(1)-(1)-(1)-(1)-(1)-(1)-(1)-(1)-(1)-	100	VV.O. Elev	Shear Chan	Shear lotai	Power Chan	Power Total	Vel Left	Vel Chnl	Vel Right	Flow Area	Top Width
		(cls)	(±)	Œ	(lp/sd ft)	(lb/sd ft)	(lb/fts)	(lb/ft s)	(ft/s)	(#/s)	(th/s)	(sq ft)	€
Lower	542	518.00	491.34	494.40	06:0	0:30	4.24	0.54	1.38	4.72	1.25	284.82	839.81
-	202												
Lower	525	95.00	491.03	492.84	0.48	0.48	1.49	1.49		3.07		17.91	16.26
rower	525	110.00	491.03	493.36	0.49	0.12	1.60	0.19	0.55	3.27	0.51	69.59	633.87
Lower	525	00.06	491.03	493.29	0.42	0.10	1.24	0.15	0.44	2.99	0.42	57.60	618.67
Lower	525	163.00	491.03	493.62	0.43	0.13	1,37	0.17	0.71	3.16	0.66	124.07	691 12
Lower	525	227.00	491.03	493.78	0.49	0.15	1.68	0.21	0.86	3.41	0.79	166 22	727 43
Lower	525	518,00	491.03	494.37	0.50	0.18	1.78	0.26	1.14	3.58	103	367 18	858 33
													0000
Lower	508	55.00	489.64	492.87	0.13	0.13	0.22	0.22		1.69		32 50	1861
Lower	508	110,00	489.64	493.39	0.14	0.03	0.25	0.03	0.42	1.83	0.25	125.46	718.56
Lower	508	90.00	489.64	493.32	0.12	0.02	0.20	0.02	0.35	1.67	020	106 90	705 1B
Гожег	508	163.00	489.64	493.63	0.14	0.04	0.27	0.03	0.53	8	0.34	16.35	760.10
Lower	508	227.00	489.64	493.79	0.18	0.05	0.38	0.05	0.65	214	0.03	245.00	707 50
Lower	508	518.00	489.64	494.36	0.24	60.0	0.63	010	0.03	040	2 0	25.00	00.707
								2	2000	9.30	CO'O	403.30	887.13
Lower	490	92.00	491.00	492.65	0.69	69.0	2.49	2.49		3.60		15.07	70.07
Lower	490	110.00	491.00	493.31	0.36	0.09	1.02	0.11	090	28.5	CFO	13.27	15,53
Lower	490	90.00	491.00	493.01	0.89	800	3.78	65.0	243	10.1	24.0	30.5	0.50
Lower	490	163.00	491.00	493.59	0.25	0.08	95.0	80.0	0.1.0	2.4.0	0.0	787.97	317.45
Lower	490	227.00	491.00	493.75	0.28	0.10	0.71	040	5 6	20.7	0.00	103.04	/33.4/
Lower	490	518.00	491.00	494 33	0.34	0 0	100	2 4	0.78	00.2	SC'O	219.74	781.00
				2	2	0.0	0.07	0.10	50.	2.81	0.80	439.71	881.94
Lower	465	55.00	490.51	97 C97	77.0	70.0	00.4	0					
lower	465	340.00	400.54	200 COV	200	10.0	00.1	S	0.23	2.96	0.23	19.20	23.37
Chinor	AGE	200	2000	433.00	8 6	BO:	7.74	0.19	0.33	3.71	0.33	49.11	415.49
owe.	207	30.00	490.51	492.87	0.57	0.30	1.99	0.85	0.49	3.52	0.49	31.18	39.41
Lower	463	163.00	490.51	493.52	0.26	0.07	0.66	0.07	0.59	2.53	0.48	165.59	741.68
Lower	465	227.00	490.51	493.67	0.31	0.09	0.88	0.10	0.73	2.81	0.59	211.03	767.78
Lower	463	518.00	490.51	494.26	0.36	0.13	1.11	0.15	1.00	3.11	0.82	428.47	870.82
Cuttor	750	00 99	27 007	100007									
	200	20.00	430.43	492.37	3.00	0.39	1.56	1,21	0.19	3.12	0.19	17.86	20.75
	000	110.00	490.45	492.93	0.68	0.34	2.66	1.04	0.60	3.91	09.0	36.28	44.20
	450	90.00	490.45	492.75	0.63	0.34	2.34	1.07	0.49	3.69	0.49	28.78	36.51
	450	163.00	490.45	493.48	0.29	0.07	0.76	90.0	0.59	2.65	0.49	156.55	734 63
	450	227.00	490.45	493.62	0.35	0.10	1.05	0.11	0.74	2.98	0.61	198 43	759 34
Lower	450	518.00	490.45	494.22	0.38	0.13	1.24	0.17	1.02	3.23	0.84	415.05	864 11
	435	55.00	490.43	491.88	1.49	1.49	7.68	7.68		5.15		10.68	12.88
	435	110.00	490.43	492.40	1.79	1.43	10.66	8.36	0.45	5.96	0.46	18.82	75.0%
	435	90.00	490.43	492.25	1.66	1.61	9.33	90.6	0.11	5.61	0.11	16.04	16.49
	435	163.00	490.43	492.78	1.93	1.18	12.53	6.71	0:00	6,49	06.0	28.65	30.98
Lower	435	227.00	490.43	493.55	0.46	0.12	1.54	0.16	0.78	3.38	0.66	172.77	746.34
													5

HEC-RAS Plan: Prop lower ineff River. Tanyard Branch Reach: Lower (Continued)

				֡									
ומפכו	NVCI OLD	L TOTAL	Min Ch El	W.S. Elev	Shear Chan	Shear Total	Power Chan	Power Total	Vel Left	Vel Chri	Vel Right	Flow Area	Top Width
Chitar	326	(CIS)	(H)	(H)	(Ib/sq ft)	(lp/sd ft)	(lb/ft s)	(lb/ft s)	(£/\s)	(fVs)	(ft/s)	(sq ft)	€
LOWE	654	518.00	490,43	494.18	0.43	0.15	1.49	0.19	1.06	3.43	0.88	393.48	856.28
Lower	415	55.00	480 88	27 101		4							
Lower	415	140.00	80.00	400.00		3	1.74	1.59	0.16	3,23	0.16	17.10	17.49
Lower	415	800	489.88	492.30	0.72	0.47	2.89	1.68	0.62	4.02	0.61	31.01	28.51
lower	415	163.00	00.00	132.11		0.45	2.46	1.60	0.50	3.76	0.50	25.92	25.07
1 ower	212	20.00	409.00	492.76		2.0	4.18	2.01	0.84	4.65	0.83	43.85	35.74
Sub.	445	00.722	28.68	493.09		0.18	6.48	0.57	0.51	5.48	0.57	70.75	457.90
1000	2	518.00	489.88	493.99	08:0	0.31	3.82	0.62	1.41	4.75	1.05	255.40	629.89
Owner	400	00	10 007	1									
Owei	400	22.00	488.97	491.77	0.21	0.18	0.45	0.37	60'0	2.14	0.09	25.82	19.48
Lower	400	110.00	488.97	492.38	0.37	0.17	1.09	0.40	0.34	2.99	0.45	45.67	47.03
Lower	400	90.06	488.97	492.18	0.32	0.16	0.86	0.39	0.27	2.74	0.34	37.37	47 10
Lower	8	163.00	488.97	492.80	0.48	0.19	1.67	0.45	0.51	3.51	0.63	69 70	67.00
Lower	400	227.00	488.97	493.19	0.53	0.10	2.01	0.19	0.60	3.79	0,00	124 20	PE. 10
Lower	400	518.00	488.97	493.99	0.51	0.15	1.96	0.22	660	988	28.0	267.05	20.40
										8	3	202,00	70.80
Lower	385	25.00	489.86	491.31	1.49	1.49	7.66	7.66		5.15		10.60	42.00
Lower	385	110.00	489.86	491.83	1.80	1.36	10.71	7.93	0.45	5.97	0.45	18 88	24.84
Lower	385	90.00	489.86	491.67	1.68	1.63	9.45	9.17	60.0	563	800	15.08	16.60
Lower	385	163.00	489.86	492.23	1.82	0.93	11.51	4.88	0.77	6.32	£	27.55	20.20
Lower	385	227.00	489.86	492.61	1.88	0.84	12.47	3,83	1.01	6.65	2 2	70.07	20.70
Гомег	385	518.00	489.86	493.95	09'0	0.19	2.49	0.30	1.13	4.12	0.97	328.24	782.50
													25.20
Lower	365	55.00	489.26	491.15	0.52	0.49	1.67	1.54	0.17	3.19	0.17	17 30	17 30
Lower	365	110.00	489.26	491.76	0.71	0.49	2.85	1.78	0.61	4.00	0.61	30.56	06.11
Lower	365	80.00	489.26	491.57	0.64	0.47	2.38	1.65	0.50	3.72	0.50	25.85	22.42
	365	163.00	489.26	492.13	0.94	0.54	4.45	2.10	0.69	4.75	0.87	41.71	35.80
	360	227.00	489.26	492.44	1.24	09:0	6.97	2.47	0.79	5.60	1.13	54.67	49.22
Lower	202	518.00	489.26	493.83	0.68	0.18	3.05	0.31	1.06	4.48	0.86	304.13	766.44
Ower	247	00 33	70 007	1,70									
	247	3 5	400.04	491.15	0.21	0.17	4.0	0.37	0.10	2.13	0.10	25.99	19.20
	500	00.01	468.34	491.76	0.37	0.20	1.11	09:0	0.40	3.00	0.39	43.35	37.65
	150	30.00	488.34	491.57	0.31	0.18	0.85	0.45	0.31	2.73	0.31	36.70	31.87
	047	163.00	488.34	492.14	0.52	0.25	1.88	0.69	0.58	3,65	0.57	60.11	48.86
	247	227.00	488.34	492.47	0.70	0.33	3.03	0.98	0.77	4.33	0.75	77.51	57.68
Lowel	04/	518.00	488.34	493.79	0,59	0.15	2.53	0.25	0.98	4.25	0.71	312.69	760.20
Ower	330	25.00	700 000	00 00									
	330	45.00	469.23	490.68	1.48	1.48	7.61	7.61		5.13		10.71	12.90
	330	30.00	409.23	491.21	1.72	1.19	10.10	6.71	0.47	5.86	0.47	19.48	24.38
	000	30.00	489.23	491.05	1.67	1.61	9.41	9.03	0.10	5.63	0.10	16.00	16.69
	200	163.00	489.23	491.66	1.83	0.80	9.77	3.76	0.89	6.01	0.88	34.77	44.52
			4KG 233	A92 45	200	000							

HEC-RAS Plan: Prop lower ineff River: Tanyard Branch Reach: Lower (Continued)

40000			-	Total (Calmidea)	(Calminou)								
Negri	NIVEI OLA	, C C C C		VV.O. EIEV	Shear Chan	Shear lotal	Power Chan	Power Total	Vei Left	Vel Chril	Vel Right	Flow Area	Top Width
		(cts)	€	Œ	(lb/sq ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(£/s)	(fVs)	(£/s)	(sq ft)	(£)
Lower	330	518.00	489.23	493.75	0.62	0.18	2.67	0.29	1.10	4.28	0.81	311.20	755.33
Compar	340	25.00	00000	03 007	i i	9							
2000	2 7	3.00	400.03	490.30	0.00	N.52	1.80	1.69	0.15	3,26	0,15	16.89	17.08
rowei	310	O.O.F.	488.59	491.16	0.74	0.50	2.99	1.81	09.0	4.06	0.59	30.18	27.30
Lower	310	90.00	488.69	490.97	29'0	0.49	2.54	1.76	0.50	3.80	0.50	25.30	23.57
Lower	310	163.00	488.69	491.61	78.0	0.51	3.98	1.88	0.81	4.59	0.78	44.34	36.22
Lower	310	227.00	488.69	492.05	1.00	0.54	5.09	1.98	0.94	5.08	0.97	62 00	45.96
Lower	310	518.00	488.69	493.61	0.77	0.18	3.69	0.35	0.97	4.82	0.99	273.01	735 16
													2
Lower	295	55.00	487.77	490.57	0.21	0.19	0.45	0.41	0.09	2.14	0.09	25.72	17.44
Lower	295	110,00	487.77	491.17	0.39	0.26	1.18	0.73	0.31	3.07	0.42	39.11	26.60
Lower	295	90.00	487.77	490.98	0.32	0.24	06.0	0.62	0.29	2.77	0.31	34.27	23.71
Lower	295	163.00	487.77	491.61	0.53	0.32	1.96	1,01	0.48	3.70	0.63	52.23	33.18
Lower	295	227.00	487.77	492.04	0.69	0.38	2.98	1.27	0.57	4 33	0.83	87.85	44.40
Lower	295	518.00	487.77	493.56	0.70	0.16	3.26	0.30	0.85	4.67	0.92	78 87	87.8C7
													0.024
Lower	280	55.00	488.66	490.11	1.49	1.49	7.63	7.63		5.14		10.70	12 an
Lower	280	110.00	488.66	490.64	1.73	1.50	10.17	8.72	0.46	5.87	0.47	18.96	18 74
Lower	280	90.00	488.66	490.48	1.67	1.64	9.35	9.21	0.10	5.62	0,10	16.03	16.25
Lower	280	163.00	488.66	491.04	1.88	1.31	12.04	7.74	0.73	6.42	0.93	27.58	25.41
Lower	280	227.00	488,66	491.47	1.94	1.30	13.19	7.46	1.19	6.80	1.28	39.55	29.75
Lower	280	518.00	488.66	493.46	0.91	0.21	4.76	0.46	1.00	5.23	1.16	241.20	714.77
					•								
Lower	260	55.00	488.12	489.99	0.56	0.53	1.82	1.71	0.14	3.27	0.14	16.84	17.01
Lower	260	110.00	488.12	490.59	0.76	0.60	3.11	2.32	09.0	4.11	0.67	28.51	21.78
Lower	260	90.00	488.12	490.40	0.68	0.56	2.59	2.06	0.48	3.82	0.55	24.56	20.32
Lower	260	163.00	488.12	491.01	0.94	0.70	4.50	2.95	0.83	4.77	0.90	38.45	25.10
Lower	260	227.00	488.12	491.44	1.13	0.77	6.10	3.48	1.02	5.39	1.06	50.26	29.44
Lower	260	518.00	488.12	493.32	0.95	0.20	5.13	0.47	0.88	5.42	1.08	216.90	695.04
Lower	245	55.00	487.20	489 99	0.24	0.17	970	7.6.0	8	2745	8	i c	
Lower	245	110.00	487.20	490 60	0.30	0.30	4 40	200	300	2 6	0.03	0/707	2.5
Lower	245	90.00	487.20	490.41	0.32	0.25	0.89	990	0.00	2,00 87.0	0.45	30.01	23.00
Lower	245	163.00	487.20	491.03	0.54	0.40	2.04	134	0.76	3.75	0.52	5 00	25.00
Lower	245	227.00	487.20	491.46	0.72	0.50	3.16	1.87	0.92	4 42	0.00	50.83	28.60
Lower	245	518.00	487.20	493.38	09:0	0.12	2.60	0.21	0.72	4 37	28.0	208 47	702 50
												-	00.30
Lower	230	55.00	488.09	489.57	1.37	1.37	6.79	6.79		4.95		11.11	13.17
Lower	230	110.00	488.09	490.09	1.69	1.37	9.79	7.73	09.0	5.81	0.55	19.47	20.43
Lower	230	90.00	488.09	489.92	1.61	1.51	8.92	8.34	0.15	5.54	0.15	16.27	17.15
Lower	230	163.00	488.09	490.48	1.84	1.46	11.73	8,55	1.21	6.37	1.02	27.80	22.38
Lower	230	227.00	488.09	490.88	2.02	1.55	13.96	9.47	1.55	6.92	1.30	37.28	24.40

HEC-RAS Plan: Prop lower ineff River: Tanyard Branch Reach: Lower (Continued)

10001	ביינים סומ												
				VV.O. EIBV	onear chan	Shear lotal	Power Chan	Power Total	Vel Left	Vel Chul	Vel Right	Flow Area	Top Width
	000	(CIS)	(H)	(E)	(lb/sd ft)	(lb/sq ft)	(lb/ft s)	(lb/ft s)	(ft/s)	(£/s)	(ft/s)	(sq ft)	(£)
Lower	257	518.00	488.09	492.09	3.25	1.66	30.91	11.82	1.65	9.51	1.47	72.57	45.08
Lower	200	55.00	487.43	A80 30	0.68	CH							
	200	440.00	24.124	100.00	0.00	70.0	1.78	1.70	0.15	3.25	0.15	16.94	16.85
	300	00.00	407.43	409.91	0.74	¥.0	2.99	2.03	0.61	4.06	0.62	29.39	23.98
	200	8 8	01 101	403.12	70.0	0.53	2,54	1.90	0.49	3.80	0.50	24.90	21.68
	200	163,00	487.43	490.35	0.89	0.63	4.13	2.51	0.88	4.64	0.89	40.83	27.48
	38	227.00	487.43	490.80	1.05	0.72	5.44	3.04	1.10	5.20	1.11	53.81	30.61
Lower	320	518.00	487.43	492.13	1.87	0.83	13.96	4.13	1.00	7.46	1.45	104.15	61.22
	185	55.00	486.52	489.31	0,21	0.20	0.46	0.42	60.0	2.15	600	25.50	17 35
	185	110.00	486.52	489.92	0.39	0.26	1.19	0.74	0.40	3.07	040	30.08	SC. 11
Lower	185	90.00	486.52	489.72	0.33	0.24	0.91	0.63	0.31	278	0.34	34 13	20.70
Lower	185	163.00	486.52	490.36	0.53	0.34	1.95	1 07	0.65	3.70	000	2 6	23.73
Lower	185	227.00	486.52	490.82	0.67	0.43	2.86	1.45	78.0	0.5	3 6	02.03	30.92
Lower	185	518,00	486.52	492.17	1.36	0.57	B.84	OF C	0.00	4.20	0.82	00.83	34.54
								55.7	18:0	0,-0	0.1	123.80	68.98
Lower	170	55.00	487.40	488.84	1.53	1.53	7.96	7.95		FC 4		00.04	000
Lower	170	110.00	487.40	489.35	1.87	1.73	11.38	10.44	0.44	908	0.40	10.36	12.80
Lower	170	90.00	487.40	489.20	1.73	1.72	9.85	983	i	22.2	P S	10.20	17.40
	170	163.00	487.40	489.75	2.00	1.58	13.16	9.91	78.0	0.00	0 03	07.00	10.02
	170	227.00	487.40	490.16	2.14	1.50	15.23	9.49	960	7.11	4 2	20.00	21.47
Lower	170	518.00	487.40	491.74	2.22	1.20	17.78	6.42	1.51	00.8	1 79	20.02	29.42
												21:00	5
	145	55.00	486.75	488.66	0.50	0.47	1.57	1.47	0.19	3 13	0.18	17.64	47.00
	145	110.00	486.75	489.28	0.70	0.56	2.76	2.09	0.68	3.97	0.50	20 S	20.1.
	145	90.00	486.75	489.08	0.63	0.51	2.30	1.82	0.53	3.69	0.23	25.30	00,00
	145	163.00	486.75	489.71	0.87	29'0	4.02	2.79	0,94	4.61	08.0	36.98	22.40
	145	227.00	486.75	490.14	1.07	0.80	5.63	3.62	1.16	527	2 5	50.03	25.23
Lower	145	518.00	486.75	491.61	1.75	1.16	12.69	6.43	1.76	7.26	1.45	93.60	34.30
													2
	130	55.00	485.90	488.66	0.22	0.21	0.49	0.47	0.07	2.19	0.07	25.07	16.58
	3	110.00	485.90	489.27	0.40	0.32	1.26	96.0	0.45	3.13	0.39	36.95	21.36
	130	90.00	485.90	489.08	0.34	0.28	96.0	0.76	0.32	2.82	0.30	32.86	20.38
	130	163.00	485.90	489.71	0.56	0.43	2.15	1.50	0.68	3.82	0.59	46.75	23.54
	200	227.00	485.90		0.75	0.55	3.36	2.17	06.0	4.50	0.78	57.42	25.71
Lower	130	518.00	485.90	491.61	1.41	0.92	9.30	4.73	1.52	6.60	1.25	100.93	34.27
- Francisco	140	00	CE (CE)										
		33.00	400.12	488.16	33.	1.53	79.7	7.97		5.21		10.56	12.79
	110	00.011	486.72	488.67	1.88	1.70	11.40	10.26	0.43	6.08	0.43	18.21	17.82
	011	90.00	486.72	488.52	1.73	1.73	9.85	9.84		5.70		15.78	16.02
	011	163.00	486.72	489.03	2.10	1.63	14.15	10.37	0.92	6.74	0.93	25.59	22.13
Lower 1	110	227.00	486.72	489.39	2.39	1.84	17.79	12.36	1.36	7.45	1.45	33.79	23.57

HEC-RAS Plan: Prop lower ineff River: Tanyard Branch Reach: Lower (Continued)

Reach	River Sta	O Total	Min Ch El	W.S. Elev	Shear Chan	Shear Tatal	Dough Chan	Designa Taket	1,646,64				***************************************
		(cfs)	(#)	سرإ أ	(lb/soft)	(lh/ea ft)	(h/#s)	10,000	Yel Lell	Vel CDIII	Vel Right	Flow Area	Top Width
Pawer	110	518 00	408.70	2000	(11 hours)	(a) beauti	(100)	21/21/	(sne)	(sni)	(s/II)	(sq ft)	Œ
	2	300	400.12	69.08	3.35	2.45	32.24	19.07	2.21	9.62	2.37	66.64	28.60
Lower	80	55,00	485.96	487.87	0.51	0.48	1 49	4.43	Ĉ, C	2.4.0	0	201	
Lower	80	110.00	485 96	488 49	890	0 40	200	7 6	0.13	0.14	0.19	14.6	17.80
- with	UB	8	405.00	2000	300	54.0	2.07	57:	0.70	3.93	0.61	31.13	25.34
- LOWGI	8 8	30.00	480.08 B. C.	488.29	0.62	0.47	2.27	1,59	0.57	3.67	0.50	26.33	23.16
Lower	80	163.00	485.96	488.92	0.84	0.56	3.78	2.12	0.92	4.52	0.83	43.21	30.16
Lower	8	227.00	485.96	489.37	0.98	0.65	4.98	2.59	1.14	5.06	1.06	57.34	33.56
Lower	80	518.00	485.96	490.83	1.50	0.94	10.12	4.23	1.57	6.73	1.65	114.76	45.49
Lower	90	55.00	485.04	487.85	0.20	0.18	0.43	0.37	0.10	2.12	0.10	26.09	18.62
Lower	99	110.00	485.04	488.47	76.0	0.27	1.11	0.73	0.46	3.01	0.48	40.25	25.31
Lower	60	90.00	485.04	488.28	0.31	0.23	0.85	0.58	0.36	270	0.37	35 30	20 00
Lower	60	163.00	485.04	488.91	0.52	0.36	1.89	1.13	0.66	3.67	020	54.85	25.52 26.90
Lower	90	227.00	485.04	489.34	0.68	0.46	2.91	1.62	0.87	4.30	0.90	64 74	34 03
Lower	90	518.00	485.04	490.77	1.27	0.81	7.96	3.65	1.37	6.27	1.53	115.44	80.10 A0.38
													20.25
Lower	40	55.00	485.92	487.36	1.53	1.53	7.96	7.96		5.21		10 58	00 04
Lower	40	110.00	485.92	487.87	1.86	1.58	11.31	9.48	0.43	908	0.43	20.00 80.00	10.40
Lower	40	90.00	485.92	487.72	1,73	1.72	98.6	9.84		574	2	, c. 2	20.00
Lower	40	163.00	485.92	488.23	2.07	1.55	13.82	9:26	1.01	69'9	106	26.43	23.64
Lower	40	227.00	485.92	488.59	2.34	1.71	17.25	11.00	1.37	7.38	1.46	35.30	26.14
Lower	40	518.00	485.92	489.83	3.22	2.23	30.35	15.89	2.23	9.42	2.27	72.55	33.95
Lower	0	55.00	484.00	485.78	29'0	29'0	2.40	2.40		3.56		15.46	15.84
Lower	0	110.00	484.00	486.28	1.01	0.91	4.73	4.18	0.58	4.67	0.56	23.98	17.98
Lower	0	90:00	484.00	486.12	06.0	0.83	3.88	3.57	0.44	4.31	0.43	21.06	17.31
Lower	0	163.00	484.00	486.67	1.28	1.08	6.97	5.67	0.86	5.45	0.83	31.20	19.56
Lower	0	227.00	484.00		1.55	1.26	9.64	7.26	1.10	6.21	1.07	39.27	21.18
Lower	0	518,00	484.00	488.43	2.50	1.76	21.30	12.61	1.81	8.52	1.61	72.24	27.60

C3. Channel Stability (BEHII)

roject: 601 East

Bank soils D50= 10-11 mm Medium Gravel

oil Bulk Density (g/cm³)
oil Bulk Density (lb/ft²)
81.16

Left Bank 13.461 Total Soil 23.387 Soil Loss (tons/yr) Loss (tons/yr)

 $(g/cm^3) = 81.16 (lb/ft^3)$ Based on ChA and CmB soils

Loc	Loc	Bank	Bankfull	Root Depth	Root	Bank	Surface	Near Bank	Comments	Location	Stream Bnk Height/	Root Depth/	Bnk Height/	Root Depth/	Root	Bank	Surface Bank Mati	Stratification	Total Bank Eros	Bank Erosion	Bank Erosion	Bank Erosion
From Sta	to Sta	Height (ft)	Height (ft)	(feet)	Density %	Angle (deg)	Prot %	11 1	Comments	Sta to Station			Bankfull Height		Density	Angle	Protection Adjustment	11 11	Value Potential	Rate (ft/yr)	Volume (ft ³ /yr)	(tons/year)
TOILISIA		neight (tt)						Stress Index		Sta to Station						3.90		Aujustitierit		Kate (IVVI)	A Acidinie (Italyi)	(toris/year)
	17	1	1.00	0.25	95	60	90	1		U	17 1.00	0.25	1.00	6.54	1.23		1.45		14.12 Low	U	U	0
17	33	1	1.00	0.25	85	65	70	 		17	16 1,00	0.25	1.00	6.54	1.68	4.40	2.71		16.33 Low	0.000	440	
33	50	1	1.00	0.25	50	70	10	1 1		33	17 1.00	0.25	1.00	6.54	4.32	4.90	9.00		25.76 Moderate	0.066	1,12	0.045
50	63	3	1.00	0.25	10	80	0	 		50	13 3.00	0.08	10.00	8.67	8.44	5.90	10.00	 	43.01 Very High	0.5	19.5	0.791
63	80	3	1.00	0.25	30	85	0	2		63	17 3.00	0.08	10.00	8.67	5.90	6.84	10.00		41.41 Very High	0.6	30.6	1.242
80	105	3	1.00	0.25	10	80	0	<u> </u>		80	25 3.00	0.08	10.00	8.67	8.44	5.90	10.00		43.01 Very High	0.5	37.5	1.522
105	160	1	1.00	0.25	90	45	80	1 1		105	55 1.00	0.25	1.00	6.54	1.45	3.17	1.90		14.06 Low	0	0	0
160	195	3	1.00	0.25	10	45	10	1		160	35 3,00	0.08	10.00	8.67	8.44	3.17	9.00		39:28 High	80.0	8.4	0.341
195	225		1.00	0.25	90	45	80	1 1		195	30 1,00	0.25	1.00	6.54	1.45	3.17	1.90		14.06 Low	0 000	es movements a division and second	0
195	262		1.00	0.25	90	60	20	1		195	67 1.00	0.25	1.00	6.54	1,45	3.90	7.22		20,11 Moderate	0,066	4,42	0.179
262	290	2	1.00	- ŏ	0	60	10	11		262	28 2,00	0.00	7.90	10.00	10.00	3.90	9.00	-	40.80 Very High	0.5	28	1.136
290	375	3	1.00	0	0	45	0	2		290	85 3,00	0.00	10,00	10.00	10.00	3.17	10.00		43.17 Very High	0.6	153	6.209
375	475	2	1.00	0.25	30	65	10	1 1		375	100 2,00	0.13	7.90	8.11	5.90	4.40	9.00		35.31 High	0.08	16	0.649
475	529	1.5	1.50	0.5	90	30	90	4		475	54 1.00	0.33	1.00	5.60	1.45	2.44	1,45		11.94 Low	0	0	0
529	595	1	1.00	0.5	95	10	95	1 1		529	66 1.00	0,50	1.00	3.90	1.23	1,45	1,23	<u> </u>	8.80 Very Low	0	0	0
595	700	1	1.00	0.5	95	10	95	11	*	595	105 1.00	0,50	1.00	3.90	1,23	1.45	1,23		8.80 Very Low	0	0	0
700	750	1	1.00	1	95	5	95	11		700	50 1.00	1.00	1.00	1.00	1,23	1.23	1.23		5.68 Very Low	0	0	0
750	825	1	1.00	0.5	95	8	95	1 1		750	75 1.00	0.50	1.00	3.90	1,23	1.36	1.23		8.71 Very Low	0	0	0
825	847	0.5	0.50	0.25	80	80	15	1 1		825	22 1.00	0.50	1.00	3.90	1.90	5,90	7.90		20.60 Moderate	0.066	0,73	0.03
847	881		1.00	0.75	75	45	75	1 1		847	34 1.00	0.75	1.00	2.68	2,32	3,17	2.32		11.48 Low	0	0	0
881	895	1	1.00	0.25	50	60	50	·}	inside pool	881	14 1.00	0.25	1,00	6,54	4.32	3.90	4.32		20.08 Moderate	0.066	0,92	0.037
895	906	2	1.00	0.33	40	45	25	4	outside bend	895	11 2.00	0.17	7,90	7.63	5.11	3.17	6.54		30.35 High	0.2	4.4	0.179
906	987	0.5	0.50	0.75	75	45	50	1 1		906	81 1.00	1.50	1.00	1.00	2,32	3,17	4.32		11.80 Low	0	0	0
987	1013	2	1.00	0.33	40	20	20	1		987	26 2,00	0.17	7.90	7,63	5.11	1,90	7,22		29.76 Moderate	0,066	3,43	0.139
1013	1029	11	1.00	0.5	60	10	15	1 1		1013	16 1.00	0.50	1.00	3.90	3,50	1,45	7.90		17.75 Low	0	0	0
1029	1060	1.5	1.00	0.5	75	10	15	11		1029	31 1,50	0,33	5,90	5,60	2,32	1,45	7.90		23.17 Moderate	0,066	3.07	0,125
1060	1188	1.5	1.00	0.75	80	45	50	11		1060	128 1.50	0,50	5,90	3.90	1.90	3.17	4.32		19.19 Low	0	0	0
1188	1216	2	1.00	0.75	80	30	70	1	······	1188	28 2,00	0,38	7.90	5,10	1.90	2,44	2.71		20.05 Moderate	0,066	3.7	0.15
1216	1263	1	1.00	0.5	85	45	50	1		1216	47 1.00	0.50	1.00	3,90	1.68	3,17	4.32		14.06 Low	0	0	0
1263	1319	0.5	0.50	0.25	85	40	70	1		1263	56 1.00	0.50	1.00	3,90	1.68	2.93	2.71		12.21 Low	0	0	0
1319	1394	1	1.00	0.3	95	30	50	1		1319	75 1.00	0.30	1.00	5.90	1.23	2.44	4.32		14.88 Low	0	0	0
1394	1425	1.5	1.00	0.3	95	37	85	1	B4 at 590	1394	31 1.50	0.20	5.90	7.22	1.23	2.78	1.68		18.80 Low	0	0	0
1425	1445	1	1.00	0.4	95	40	95	1		1425	20 1.00	0.40	1.00	4.90	1.23	2.93	1.23		11.28 Low	0	0	0
1445	1481	1.25	1.00	0.4	90	30	90	1		1445	36 1.25	0.32	4.32	5.70	1.45	2.44	1:45		15.36 Low	0	0	0
1481	1487	3	1.00	0.4	40	15	10	4		1481	6 3.00	0.13	10.00	8.11	5.11	1.68	9.00		33.89 High	0.2	3.6	0.146
1487	1498	11	1.00	0.5	65	15	50	3		1487	11 1.00	0.50	1.00	3.90	3,11	1.68	4.32		14.00 Low	0	0	0
1498	1554	1.5	1.00	0.75	75	45	75	1		1498	56 1.50	0.50	5.90	3.90	2.32	3.17	2.32		17.60 Low	0	0	0
1554	1675	1	1,00	0.75	85	45	90	1		1554	121 1.00	0.75	1.00	2.68	1.68	3.17	1.45		9.98 Very Low	0] 0	0
1675	1685	1	1.00	0.5	75	15	10	3		1675	10 1.00	0.50	1.00	3.90	2,32	1.68	9.00		17.89 Low	0	0	0
1685	1718	1	1.00	0.75	90	35	80	1	cross section #5	1685	33 1.00	0.75	1.00	2.68	1.45	2.68	1,90		9.71 Very Low	0] 0	0
1718	1755	1.5	1.00	0.75	85	30	40	1		1718	37 1,50	0,50	5.90	3,90	1.68	2.44	5.11		19,02 Low	0	0	0
1755	1792	2.5	1.00	0.75	80	10	30	4	outside bend	1755	37 2.50	0.30	8,62	5,90	1.90	1.45	5,90		23.77 Moderate	0,1	9.25	0.375
1792	1836	1	1.00	0.3	80	45	75	1		1792	44 1.00	0.30	1.00	5,90	1.90	3,17	2.32		14.29 Low	0	0	0
1836	1867	2	1.00	1.5	75	40	30	1	inside	1836	31 2,00	0.75	7.90	2.68	2.32	2,93	5,90		21.72 Moderate	0.066	4.09	0.166
1867	1895	1	1.00	0.75	75	45	80	3	outside bend	1867	28 1.00	0.75	1.00	2.68	2.32	3.17	1,90		11.07 Low	0	0	0
1895	2015	0.5	0.50	0.75	87	35	40	1	from woods to muddy area	1895	120 1.00	1.50	1.00	1.00	1.59	2.68	5.11		11.38 Low	0	0	0
		0.75	1.00	1.25	85	40	50	1	wooded area near field	0	240 0.75	1.67	1.00	1.00	1.68	2,93	4.32		10.92 Low	0	0	0

Field Data Collected Project: 601 East

Right Bank Bank soils D50= 10-11 mm Medium Gravel

Soil Bulk Density (g/cm³)

Soil Bulk Density (lb/ft²)

1 (g/cm³) = 81.16 (lb/ft³)

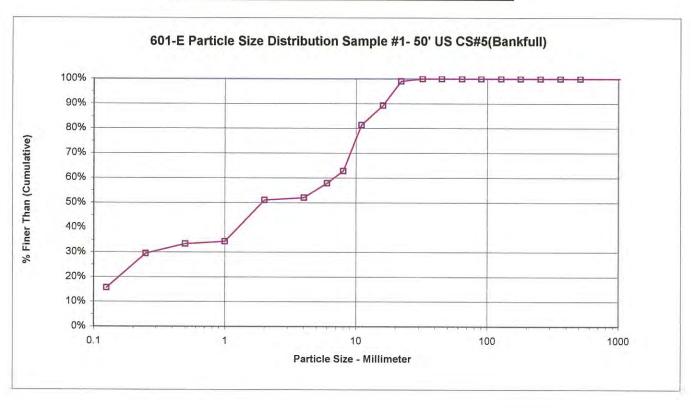
Based on ChA and CmB soils

Right Bank 9.926 Soil Loss (tons/yr)

			1		1 -	1 5 .	TO A	W 10 10 1			T 01	T 5 TO TO	D 10 11	I BILLIAN	In the state	5	1 5	1 0 1	I D. L.MH	1 Charles - 1 - 1	T-4-1	Paul Fare	Deal Francis	I Deal Francisco	I Danie Francis
From Cto	Loc	Bank		Root Depth		Bank	Surface	Near Bank	Comments	Location Sta to Station	Stream Length	Bnk Height/ Bankfull Height	Root Depth/ Bank Ht.	Bnk Height/ Bankfull Heigh	Root Depth/	Root	Bank Angle	Surface Protection	Bank Matl Adjustment	Stratification Adjustment	Total Value	Potential	Bank Erosion Rate (ft/yr)	NEW YORK AND ADDRESS OF THE OWNER.	The state of the s
From Sta	to Sta	Height (It)	Height (ft)	(feet)	/	Angle (deg)	-	Stress Index		Sta to Station		1.00		The state of the s		1.23	4.40	1.45	Adjustment	Adjustment	14.62	Low	O O	Volume (it /yr	(toris/year)
47	17	1	1.00	0.25	95	65	90	1		47	17	1.50	0.25 0.17	1.00 5.90	6.54 7.63	1.23	4.40	2.71			22.54	Moderate	0.066	1.58	0.064
17	33	1.5	1.00	0.25	80	65	70	1	ata 46 haadast	33	17	2.00	0.17	7.90	8.11	4.32	2.44	9.00		-	31.77	High	0.08	2.72	0.064
33	50	2	1.00	0.25	50	30 60	10	1	sta 46 headcut	50	13	3.00	0.13	10.00	8.67	7.22	3.90	10.00			39.79	High	0.08	3.12	0.117
63	63	3	1.00	0.25	20			1		63	17	1.50	0.00	5.90	10.00	10.00	5.40	10.00			41.30	Very High	0.6	15.3	0.624
	80	1.5	1.00	0	0	75	0	2		80	25	3.00	0.00	10.00	10.00	10.00	5.90	10.00		-	45.90	Very High	0.5	37.5	1.53
80	105	3	1.00	0		80	0	1				2.00	0.00	7.90	10.00	10.00	2.44	10.00			40.34	Very High	0.5	55	2.244
105	160	2	1.00	0.25	0	30 45	0	1		105	55 35	2.00	0.00	7.90	8.11	8.44	3.17	9.00		-	36.62	High	0.08	5.6	0.228
160 195	195	2	1.00		10	45	10	+ +	sta 225 headcut	195	30	2.00	0.00	7.90	10.00	10.00	3.17	10.00			41.07	Very High	0.5	30	1.224
	225	25	1.00	0			0	1		225	37	2.50	0.00	8.62	8.44	4.32	4.90	10.00		-	36.28		0.08	7.4	0.302
225	262	2.5	1.00	0.25	50	70	0	1	sta 262 headcut	262	28	3.00	0.00	10.00	10.00	10.00	3.17	10.00			43.17	High Von High	0.5	42	1.714
262	290	3	1.00	0	0	45	0	1		290		3.00	0.00	10.00	8.67	5.90	3.17	10.00		-	37.74	Very High	0.1	25.5	1.04
	375	3	1.00	0.25	30	45	0	1			85	1.00		1.00	6.54	1.90		2.71			15.32	High Low	0.1	25.5	1.04
375	487	1 1 5	1.00	0.25	80	45 60	70	1 4		375 487	112 25	1.00	0.25	1.00	7.63	5.90	3.17	9.00			27.43	Moderate	0.1	3,75	0.153
487 512	512	1.5	1.50	0.25 0.25	30 90	15	10	4		512	83	1.00	0.17	1.00	6.54	1.45	1.68	1.45		-	12.12	Low	0.1	0	0.155
	595 700	-	1.00	0.25	95	10	95	1	ata 014 was ation 1	595	105	1.00	0.25	1.00	2.68	1.23	1.45	1.43			7.58	Very Low	0	0	0
595			1.00			8		1	sta 614 xsection 1	700	50	1.00	0.75	1.00	2.68	1.23	1.45	1.23			7.49	Very Low	0	0	0
700 750	750 825	-	1.00	0.75 0.5	95 95	10	95	1	sta 770 xsection 2	750	75	1.00	0.75	1.00	3.90	1.23	1.45	1.23		-	8.80	Very Low	0	0	0
825	837	0.5	0.50	0.5	75	80	95 45	1	Sta 770 xSection 2	825	12	1.00	0.50	1.00	3.90	2.32	5.90	4.71			17.83	Low	0	0	0
837	881	0.5	0.50	0.25	40	80	40	1		837	44	1.00	0.40	1.00	4.90	5.11	5.90	5.11		-	22.02	Moderate	0.066	1,45	0.059
		0.5				45		1		881	14	1.49	0.40	5.84	5.60	3.11	3.17	3.50			21.22	Moderate	0.066	0.92	0.038
881	895 905	- 1	0.67 1.00	0.33	65 65	50	60	1	outside pool	895	10	2.00	0.33	7.90	8.11	3.11	3.41	1.90			24.43	Moderate	0.066	1.32	0.054
895	987	2	0.50	0.25	70	40	80	1	inside bend	905	82	1.00	1.00	1.00	1.00	2.71	2.93	1.68			9.31	Very Low	0.000	0	0.054
905	1013	0.5	1.00	0.33	45	10		1		987	26	2.00	0.17	7.90	7.63	4.71	1.45	2.32			24.01	Moderate	0.066	3.43	0.14
987 1013	1013	0.67	0.67	0.35	40	10	75 75	-		1013	16	1.00	0.17	1.00	5.20	5.11	1.45	2.32			15.08	Low	0.000	0.45	0.14
	1060	1.5	1.00	0.25	80	10	85	1		1029	31	1.50	0.33	5.90	5.60	1.90	1.45	1.68			16.53	Low	0	0	0
1060	1211	1.5	1.00	0.5	80	15	80	3		1060	151	1.00	0.50	1.00	3.90	1.90	1.68	1.90			10.38	Low	0	0	0
1211	1263	1.5	1.50	0.75	70	20	70	1		1211	52	1.00	0.50	1.00	3.90	2.71	1.90	2.71			12.23	Low	0	0	0
	1319	0.33	0.33	0.75	80	55	70	1		1263	56	1.00	1.52	1.00	1.00	1.90	3.66	2.71			10.27	Low	0	0	0
1319	1319	1.25	1.00	0.5	75	20	70	1		1319	75	1.25	0.80	4.32	2.44	2.32	1.90	2.71			13.68	Low	0	0	0
			1.00	1.25	75	25	80	1		1394	31	2.50	0.50	8.62	3.90	2.32	2.19	1.90		-	18.93	Low	0	0	0
1394	1425	2.5	1.00	1.25	75	35	70	1		1425	20	2.00	0.63	7.90	3.27	2.32	2.68	2.71		-	18.88	Low	0	0	0
1445	1481	1.5	1.00	1.75	80	45	80	1		1445	36	1.50	1.17	5.90	1.00	1.90	3.17	1.90	-		13.87	Low	0	0	0
	1498	1.75	0.75	1.75	75	40	75	1		1481	17	2.33	0.57	8.41	3.56	2.32	2.93	2.32			19.52	Low	0	0	0
1498	1547	1.75	1.00	1	75	32	75	1		1498	49	2.00	0.50	7.90	3.90	2.32	2.54	2.32			18.97	Low	0	0	0
1547	1558	1.5	1.00	0.33	60	45	80	4		1547	11	1.50	0.22	5.90	6.95	3.50	3.17	1.90			21.42	Moderate	0.1	1.65	0.067
1558	1650	0.75	0.75	0.75	75	30	85	1		1558	92	1.00	1.00	1.00	1.00	2.32	2.44	1.68		-	8.43	Very Low	0	1.00	0.007
1650	1685	0.75	1.00	0.75	85	12	80	1		1650	35	1.00	0.75	1.00	2.68	1.68	1.54	1.90			8.80	Very Low	0	0	0
	1718	4	1.00	0.75	85	35	85	1	Ben's xsection 4	1685	33	1.00	2.00	1.00	1.00	1.68	2.68	1.68			8.03	Very Low	0	0	
	1755	2.75	1.00	1.75	85	12	75	1	Den's xsection 4	1718	37	2.75	0.64	8.94	3.22	1.68	1.54	2.32			17.69	Low	0	0	
	1792	2.70	1.00	1.75	75	45	80	1		1755	37	2.00	0.50	7.90	3.90	2.32	3.17	1.90			19.19	Low	0	0	1
1792	1809	2	1.00	1	65	5	65	3	eroding outer bank	1792	17	2.00	0.50	7.90	3.90	3.11	1.23	3.11			19.19	Low	0	0	
1809	1830		0.75	0.45	65	29	55	1		1809	21	3.00	0.20	10.00	7.22	3.11	2.39	3.90			26.62	Moderate	0.066	3.1185	0.12
1830	1845	2.25 3.25	0.75	1	75	5	80	3	near pump house slight erosion	1830	15	6.50	0.20	10.00	5.80	2.32	1.23	1.90			21.24	Moderate	0.000	1.95	0.0
1845	1867	3.25	1.00	2.25	80	5	85	4		1845	22	3.25	0.69	10.00	2.97	1.90	1.23	1.68		-	17.77	Low	0.04	0	0.0
1867	1895	3.23	0.50	1.25	75	45	75	1	erosion outer bend inner bend	1867	28	2.00	1.25	7.90	1.00	2.32	3.17	2.32			16.70	Low	0	0	
	2015	0.5	0.50	0.75	85	35	45	1 1	to the mucky area	1895	120	1.00	1.50	1.00	1.00	1.68	2.68	4.71			11.07	Low	0	0	1
ear road	2015	0.75	1.00	1.5	85	40	50	1	to the mucky drea	near road	50	0.75	2.00	1.00	1.00	1.68	2.93	4.71			10.92	Low	0	0	

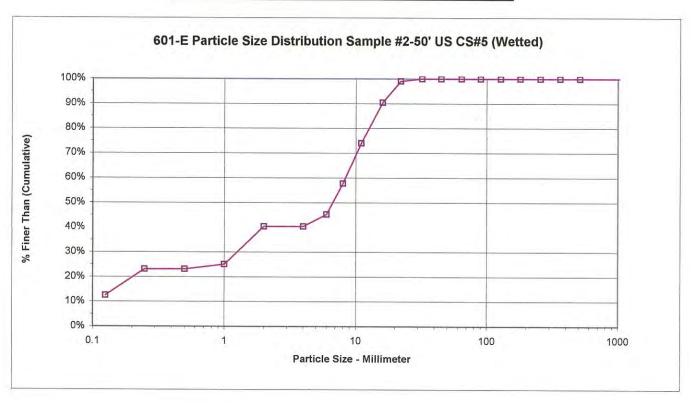
			PEBBLE C	COUNT				
Project:	601 East					Date:	1/3/201	13
Location:	50' Upstream	Cross Section	18/B5 (Bai	nkfull)				
				Particle	Counts			
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	8	0	8	8%	8%
	Very Fine	.062125	S	8	0	8	8%	16%
	Fine	.12525	Α	14	0	14	14%	29%
	Medium	.2550	N	4	0	4	4%	33%
	Coarse	.50 - 1.0	D	1	0	1	1%	34%
.0408	Very Coarse	1.0 - 2.0	S	17	0	17	17%	51%
.0816	Very Fine	2.0 - 4.0		1	0	1	1%	52%
.1622	Fine	4.0 - 5.7	G	6	0	6	6%	58%
.2231	Fine	5.7 - 8.0	R	5	0	5	5%	63%
.3144	Medium	8.0 - 11.3	A	19	0	19	19%	81%
.4463	Medium	11.3 - 16.0	V	8	0	8	8%	89%
.6389	Coarse	16.0 - 22.6	E	10	0	10	10%	99%
.89 - 1.26	Coarse	22.6 - 32.0	L	1	0	1	1%	100%
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	0	0	0	0%	100%
1.77 - 2.5	Very Coarse	45.0 - 64.0		0	0	0	0%	100%
2.5 - 3.5	Small	64 - 90	C	0	0	0	0%	100%
3.5 - 5.0	Small	90 - 128	0	0	0	0	0%	100%
5.0 - 7.1	Large	128 - 180	В	0	0	0	0%	100%
7.1 - 10.1	Large	180 - 256	::::::L:::::::	0	0	0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	100%
14.3 - 20	Small	362 - 512	\mathbf{L}	0	0	0	0%	100%
20 - 40	Medium	512 - 1024	D	0	0	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	100%
	Bedrock		BDRK	0	0	0	0%	100%
			Totals	102	0	102	100%	100%

d16 d3	5 d50	d84 d95
0.1	0 19	127 195



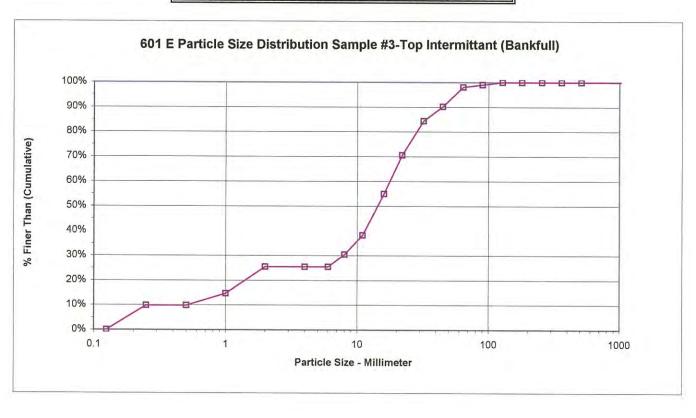
			PEBBLE C	COUNT				
Project:	601 East					Date:	1/3/201	13
Location:	50' Upstream	Cross Section	18/B5 (We	etted Perime	ter)			
				Particle	Counts			
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	9	0	9	9%	9%
	Very Fine	.062125	S	4	0	4	4%	13%
	Fine	.12525	Α	11	0	11	11%	23%
	Medium	.2550	N	0	0	0	0%	23%
	Coarse	.50 - 1.0	D	2	0	2	2%	25%
.0408	Very Coarse	1.0 - 2.0	S	16	0	16	15%	40%
.0816	Very Fine	2.0 - 4.0		0	0	0	0%	40%
.1622	Fine	4.0 - 5.7	G	5	0	5	5%	45%
.2231	Fine	5.7 - 8.0	R	13	0	13	13%	58%
.3144	Medium	8.0 - 11.3	Α	17	0	17	16%	74%
.4463	Medium	11.3 - 16.0	V	17	0	17	16%	90%
.6389	Coarse	16.0 - 22.6	E	9	0	9	9%	99%
.89 - 1.26	Coarse	22.6 - 32.0	L	1	0	1	1%	100%
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	0	0	0	0%	100%
1.77 - 2.5	Very Coarse	45.0 - 64.0		0	0	0	0%	100%
2.5 - 3.5	Small	64 - 90	С	0	0	0	0%	100%
3.5 - 5.0	Small	90 - 128	0	0	0	0	0%	100%
5.0 - 7.1	Large	128 - 180	В	0	0	0	0%	100%
7.1 - 10.1	Large	180 - 256	<u>L</u>	0	0	0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	100%
14.3 - 20	Small	362 - 512	£	0	0	0	0%	100%
20 - 40	Medium	512 - 1024	D	0	0	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	100%
	Bedrock		BDRK	0	0	0	0%	100%
			Totals	104	0	104	100%	100%

d16	d35	d50	d84	d95
0.2	1.7	6.8	14.0	19.2



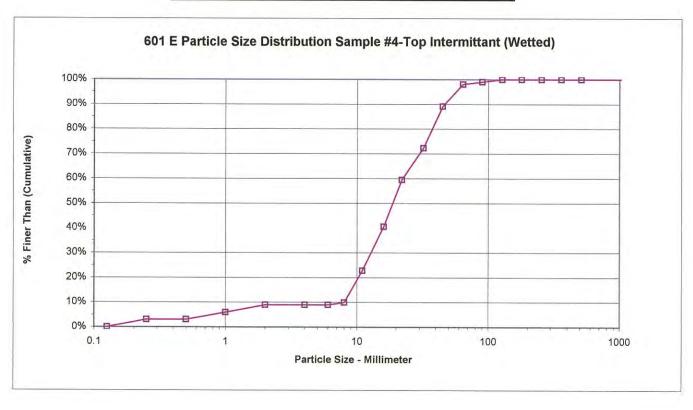
			PEBBLE C	COUNT				
Project:	601 East					Date: 1-3-2	013	
Location:	Top (Intermitta	ant) Bankfull						
				Particle	Counts			
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	0	0	0	0%	0%
	Very Fine	.062125	S	0	0	0	0%	0%
	Fine	.12525	Α	10	0	10	10%	10%
	Medium	.2550	N	0	0	0	0%	10%
	Coarse	.50 - 1.0	D	5	0	5	5%	15%
.0408	Very Coarse	1.0 - 2.0	S	11	0	11	11%	25%
.0816	Very Fine	2.0 - 4.0		0	0	0	0%	25%
.1622	Fine	4.0 - 5.7	G	0	0	0	0%	25%
.2231	Fine	5.7 - 8.0	R	5	0	5	5%	30%
.3144	Medium	8.0 - 11.3	Α	8	0	8	8%	38%
.4463	Medium	11.3 - 16.0	V	17	0	17	17%	55%
.6389	Coarse	16.0 - 22.6	E	16	0	16	16%	71%
.89 - 1.26	Coarse	22.6 - 32.0	L	14	0	14	14%	84%
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	6	0	6	6%	90%
1.77 - 2.5	Very Coarse	45.0 - 64.0		8	0	8	8%	98%
2.5 - 3.5	Small	64 - 90	C	1	0	1	1%	99%
3.5 - 5.0	Small	90 - 128	0	1	0	1	1%	100%
5.0 - 7.1	Large	128 - 180	В	0	0	0	0%	100%
7.1 - 10.1	Large	180 - 256		0	0	0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	100%
14.3 - 20	Small	362 - 512	L	0	0	0	0%	100%
20 - 40	Medium	512 - 1024	D	0	0	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	100%
	Bedrock		BDRK	0	0	0	0%	100%
			Totals	102	0	102	100%	100%

d16	d35	d50	d84	d95
1.1	9.8	14.5	31.8	56.6



			PEBBLE C	COUNT				
Project:	601 East					Date: 1-3-2	013	
Location:	Top (Intermitta	ant) (Wetted)						
				Particle	Counts			
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	0	0	0	0%	0%
	Very Fine	.062125	S	0	0	0	0%	0%
	Fine	.12525	Α	3	0	3	3%	3%
	Medium	.2550	N	0	0	0	0%	3%
	Coarse	.50 - 1.0	D	3	0	3	3%	6%
.0408	Very Coarse	1.0 - 2.0	S	3	0	3	3%	9%
.0816	Very Fine	2.0 - 4.0		0	0	0	0%	9%
.1622	Fine	4.0 - 5.7	G	0	0	0	0%	9%
.2231	Fine	5.7 - 8.0	R	1	0	1	1%	10%
.3144	Medium	8.0 - 11.3	Α	13	0	13	13%	23%
.4463	Medium	11.3 - 16.0	V	18	0	18	18%	41%
.6389	Coarse	16.0 - 22.6	E	19	0	19	19%	59%
.89 - 1.26	Coarse	22.6 - 32.0	L	13	0	13	13%	72%
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	17	0	17	17%	89%
1.77 - 2.5	Very Coarse	45.0 - 64.0		9	0	9	9%	98%
2.5 - 3.5	Small	64 - 90	C	1	0	1	1%	99%
3.5 - 5.0	Small	90 - 128	0	1	0	1	1%	100%
5.0 - 7.1	Large	128 - 180	В	0	0	0	0%	100%
7.1 - 10.1	Large	180 - 256	L.	0	0	0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	100%
14.3 - 20	Small	362 - 512	L.	0	0	0	0%	100%
20 - 40	Medium	512 - 1024	D	0	0	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	100%
	Bedrock		BDRK	0	0	0	0%	100%
			Totals	101	0	101	100%	100%

d16	d35	d50	d84	d95
9.4	14.4	19.0	41.1	57.6



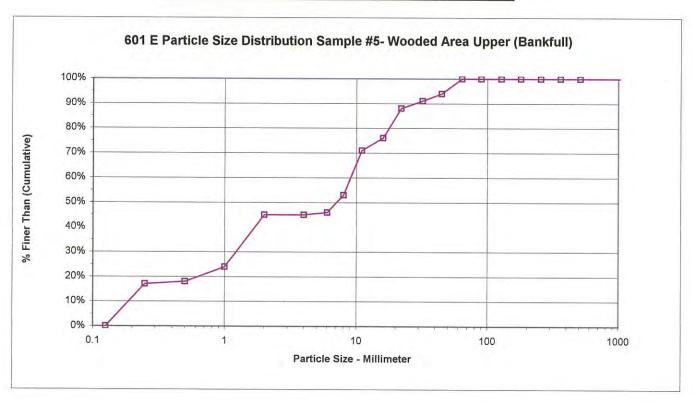
			PEBBLE C	COUNT				
Project:	601 East					Date: 1-3-2	013	
Location:	(Wooded Are	a) Pump Hous	e (Wetted)					
				Particle	Counts			
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	0	0	0	0%	0%
	Very Fine	.062125	S	0	0	0	0%	0%
	Fine	.12525	Α	1	0	1	1%	1%
	Medium	.2550	N	1	0	1	1%	2%
	Coarse	.50 - 1.0	D	6	0	6	6%	8%
.0408	Very Coarse	1.0 - 2.0	S	15	0	15	15%	22%
.0816	Very Fine	2.0 - 4.0		0	0	0	0%	22%
.1622	Fine	4.0 - 5.7	G	5	0	5	5%	27%
.2231	Fine	5.7 - 8.0	R	10	0	10	10%	37%
.3144	Medium	8.0 - 11.3	Α	15	0	15	15%	51%
.4463	Medium	11.3 - 16.0	V	15	0	15	15%	66%
.6389	Coarse	16.0 - 22.6	E	11	0	11	11%	77%
.89 - 1.26	Coarse	22.6 - 32.0	L	11	0	11	11%	87%
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	7	0	7	7%	94%
1.77 - 2.5	Very Coarse	45.0 - 64.0		6	0	6	6%	100%
2.5 - 3.5	Small	64 - 90	C	0	0	0	0%	100%
3.5 - 5.0	Small	90 - 128	0	0	0	0	0%	100%
5.0 - 7.1	Large	128 - 180	В	0	0	0	0%	100%
7.1 - 10.1	Large	180 - 256	$\mathbf{L}_{\mathbf{k}}$	0	0	0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	100%
14.3 - 20	Small	362 - 512	L	0	0	0	0%	100%
20 - 40	Medium	512 - 1024	D	0	0	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	100%
	Bedrock		BDRK	0	0	0	0%	100%
			Totals	103	0	103	100%	100%

d16	d35	d50	d84	d95
1.6	7.6	10.7	28.8	47.7



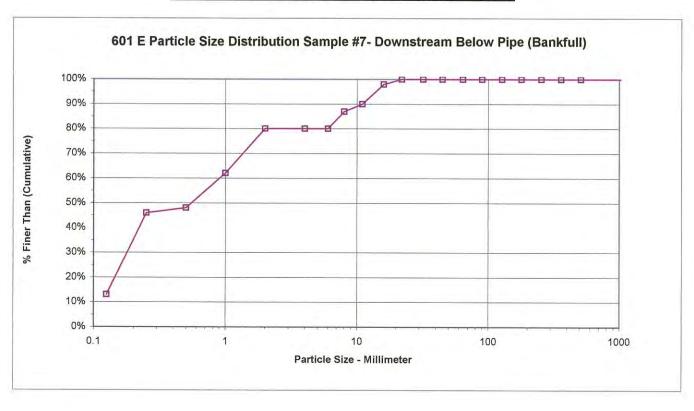
			PEBBLE C	COUNT				
Project:	601 East					Date: 1-3-2	013	
Location:	(Wooded Are	a) Pump Hous	e (Bankfull)					
				Particle	Counts			
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	0	0	0	0%	0%
	Very Fine	.062125	S	0	0	0	0%	0%
	Fine	.12525	Α	17	0	17	17%	17%
	Medium	.2550	N	1	0	1	1%	18%
	Coarse	.50 - 1.0	D	6	0	6	6%	24%
.0408	Very Coarse	1.0 - 2.0	S	21	0	21	21%	45%
.0816	Very Fine	2.0 - 4.0		0	0	0	0%	45%
.1622	Fine	4.0 - 5.7	G	1	0	1	1%	46%
.2231	Fine	5.7 - 8.0	R	7	0	7	7%	53%
.3144	Medium	8.0 - 11.3	Α	18	0	18	18%	71%
.4463	Medium	11.3 - 16.0	V	5	0	5	5%	76%
.6389	Coarse	16.0 - 22.6	E	12	0	12	12%	88%
.89 - 1.26	Coarse	22.6 - 32.0	L	3	0	3	3%	91%
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	3	0	3	3%	94%
1.77 - 2.5	Very Coarse	45.0 - 64.0		6	0	6	6%	100%
2.5 - 3.5	Small	64 - 90	C	0	0	0	0%	100%
3.5 - 5.0	Small	90 - 128	0	0	0	0	0%	100%
5.0 - 7.1	Large	128 - 180	В	0	0	0	0%	100%
7.1 - 10.1	Large	180 - 256	L	0	0	0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	100%
14.3 - 20	Small	362 - 512	L	0	0	0	0%	100%
20 - 40	Medium	512 - 1024	D	0	0	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	100%
	Bedrock		BDRK	0	0	0	0%	100%
			Totals	100	0	100	100%	100%

d16	d35	d50	d84	d95
0.2	1.5	7.1	20.0	48.2



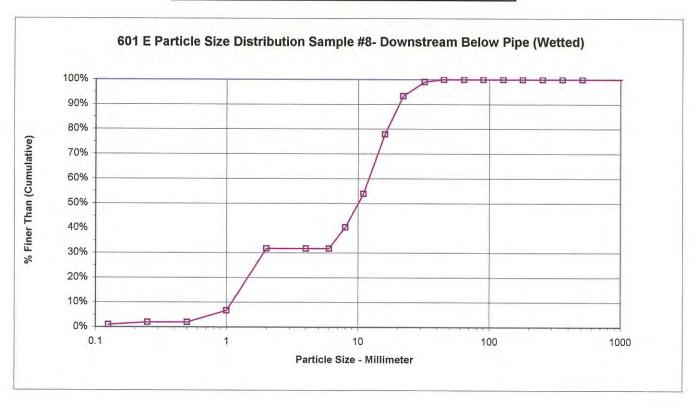
			PEBBLE C	OUNT				
Project:	601 East					Date: 1-3-2	013	
Location:	Downstream I	Below Pipe (Ba	ankfull)					
				Particle	Counts			
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	8	0	8	8%	8%
	Very Fine	.062125	S	5	0	5	5%	13%
	Fine	.12525	Α	33	0	33	33%	46%
	Medium	.2550	N	2	0	2	2%	48%
	Coarse	.50 - 1.0	D	14	0	14	14%	62%
.0408	Very Coarse	1.0 - 2.0	S	18	0	18	18%	80%
.0816	Very Fine	2.0 - 4.0		0	0	0	0%	80%
.1622	Fine	4.0 - 5.7	G	0	0	0	0%	80%
.2231	Fine	5.7 - 8.0	R	7	0	7	7%	87%
.3144	Medium	8.0 - 11.3	Α	3	0	3	3%	90%
.4463	Medium	11.3 - 16.0	V	8	0	8	8%	98%
.6389	Coarse	16.0 - 22.6	E	2	0	2	2%	100%
.89 - 1.26	Coarse	22.6 - 32.0	L	0	0	0	0%	100%
1.26 - 1.77	Very Coarse		S	0	0	0	0%	100%
1.77 - 2.5	Very Coarse	45.0 - 64.0		0	0	0	0%	100%
2.5 - 3.5	Small	64 - 90	C	0	0	0	0%	100%
3.5 - 5.0	Small	90 - 128	0	0	0	0	0%	100%
5.0 - 7.1	Large	128 - 180	В	0	0	0	0%	100%
7.1 - 10.1	Large	180 - 256		0	0	0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	100%
14.3 - 20	Small	362 - 512	L	0	0	0	0%	100%
20 - 40	Medium	512 - 1024	D	0	0	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	100%
	Bedrock		BDRK	0	0	0	0%	100%
			Totals	100	0	100	100%	100%

d16	d35	d50	d84	d95
0.1	0.2	0.6	7.1	14.1



			PEBBLE C	COUNT				
Project:	601 East					Date: 1-3-2	013	
Location:	Downstream B	Below Pipe (we	etted perime	eter)				
				Particle	Counts			
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	0	0	0	0%	0%
	Very Fine	.062125	S	1	0	1	1%	1%
	Fine	.12525	Α	1	0	1	1%	2%
	Medium	.2550	N	0	0	0	0%	2%
	Coarse	.50 - 1.0	D	5	0	5	5%	7%
.0408	Very Coarse	1.0 - 2.0	S	26	0	26	25%	32%
.0816	Very Fine	2.0 - 4.0		0	0	0	0%	32%
.1622	Fine	4.0 - 5.7	G	0	0	0	0%	32%
.2231	Fine	5.7 - 8.0	R	9	0	9	9%	40%
.3144	Medium	8.0 - 11.3	Α	14	0	14	13%	54%
.4463	Medium	11.3 - 16.0	V	25	0	25	24%	78%
.6389	Coarse	16.0 - 22.6	E	16	0	16	15%	93%
.89 - 1.26	Coarse	22.6 - 32.0	L.	6	0	6	6%	99%
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	1	0	1	1%	100%
1.77 - 2.5	Very Coarse	45.0 - 64.0		0	0	0	0%	100%
2.5 - 3.5	Small	64 - 90	C	0	0	0	0%	100%
3.5 - 5.0	Small	90 - 128	0	0	0	0	0%	100%
5.0 - 7.1	Large	128 - 180	В	0	0	0	0%	100%
7.1 - 10.1	Large	180 - 256	E E	0	0	0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	100%
14.3 - 20	Small	362 - 512	Ŀ	0	0	0	0%	100%
20 - 40	Medium	512 - 1024	D	0	0	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	100%
	Bedrock		BDRK	0	0	0	0%	100%
			Totals	104	0	104	100%	100%

d16	d35	d50	d84	d95
1.4	6.8	10.1	18.4	25.0



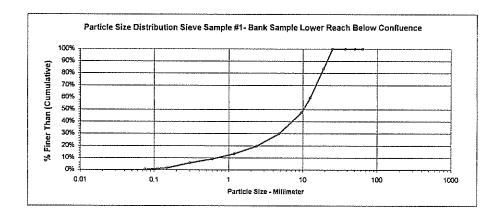
Pavement Type: Bank Soil Sample
Sample Date: 1/4/2013
Project: 601 East Existing Conditions
Location: Below confluence of 2 tributaries in lower reach

Largest Particle on bar ====	:=>	N/A

Sieve Size	Sleve Size (mm)	Sleve Weight (Lbs)	Sieve + Sample Welght (Lbs)	Sieve + Sample Welght (Lbs)	Sieve + Sample Welght (Lbs)	Sleve + Sample Weight (Lbs)	Total Weight (Lbs)
2 1/2 inch	63	1.175					0
2 inch	50	1.195					0
1 1/2 inch	37.5	1.25					0
1 inch	25	1.23					0
3/4 inch	19	1.245	1.96	WIII-1000			0.715
1/2 inch	12.5	1.21	2.27				1.08
3/8 inch	9.5	1.225	1.76				0.535
No. 4	4.75	- 1.145	1.92				0.775
No. 8	2.36	1.07	1.51		·· ·		0.44
No. 16	1.18	0.955	1.24				0.285
No. 30	0.6	0.9	1.09			ï	0.19
No. 50	0.3	0.815	0.96		. T		0.145
No. 100	0.15	0.775	0.96				0.185
No. 200	0.075	0.765	0.81		Į.		0.045
Passing 200	<0.075	1.08	1.1				0.02

Total Sample Weight =======> 4.395

ocation: Project:	0		Sieve Sample	#1		
Inches	Sleve	Millimeter		Wt. Retained (lbs)	% Passing	% Cumulative
	Size	< #200	S/C	0.02	0.46%	0.46%
0.0029	#200	0.0750	(())) (()(S ()()()()()	0.045	1.02%	1.48%
0.0059	#100	0.150	(48646)A 64666	0.185	4.21%	5,69%
0.0117	#50	0.30		0.145	3.30%	8,90%
0.0234	#30	0.60		0.19	4.32%	13,31%
0.0469	#16	1.18	: S	0.285	6.48%	19.80%
0.0937	#8	2.36	::::::::::::::::::::::::::::::::::::::	0.44	10.01%	29.81%
0.187	#4	4.75	G R	0.775	17.63%	47.44%
0.374	3/8"	9.50	1200103-800300	0.535	12.17%	59.61%
0.5	1/2"	12.50	A V	1.06	24.12%	83.73%
0.748	3/4"	19.0	Light Control	0.715	16,27%	100.00%
0.9843	1"	25.0	[16]	0	0.00%	100.00%
1.4784	1 1/2"	37.5	(100 ± 100	0	0.00%	100,00%
1.9685	2"	50.0		0	0.00%	100.00%
2.5	2 1/2"	63.0	100 00 CO 000 C	1 0	0.00%	100.00%
				0	0.00%	100,00%
				0	0.00%	100.00%
				0	0.00%	100.00%
			600 000 B (0000)	0	0.00%	100,00%
				0	0.00%	100.00%
				0	0,00%	100.00%
NATION AND AND AND AND AND AND AND AND AND AN			(4) (4) (1) (4)	0	0.00%	100.00%
	Bedrock		20RK	0	0.00%	100.00%
			Totals	4,395	100%	100%



Pavement Type: Sample Date: Project:

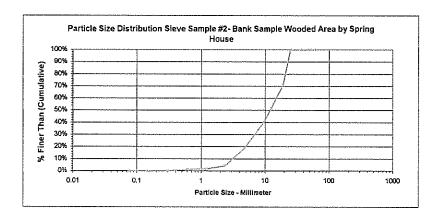
Bank Sample 1/3/2013 601 East Existing Conditions Upper Wooded Area by Spring House

Location: Largest Particle on bar ====>

Sleve Size	Sieve Size (mm)	Sleve Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sjeve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Total Welght (Lbs)
2 1/2 inch	63	1.175				T	
2 inch	50						0
1 1/2 inch	37.5	1.195					0
1 inch	25	1.23			<u></u> ,		0
3/4 inch	19	1.245	1.94			i	0.695
1/2 inch	12.5	1.21	1,67				0.48
3/8 inch	9.5	1.225	1.51				0.285
No. 4	4.75	1.145	1.66				0.515
No. 8	2.36	1.07	1.42	•			0.35
No. 16	1.18	0.955	1.02				0.065
No. 30	0.6	0.9	0.91				0.01
No. 50	0.3	0.815	0.84				0.025
No. 100	0.15	0.775					0
No. 200	0.075	0.765					0
Passing 200	<0.075	1.08				l	0

Total Sample Weight =======> 2.405

			Sieve Sample	#2		
Location: Project:	0					
Inches	Sieve	Millimeter		Wt. Retained (ibs)	% Passing	% Cumulative
~	Size	< #200	s/c	C	0.00%	0.00%
0.0029	#200	0.0750	[(c) (c) S ((c) (c)	0	0.00%	0.00%
0.0059	#100	0.150	169206	0	0.00%	0.00%
0.0117	#50	0.30	News to	0.025	1.04%	1.04%
0.0234	#30	0.60	120 D 3 D 3 D 3 D 3 D 3 D 3 D 3 D 3 D 3 D	0.01	0.42%	1.48%
0,0469	#16	1.18	John Strong	0.085	2.76%	4,16%
0.0937	#8	2.36	Comments of the Comments	0.35	14,55%	18.71%
0.187	#4	4.75	14.5.12 R-12.5.1	0.515	21.41%	40.12%
0.374	3/8"	9.50	A-0	0.285	11.85%	51.98%
0.5	1/2"	12.50	15332 V 34333	0.46	19.13%	71.10%
0.748	3/4"	19.0	Process English	0.695	28,90%	100.00%
0.9843	1"	25.0		0 }	0.00%	100.00%
1.4764	1 1/2	37.5	\$350 S	0 1	0.00%	100.00%
1.9885	2'	50.0	100000000000000000000000000000000000000	0	0.00%	100.00%
2.5	2 1/2"	63.0	\$ 0.000 C 0.000 E	0	0.00%	100.00%
			100000000000000000000000000000000000000	0	0.00%	100.00%
	!		F100000 B 000000	0	0,00%	100.00%
	<u> </u>		<u> Passagensag</u>	0	0.00%	100.00%
			1334 St. B-1336 R	0	0.00%	100.00%
				0	0.00%	100.00%
			1300 (10 b 10 c)	0	0,00%	100.00%
			Programme Reserved	0	0.00%	100.00%
and an analysis and an an	Bedrock		BDRK	0	0.00%	100.00%
			Totals	2.405	100%	100%



Pavement Type: Sample Date: Project:

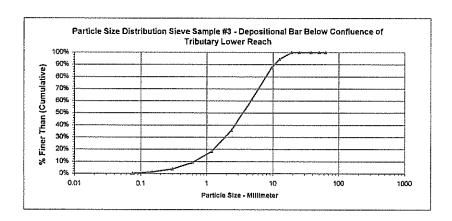
Depositional Bar 1/4/2013 601 East Depositional Bar in channel below confluence of 2 tributaries at lower stream segment below road

Location: Deposition:

Siève Size	Sieve Size (mm)	Sieve Weight (Lbs)	Sleve + Sample Weight (Lbs)	Sieve + Sample Welght (Lbs)	Sieve + Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Total Weight (Lbs)
2 1/2 inch	63	1,175					C
2 inch	50	1,195					0
1 1/2 inch	37.5	1.25		***			0
1 inch	25	1.23					0
3/4 inch	19	1.245					0
1 <i>1</i> 2 inch	12.5	1.21	1,49	1.45			0.52
3/8 inch	9.5	1.225	1.52	1.59			0.66
No. 4	4.75	1.145	2.54	2.23			2.48
No. 8	2.36	1.07	2.36	2.15			2.37
No. 16	1.18	0.955	1.83	1.72]	1.64
No. 30	0.6	0.9	1.35	1.31			0.88
No. 50	0.3	0.815	1.07	1.05			0.49
No. 100	0.15	0.775	0.89	0.89			0.23
No. 200	0.075	0.765	0.81	0.83			0.11
Passing 200	<0.075	1.08	1.1	1			0.02

Total Sample Weight =======> 9.38

ocation: Project:	o		Sieve Sample i	# 3		
Inches	Sieve	Millimeter		Wt. Retained (lbs)	% Passing	% Cumulative
	Size	< #200	s/c	0.02	0.21%	0.21%
0.0029	#200	0.0750	10000 S . 1000	0.11	1.17%	1.39%
0.0059	#100	0.150		0.23	2.45%	3.64%
0.0117	#50	0.30	1 1 1 1 2 N 1 1 1 1 2 1 2 1 2 1 2 1 2 1	0.49	5.22%	9.06%
0.0234	#30	0.60	D	0.86	9.17%	18.23%
0.0460	#16	1.13	in in since	1.64	17.45%	35.71%
0.0937	#8	2.38		2.37	25.27%	60.98%
0.187	#4	4.75	R. B.	2.48	26.44%	87.42%
0.374	3/8"	9.50	A STATE OF THE	0.66	7,04%	94,46%
0.5	1/2"	12.50	ν,	0.52	5.54%	100.00%
0.748	3/4"	19.0	V.	0	0.00%	100.00%
0.9843	1"	25.0	s i	0	0.00%	100,00%
1.4764	1 1/2"	37.5	\$	0	0.00%	100,00%
1.9685	2'	50.0		0	0.00%	100.00%
2.5	2 1/2"	63.0	1.00 00 \$ 000 00	0	0.00%	100,00%
			100 00 Q 000 00	0	0.00%	100,00%
			1000000 B100000	0	0.00%	100.00%
				0	0.00%	100.00%
			В	0	0.00%	100.00%
	1			0	0.00%	100.00%
				0	0.00%	100.00%
	·		1. 13. R . 1. 1. 1.	0	0.00%	100.00%
	Bedrock		BORK	0	0.00%	100.00%
garana Turkur			· Totals	9.38	100%	100%



Sieve Sample #4 Pavement Type: Sample Date: Project: Location:

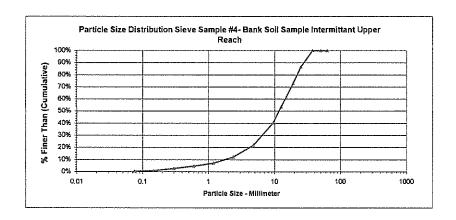
Bank Soll Sample	
1/3/2013	
601 East Existing Conditions	
Intermittant upper roadh	

Location: Intermittant upper reach
Largest Particle on bar =====> N/A

Sleve Size	Sieve Size (mm)	Sleve Weight (Lbs)	Sieve + Sample Weight (Lbs)	Sieve + Sample Weight (Lbs)	Sleve + Sample Welght (Lbs)	Sievo +Sample Welght (Lbs)	Total Weight (Lbs)
2 1/2 inch	63	1.175				1	О
2 inch	50	1,195					0
1 1/2 inch	37,5	1,25				<u> </u>	0
1 inch	25	1.23	2.03				0.8
3/4 inch	19	1.245	2.05				0.805
1/2 inch	12.5	1.21	2.37				1.16
3/8 inch	9.5	1.225	2.01				0.785
No. 4	4.75	1.145	2.25				1.105
No. 8	2.38	1.07	1.65				0.58
No. 16	1.18	0.955	1.25				0.295
No. 30	0.6	0.9	1.05			ĺ	0.15
No. 50	0,3	0.815	0.93				0.115
No. 100	0.15	0.775	0.88				0.105
No. 200	0.075	0.765	8.0				0.035
Passing 200	<0.075	1.08	1.1			l	0.02

Total Sample Weight ======> 5,955

Location: Project:	0		Sieve Sample #4					
Inches	Sieve Size	Millimeter < #200	sic	Wt. Retained (lbs)	% Passing 0.34%	% Cumulative		
0.0029	#200	0.0750	S S	0.035	0.59%	0.92%		
0.0029	#100	0.0750		0.035	1.76%	2.69%		
	#100		Notes N					
0.0117	į I	0.30	b	0.115	1.93%	4.82%		
0.0234	#30	0.60		0.15	2.52%	7.14%		
0.0469	#16	1,18	Š.	0.295	4.05%	12.00%		
0.0937	#8	2.36	G	0.58	9.74%	21.83%		
0.187	#4	4.75	1500000 R 0000000	1.105	18.56%	40.30%		
0.374	3/8"	9.50	TO CHARLES	0.785	13,18%	53,57%		
0.5	1/2"	12,50	The Control of the Co	1.18	19.48%	73.05%		
0.748	3/4"	19.0	1333336	0.805	13.52%	80.57%		
0,9843	1"	25.0	s s	8.0	13.43%	100.00%		
1.4764	1 1/2"	37.5	S	Q.	0,00%	100.00%		
1,9685	2'	50.0		0	0.00%	100.00%		
2.5	2 1/2"	63.0	135 34 G 100 30	0	0.00%	100.00%		
			10000 9 00000	0	0,00%	100.00%		
	1		NAME OF BRIDE	0	0.00%	100.00%		
				0	0.00%	100.00%		
			B	0	0.00%	100.00%		
			132 324 20 33	o l	0.00%	100,00%		
			Programme Programme (Co.)	0	0.00%	100.00%		
			23000 R 20000	0	0.00%	100.00%		
	Bedrock		BDRK	0	0.00%	100.00%		
			Totals	5,955	100%	100%		



Pavement Type: Sample Date: Project: Location:

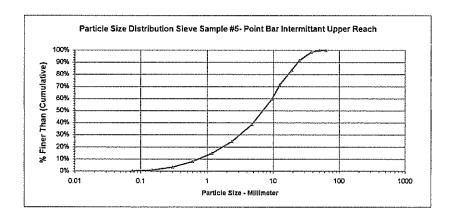
Point Bar Sample 1/3/2013 601 East Existing Conditions Intermittant upper reach

Largest Particle on bar =====>

(5		S				/ATANAMA ALEATANNIA	
Sleve Size	Sleve Size (mm)	Sieve Welght (Lbs)	Sieve + Sample Weight (Lbs)	Sleve + Sample Weight (Lbs)	Sleve + Sample Welght (Lbs)	Sieve +Sample Weight (Lbs)	Total Weight (Lbs)
	·						
2 1/2 inch	63	1.175					. 0
2 inch	50	1.195					0
1 1/2 inch	37.5	1,25		1.6			0.35
1 inch	25	1.23	1.74	1.79	1.79		1.63
3/4 inch	19	1.245	1.77	1.92	1.93		1.885
1/2 inch	12.5	1,21	2.07	2.37	2.08		2.89
3/8 inch	9.5	1.225	2,25	1.94	2.3		2.815
No. 4	4.75	1.145	2.48	2.63	1.84	2.56	4.93
No. 8	2.36	1.07	1.82	2.11	1.37	2.3	3.32
No. 16	1.18	0.955	1.34	1.68	1.39	1.7	2.29
No. 30	0.6	0.9	1.18	1.33	1.29	1-41	1.61
No. 50	0.3	0.815	0.95	1.13	1.12	1,19	1,13
No. 100	0.15	0.775	0.86	0.92	0.95	0.95	0.58
No. 200	0.075	0.765	0.79	0,81	0.8	0.8	0.14
Passing 200	<0.075	1.08	1.09	1.09	1.09	1.1	0.05

Total Sample Weight ======== 23.62

Sieve Sample #4 Location: 0 Protect:							
Inches	Sleve	Millimeter		Wt. Retained (lbs)	% Passing	% Cumulativ	
	Size	< #200	s/c	0.05	0.21%	0.21%	
0.0029	#200	0,0750	::::::::::::::::::::::::::::::::::::::	0.14	0.59%	0.80%	
0.0059	#100	0.150	11.150 (A) 11.150	0.58	2.40%	3,26%	
0.0117	#50	0.30	A SECTION AND A	1.13	4.78%	8.04%	
0.0234	#30	0.60	D111111	1.61	6.82%	14.86%	
0.0460	#16	1.18	STATE OF STA	2.29	9.70%	24.58%	
0.0937	#8	2.36		3.32	14.06%	38.61%	
0.187	#4	4.75	R	4.93	20.87%	59,48%	
0.374	3/8"	9.50	A CONTRACTOR	2.815	11,92%	71.40%	
0.5	1/2"	12,50	100 00 V	2.89	12.24%	83.64%	
0.748	3/4"	19.0	E L S	1.085	7.98%	91.62%	
0.9843	1"	25.0		1.63	6.90%	98,52%	
1.4764	1 1/2"	37.5	130000 S 000000	0.35	1.48%	100.00%	
1.9685	2"	50.0	344024464	0	0.00%	100.00%	
2,5	2 1/2"	63.0	::::::::::::::::::::::::::::::::::::::	0	0.00%	100,00%	
			o constant	. 0	0.00%	100.00%	
	!	ļ	1451 000 1 g 1360 146	0	0.00%	100.00%	
			Same and the contract	0	0.00%	100.00%	
		<u> </u>	Control Brooking	0	0.00%	100.00%	
	1		procession and the	0	0.00%	100.00%	
	i		D	0	0.00%	100.00%	
			144 154 R 144 144 1	0	0.00%	100.00%	
	Bedrock		BDRK:	0	0.00%	100.00%	
0,4241474147454747414141	1,10,10,10,10,10,10,10,10,10,10,10,10,10		Totals	23.62	100%	100%	



Pavement Type: Sample Date: Project: Location:

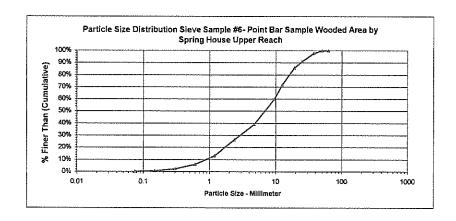
Bank Soil Sample 1/3/2013 601 East Existing Conditions

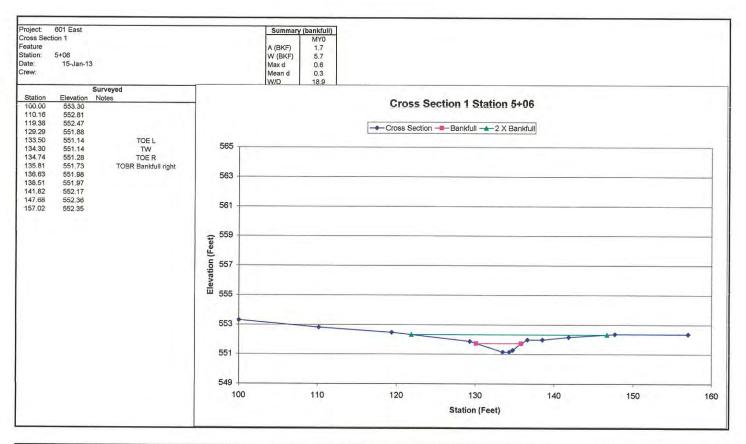
Location: Intermittant upper reach
Largest Particle on bar ====> 2.3 inches

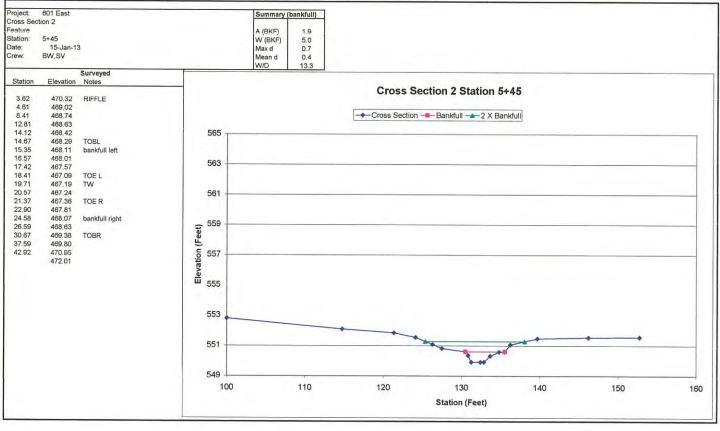
Sieve Size	Slava Size (mm)	Sleve Weight (Lbs)	Sleve + Sample Weight (Lbs)	Sieve + Sample Weight (Lbs)	Sieve + Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Tota! Weight (Lbs)
2 1/2 inch	63	1.175	1.175			<u> </u>	0
2 inch	50	1.195	1.195				0
1 1/2 inch	37.5	1.25	1,25	1.65			0.4
1 inch	25	1.23	1.89	1.72			1.15
3/4 inch	19	1.245	1.89	1.53			0.93
1/2 inch	12.5	1.21	2.85	1.98			2.41
3/8 inch	9.5	1.225	2.5	2			2.05
No. 4	4.75	1,145	3.42	2.47			3.8
No. 8	2.36	1.07	2.64	1.7			2.2
No. 16	1.18	0.955	2.3	1.89			2.28
No. 30	0.6	0.9	1.46	1.57			1.23
No. 50	0.3	0.815	1.09	1.17			0.63
No. 100	0.15	0.775	0.91	0.9			0.26
No. 200	0.075	0.765	0.81	0.82		-	0.1
Passing 200	<0,075	1.08	1.09	1.1			0.03

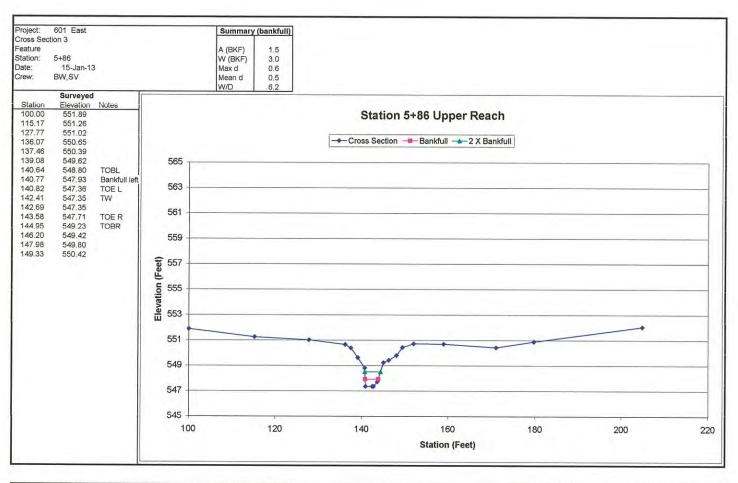
Total Sample Weight =======> 17.27

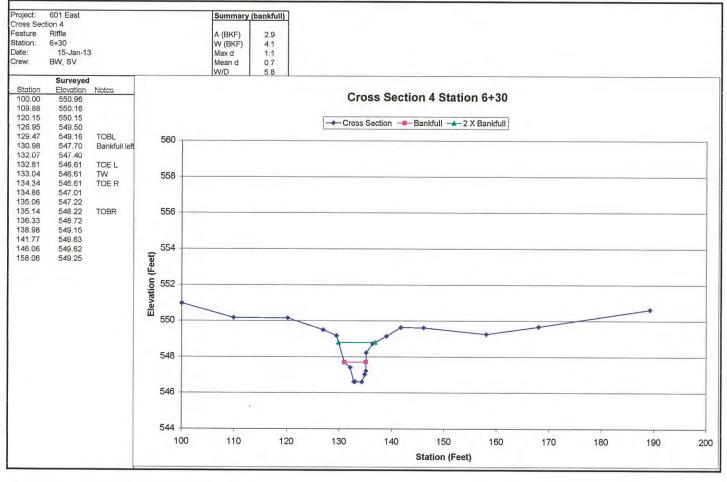
Sieve Sample #4 Location: 0 Project:								
Inches	Sleve Size	Millimeter < #200	 	Wt. Retained (lbs)	% Passing 0.17%	% Cumulative 0.17%		
0.0029					***************************************	-		
	#200	0.0750		0.1	0.58%	0,75%		
0.0059	#100	0.150	100000	0.26	1.51%	2.26%		
0.0117	#50	0.30	(All Property Name of the All	0.63	3.65%	5.91%		
0.0234	#30	0.60	Participation (Control of Control	1.23	7.12%	13.03%		
0.0469	#16	1.18	, s	2.28	13.20%	26.23%		
0.0937	#8	2.36	G ····	2.2	12.74%	38.97%		
0.187	#4	4.75	R	3.6	20.85%	59.81%		
0.374	3/6"	0.50		2.05	11.87%	71.69%		
0.5	1/2"	12.50	V	2.41	13.95%	85,64%		
0.748	3/4"	19.0	10 E 10 E	0.93	5,39%	91.02%		
0.9843	1"	25.0	The state of the state of the state of	1.15	8.68%	97.68%		
1.4764	1 1/2"	37.5	ŝ	0.4	2.32%	100.00%		
1.9685	2"	50.0	144514444444444444444444444444444444444	0	0.00%	100.00%		
2.5	2 1/2"	63,0	10:10:00 (X 10:00:00)	0	0.00%	100.00%		
				0	0.00%	100.00%		
			100000000000000000000000000000000000000	0	0.00%	100.00%		
	1		Language Francisco	0	0.00%	100.00%		
			district Brancher	0	0.00%	100.00%		
	1			0	0.00%	100,00%		
			(100 to 100 to 1	0	0.00%	100.00%		
			1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	0	0.00%	100.00%		
	Bedrock		BDRK	Û	0.00%	100.00%		
	****		· Totals	17.27	100%	100%		

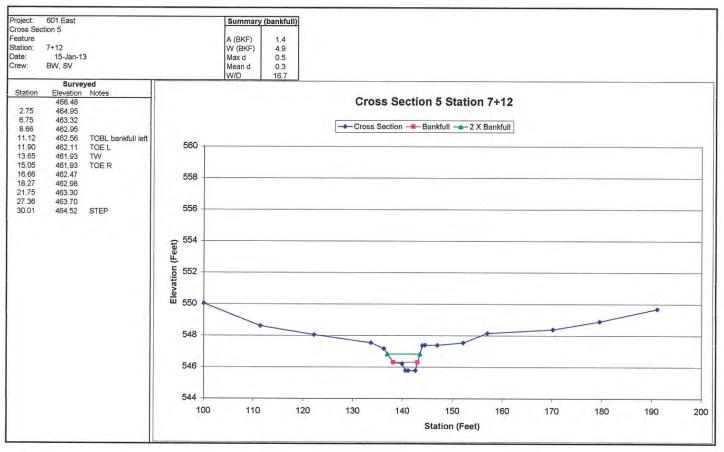


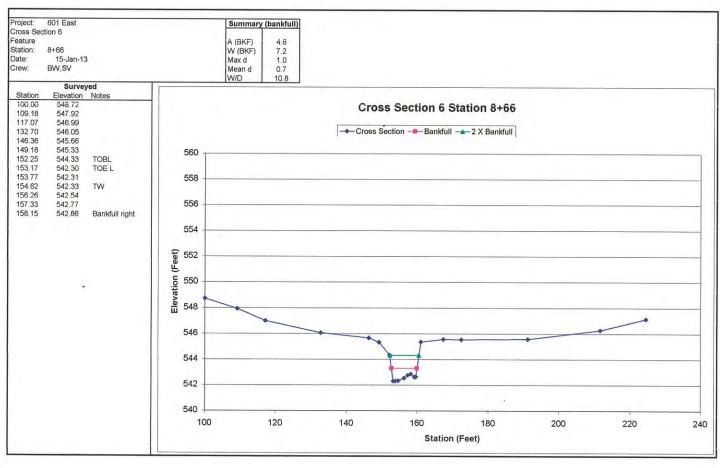


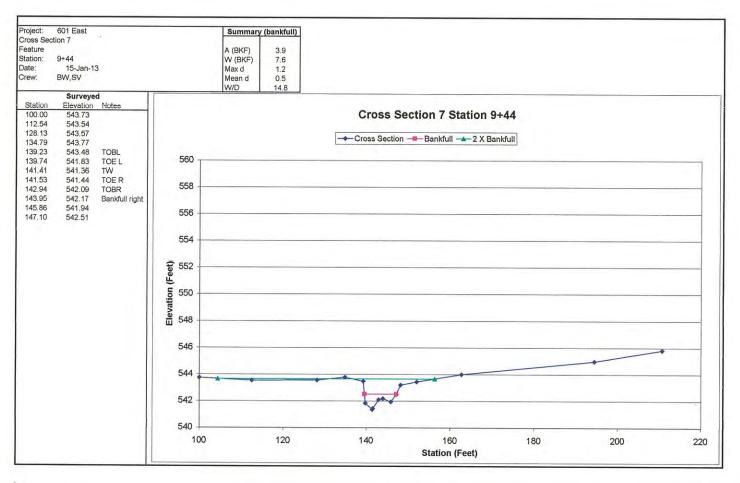


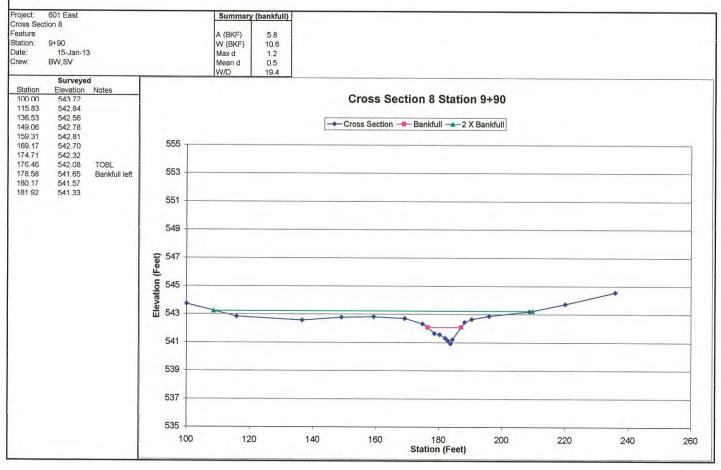


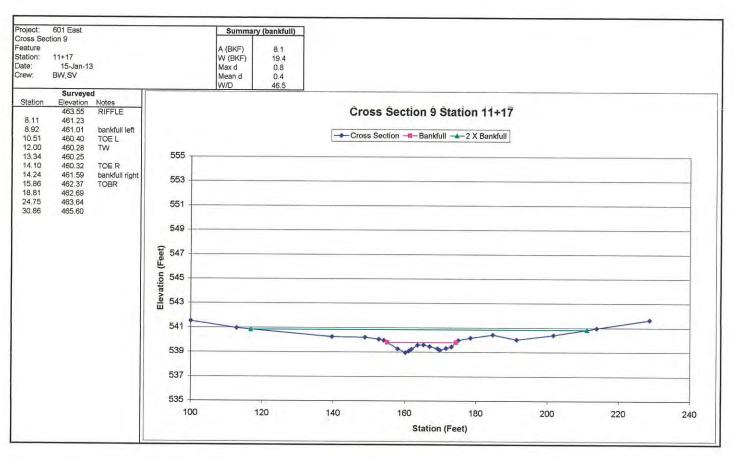


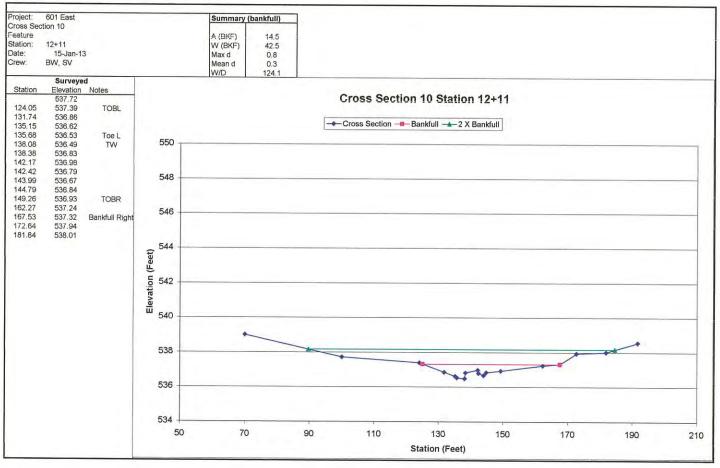


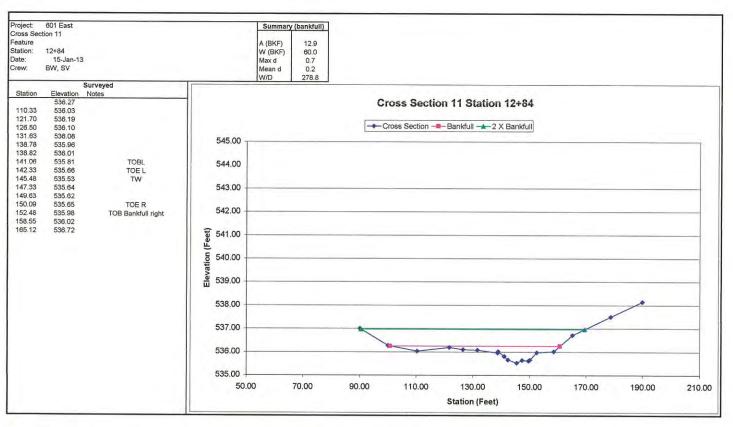


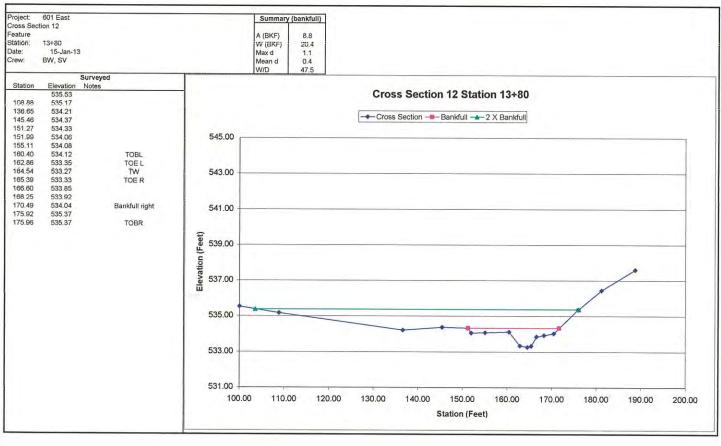


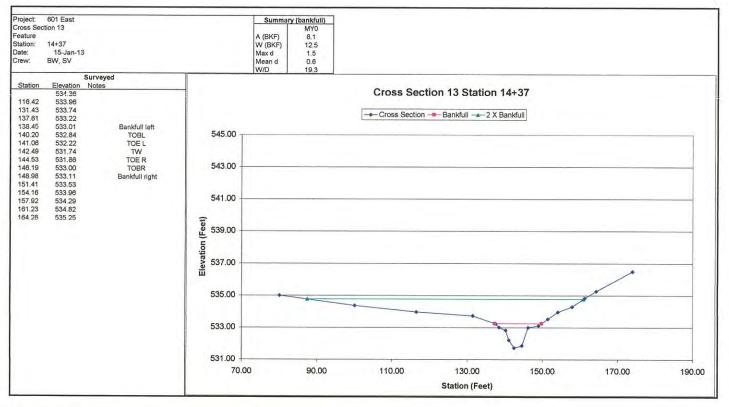


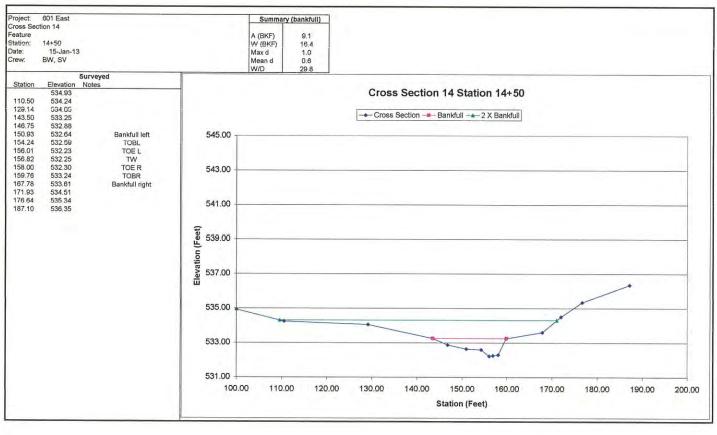


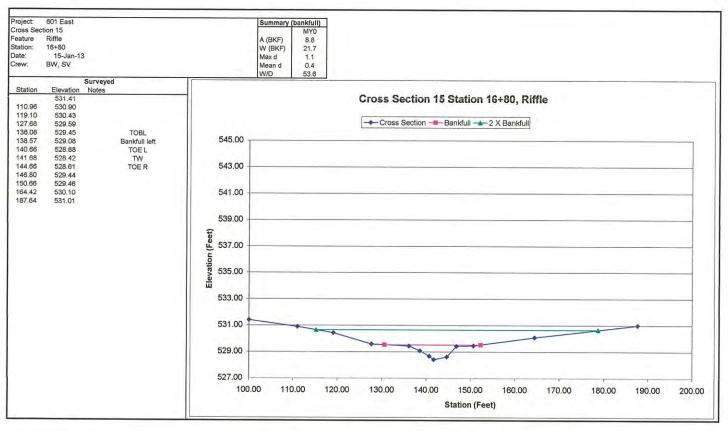


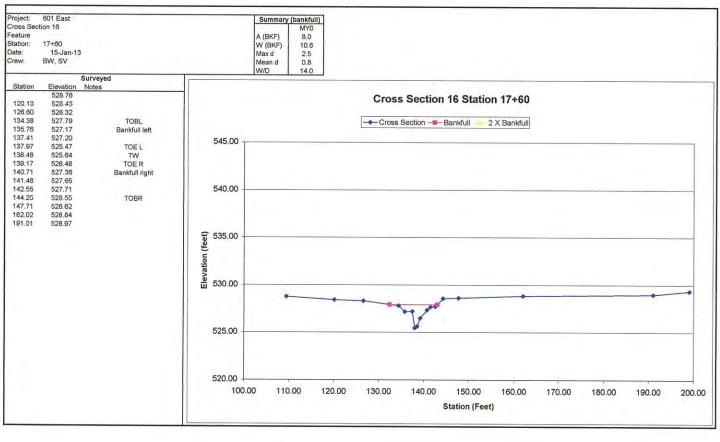


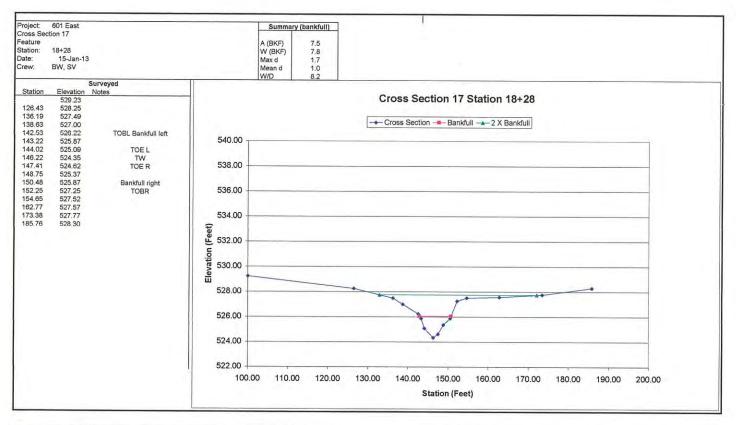


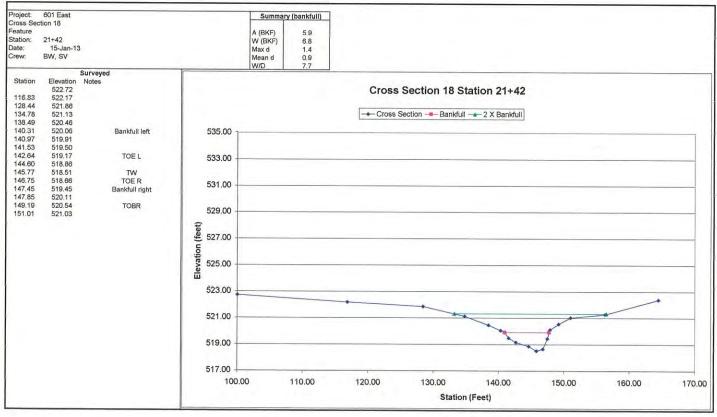


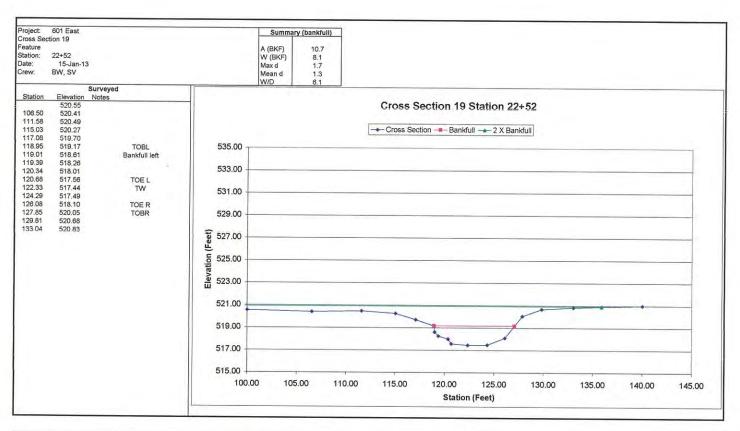


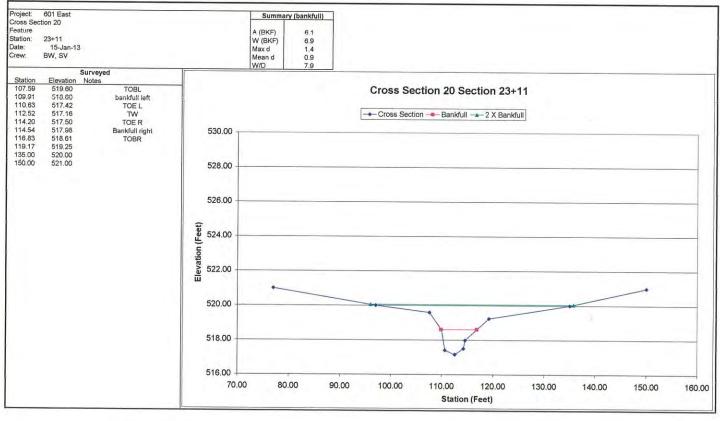


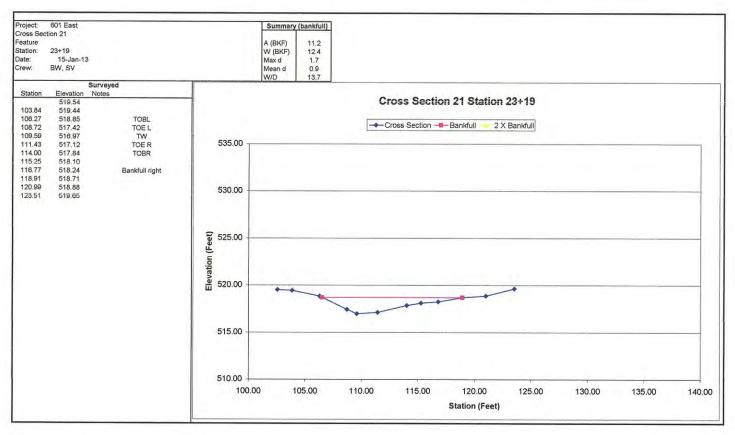


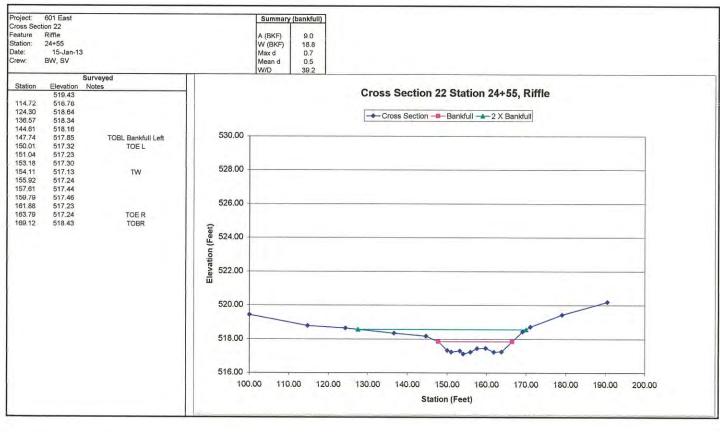


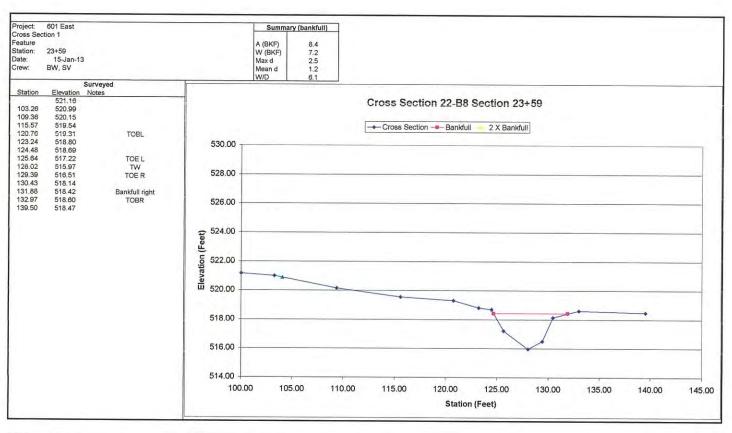


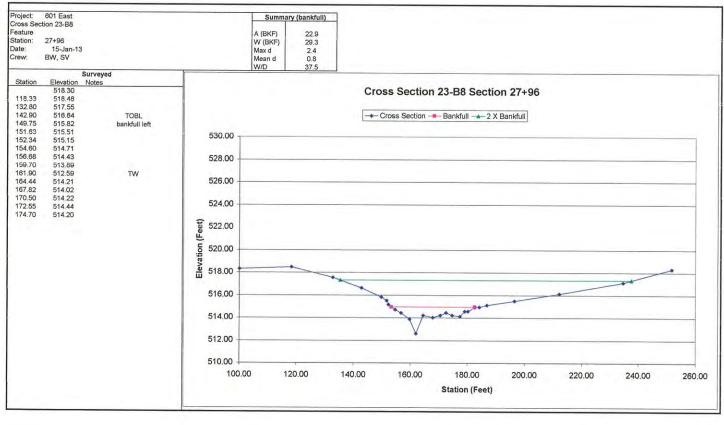


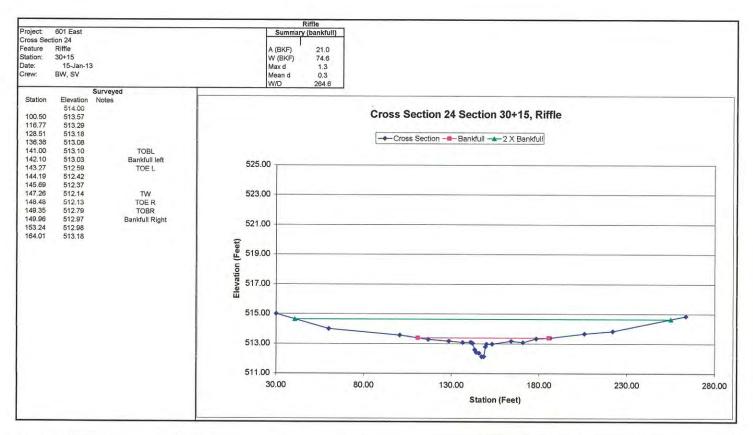


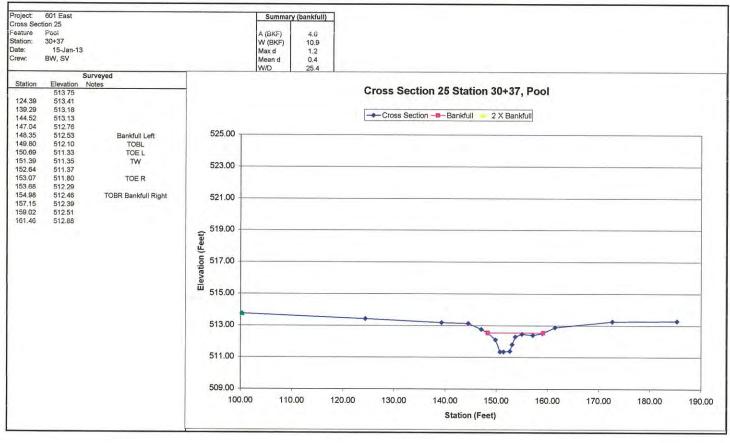


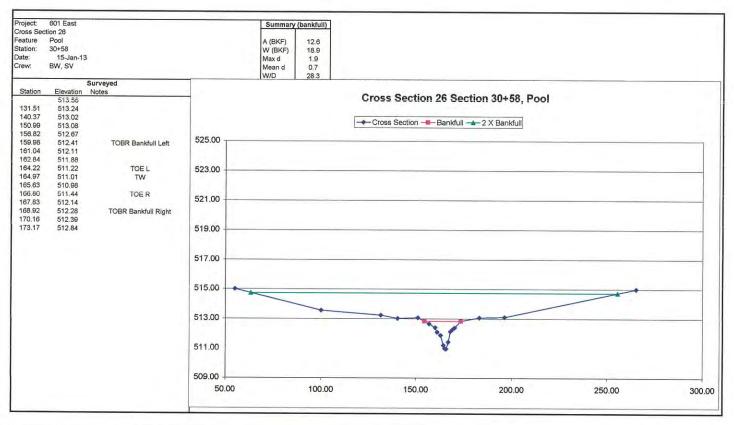


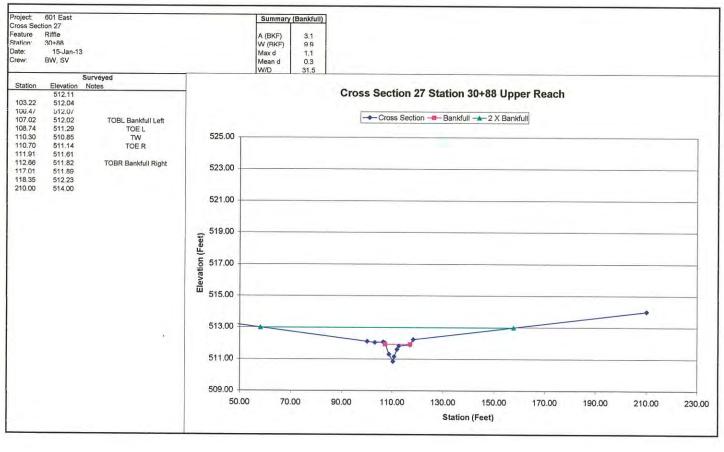




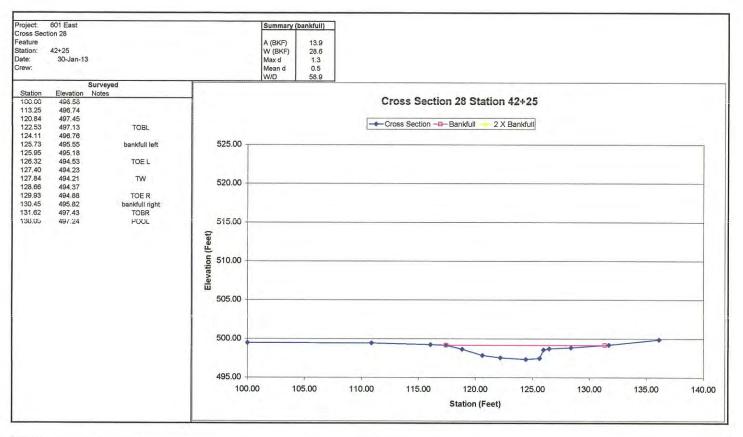


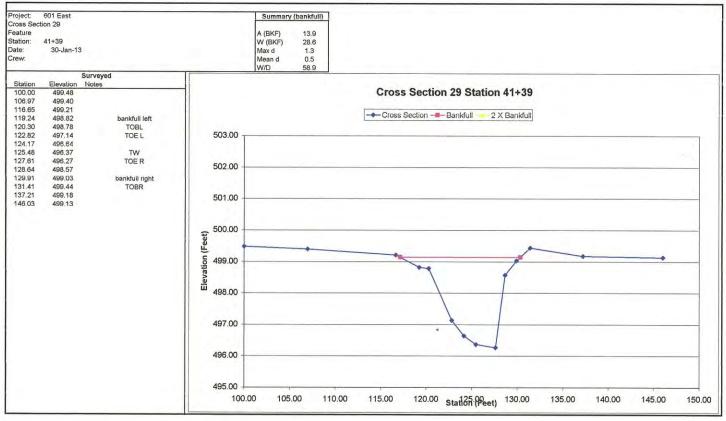


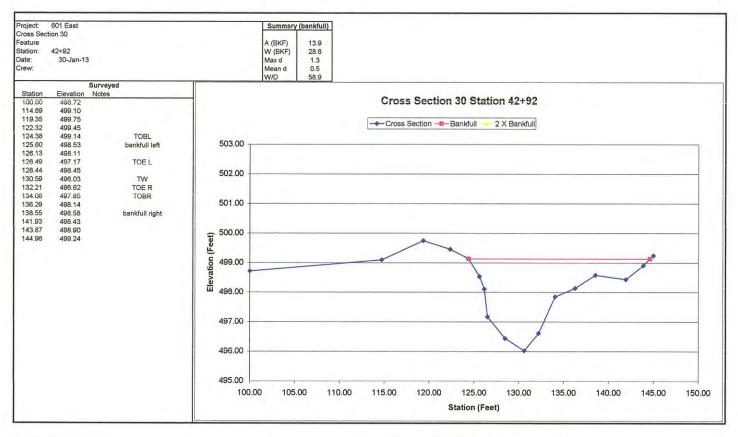


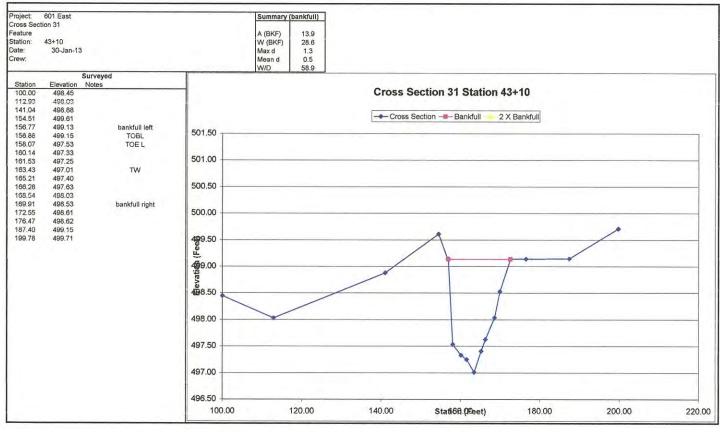


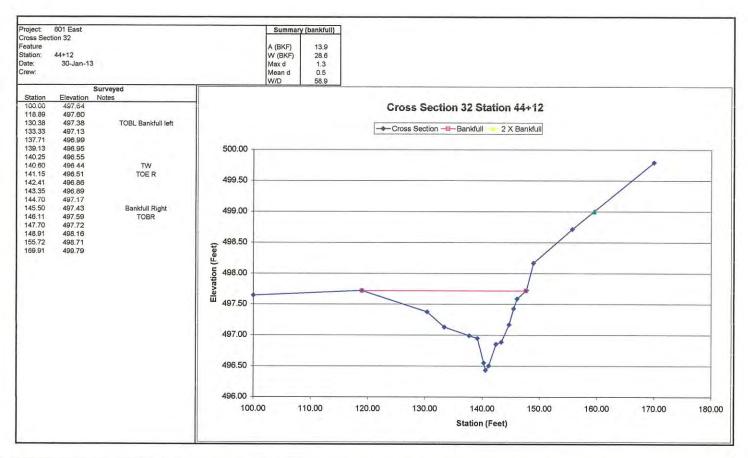
Below Lansford Road, Active Channel

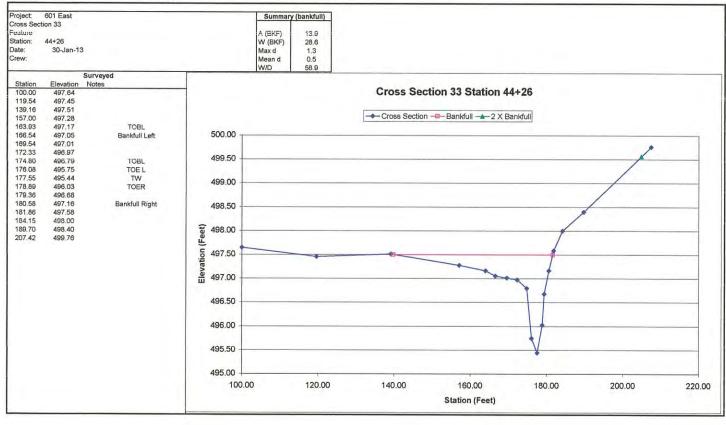


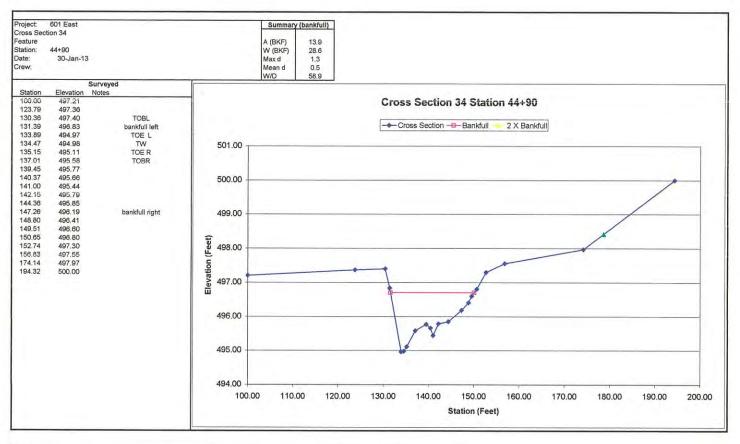


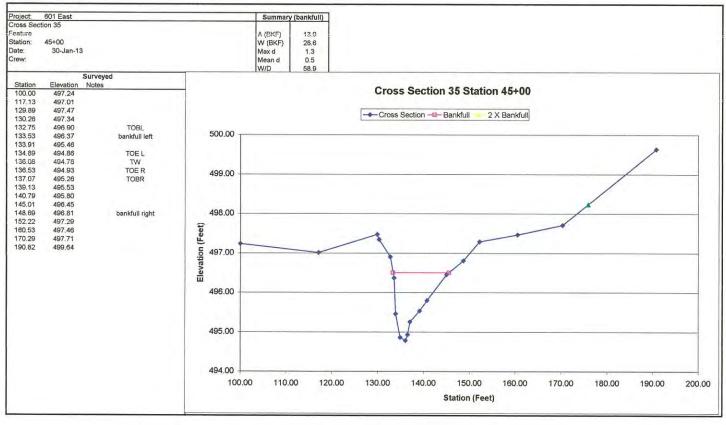


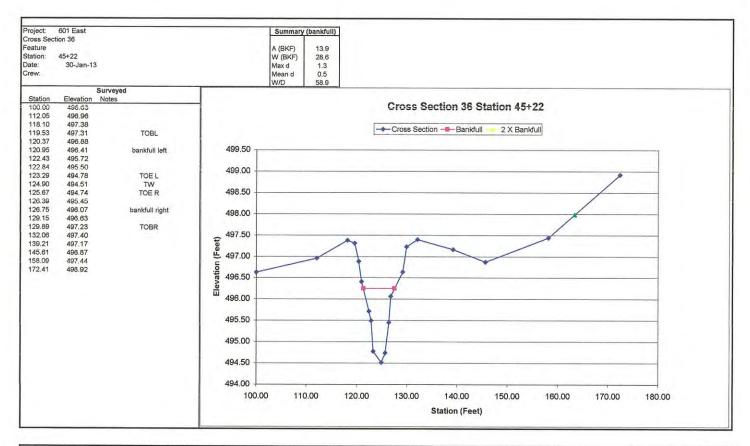


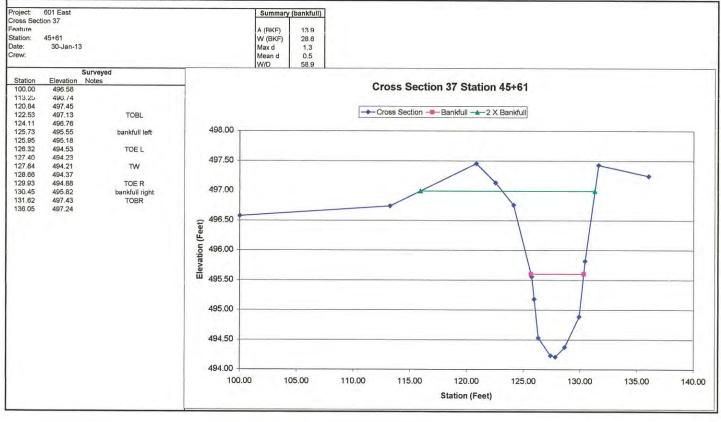






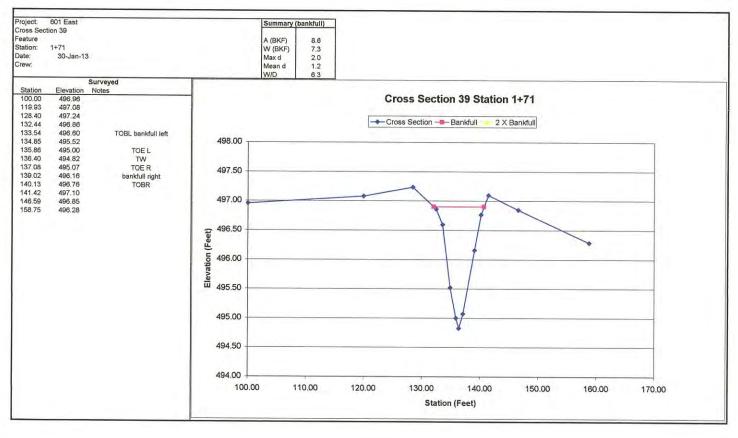


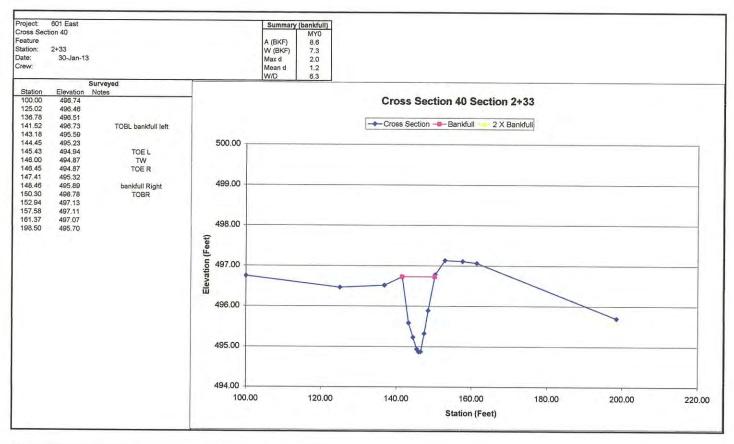


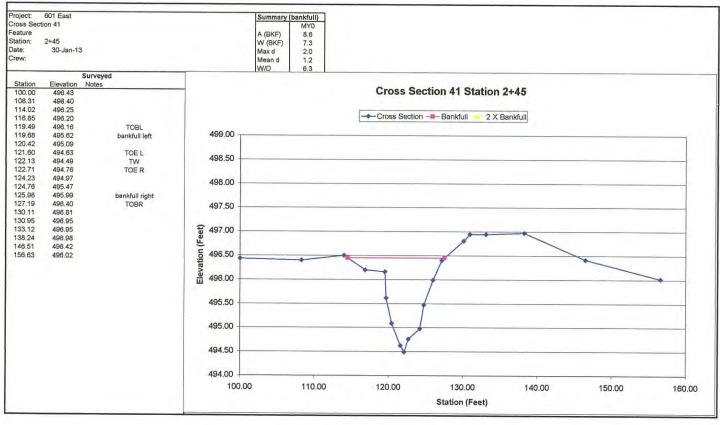


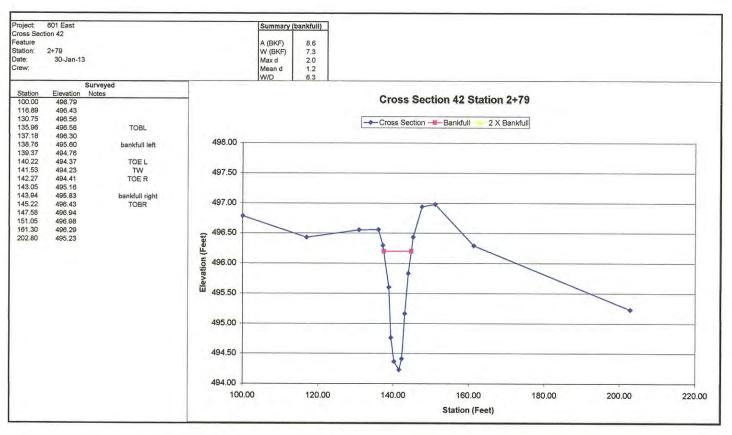
Below Lansford Road, Relic Channel

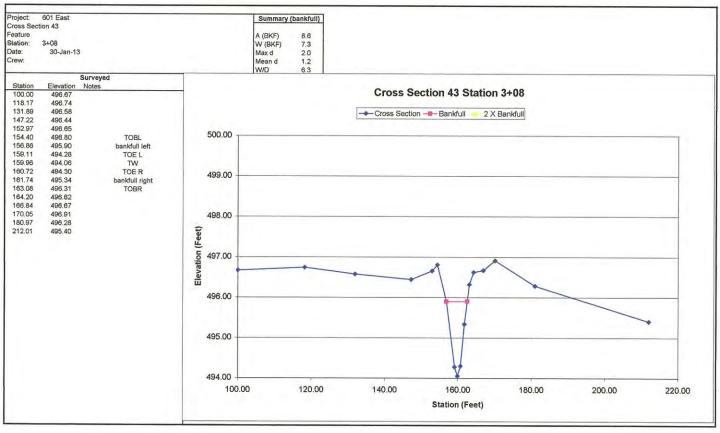
roject: ross Sec	601 East				Summary	(bankfull)					
ature ation: te: ew:	1+34 30-Jan-13				A (BKF) W (BKF) Max d Mean d W/D	8.6 7.3 2.0 1.2 6.3					
tation 00.00 15.51 20.91 23.19	Elevation 497.00 497.23 497.51 496.93		TOBL				Cross Section	ection 38, Station	1 1+34 Bankfull		
24.50 25.67 26.67 28.15 28.59 29.75 33.21 49.56	496.55 495.73 495.35 495.45 496.38 497.13 497.22 496.60	ban	nkfull left TOE L TOW TOE R kfull right TOBR	499.50 — 498.50 — 498.50 — 497							
				496.50 496.50 495.50 495.00 100.00)	110.00	120.00	130.00 Station (Feet)	140.00	150.00	160.00

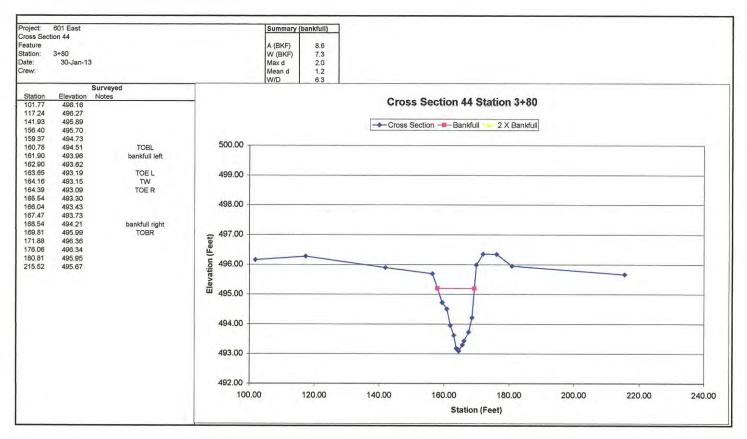


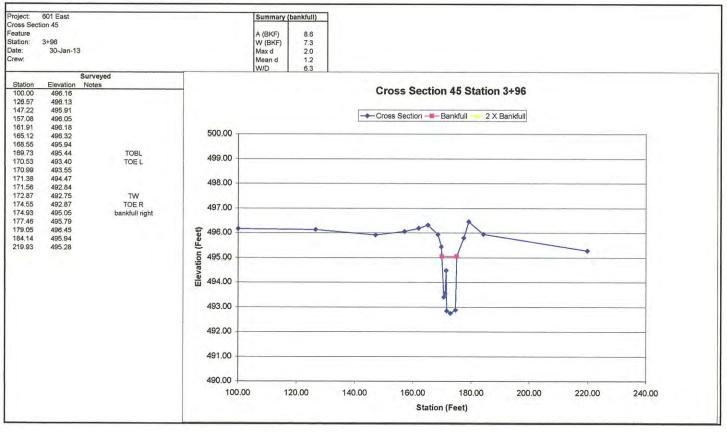


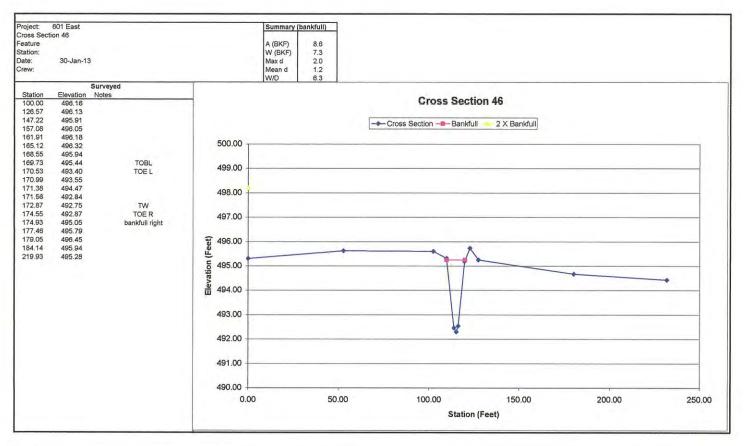


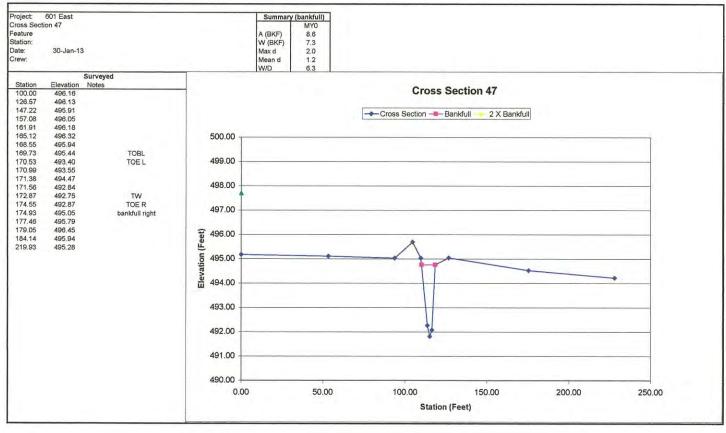


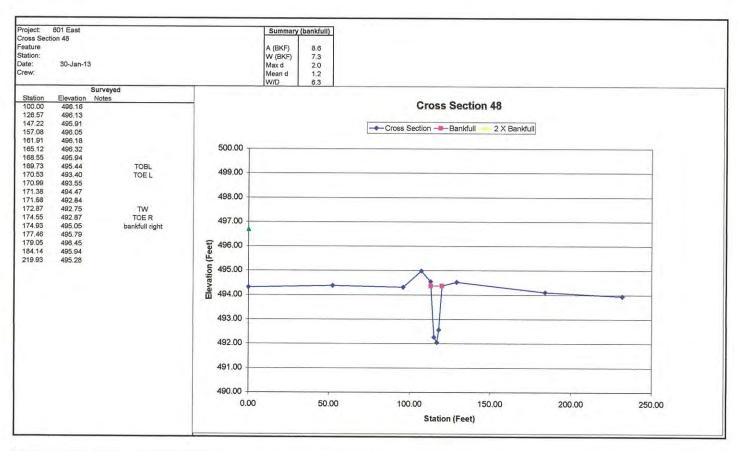


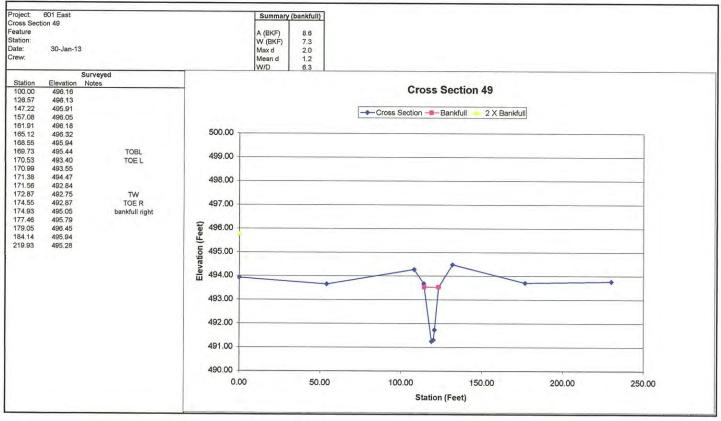


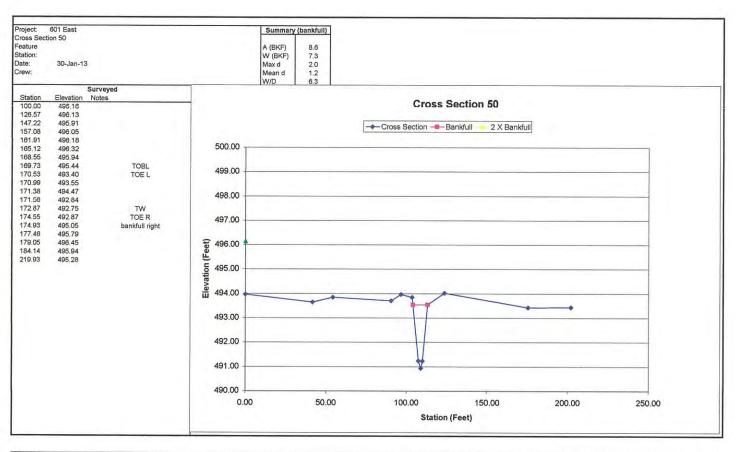


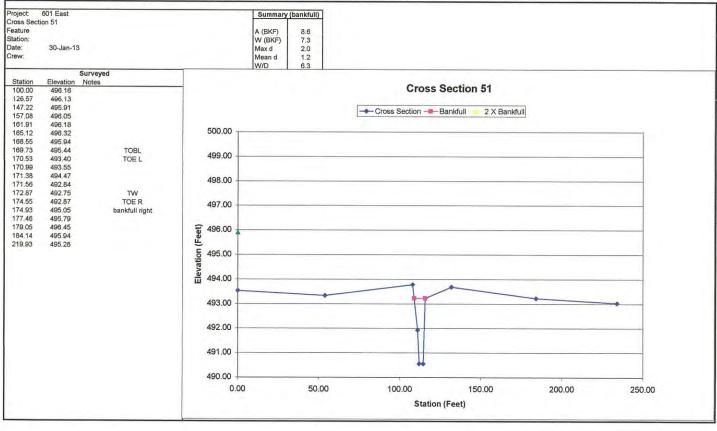


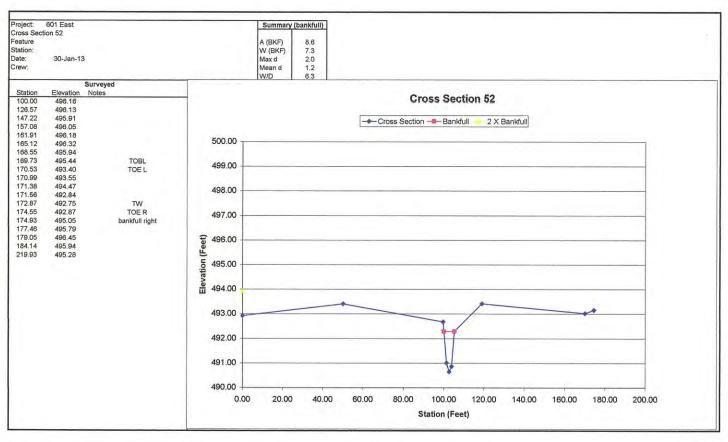


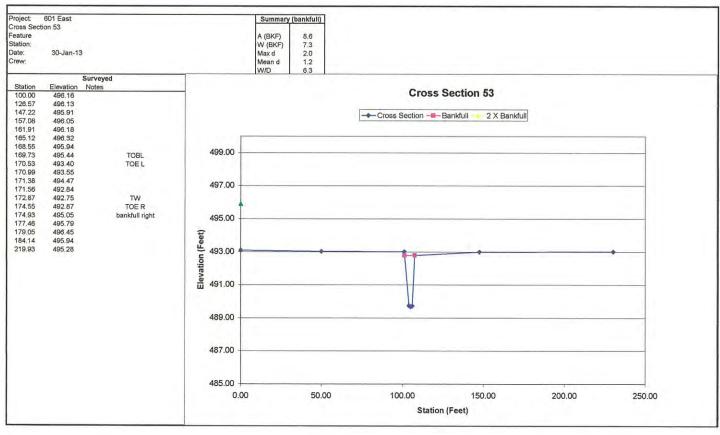


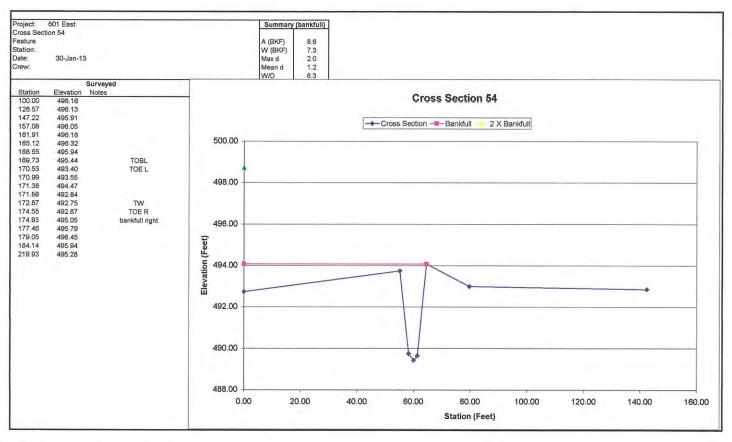


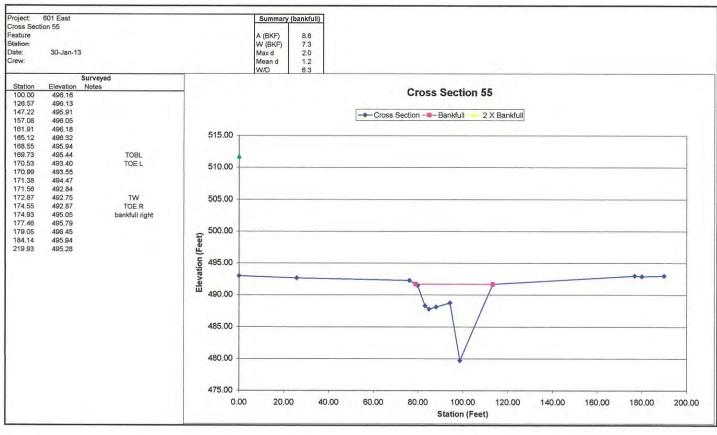


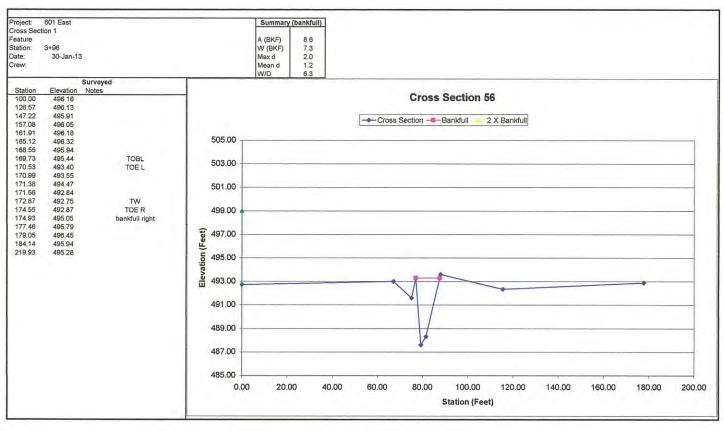


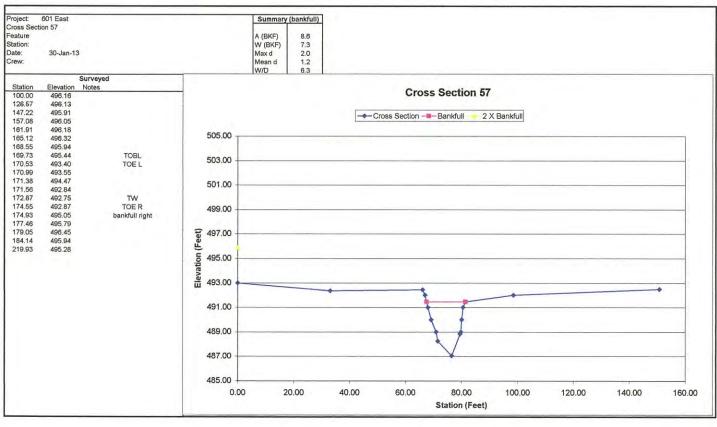


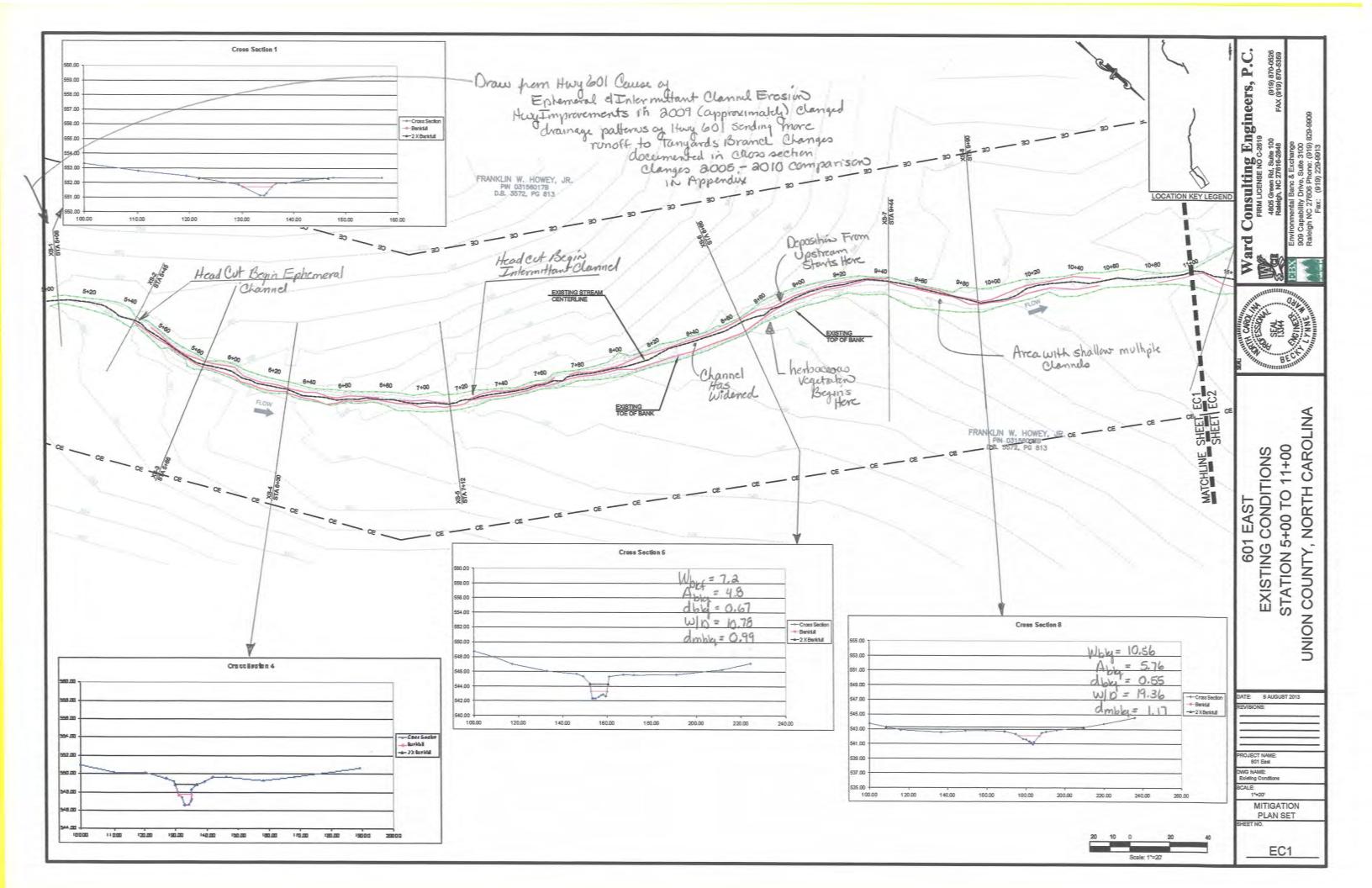


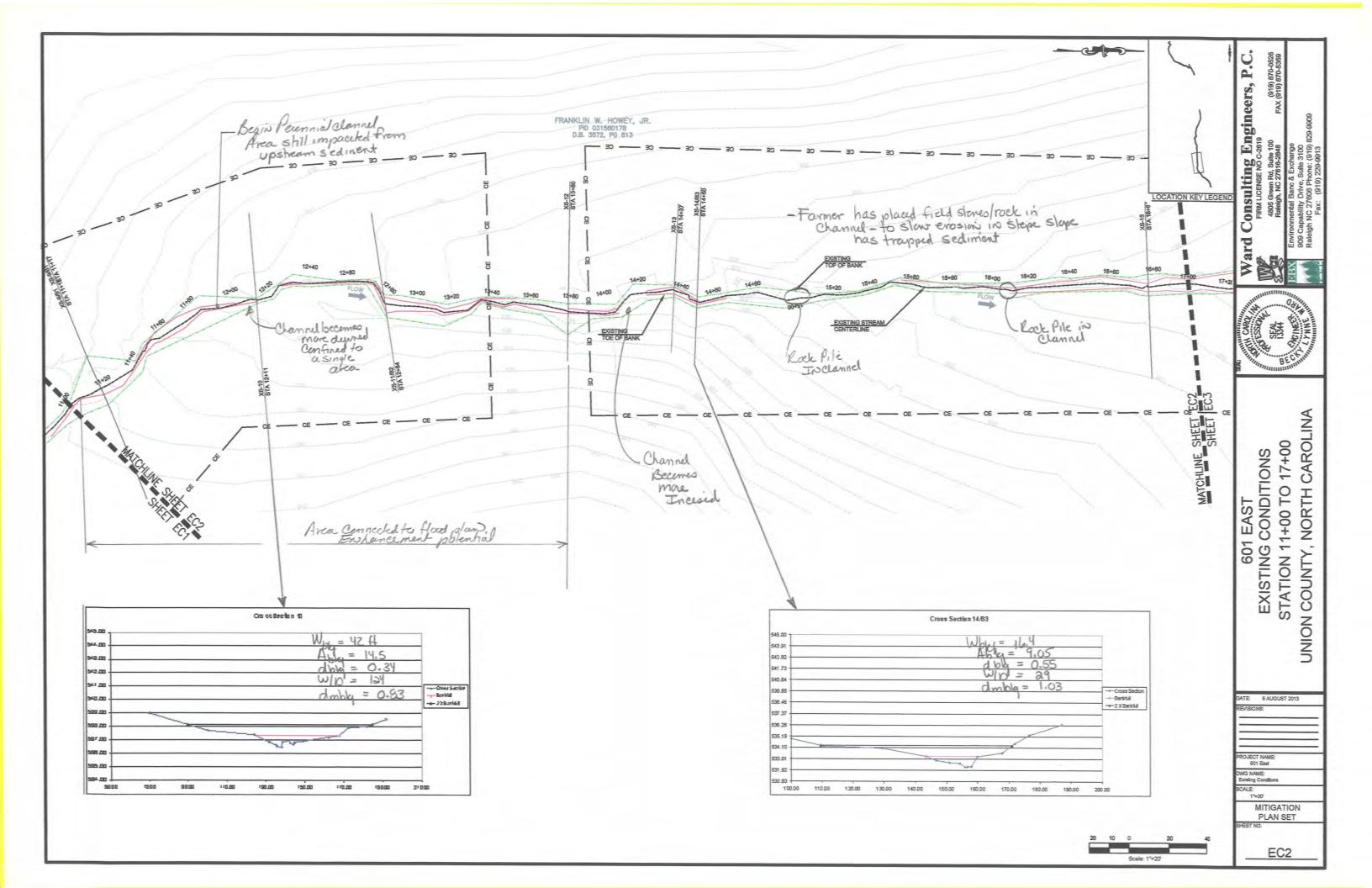


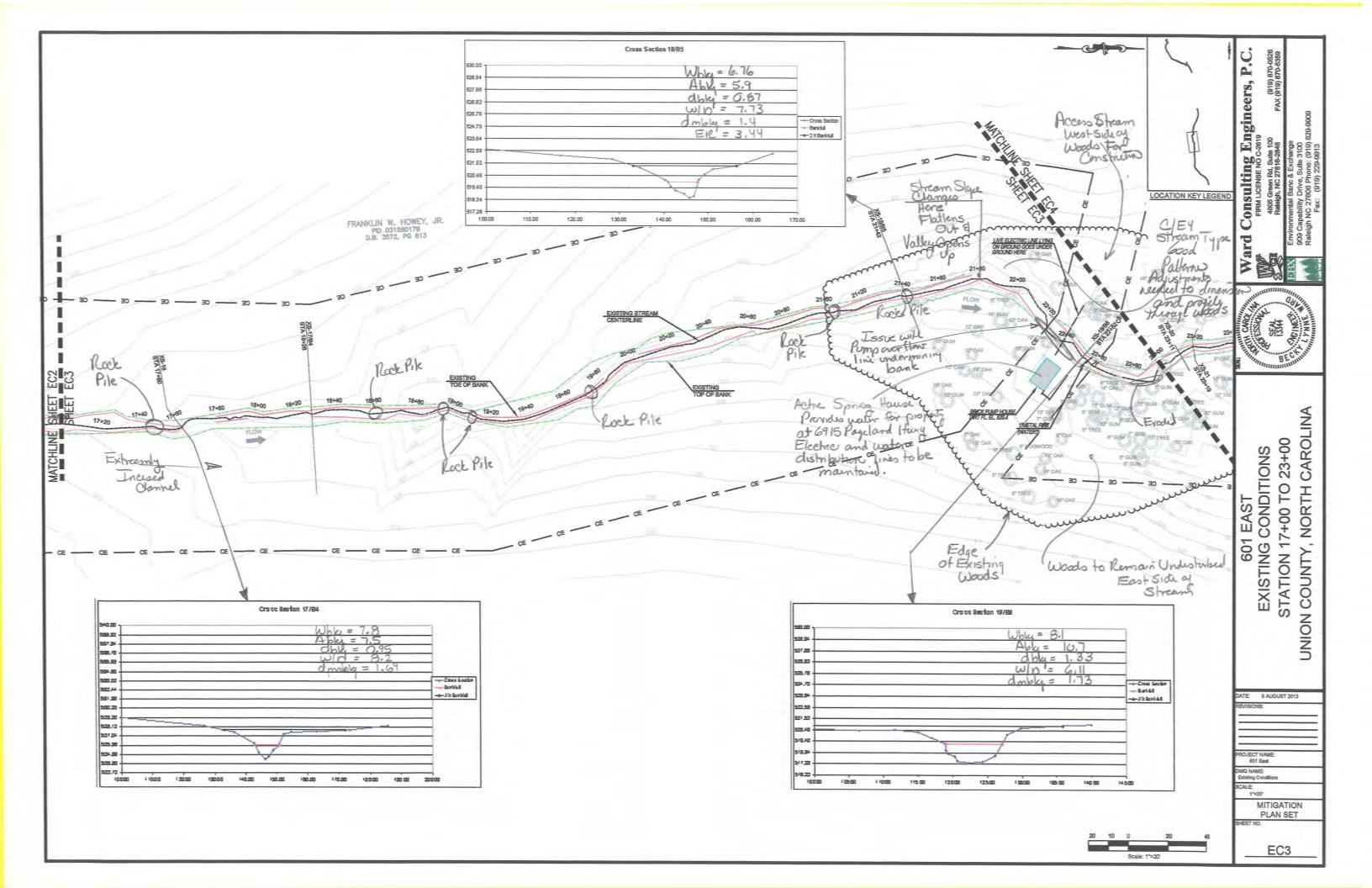


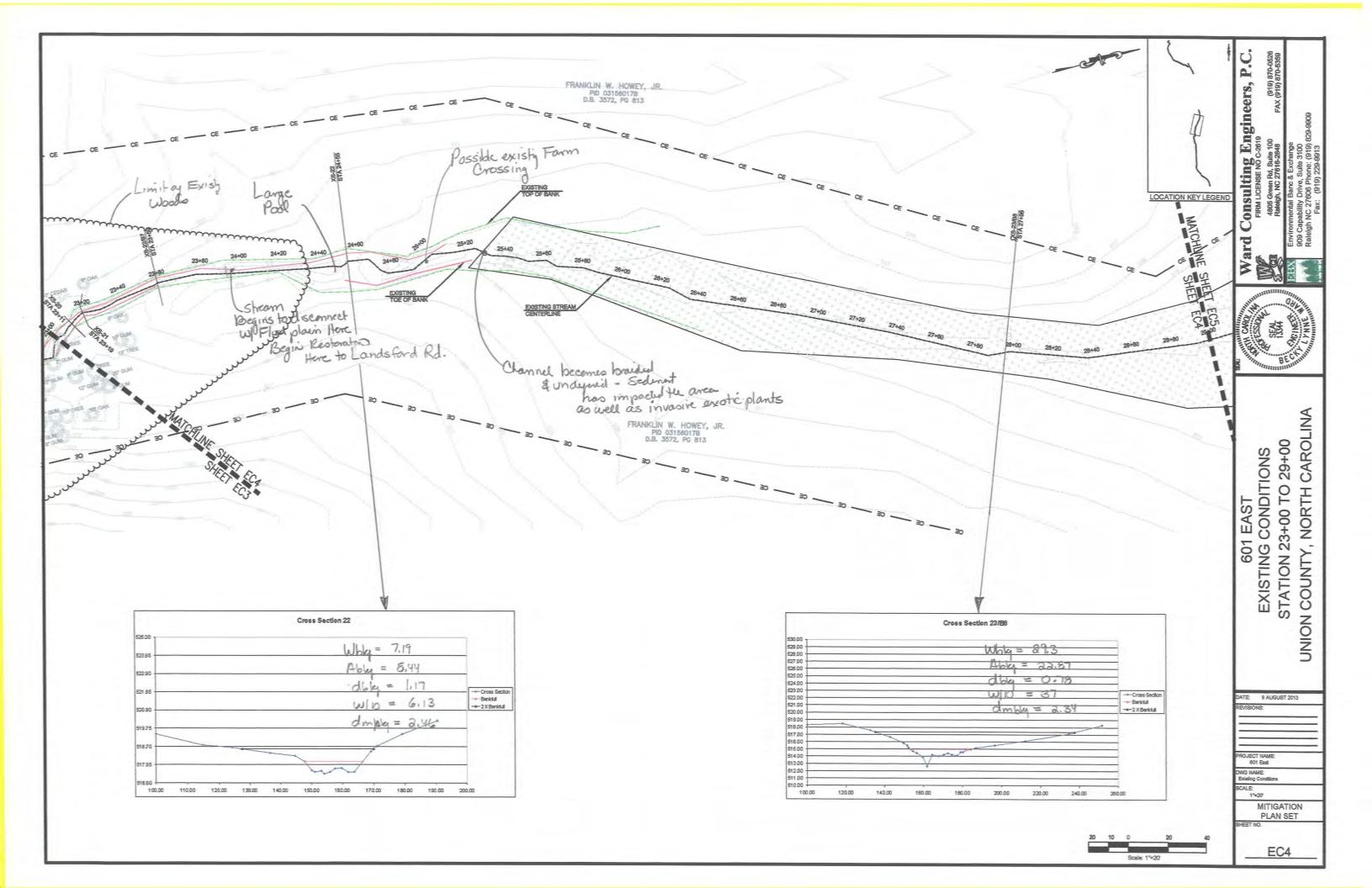


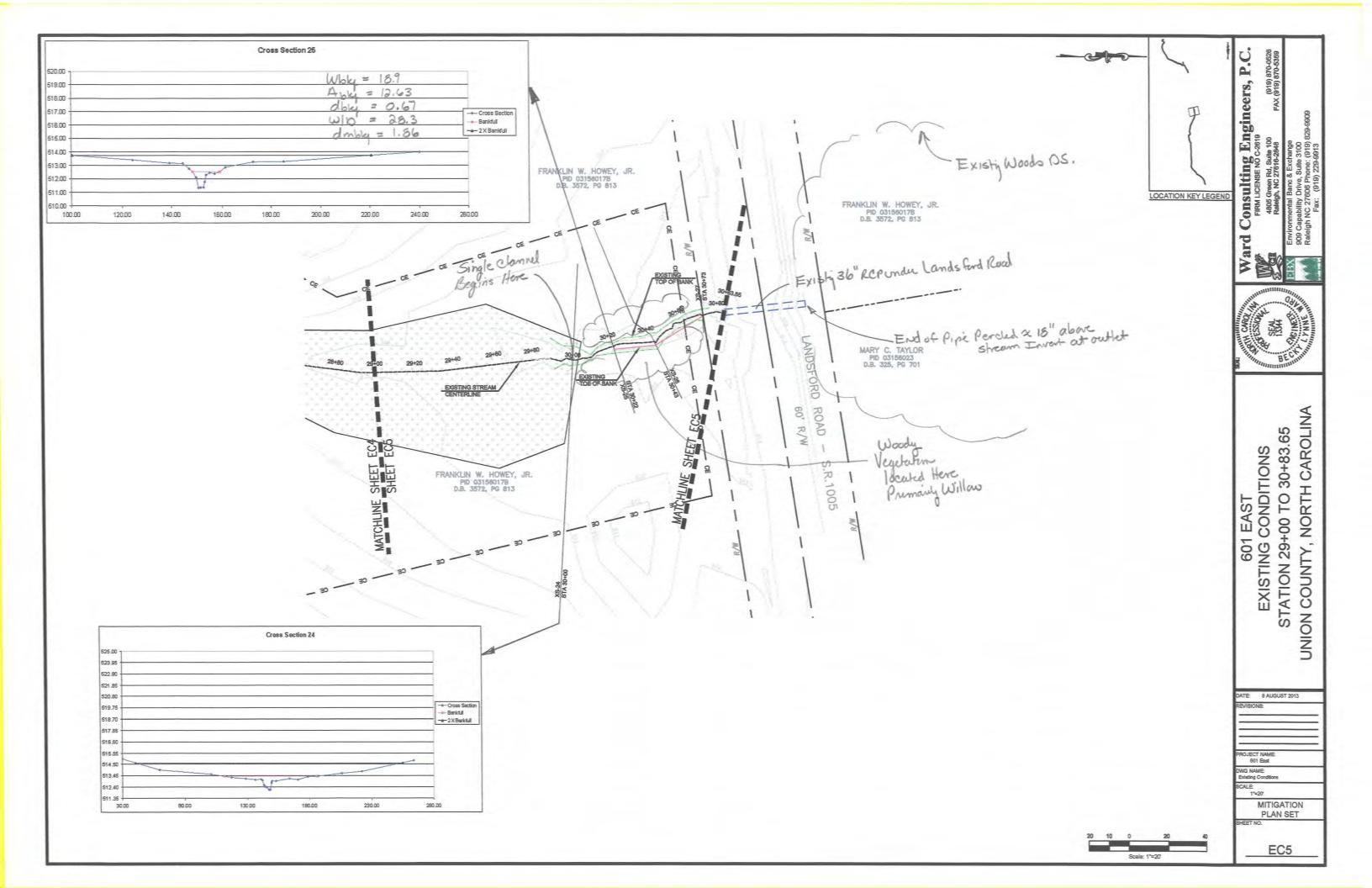


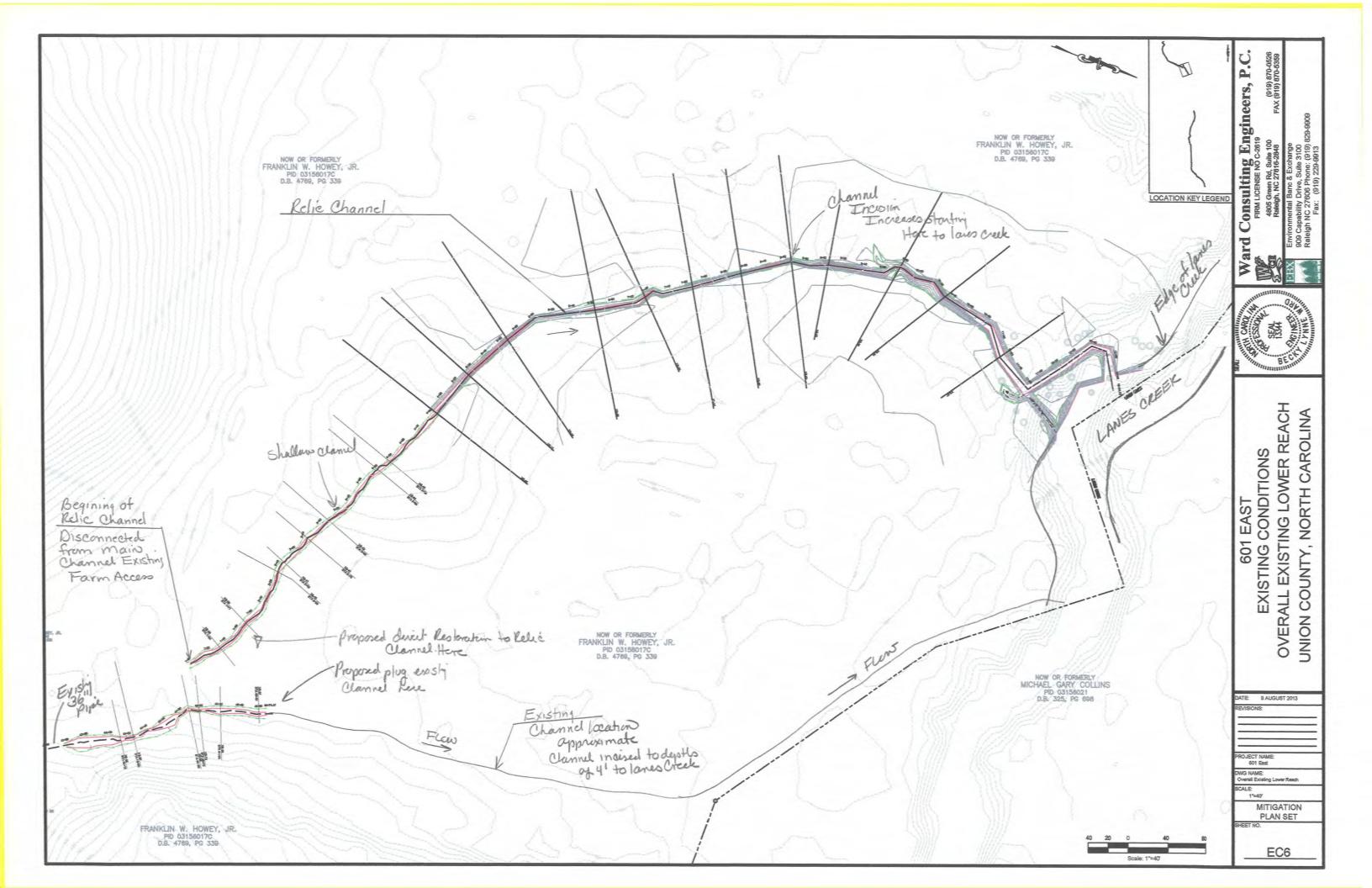


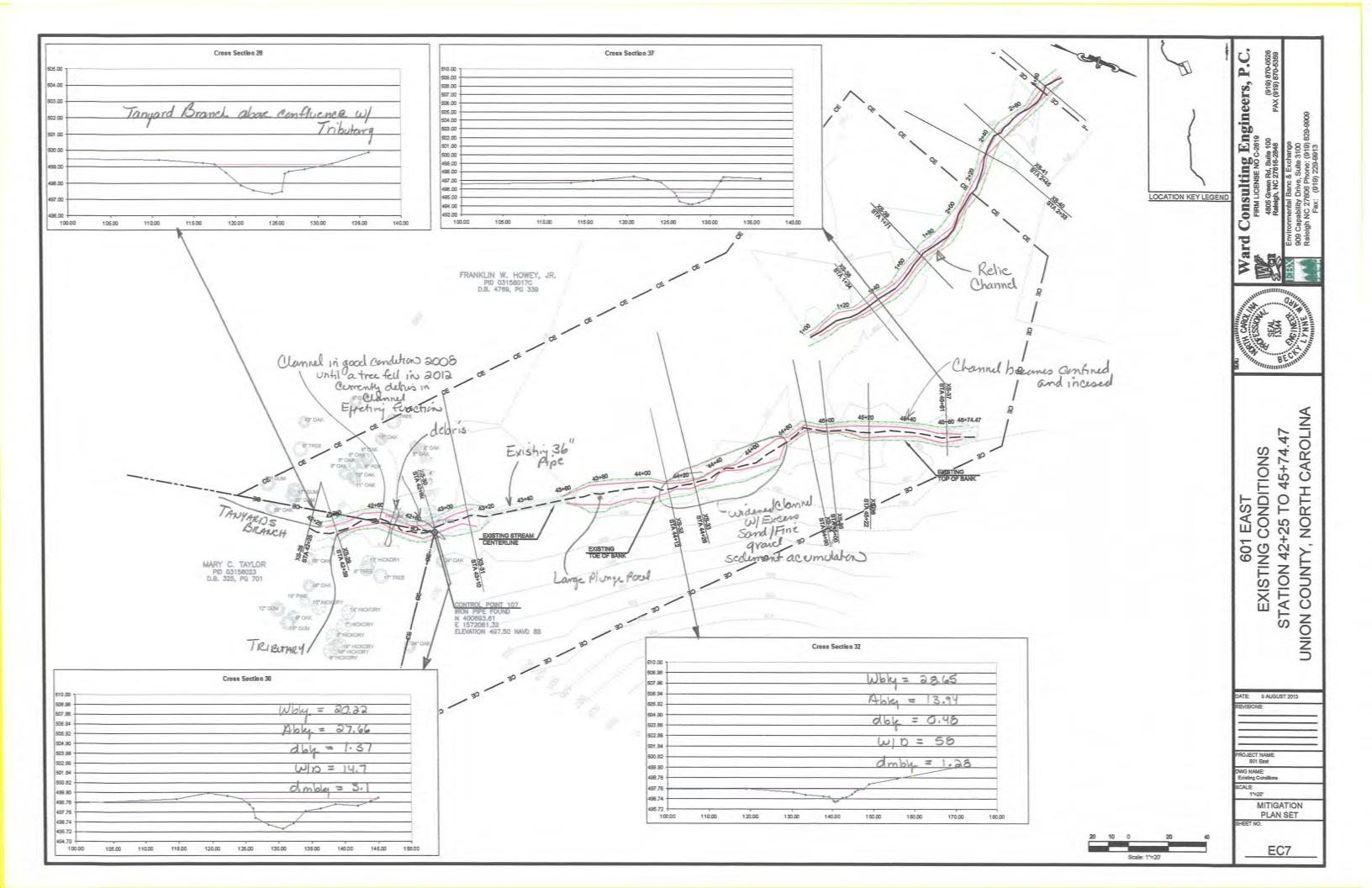


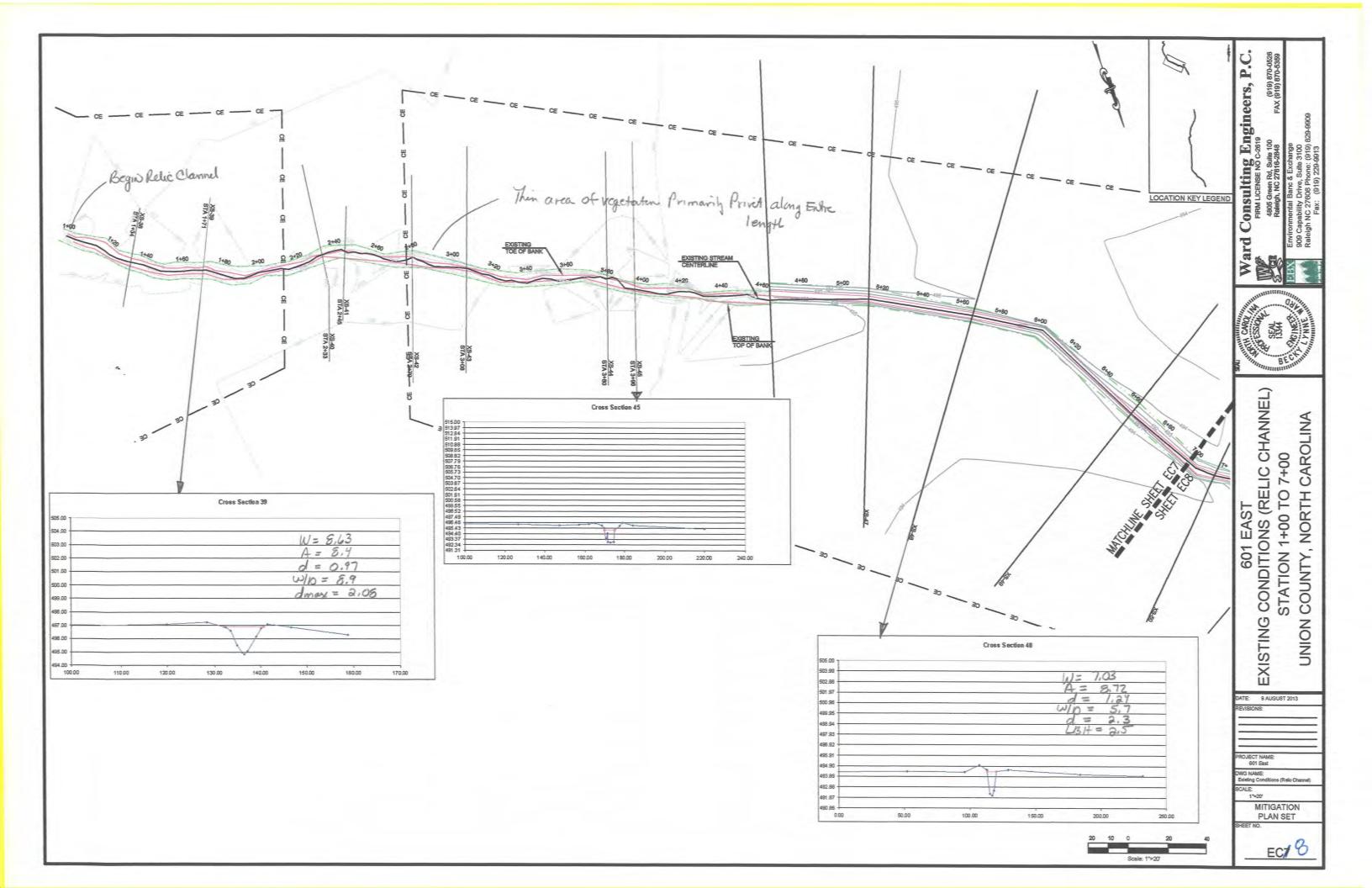


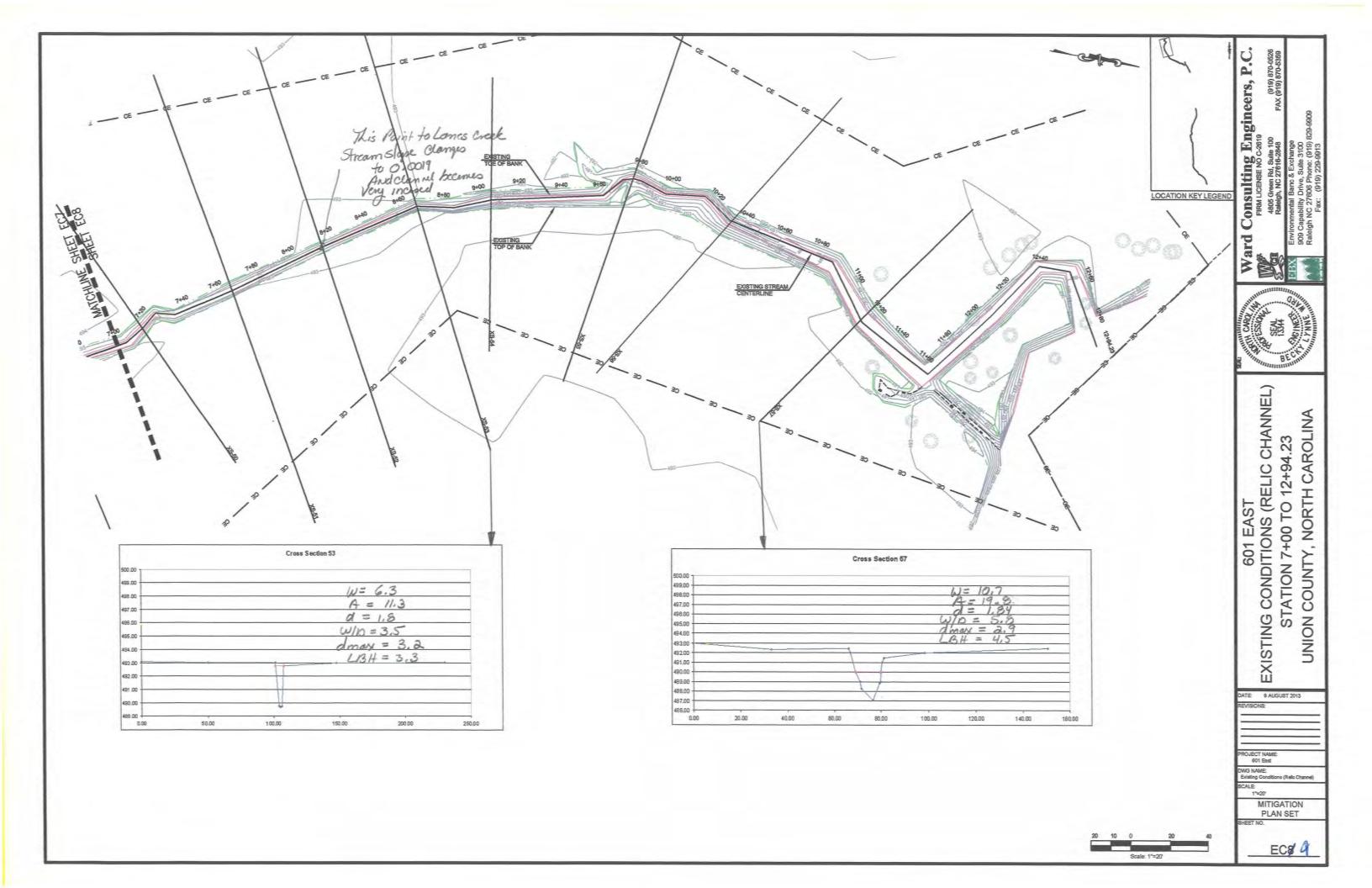












0 =1 n= 0 = 0	Regiona	al Cuncs - NC Rural	Picament			3-10-13
	Drainage Area C	Symi) Bankfull Symi) X-sect Arca(H²)	Discharge (cts)	Bankfall Width(Ht)	Bankfull Dopoth (pt)	Regression Equation
ı Pad	601 East		/0	to the processor and the state of the state		(1.5yr-2yr)
Soutation	0- 0-117	4,89	(Range) 18.65-65)	- 5-7	0.75	, (24-30)
H 0	@ 0.166	6.32	_32(B-80)	6.4	0.84	(32-35)
Cert 2	0" clanul 3-0.212	7.46	29(9-90)	7,-	0.91	(39-45)
E E	(y- 0.5a	13.74	56(18-170)	115	1.22	(76-85)
Carl 3	Cland S- 0.56 "B" cland.	, १५. ५५	60(20-180)	12	1.a5	(79-90)
AND THE REAL PROPERTY.	1	Area y = 21.43 x 0.6	*	د ۱۳۶۱ بیر د م د د د مختلف	•	·
E E E		U		. 19		
	Discharge	U			and and the second sec	
	MidHL	4= 11.89 x 0.43				
	Depth	$y = 1.5 x^{0.32}$	units , at their subdistrict designer to strang star designation parameter parameter designation designation and the subdistrict designation and the subdi	1984 til 3 Med Fridade Strikelin Streete somföret den Street (Me. 1971) Streete	n S. C. Tomos and P. C.	
	and the second of the second o		ed . Marridova commune acresiano companso de commune de			
A CONTRACTOR OF THE CONTRACTOR	React 1	- Field Marph Data-		Regunal	Euc Oak -	Region Eguno
		Prvy = 23.67 (18: Why = 20.97 (6	76~69.9\	(N) bles = 1	a3(8-80) 6.5 =	Design Q = 24cts
		$d_{blq} = 0.50 \text{ (a}$ $A_{blq} = 8.3 \text{ (a}$	<u> </u>	d bly = Abby =	CACH .	V /
	Reach 2	by.		•		
	<u>TOEBOT IX</u>	Gaug = 23.96 (12.	1-29.6)	Q AVg =	29 (9-90)	Requision Equip
DA CERTIFICAÇÃO		Whit = 25.3 (6.9 dby = 0.73 (.28	5 ~ 1,33.)	Obles - Clotes - Ables	· '' '	lenging = albers.
		Abkf = 11.9 (6.1.	- al)	A bleg	= 7.5	
	Read	Relie Clannel still teperaphy wil	Seen a partin	or bankfull bive elw 4	flow due to	the desired to old -
		9- and by	Spect form xs	31 = 648	cls	
		Avg. Q - sect. 32-37 29.66		-scot (38-4 18 27.2	5) Kelvi Chomm	Regumo Equa
		36.63		27.6 26.1		7
3-74 to 6 s p 20 s p 20 s p 20 s		$\frac{2557}{8206/3} = 30.7cfs.$	560 Y	46= 23.67		Dasignia 55cts
		TOTAL Q	= 30.7+24	\$.54.7		
		,		u		•

Overbandes of FP- ady puscehow

Sedement Compensance -

Dyot of plan / water surjace slope required to more largest particle

Detarmine Chihaid Dimensionless Shear Stress $7c^* = 0.0834 \left(\frac{di}{ds_0}\right)^{-0.872}$

 $d_{5}^{*} = \text{bed moternal } d_{50} = 19.0 \text{ mm}$ $\hat{d}_{50} = \text{bar sample } d_{50} = 7.0 \text{ mm}$ $Y_{c}^{*} = 0.0834 \left(\frac{19}{7}\right)^{.872}$ $Y_{c}^{*} = 0.035$

Upper Reads

Lower Reads

B" Type Sheam 5=0.017 Hft "C" Type Stream 5=0.0069 Hft

5=0.0056444

Max Size Particle movey 2" = 0.1674+ = D

d= 1/2* (1.65)(D)

Upper Reads

lower Reads

d= 0.035(1.65)(0.167)
0.017
d= 0.57++ 0k-1'design

d= 0.035 (1.65)(.167)
0.014
d= 0.85 # ok 1.2 design

d = 0.035 (1.65)(0.167)
0.0069

d = 0.035 (1.65)(0.167) 0.0056

d= 1.39 ft. de 1.4' design

d= 1.72 ok 1.7 design

```
"B" Clannel
              Velocities & Stear stresses for design
                             7+60 to 11+81
                  Peunnial 11+81 to 22+43
   Velocity Ranges -
                        Max
        bankfall
                           4.5
      axbankfull
                           5. Q
                                           1.36-1.53
        10 year
                        5.3-6.2
                                           1.6- 6, 1
       100 year.
                                         a - 2.3
                 allowable velocity for sciles & 3.0
Regels well not fold we out armony-
             design for skew stress is clamed = 2.0
       Stulls deagram Stear of 2.0 -> 350 mm Hushold of
                 350 mm x 1/m = 13.77" 214" store will a5.4 mm
       100 year Sterm Design -
                 Class II Rep Rap 9"-23" - ang 14" (29" deep)
    Bonkyull Design - Y = 1.25 Sheldo degram = 7 200 mm
            200 mm » IIn = 8" diameter
                 Class 13 - 5-12" Avg 8" (12"deep)
Upper Reach -
     Design For 7 = 1.5 2 10 year design storm
Skulds deagram => 250 mm
         250 mm = 9.81n =10"
                  Class I Rep Rap = 5-17" Avg 10" (18" deep)
        Increase Reple to Class I for - Stations
            8100
            1540
            15+97
            20+85
            22+91
```

			R STATE OF THE STA	- WINWA
Lower Re	od Stea	e Stress -	Clannel "B"	5-5-2013
RAS	STROAM			
STATIO		FEATURE	Highost Sheer	Strom Event
4+80	53160	HR	1.20	2 year
4+35	54+25	HR	1.95	5 year
3+60	54 +80	HR	1.89	10 year
3+65	54 1 95	ER	/. 3a	10 year
3 <i>+</i> a7	<i>5</i> 5+33	HR	1.66	ax bankfull
<i>à+</i> 73	55+67	HR	1.96	100 year
2+60	56+00	ER	1.11	Dycor
2+30	56+30	HR	3.47 (1.53 ble	f) 100 yr
2+10	56+50	ER	1.83	1004r
1+90	56+70	CP	1.36	100yr
1+70	56+90	HR	2.35	10 yr
1+50	57+10	ER	1.70	106 gr
1+30	67+30	CP	1.36	100 yr
1+10	67+ 5 0	HR	3.35 (1.53 b	ky) 100 yr
80	57+80	ER	1.50	100 yr
60	58+00	CP	1. a7	100 yr
40	58+20	1+R	3.23 (1.53	by) 100yr
O	58+60	EK	2.50 (1.3	- 1 · · · · · · · · · · · · · · · · · ·
-				- yı , , , , , , , , , , , , , , , , , ,

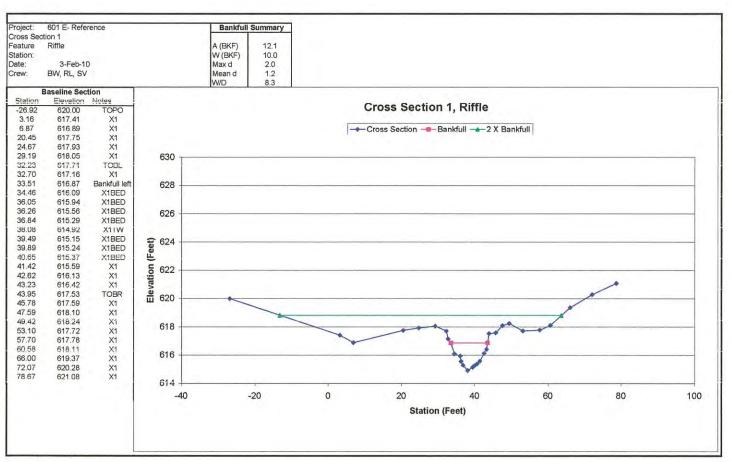
Sheildolune Threshold of Motion

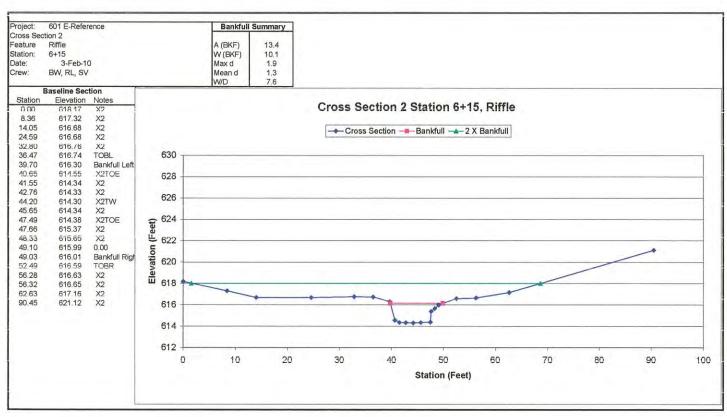
Averag = 1.95 #1sf = 340/25.4 = 13.5 incles

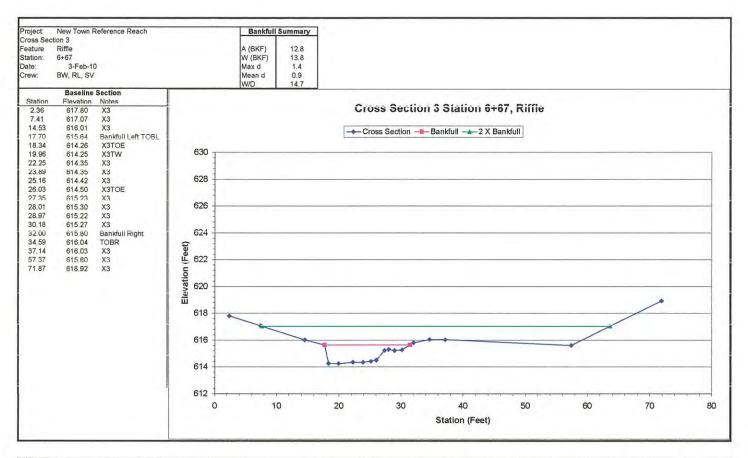
Highest 10 year Event = 2.35 #sf = 375 mm = 15 incles Highest Shear 100 year = 3.47 /sf= 200 mm = 24 inclis

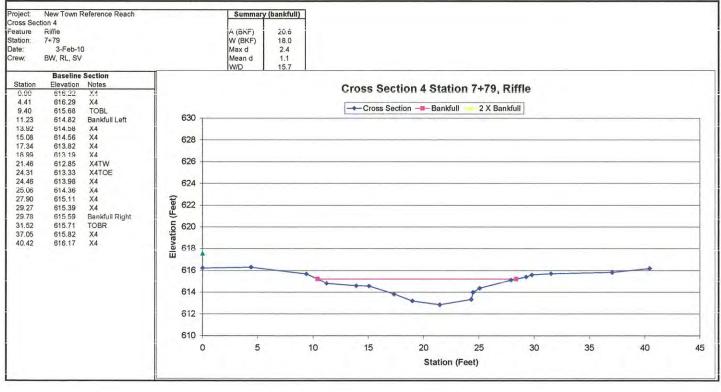
Construct Ryples of Boulders & Class II Rip Rays -

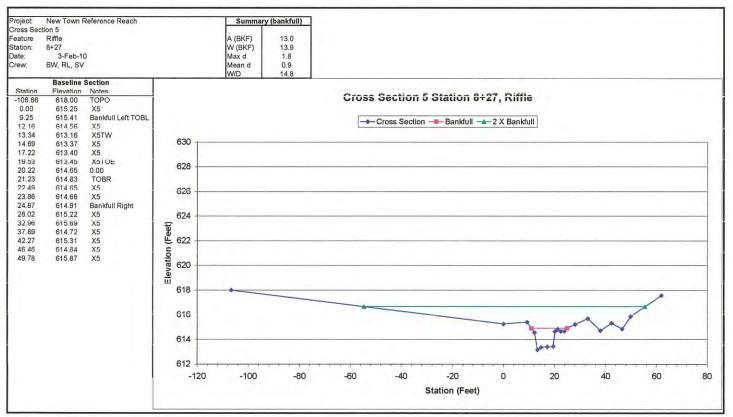
Reference Reach 1-Underwood Creek

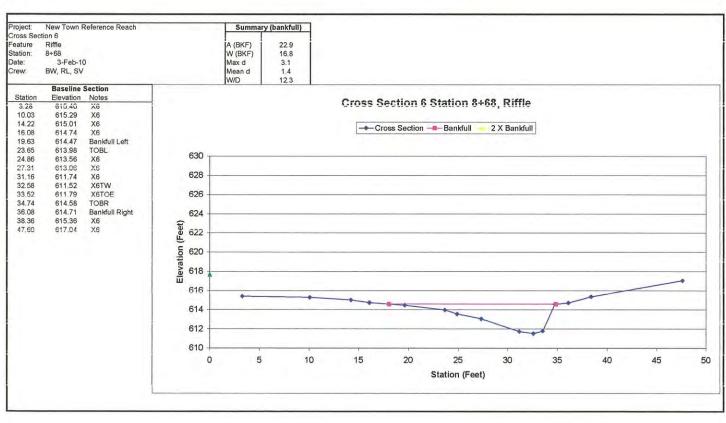


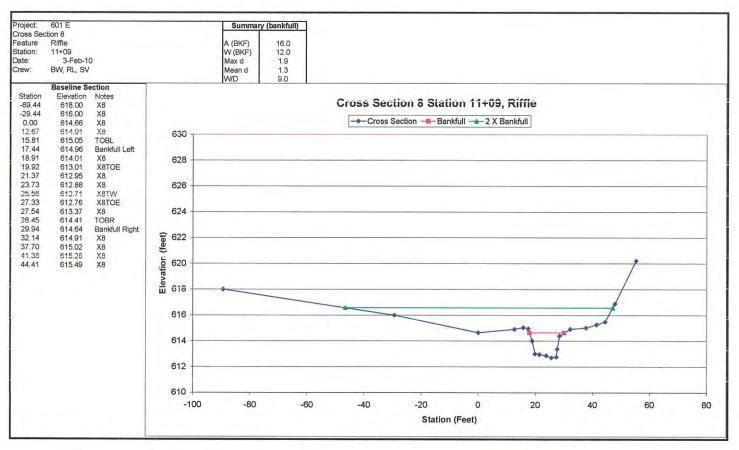


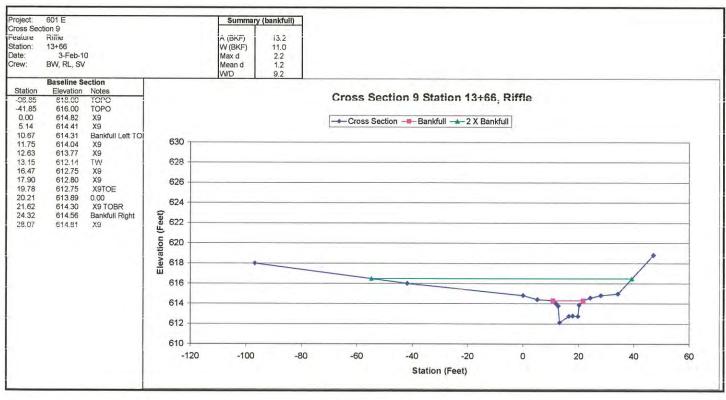


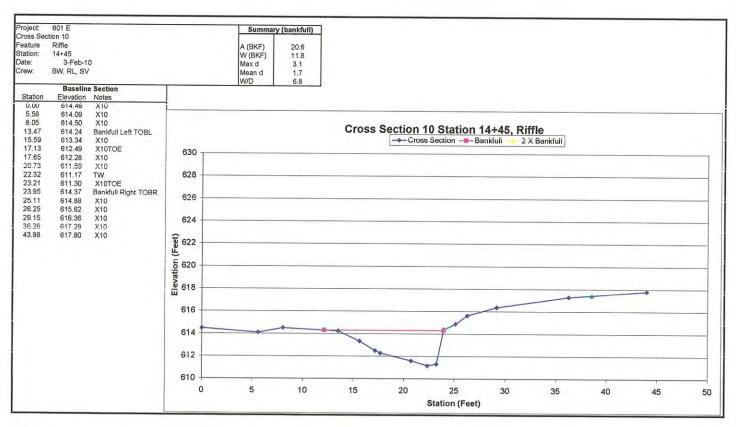


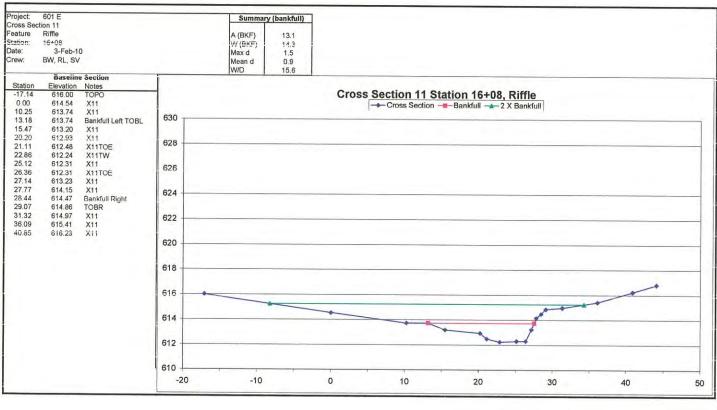






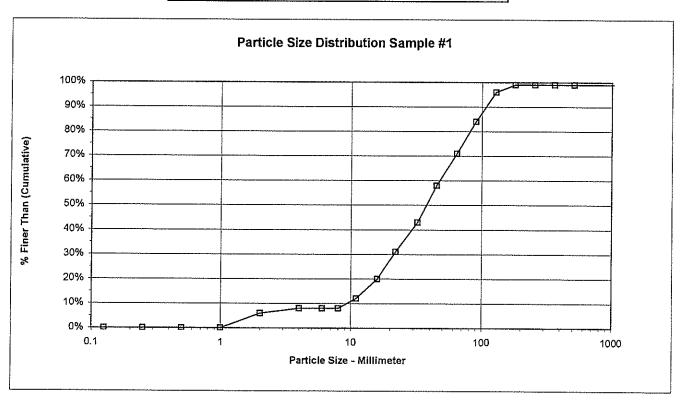






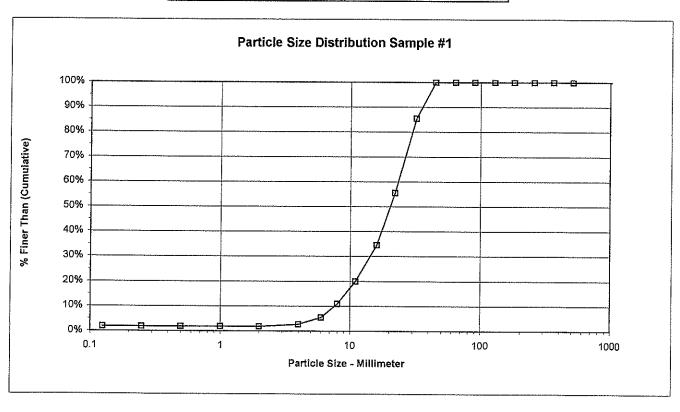
		***************************************	PEBBLE (COUNT						
Project:	601 East Und	lerwood Creek	Reference	Reach (We	etted Perime	Date:	2/2/2010	Ö		
Location:	XS-3					•				
	Particle Counts									
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative		
	Silt/Clay	< 0.062	S/C	0	0	0	0%	0%		
	Very Fine	.062125	S	0	0	0	0%	0%		
	Fine	.12525	Α	0	0	0	0%	0%		
ĺ	Medium	.2550	· · · N	0	0	0	0%	0%		
	Coarse	.50 - 1.0	D	0	0	0	0%	0%		
.0408	Very Coarse	1.0 - 2.0	S	6	0	6	6%	6%		
.0816	Very Fine	2.0 - 4.0		2	0	2	2%	8%		
.1622	Fine	4.0 - 5.7	G	0	0	0	0%	8%		
.2231	Fine	5.7 - 8.0	R	0	0	0	0%	8%		
.3144	Medium	8.0 - 11.3	Α	4	0	4	4%	12%		
.4463	Medium	11.3 - 16.0	V	8	0	8	8%	20%		
.6389	Coarse	16.0 - 22.6	E	11	0	11	11%	31%		
.89 - 1.26	Coarse	22.6 - 32.0	L.	12	0	12	12%	43%		
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	15	0	15	15%	58%		
1.77 - 2.5	Very Coarse	45.0 - 64.0		13	0	13	13%	71%		
2.5 - 3.5	Small	64 - 90	C C	13	0	13	13%	84%		
3.5 - 5.0	Small	90 - 128	0	12	0	12	12%	96%		
5.0 - 7.1	Large	128 - 180	В	3	0	3	3%	99%		
7.1 - 10.1	Large	180 - 256	L.	0	0	0	0%	99%		
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	99%		
14.3 - 20	Small	362 - 512	1	0	0	0	0%	99%		
20 - 40	Medium	512 - 1024	D	0	0	0	0%	99%		
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	99%		
	Bedrock		BDRK	1	0	1	1%	100%		
			Totals	100	0	100	100%	100%		

	d16	d35	d50	d84	d95
I	13.5	25.3	38.1	90.0	124.8



			PEBBLE (COUNT			4. H. T	
Project:	601 East, Un	derwood Cree	k Reference	etted)	Date:	2/2/2010)	
Location:	Between XS-				······			
				Particle	Counts		· · · · · · · · · · · · · · · · · · ·	
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	2	0	2	2%	2%
	Very Fine	.062125	S	0	0	0	0%	2%
	Fine	.12525	Α	0	0	0	0%	2%
	Medium	.2550	N.	0	0	0	0%	2%
	Coarse	.50 - 1.0	D	0	0	0	0%	2%
.0408	Very Coarse	1.0 - 2.0	S	0	0	0	0%	2%
.0816	Very Fine	2.0 - 4.0		1	0	1	1%	3%
.1622	Fine	4.0 - 5.7	G	3	0	3	3%	5%
.2231	Fine	5.7 - 8.0	R	6	0	6	5%	11%
.3144	Medium	8.0 - 11.3	Α	10	0	10	9%	20%
.4463	Medium	11.3 - 16.0	V	16	0	16	15%	35%
.6389	Coarse	16.0 - 22.6	E	23	0	23	21%	55%
.89 - 1.26	Coarse	22.6 - 32.0	L	33	0	33	30%	85%
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	16	0	16	15%	100%
1.77 - 2.5	Very Coarse	45.0 - 64.0		0	0	0	0%	100%
2.5 - 3.5	Small	64 - 90	C	0	0	0	0%	100%
3.5 - 5.0	Small	90 - 128	0	0	0	0	0%	100%
5.0 - 7.1	Large	128 - 180	В	0	0	0	0%	100%
7.1 - 10.1	Large	180 - 256	L.	0	0	0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0	0	0	0%	100%
14.3 - 20	Small	362 - 512	L	0	0	0	0%	100%
20 - 40	Medium	512 - 1024	D	0	0	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0	0	0	0%	100%
	Bedrock		BDRK	0	0	0	0%	100%
			Totals	110	0	110	100%	100%

d16	d35	d50	d84	d95
9.7	16.1	20.4	31.5	40.5



Sieve Sample #1 Pavement Type: Sample Date: Project: Location: Sample Date:
Project: 601
Location: Upr

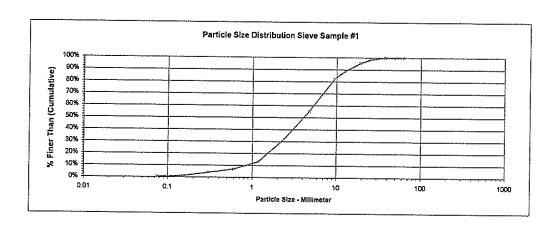
· · · · · · · · · · · · · · · · · · ·				
11 East	 	 		
pper Reach	 	 	***************************************	 *******

inches: 1.8; 1.6; 1.7; 1.7; 1.2; 1.3; 1.4; 1.4; 1.0; 1.1; 1.7

Sleve Size	Sleve Size (mm)	Sleve Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sleve +\$ample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Total Welght (Lbs)
2 1/2 inch	63	1,175							
2 inch	50	1.195		770.0.		**			
1 1/2 inch	37.5	1.25							
1 inch	25	1.23		1,42	1.25			-	
3/4 inch	19	1.245	1.31	1,54	1,29				0.2
1/2 inch	12.5	1,21	1.43	1.61	1.465				0,40
3/8 inch	9.5	1.225	1.5	1.58	1,44	· · · · · · · · · · · · · · · · · · ·			0.87
No. 4	4.75	1,145	2.29	2.47	2.2				0.84
No. 8	2.36	1.07	1.62	2.475	2.175	~			3.52
Vo. 16	1.18	0.955	2	1,74	1.57				3.0
Vo. 30	0.6	0.9	1,29	1,15	1.05				2.44
No. 50	0.3	0,815	0.98	0.92	0,92				0.7
No. 100	0.15	0.775	0.95	0.92	0.84				0,37
Vo. 200	0.075	0.765	0.79	0.79	0,77				0.38
Passing 200	<0.075	1.08	1.095	1,09	1,15				0,059

Total Sample Weight ======>

Location: Project:	0		Sieve Sample	#1		
Inches	Sieve Size	Millimeter <#200	77779 86 7777	Wt. Retained (lbs)	% Passing 0.73%	% Cumulative
0,0029 0,0059	#200 #100	0.0750	s:	0.055	0.42%	1,15%
0.0039	#50	0.150	N.	0.385 0.375	2,95% 2,07%	4.09% 6.97%
0.0234 0.0469	#30	0.60	0	0,79	6,05%	13.01%
0.0469	#16 #8	1.18 2.36	100000 8 00000	2.445	18.71%	31.73%
0.187 0.374 0.5 0.748 0.0843	#4 3/8" 1/2" 3/4" 1"	4.75 9.50 12.50 19.0 25.0	G R A V E	3.06 3.525 0.845 0.875 0.405	23,42% 26,98% 6,47% 6,70% 3,10%	55.15% 82.13% 88.60% 95.29% 98.30%
1.4764 1.9685	1 1/2" 2"	37.5 50.0	\$	0.21 0 0	1,61% 0,00% 0.00%	100.00% 100.00% 100.00%
2.5	2 1/2*	63.0	0 0 8	0 0 0	0.00% 0.00% 0.00% 0.00%	100,00% 100,00% 100,00% 100,00%
			B L D	0 0 0	0.00% 0.00% 0.00% 0.00%	100.00% 100.00% 100.00% 100.00%
	Bedrock		BORK Totals	0 13.065	0.00% 100%	100.00% 100%



Sieve Sample #2 Pavement Type: Sample Date: Project: Location: Sample Date:
Project: 601
Location: 5m:
Largest Particle on bar ===>

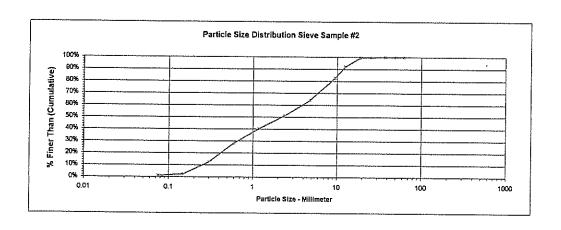
1 Eest	 *********	*****	
naller Trib	 		 · · · · · · · · · · · · · · · · · · ·

inches: 2.0; 1.8; 1.6; 1.2; 1.1; 0.9; 1.2; 1.1

Sleve Size	Sieve Size (mm)	Sleve Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sieve +Sampte Welght (Lbs)	Total Weight (Lbs)
2 1/2 inch	63	1,175							
2 inch	50								
1 1/2 inch	37,5	1,25		***************************************					
1 inch	25	1.23		1.265					0.03
3/4 inch	19	1.245		1.26	1.27				0.03
1/2 inch	12.5	1.21	1,525	1.79	1,41	1.29			1.17
3/8 inch	9.5	1.225	1.59	1.755	1.59	1,465	~~~		1.
No. 4	4.75	1.145	1,905	1,97	2,01	1.63			2.93
No. 8	2.38	1.07	1.587	1.475	1.78	1.51			2.07
No. 16	1.18	0,955	1,355	1.215	1,625	1,34			1,71
No. 30	0.6	0.9	1.26	1.09	1,78	1.35			1.8
No. 50	0.3	0.815	1.273	1.07	1.98	1.45			2.51:
No. 100	0.15	0.775	1.34	1,07	1,138	1,13		·	1,57
No. 200	0.075	0.765	0.875	0.81	0.8	0.8			0.22
Passing 200	< 0.075	1.08	1,193	1,13	1,095	1.09		-	0,16

Total Sample Weight ========>

Location: Project:	0		Sieve Sample	#2		
Inches	Sleve Size	Ml/limeter <#200	Section 1	Wt. Retained (lbs)	% Passing	% Cumulative
0.0029 0.0059 0.0117 0.0234 0.0469	#200 #100 #50 #30 #16	0.0750 0.150 0.30 0.60 1.18	5 A N O	0.225 1.578 2.513 1.88 1.715	1.42% 9.96% 15.67% 11.67% 10.63%	2.48% 12.45% 28.32% 40,15% 51.02%
0.0357 0.187 0.374 0.5 0.748 0.9843 1.4784 1.9685	#4 9/8" 1/2" 3/4" 1" 1 1/2" 2"	2.36 4.75 9.50 12.50 19.0 25.0 37.5 50.0	G R A V E L S	2.072 2.935 1.5 1.175 0.04 0.035 0	13.08% 18.53% 9.47% 7.42% 0.25% 0.22% 0.00% 0.00%	64.10% 82.63% 92.11% 99.53% 99.78% 100.00% 100,00%
2.5	2 1/2"	63.0	0 9 B	0 0 0 0	0.00% 0.00% 0.00% 0.00% 0.00%	100.00% 100.00% 100.00% 100.00%
	Bedrock		D R BDRK	0 0	0.00% 0.00% 0.00% 0.00%	100.00% 100.00% 100.00%
			Totals	15.836	100%	100%



Sieve Sample #3 Pavement Type: Sample Date: Project: Location: Pavement Type:
Sample Date:
Project:
Location:
Reft
Largest Particle on bar ====>

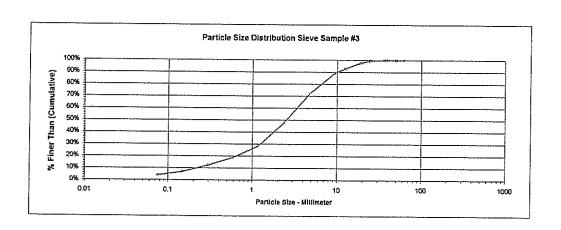
	·	 W	
1 East			
ference Reach		 	 10.00.00

Inches: 2.0; 0.9; 1.2; 1.3; 1.3; 1.9; 2.0; 1.5; 1.4; 1.4; 1.5

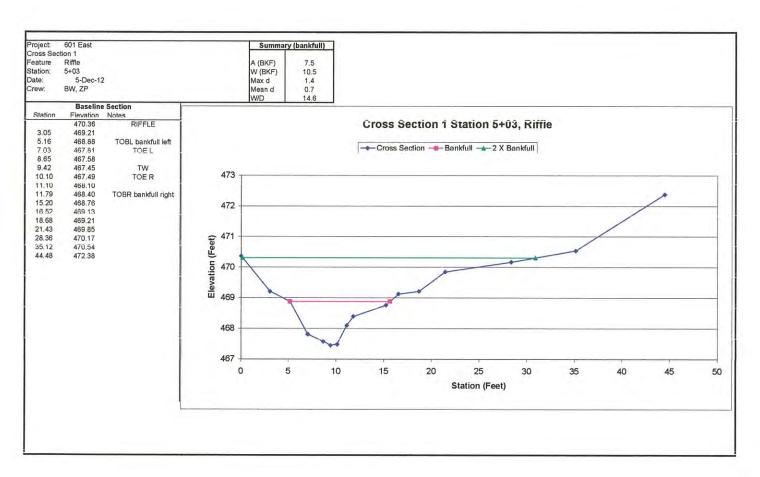
Sieve Size	Sleve Size (mm)	Sieve Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sieve +Sample Welght (Lbs)	Sieve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Total Weight (Lbs)
2 1/2 inch	63	1.175							
2 inch	50	1,195	*********						
1 1/2 inch	37.5	1,25							
1 inch	25	1.23				1.3			0.07
3/4 inch	19	1.245	1.39			1,44			0.0
1/2 inch	12.5	1.21	1,43	1,4	1.63	1.24			0.86
3/8 inch	9.5	1,225	1.35	1.39	1,55	1,28			0.67
No. 4	4.75	1.145	1,97	2.02	2.19	1,52			3.12
No. 8	2.36	1.07	2.37	2.31	2.17	1.85			4.42
No. 16	1.18	0.955	1.96	1.97	1.73	1.67			3.51
No. 30	0.6	0.9	1,31	1.37	1.24	1.4			1.72
No. 50	0.3	0.815	1.05	1,19	1.01	1.19			1.18
No. 100	0.15	0.775	1,15	0.99	0.91	1.05			1.10
No. 200	0.075	0.765	0.82	0.91	0.87	0.98	***		0.52
Passing 200	<0.075	1.08	1.25	1.33	1.27	1.19			0.72

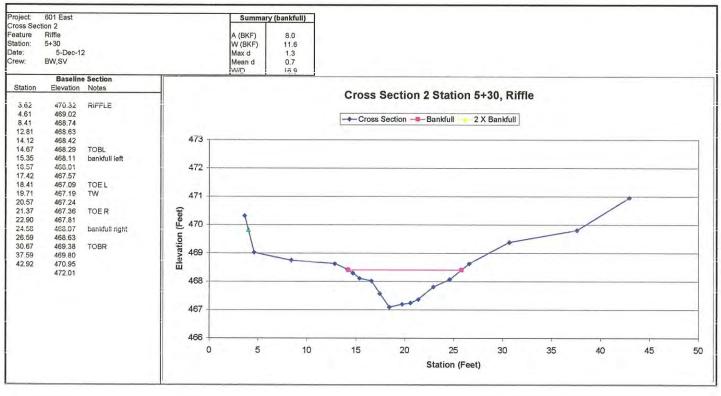
Total Sample Weight

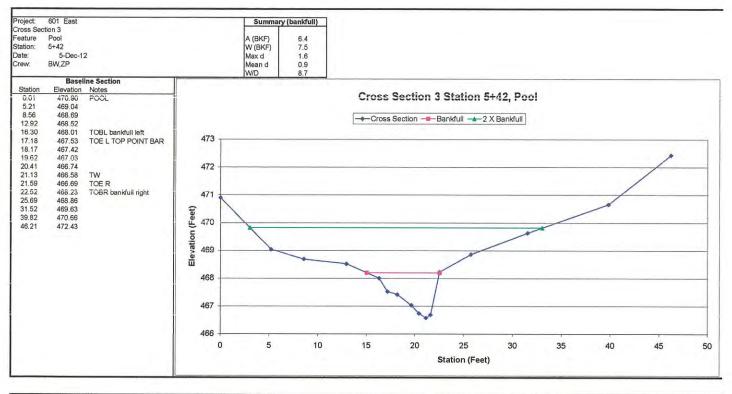
Location: Project:	0		Sieve Sample	#3		
Inches	Sleve Size	Millmeter		Wt. Retained (lbs)	% Passing	% Cumulative
		< #200	s/c	0.72	3.97%	3.97%
0,0029	#200	0.0750	THE SHOE	0.52	2.87%	6.84%
0.0059	#100	0.150	\$1000 (CO)	1 1	5.52%	12.30%
0.0117	#50	0,30	1000 (A) NA (A) (A)	1.18	0.51%	18.88%
0.0234	#30	0.60		1.72	9.49%	28.35%
0.0469	#16	1,18	S. C.	3,51	19.36%	47.71%
0.0937	#8	2.36	TO CONTRACT	4.42	24.38%	72.09%
0.187	#4	4.75	Process of	3.12	17.21%	89.30%
0.374	3/8"	9.50	200 (A) (A) (A)	0.67	3.70%	93.00%
0.5	1/2"	12.50	100000000000000000000000000000000000000	0.86	4.74%	97.74%
0.748	3/4"	19.0	2000年1993年	0.34	1,88%	99.61%
0.9843	1"	25.0	133 (0.42)	0.07	0.39%	100.00%
1.4764	1 1/2"	37.5	S	0	0.00%	100.00%
1.9665	2"	50.0	530000000000000000000000000000000000000	0	0.00%	100,00%
2.5	2 1/2"	63.0	Company Comment	0	0.00%	100.00%
			(33.55 Q 3.55)	0	0.00%	100.00%
			100000	0	0.00%	100.00%
			[14000000000000000000000000000000000000	0	0.00%	100,00%
			B	0	0.00%	100.00%
			10000040000	0	0.00%	100.00%
			[::::::0 -::::::0	0	0.00%	100.00%
			la contraction of	0	0.00%	100.00%
	Bedrock		BDRK	0	0.00%	100.00%
			Totals	18.13	100%	100%

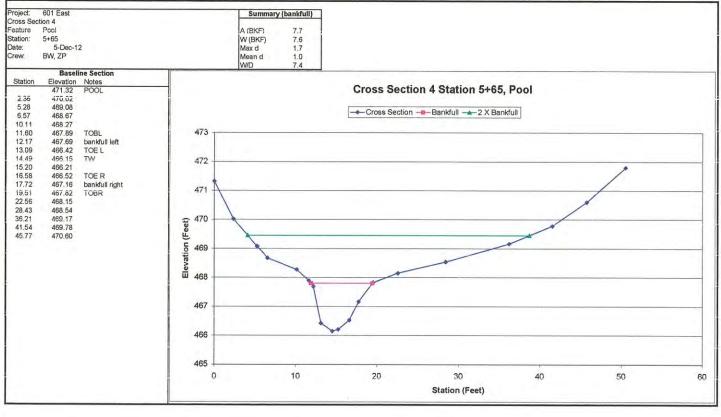


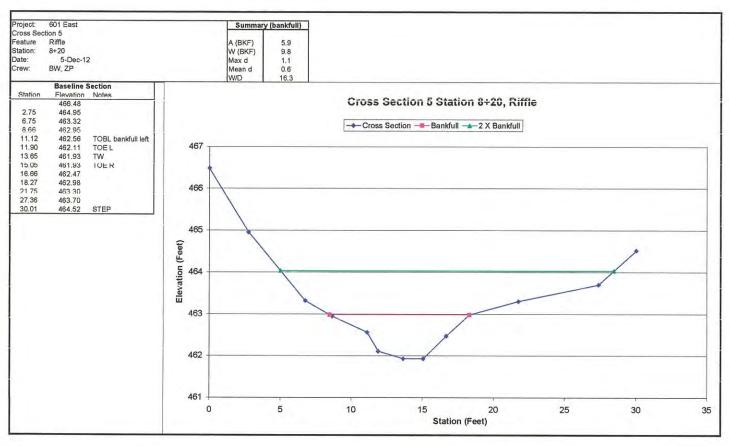
Reference Reach 2-Richardson Creek

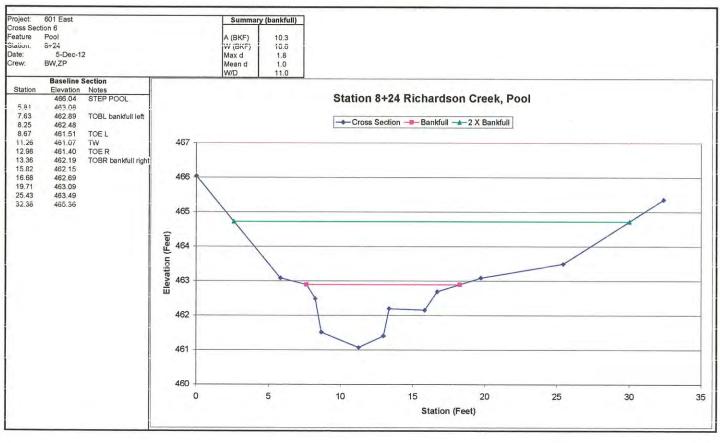


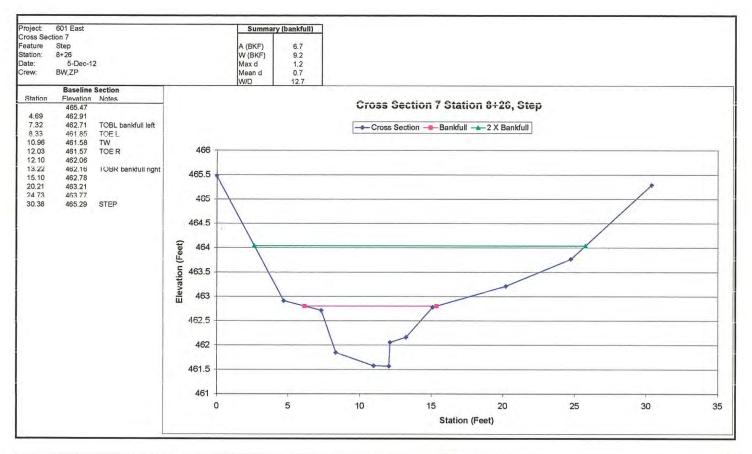


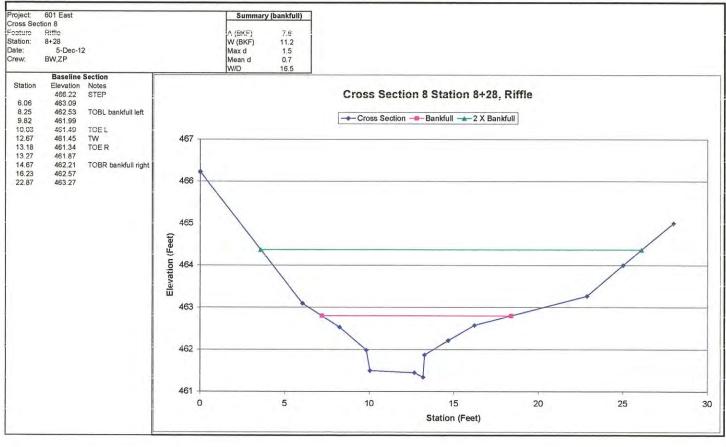


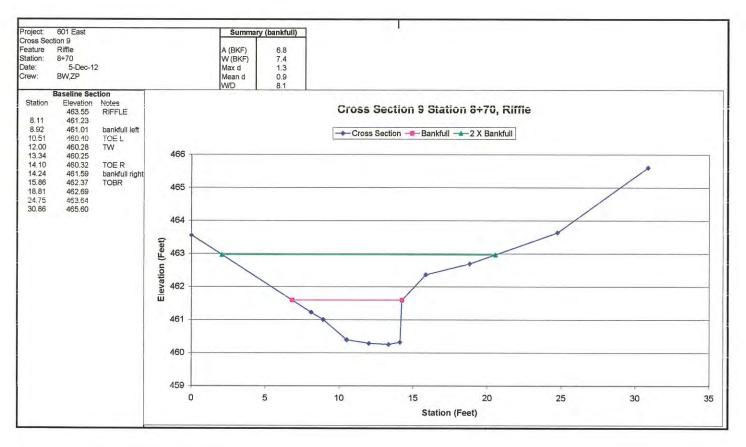


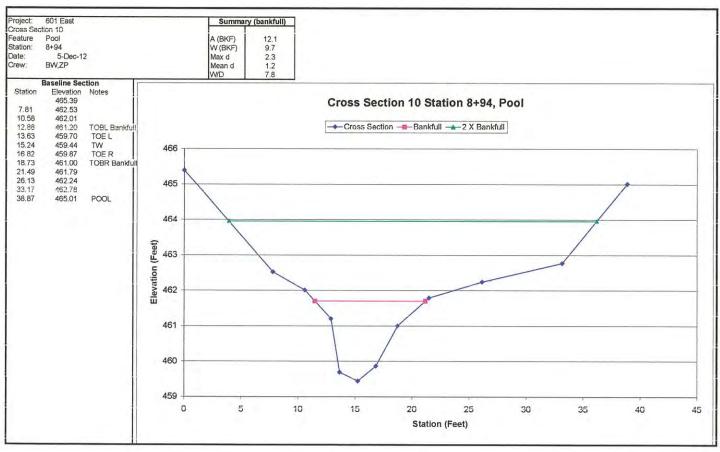


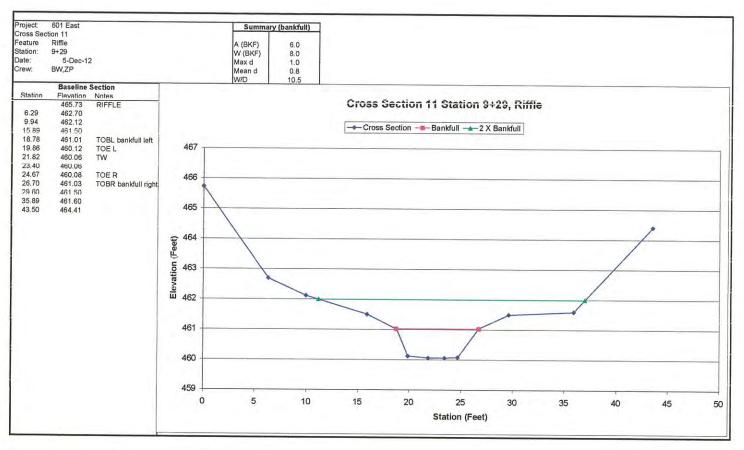


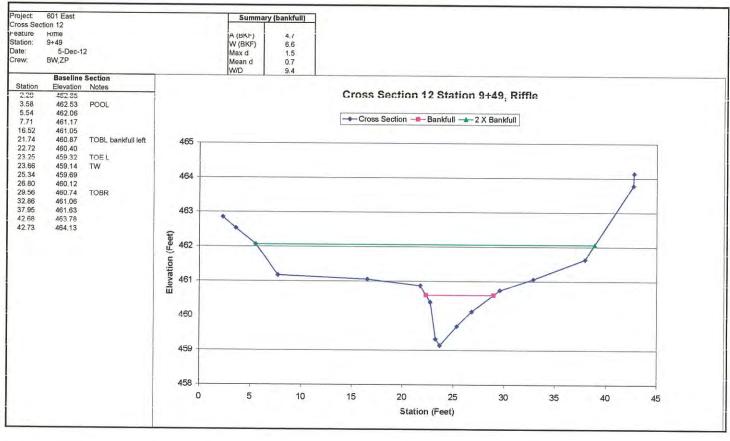






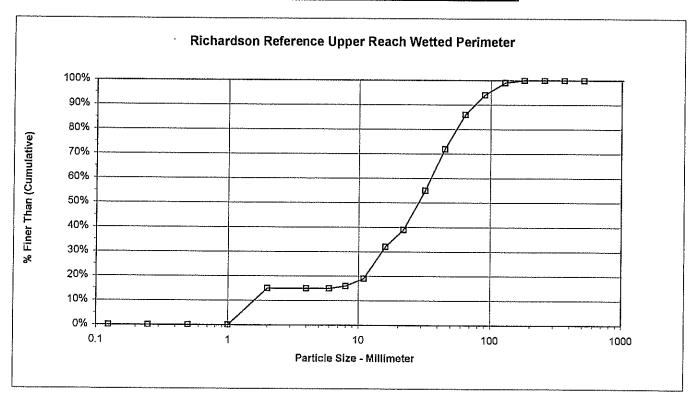






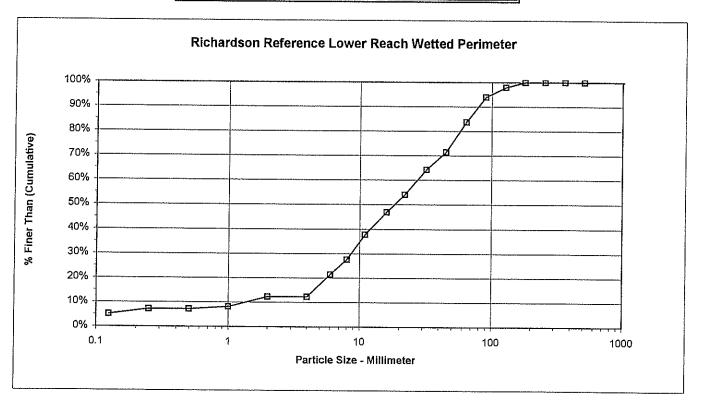
	PEBBLE COUNT									
Project:	REF Richards					Date:	12/6/2012	>		
Location:	Upper Reach	Wetted Perim	eter							
	· · · · · · · · · · · · · · · · · · ·			Particle	Counts					
Inches	Particle	Millimeter		Riffles	Pools	Total No.	Item %	% Cumulative		
	Silt/Clay	< 0.062	S/C	0		0	0%	0%		
	Very Fine	.062125	S	0		0	0%	0%		
	Fine	.12525	A	0		0	0%	0%		
	Medium	.2550	N	0		0	0%	0%		
	Coarse	.50 <i>-</i> 1.0	D	0		0	0%	0%		
.0408	Very Coarse	1.0 - 2.0	S	15		15	15%	15%		
.0816	Very Fine	2.0 - 4.0		0		0	0%	15%		
.1622	Fine	4.0 - 5.7	G	0		0	0%	15%		
.2231	Fine	5.7 - 8.0	R	1		1	1%	16%		
.3144	Medium	8.0 - 11.3	A	3		3	3%	19%		
.4463	Medium	11.3 - 16.0	V	13		13	13%	32%		
.6389	Coarse	16,0 - 22.6	E	7		7	7%	39%		
.89 - 1.26	Coarse	22.6 - 32.0	L	16		16	16%	55%		
1.26 - 1.77	Very Coarse		S	17		17	17%	72%		
1.77 - 2.5	Very Coarse	45.0 - 64.0		14		14	14%	86%		
2.5 - 3.5	Small	64 - 90	С	8		8	8%	94%		
3.5 - 5.0	Small	90 - 128	O	5		5	5%	99%		
5.0 - 7.1	Large	128 - 180	В	1		1	1%	100%		
7.1 - 10.1	Large	180 - 256		0		0	0%	100%		
10.1 - 14.3	Small	256 - 362	В	0		0	0%	100%		
14.3 - 20	Small	362 - 512		0		0	0%	100%		
20 - 40	Medium	512 - 1024	D	0		0	0%	100%		
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0		0	0%	100%		
	Bedrock		BDRK	0		0	0%	100%		
			Totals	100	00	100	100%	100%		

d16	d35	d50	d84	d95
8.0	18.6	28.9		97.6



			PEBBLE (COUNT				
Project:	REF Richards			•		Date:	12/6/201	2
Location:	Lower Reach	Wetted Perim	eter					
				Particle	Counts			· · · · · · · · · · · · · · · · · · ·
Inches	Particle	Millimeter	<u> </u>	Riffles	Pools	Total No.	Item %	% Cumulative
	Silt/Clay	< 0.062	S/C	2		2	2%	2%
	Very Fine	.062125	S	3		3	3%	5%
	Fine	.12525	A	2		2	2%	7%
	Medium	.2550	N	0		0	0%	7%
	Coarse	.50 - 1.0	D	1		1	1%	8%
.0408	Very Coarse	1.0 - 2.0	S	4		4	4%	12%
.0816	Very Fine	2.0 - 4.0		0		0	0%	12%
.1622	Fine	4.0 - 5.7	G	9		9	9%	21%
.2231	Fine	5.7 - 8.0	R	6		6	6%	28%
.3144	Medium	8.0 - 11.3	A	10		10	10%	38%
.4463	Medium	11.3 - 16.0	V	9		9	9%	47%
.6389	Coarse	16.0 - 22.6	E	7		7	7%	54%
.89 - 1.26	Coarse	22.6 - 32.0	L	10		10	10%	64%
1.26 - 1.77	Very Coarse	32.0 - 45.0	S	7		7	7%	71%
1.77 - 2.5	Very Coarse	45.0 - 64.0		12		12	12%	84%
2.5 - 3.5	Small	64 - 90	С	10		10	10%	94%
3.5 - 5.0	Small	90 - 128	O	4		4	4%	98%
5.0 - 7.1	Large	128 - 180	В	2		2	2%	100%
7.1 - 10.1	Large	180 - 256		0		0	0%	100%
10.1 - 14.3	Small	256 - 362	В	0		0	0%	100%
14.3 - 20	Small	362 - 512		0		0	0%	100%
20 - 40	Medium	512 - 1024	D	0	ı	0	0%	100%
40 - 80	Lrg- Very Lrg	1024 - 2048	R	0		0	0%	100%
	Bedrock		BDRK	0		0	0%	100%
			Totals	98	0	98	100%	100%

d16	d35	d50	d84	d95
4.8	10.2	18.6	64.8	100,5



Sieve Sample #1

Pavement Type: Sample Date: Project:

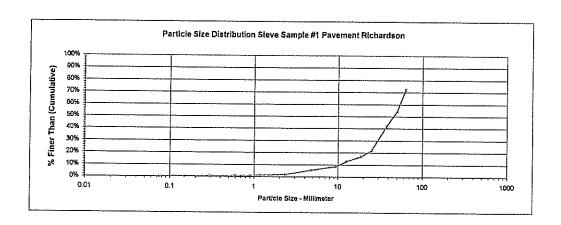
Pavement Sample 12/8/2012 For 601 East Project

Location: Reference Reach Richardson
Largest Particle on bar ====> N/A

Sleve Size	Sleve Size (mm)	Sleve Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Total Weight (Lbs)
2 1/2 inch	63	1.175	1,98	2,45					
2 inch	50	1,195	1.69	2.43					2.0
1 1/2 inch	37.5	1.25	2.16	1.27					1,3:
1 inch	25	1.23		1.35					0.93
3/4 inch	19	1.245	1.61	1.25					1.47 0.37
1/2 inch	12,5	1,21	1.45	1.29					0.3
3/8 inch	9.5	1.225	1.35	1.4					0.3
No. 4	4.75	1.145	1.29	1.23		****			0.23
No. 8	2.38	1.07	1,11	1.3					0.27
No. 16	1.18	0.955	0.96	1					0.05
No. 30	0.6	0.9	0.92	0.915					0.035
No. 50	0.3	0.815	0.817	0.818				~	0.005
No. 100	0.15	0.775	0.8	0.779					0.029
No. 200	0.075	0.765	0.77	0.77					0.01
Passing 200	<0.075	1.08	1.09	1.085		i			0.015

Total Sample Weight =======>

Location: Project:	0		Richardson Sieve Sample #1- Pavement						
Inches	Sleve Size	Millimeter <#200	Section Section	Wt. Retained (lbs)	% Passing	% Cumulative			
0.0029	Commence of the commence of th	The state of the s		0.015	0.20%	0.20%			
	#200	0.0750	S	0,01	0.13%	0.34%			
0.0059	#100	0.150	A.	0.029	0.39%	0.73%			
0,0117	# 50	0.30	BOOK NEEDS	0,005	0.07%	0,80%			
0.0234	#30	0.80	D	0.035	0.47%	1,27%			
0,0469	#16	1.18		0.05	0.67%	1.94%			
0.0937	#8	2,36	G. C. C.	0.27	3.64%	5.58%			
0.187	#4	4.75	133 135 (R) 135 135	0.23	3.10%	8.69%			
0.374	3/8"	9.50	A	0.3	4.05%	12.73%			
0.5	1/2"	12.50	V	0.32	4.32%	17.05%			
0.748	3/4"	19.0		0.37	4.99%	22,04%			
0.9843	1"	25.0	46000 L 100000	1.47	19.83%	41.87%			
1.4764	1 1/2"	37.5	(1) (1) (S) (1) (1)	0.93	12.54%	54.41%			
1.9885	2"	50.0		1.32	17.80%	72.21%			
2.5	2 1/2"	63.0	100 100 C 100 C 100 C	2.08	27.79%	100.00%			
			O: :::::::	0	0.00%	100.00%			
			B	0	0,00%	100,00%			
				0	0.00%	100.00%			
	[]		100 100 B	0	D.00%	100.00%			
	1		[68:58: <u>#</u> 88:686]	0	0.00%	100.00%			
	1		144.00. 9 0.00001	0	0.00%	100,00%			
			State of Residence	0 1	0.00%	100.00%			
	Bedrock		:::::XRQB::::::	0	0.00%	100.00%			
amento in the second			Totals	7.414	100%	100%			



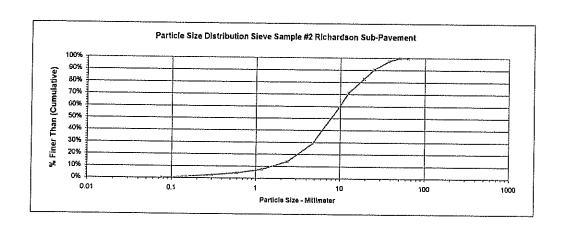
Sieve Sample #2 Pavement Type: Sample Date: Project; Location:

Sub-Pavement Sample 12/6/2013 For 601 East Location: Richardson Reference Reach
Largest Particle on bar ====> N/A

Sleve Size	Sieve Size (mm)	Sleve Weight (Lbs)	Sieve +Sampte Weight (Lbs)	Sleve +Sample Weight (Lbs)	Slave +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Slava +Sample Weight (Lbs)	Total Weight (Lbs)
2 1/2 inch	63	1.175	4 4 7 2						
2 inch	50	1,195	1,175		1,175				
1 1/2 inch	37.5	1.25	1.47	1.195	1.195				
1 inch	25	1.23	1.76	1.63	1.25	- III			G.6
3/4 inch	19	1.245	2.44	1.78	1.23				1.5
1/2 inch	12.5	1.21	2.39	2.6	1.21				1.73
3/8 inch	9.5	1.225	2.41	1,99	2,11			<u> </u>	2.57
No. 4	4.75	1,145	3.81	2.68	3.42				2.835
No. 8	2.38	1.07	2.32	2.01	2.27				0.455
No. 16	1.18	0.955	1.42	1.61	1.3		*****		3.39 1.465
No. 30	0.8	0,9	1.08	1,28	1.02				0.68
No. 50	0.3	0.815	0.91	1.08	0.88				0.425
No. 100	0.15	0.775	0.835	0.93	0.85			·	
No. 200	0.075	0.765	0.815	0.85	0.83				0.29 0.2
Passing 200	<0.075	1.08	1.12	1.11	1.09				0.08

Total Sample Weight ========>

Location: Project:	0		Richardson Sieve Sample #2 Sub Pavement						
Inches	S(eve S)ze	Millimeter < #200	See Section	Wt. Retained (lbs)	% Passing 0.36%	% Cumulative			
0.0029	#200	0.0750	S	0.2					
0.0059	#100	0.150		1	0.90%	1.26%			
0.0117	#50	0.30	las de la como	0.29	1.30%	2.58%			
0.0234	#30			0.425	1.91%	4.48%			
******	, 1	0.60	100 (C 9 50) (C	0.68	3.06%	7,53%			
0.0469	#16	1.18	8	1.465	8.59%	14.13%			
0.0937	#8	2.38	1 (1 C)	3.39	15,25%	29.37%			
0.187	#4	4.75	[1000 R.1100 C	6.455	29.04%	58,41%			
0.374	3/8"	9.50	CONTROL ACTION	2.835	12.75%	71.17%			
0.5	1/2"	12.50	V-1000	2.57	11,58%	82,73%			
0.748	3/4"	19.0	E E E	1,73	7.70%	00.51%			
0.9843	1"	25.0		1,61	6.79%	97,30%			
1.4784	1 1/2"	37.5		0.6	2.70%	100,00%			
1.9085	2"	50.0		0	0.00%	100,00%			
2.5	2 1/2"	63.0	24512602244	0	0.00%	100.00%			
			14444 (0 4444)	0 1	0.00%	100.00%			
				0	0.00%	100.00%			
		B77::::	56664665666	0	0.00%	100.00%			
	1		1444544 B 444444	o !	0.00%	100.00%			
]			0	0.00%	100.00%			
	}		1000 (b 1000)	o	0.00%	100.00%			
			Control Residence	0	0.00%	100.00%			
Maria Patricia de Caraciones d	Bedrock		BDRK	0	0.00%	100.00%			
			Totals	22.23	100%	100%			



Sieve Sample #3

Pavement Type: Poir
Sample Date:
Project: For:
Location: Rich
Largest Particle on bar ====>

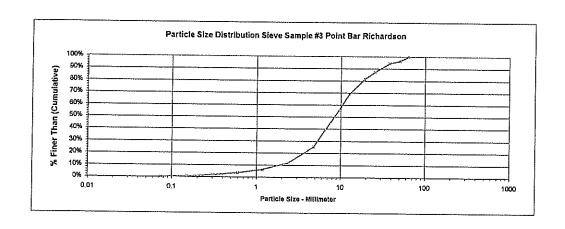
int Bar Sample		****
12/6/2013		
r 601 East		
hardson Reference		
2.5	Samples 2.0,2.5,1,8	

Samples 2.0,2.5,1,8

Sieve Size	Slave Size (mm)	Sieve Welght (Lbs)	Sleve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Slave +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Tota! Weight (Lbs)
2 1/2 inch	63	1.175							- 1
2 inch	50	1.195		· · · · · · · · · · · · · · · · · · ·					
1 1/2 inch	37.5	1,25			4.50	2.14			0.94
1 inch	25	1.23	1.43	1.68	1.38	1.68			0.54
3/4 inch	19	1.245	1,49	1.61	1.59	2.17			1.95
1/2 inch	12.5	1.21	1,78	2.23	1.64 2.18	1.77			1.53
3/8 inch	9.5	1.225	1.91	2.21	2.22	2.05 2.13			3.4
No. 4	4.75	1,145	2.53	3.31	3.45	3,42	· · · · · · · · · · · · · · · · · · ·		3.57
No. 8	2.36	1.07	1.67	1,93	2.1	2.17			8.13
No. 16	1.18	0.955	1.19	1.31	1.35	1,49			3.59
No. 30	0.6	0.9	1.01	1.04	1,08	1,21			1.52
No. 50	0.3	0.815	0.87	0.91	0.92	1.04			0.72
No. 100	0.15	0.775	0.81	0.83	0.84	0.91			0.40
No. 200	0.075	0.765	0.79	0.8	0.8	0.81			0.14
Passing 200	<0.075	1.08	1.09	1.08	1,1	1,11			0.08

Total Sample Weight =======>

Location: Project:	0		Richardson Sieve Sample #3 Point Bar Sample							
Inches	Sleve	Millimeter	T The second second	Wt. Retained (lbs)	% Passing	% Cumulative				
	Size	< #200	S/C···	0.08	0.22%	0.22%				
0.0029	#200	0.0750	S	0.14	0.52%	0.74%				
0.0059	#100	0.150	1960 (CAR 1981)	0.29	1.08%	1.82%				
0.0117	#50	0.30	No.	0.48	1.79%	3.61%				
0.0234	#30	0.60	\$100 0 00000	0.72	2.68%	6.29%				
0.0469	#16	1.18	s	1.52	5.66%	11.95%				
0.0937	#6	2.36	Control Grande	3.59	13.36%	25,31%				
0.187	#4	4.75	100000000000000000000000000000000000000	8.13	30.26%	55.57%				
0.374	3/8"	9.50	Α	3,57	13.20%	68.86%				
0.5	1/2"	12.50	v.	3.4	12.68%	81.52%				
0.748	3/4"	19,0	上的印度的	1.53	5.70%	87.21%				
0.9843	1"	25.0	[6:00:00 to 00:00]	1,95	7.26%	94.47%				
1.4764	1 1/2"	37.5	::::::s:::::::::::::::::::::::::::::::	0.54	2.01%	98.48%				
1,9685	2"	50.0	100000000000000000000000000000000000000	0.945	3.52%	100.00%				
2.5	2 1/2"	63,0	13000000000000000000000000000000000000	0	0.00%	100.00%				
	}		0.000	0	0.00%	100.00%				
			B(100)	0]	0.00%	100.00%				
			[100000][100000]	0	0.00%	100.00%				
	1 1		100000 B00000	0	0.00%	100.00%				
	1		[15:30 5 :333]	0	0.00%	100.00%				
			[6833] 33344	0	0.00%	100.00%				
			(COLORES AND A	0	0.00%	100.00%				
***************************************	Bedrock		BDRK ::::	0	0.00%	100.00%				
			· Totals	26,865	100%	100%				



Sieve Sample #4 Pavement Type: Sample Date: Project: Location:

Bank Soil Sample 12/6/2012 For 601 East

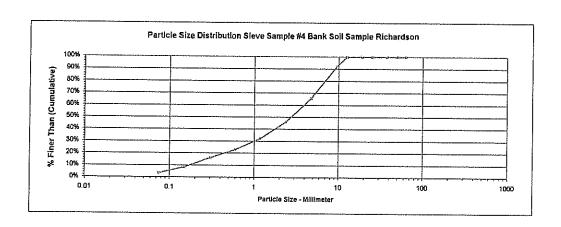
Largest Particle on bar ====>

Richardson Reference Reach

Sleve Size	Sleve Size (mm)	Sleve Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sieve +Sample Welght (Lbs)	Sieve +Sample Weight (Lbs)	Total Weight (Lbs)
2 1/2 inch	63	1,175	1.175					1	
2 inch	50	1.195	1.195						
1 1/2 inch	37.5	1.25							
1 inch	25	1,23	1.23	***************************************	******				
3/4 inch	19	1.245	1.245				*****		
1/2 inch	12.5	1,21	1.21						
3/8 inch	9.5	1,225	1.37			-			0.14
No. 4	4.75	1.145	1.63				m.au.		0.14
No. 8	2.36	1.07	1.43						0.3
No. 16	1.18	0.955	1,21						0,25
No. 30	0.6	0,9	1.07						0,23
No. 50	0.3	0.815	0.94						0.12
No. 100	0.15	0.775	0.915						0.14
No. 200	0.075	0.765	0.86		110-00-1-1-1-1				0,09
Passing 200	<0.075	1.08	1.14		*****				0.03

Total Sample Weight =======>

Location; Project;	0		Sieve Sample #4 Bank Soil Sample Richardson							
Inches	Sieve Size	Millimeter <#200		Wt. Retained (lbs)	% Passing 3.27%	% Cumulative				
0.0029	#200	0.0750	S	0.095						
0.0059	#100	0.150			5.18%	8.45%				
0.0117	#50	0.130	The second	0.14	7.63%	18.08%				
		_,	No.	0.125	6.81%	22.89%				
0.0234	#30	0.60	D.	0.17	9.26%	32,15%				
0.0469	#16	1.18		0.255	13.90%	46.05%				
0.0937	#8	2.36	G	0.36	19.62%	65,67%				
0.187	#4	4.75	100000000000000000000000000000000000000	0,485	28.43%	92.10%				
0.374	3/8"	9,50	Attended Attended	0.145	7.90%	100.00%				
0,5	1/2"	12.50	v	0	0.00%	100.00%				
0.748	3/4"	19.0	133 33 15 33 33	0]	0.00%	100.00%				
0.9843	1*	25.0		0	0.00%	100.00%				
1.4764	1 1/2"	37.5	\$	0	0.00%	100,00%				
1.9685	2"	50.0		0	0.00%	100.00%				
2.5	2 1/2"	63.0	30000 C13550	0	0,00%	100.00%				
			0	0 }	0.00%	100.00%				
	1			0	0.00%	100.00%				
			\$151551 <u>5</u> 166665	0	0.00%	100.00%				
	1		500000B050000	0	0.00%	100.00%				
	1		100 400 4000	0	0.00%	100,00%				
	ļ l			0	0.00%	100.00%				
	<u> </u>		Proceedings (Control	<u> </u>	0.00%	100.00%				
	Bedrock		BDRK	0	0.00%	100.00%				
		11 (17 (17 (17 (17 (17 (17 (17 (17 (17 (Totals	1.835	100%	100%				



Sieve Sample #5

 Pavement Type:
 Material on Glide being deposited

 Sample Date:
 12/8/2012

 Project:
 For 601 East

 Location:
 Richardson Reference Reach

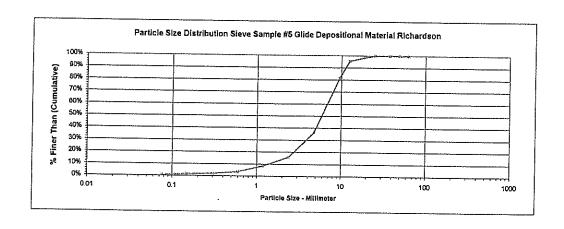
 Largest Particle on bar ====>
 N/A

Sieve Size	Sleve Size (mm)	Sieve Weight (Lbs)	Sieve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Slave +Sample Weight (Lbs)	Sleve +Sample Weight (Lbs)	Total Weight (Lbs)
2 1/2 inch								C Vietaux (EDS)	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
****	63	1.175	1.175						
2 inch	50	1.195	1.195						
1 1/2 inch	37.5	1.25	1.25				******		
1 inch	25	1.23	1.23						
3/4 inch	19	1,245	1,26						
1/2 inch	12.5	1.21	1.24						0.015
3/8 inch	9.5	1,225	1,37						0.03
No. 4	4.75	1.145	1.8						0.145
No. 8	2.36	1.07	1,28						0.455
No. 16	1,18	0.955	1.03						0.21
No. 30	0.6	0.9	0,95						0.075
No. 50	0.3	0.815	0.83						0.05
No. 100	0.15	0.775	0.78					 -,	0.015
No. 200	0.075	0.765	0.77				· · · · · · · · · · · · · · · · · · ·		0.005
Passing 200	≺0.075	1.08	1.09						0.005

Total Sample Weight ========

1.015	

.ocation: !roject:	Sieve Sample #5 Glide Material Deposition Richardson o o							
Inches	Sieve	Millimeter	1	Wt. Retained (lbs)	% Passing	% Cumulativ		
	Size	< #200	S/C	0.01	0.99%	0.99%		
0.0029	#200	0.0750	5 (15)	0.005	0.49%	1,48%		
0.0059	#100	0.150	100 100 A 00 000	0.005	0.49%	1.97%		
0.0117	#50	0.30	100 (200 NO 100 B)	0.015	1.48%	3.45%		
0.0234	#30	0.60	D. 35.6	0.015	4.93%	1		
0.0469	#16	1.18	s s	0.075	7.39%	6.37%		
0.0937	#8	2.36	-tofoppi nistatele elektric	The state of the s		15.78%		
0.187	#4	4.75		0.21	20.69%	36.45%		
0.374	3/8"	0.50		0.455 0.145	44.83%	81,28%		
0.5	1/2"	12.50		0.03	14.29% 2.96%	95.57%		
0.748	3/4"	19.0	100000000000000000000000000000000000000	0.03	2,60% 1,48%	08.52%		
0.9843	1"	25.0		0.013	0.00%	100.00%		
1.4764	1 1/2"	37.5	Process Services	ň	0.00%	100.00%		
1.9685	2"	50.0	E3532 35532	ĭ	0.00%	100,00%		
2.5	2 1/2"	63.0	00000C000000	0	0.00%	100.00%		
			o`	0	0.00%	100.00%		
	1		Barrier B	ŏ	0.00%	100.00%		
				ōl	0.00%	100,00%		
			B	0	0.00%	100.00%		
	į		for the second	ō	0.00%	100.00%		
			Para bit is	0	0.00%	100.00%		
			Describer (0	0.00%	100.00%		
The second second	Bedrock		BORK	0	0.00%	100.00%		
			Totals	1.015	100%	100%		



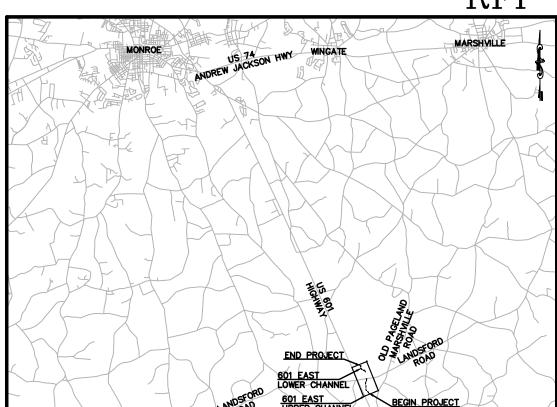
Appendix D. Project Plan Sheets

CONSTRUCTION PLANS FOR EAST

STREAM AND WETLAND RESTORATION PROJECT UNION COUNTY, NORTH CAROLINA EEP CONTRACT DENR NO:004925



RFP 16-004110





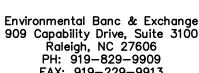
SURVEY DATA PROVIDED BY:



909 MARKET STREET WILMINGTON, NC 28401 (910) 762-4200 NC LICENSE NO. F-0374

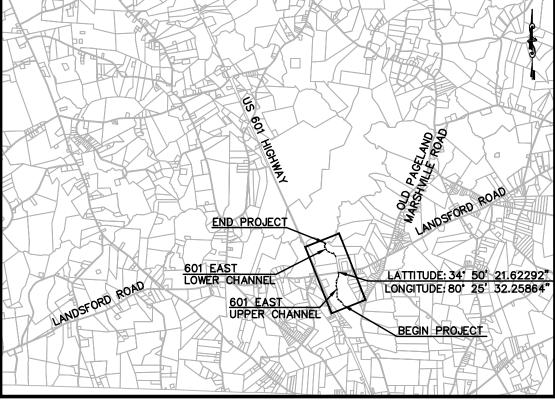
STREAM DESIGNER:

Ward Consulting Engineers 4805 Green Road Raleigh, NC 27616 NC LICENSE NO: C-2619 PH: 919-870-0526 FAX: 919-870-5359



FULL DELIVERY PROVIDER:

909 Capability Drive, Suite 3100 Raleigh, NC 27606 PH: 919-829-9909 FAX: 919-229-9913



LOCATION MAP

INDEX OF SHEETS

SHEET NO. T1 L1 TCS1-TCS2 GNI D1-D5 PP1-PP8 VP1-VP12 CEM1-CEM2

TITLE SHEET LEGENDS SYMBOLS AND SHEET KEY
TYPICAL CONSTRUCTED CROSS SECTIONS
GENERAL NOTES AND CONSTRUCTION SEQUENCE DETAILS PLAN AND PROFILE PLANTING PLANS CONSERVATION EASEMENT MARKING PLAN

> **PRELIMINARY** NOT FOR CONSTRUCTION

Consulting FIRM LICENSE NO

CAROLINA SHEET EAST

NORTH TITLE COUNTY, UNION

601

DATE: 5 SEPT 2013 2EVISIONS

WG NAME: Construction Title Shee: ALE: NTS

MITIGATION PLAN SET

T1

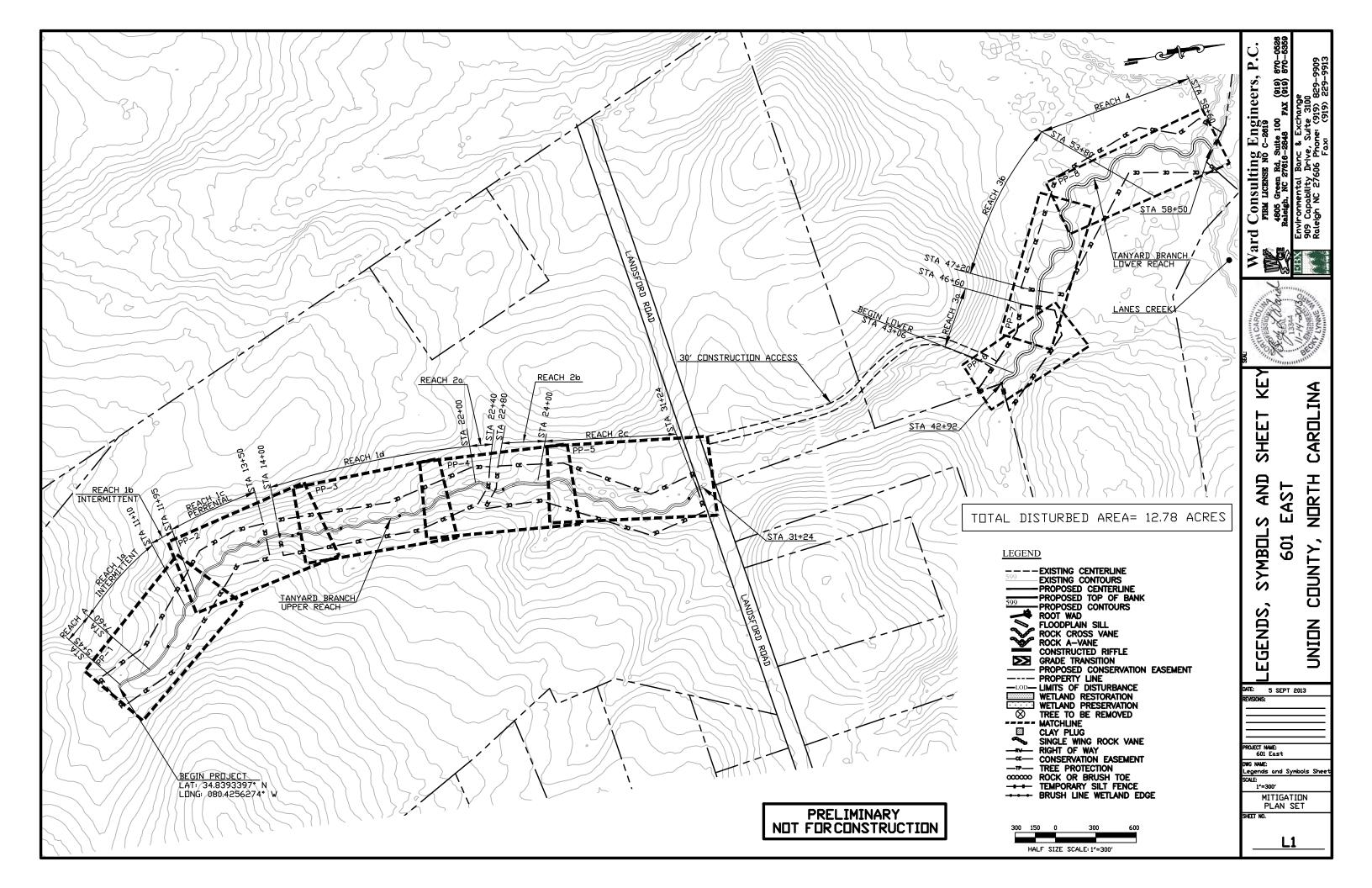
VICINITY MAP

The Catena Group Inc. 410-B Millstone Drive Hillsborough, NC 27278 PH: 919-732-1300 FAX: 919-732-1303

NATURAL SYSTEMS INVESTIGATION:

NCEEP CONTACT: PAUL WIESNER (828) 273-1673 WARD CONSULTING ENGINEERS CONTACT: BECKY WARD. PE (919) 870-0526

ENVIRONMENTAL BANC AND EXCHANGE CONTACT: (919) 829-9909

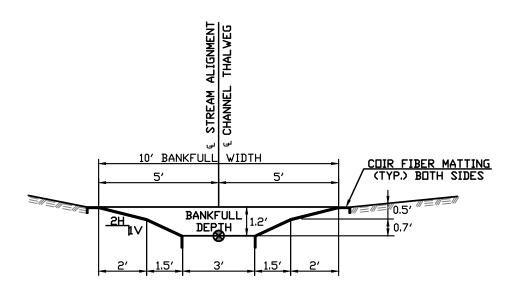


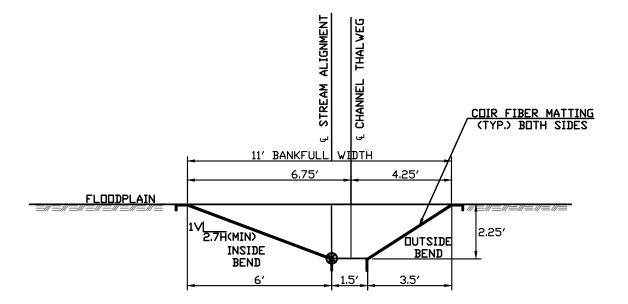
- NOTES:

 1. CONTRACTOR TO PROVIDE A SMOOTH TRANSITION
 BETWEEN THE RIFFLE AND POOL SECTIONS SHOWN BELOW.

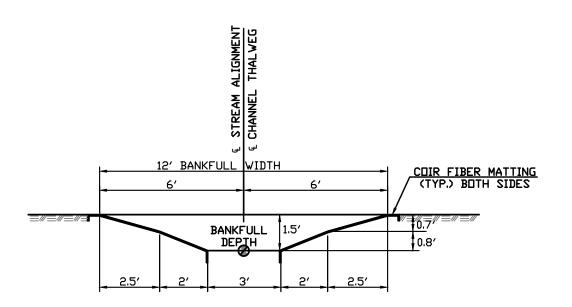
 2. DINDICATES THE STREAM CENTERLINE ALIGNMENT AS IDENTIFIED
 ON THE PLAN AND PROFILE SHEETS.
- 3. $\[\]$ OF STREAM FOR HORIZONTAL LAYOUT AND $\[\]$ OF THALWEG
- MAYBE AT DIFFERENT LOCATIONS IN POOL SECTIONS.

 4. USE 700 GRAM COIR FIBER MATTING BLANKET WESTERN EXCELSION CORPORATION COIR MAT 700 OR APPROVED EQUAL.

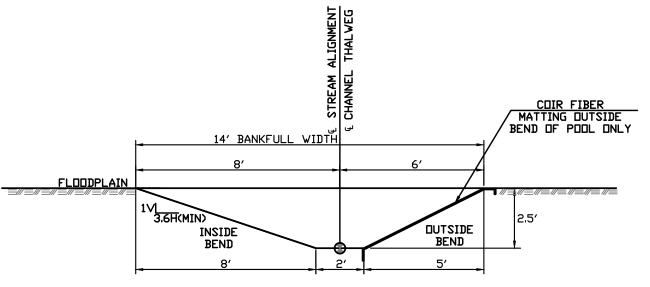












PROPOSED RIFFLE SECTION (REACH 2)

SCALE: NOT TO SCALE



PRELIMINARY NOT FOR CONSTRUCTION

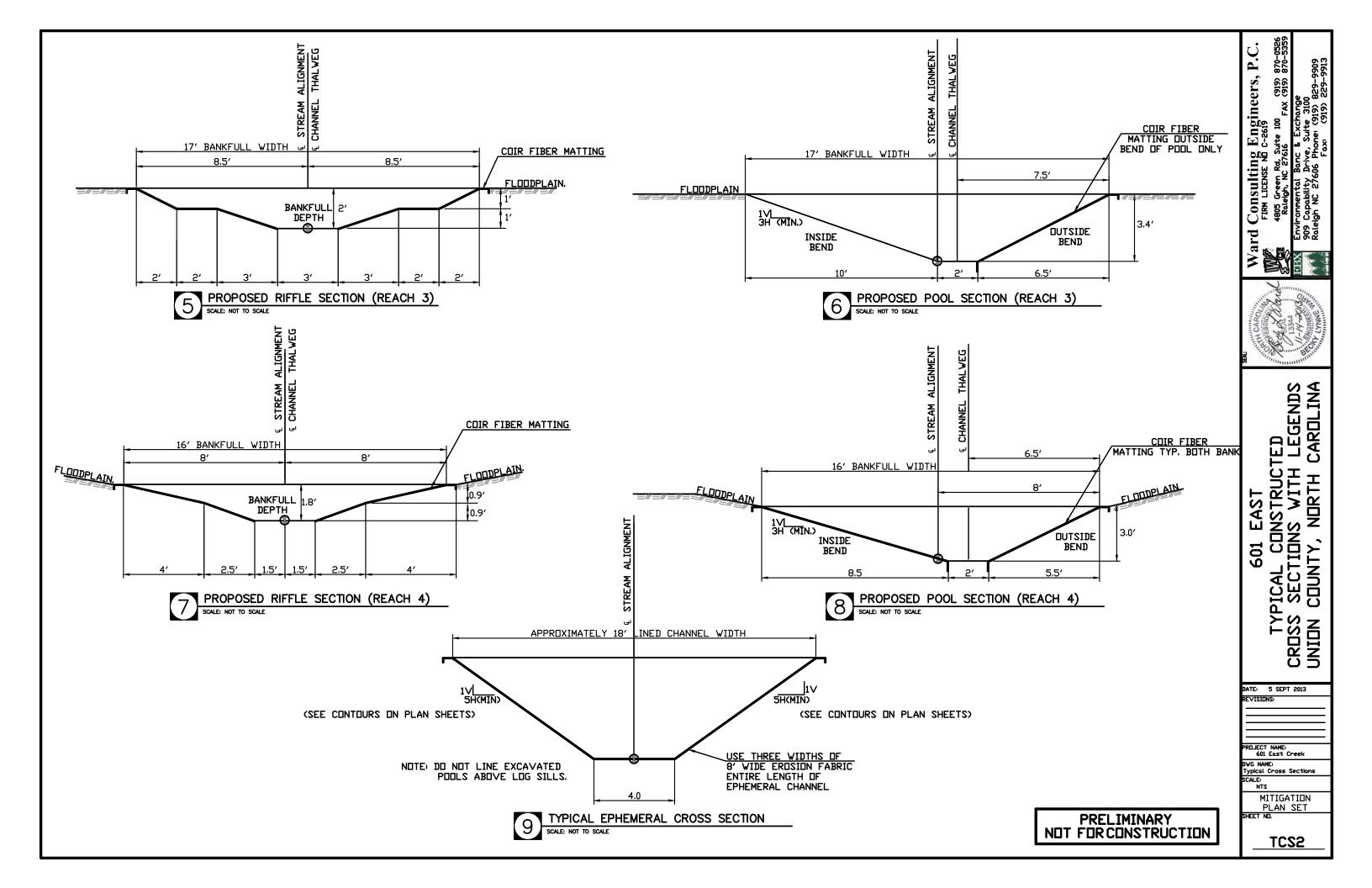
TYPICAL CONSTRUCTED SS SECTIONS WITH LEGENDS IN COUNTY, NORTH CAROLINA 601 CROSS

Consulting Engineers, FIRM LICENSE ND C-2619

Ward

DATE: 5 SEPT 2013 ROJECT NAME: 601 East Creek DWG NAME: Typical Cross Sections MITIGATION
PLAN SET

TCS1



GENERAL NOTES:

- Contractor shall verify locations and elevations of all existing utilities inside the construction corridor. The contractor is responsible for having all utilities located 48 hours prior to mobilization to the site. "Call before you dig." Toll free number (811)
- The Contractor shall follow OSHA guidelines and utility owner guidelines when working near utilities.
- All construction and materials shall be constructed to standards provided on the plans.
- Contractors shall verify all dimensions in field. Any discrepancies thereof shall be reported to the owner and designer, prior to proceeding with the work.
- 5. No trees not shown for removal on the plans shall be removed without the Designers approval unless they are in the new channel alignment. All trees and debris to be mulched onsite or properly disposed of offsite. Remaining tree stumps to be no more than 12" from existing ground.
- Base topographic and planimetric information generated from Union County GIS data and field surveys.
- No subsurface data is made available to the Contractor for this project.
 The Contractor shall be responsible for making his own subsurface investigations as they relate to this project.
- Benchmark controls are shown on the Staking Plan. The Contractor is
 responsible for performing the construction survey. The Designer will
 coordinate available auto-cad drawing files to the surveyor for the
 proposed design and base survey data obtained in the design phase of
 the project.
- 9. Plan Vertical Datum: NAVD 1988
- 10.Plan Horizontal Datum: NC State Plane Coordinates NAD 83
- 11.No Flood Hazard zones exist on this project according to FEMA Floodway map for Tanyard Branch. Lanes Creek and Mills Creek South are FEMA regulated.
- 12.In the event of a storm, the owner will not accept any liability for damaged equipment, tools, materials, or other items needed to complete the work. The contractor will be responsible for removal or protection of any equipment that could be affected by storm flows.
- 13. Temporary construction access to the site to be improved only as necessary in areas unsuitable for construction equipment passage by the Contractor. All access improvements to the roadway, gates, and fences required for construction to remain for future use by landowner. Existing farm fields used for construction access will be repaired to original conditions or better by the contractor.
- 14. The Contractor shall be responsible for repairing any damaged items during construction including by not limited to, existing roads, gates, fences, etc.
- 15. The Contractor shall make every effort to prevent damage to trees within the tree protection area. In the event of damage, repair any damage to the crown, trunk, or root system immediately.
 - Roots: Repair roots by cutting off damage areas and painting them with tree paint. Spread peat moss or moist topsoil over exposed roots.
 - Tree Bark: Repair damage to bark by trimming around damaged area, taper the cut to provide drainage, and paint the tree paint.
 - c. Tree Limbs: Cut off all damaged tree limbs above the tree collar at the trunk or main branch. Use a separate cut to avoid peeling bark from healthy area of the tree.

ACCESS, STAGING AND STOCKPILE AREA NOTES:

- Construction equipment limited to only areas within the limits of disturbance as shown on the plans. All parking and staging to be limited to areas shown on plan.
- 2. All areas outside the shown disturbance limit or conservation easement to remain in their natural condition.
- All construction to be performed from the top of bank, no equipment will be permitted to work from the channel bed or cross the streams except at designated locations as shown on the plans.
- 4. Every effort shall be taken to minimize disturbance in the stream channel and in gaining access to and from the work area.
- Access and staging areas have been shown on the plans. Staking of the access areas shall be approved by the Designer before construction commences.
- The contractor shall establish stockpile areas along the project, as necessary, to carry out the work. All stockpile areas must be inside the limits of construction and approved by the Designer. Stockpile areas should not be located within forested areas. Silt fence shall be

- required in areas where loose soil has been placed in the staging and stockpilling areas. The contractor is responsible for the temporary protection and permanent stabilization of all soil stockpiles on site as well as soil internally transported within the project site.
- 7. Temporary access areas which go through agricultural fields are to be planted with temporary seed mix.

MATERIALS NOTES

- The Contractor is responsible for stockpiling all materials as stated above.
- Topsoil: the upper 6 inches of topsoil shall be saved from areas that will be disturbed by excavation, fill, access areas, or compaction equipment. Topsoil shall be kept separate from any site spoil. Upon completion of construction, topsoil will be spread at a depth of 4 to 6 inches over areas to be planted. See planting plans.
- 3. Stream Bed Material: Stream bed material deemed suitable by the designer. Shall be saved from areas of the exiting stream that will be impacted by construction. These areas will be flagged by the designer prior to construction. Excavated bed materials will be utilized in close proximity to their location of excavation, and will not require extensive hauling. This excavated bed material will be used to seed the newly constructed stream riffles.
- 4. Site Spoil: All remaining excavated materials other than topsoil and stream bed material shall be considered site spoil. The site spoil shall be stockpiled separately. Suitable site spoil shall be saved for later use as backfill of the abandoned channel. All excess soil shall be wasted on site in designated areas or hauled off site.

EROSION CONTROL NOTES:

Total Disturbed Area = 12.78 Ac

Project Soil Types Carolina Slate Belt: Badin, Chewacla, Cid, Mecklenburg, and Tarrus.

- The contractor shall exercise precautions throughout the construction sequence to prevent erosion and siltation. Erosion control measures shall be installed and maintained in accordance with the project plans, North Carolina Sedimentation and Erosion Control Guidelines, and as directed by the designer. All sedimentation and erosion
- The owner and financially responsible party for this project is Environmental Banc and Exchange.
- Construction work shall be in compliance with regulations of the National Pollutant discharge Elimination System (NPDES) stormwater general permit. The Contractor shall be responsible for installing a RAIN GAUGE on the project site & for recording daily rainfall amounts during construction.
- 4. The contractor shall be responsible for maintenance of all erosion control measures during construction. The measures shall be maintained continuously, relocated when and as necessary, and shall be checked for maintenance issues after every rainfall.
- 5. All disturbed areas to be seeded to specifications unless otherwise noted on the planting plan. Seeded areas shall be checked regularly and shall be watered, fertilized, reseeded and mulched as necessary to obtain a dense stand of grass. All disturbed areas that are not otherwise stabilized shall be top soiled and seeded, temporarily or permanently in accordance with the North Carolina sediment control regulations. Permanent seeding and grass establishment is required prior to project completion and acceptance.
- 6. The Contractor shall provide ground cover as soon as practable but in the event within 14 days on disturbed flat areas and 7 days on all perimeter dikes, swales, ditches perimeter slopes and slopes steeper then 3 horizontal to 1 vertical. Permanent ground cover shall be established within 15 working days or 90 calendar days (whichever is shorter) following completion of construction.
- 7. All temporary erosion and sediment control measures shall be removed with in 21 days after final site stabilization or after the temporary measures are no longer needed. Trapped sediment and the disturbed soil areas resulting from the disposition of temporary measures shall be permanently stabilized to prevent further erosion and sedimentation.
- The Contractor shall only conduct bank and stream bed work, including all in-stream, grading bank stabilization, and in-stream structures on a section of stream that can be entirely stabilized before turning flow into the newly constructed channel.
- If any soil is transported offsite, it is the contractor's responsibility to ensure that this action is conducted in a manner that is consistent with the approved erosion control permit.

- 10. Construction entrances shall be installed at all access locations as shown on the plans. When a crushed stone construction entrance has been covered with soil or has been pushed into the soil by construction traffic, it shall be replaced with a depth of stone equal to that of the original application.
- 11. The Contractor shall keep all surrounding public roadways and drainage systems free from dirt, mud and construction debris at all times. Where sediment is transported onto a paved or public road surface, the road surface shall be cleaned thoroughly at the end of each day. Sediment shall be removed form the roads by shoveling or sweeping and transported to a sediment control disposal area. Street washing shall be allowed only after excess sediment is removed.
- 12. During construction the Contractor shall be responsible for installing additional erosion control measures not shown of the plans but necessary to control excess sediment, if determined to be necessary by the Designer. Additional soil stockpile areas will be pre-approved by the engineer and will have appropriate silt fencing installed around in

SEQUENCE OF CONSTRUCTION EVENTS

A General Initial Site Preparation

- 1. Perform all utility identification and marking/flagging as necessary.
- The contractor shall set up a pre-construction meeting with the local erosion control inspector, and the project engineer. The contractor shall schedule this meeting a minimum of 48 hours prior to any land disturbing activity.
- 3. Install construction entrance(s) and access road. The construction entrance(s) and staging area(s) identified on the plans provide the only access points in to the limits of disturbance. No additional access points shall be used without approval of the designer and modifications of the erosion control permit.
- Stake and mark sensitive areas and trees/vegetation to be saved. (Coordinate with Designer).
- 5. Stake construction limits, clearing limits and stream access locations as shown on the plans or as directed by the designer.
- 6. Install sediment/erosion control fencing as shown on the plans and all other erosion control measures as necessary to begin clearing and grading operations in accordance with the approved erosion control plan. Erosion control measures shall be installed and maintained in accordance with the project plans and special provisions, North Carolina sediment and erosion control guidelines and as directed by the designer. The contractor shall exercise every reasonable precaution throughout the construction of the project to prevent erosion and siltation. When the measures are complete call for an inspection by the local erosion control inspector.
- 7. Identify staging and stockpile areas as shown on plans. (Coordinate with Designer) All excavated material shall be stockpiled within the limits of disturbance for later use as embankment material or disposal. The contractor is responsible for installing appropriate stabilization measures around the stockpile area(s) to prevent erosion and sedimentation.
- Perform clearing and selective vegetation removal operations. All woody vegetation on site smaller than 6" to be shredded to mulch and stockpiled to be used to amend the soil in the floodplain or disposed of offsite.
- Clear any debris from the stream. Dispose of according to the plans and specifications or as directed by the Designer.
- 10. Install temporary crossings as shown on the plans. The permanent stream crossings will not be installed until the channel construction in that area is completed in conjunction with the crossing. The culvert permanent crossings and temporary crossings as shown on the plans will serve as the only stream crossing locations for Tanyard Branch.

B Stream Restoration Area Construction

- It is up to the discretion of the contractor to determine the length of daily work areas in accordance with the following provisions:
 - a. All excavation shall be performed in dry or isolated sections of the channel.
 - b. The contractor shall only conduct stream work, including all instream structures, grading, stabilization measures, seeding, mulching, and matting work, on a section of stream that can be completed within a single day. Each section of completed stream must be stabilized and matted before flow can be returned into the channel.

- c. Temporary pumps shall be utilized by the contractor in portions of the stream to divert normal flow from and dewater the work area. The pumps and bypass or dewatering layouts used by the contractor shall meet all requirements specified in these plans. The temporary pump shall be installed and removed in accordance with the manufactures guidelines. The contractor shall be responsible for utilizing pump(s) sufficient to bypass the normal flow and dewater the work area.
- d. All disturbed soils will be seeded for vegetative stabilization in accordance with the temporary and permanent seeding specifications in the special provisions and as listed on the planting plan notes sheet VP 1-2 of the construction set.
- The Contractor shall work from upstream to downstream when doing work in the existing channel. The Contractor shall maintain a temporary rock silt screen downstream of any work in the live stream.
- Amend soils; stabilize with erosion control matting, and seed daily as construction proceeds downstream.
- Construct ephemeral channel improvements at the top of the project to station 7+60 the beginning of the intermittent channel.
- Pump around Tanyard Branch from station 7+60 to 13+50 as needed and construct the channel and floodplain grading, stabilizing the channel daily as work progresses.
- Pump around to construct permanent stream crossing at Station 13+75.
 Install pipe to the lines and grades as called for on the plans.
- Pump around Tanyard Branch from 14+00 to 22+50 to construct the channel and floodplain basins at concentrated overland flow locations.
 Stabilize all work areas daily as work progresses.
- Pump around Tanyard Branch from 22+50 to 25+80. Construct channel and floodplain improvements.
- Construct the channel from 25+80 to 30+80 adjacent to the existing channel. Contractor to minimize construction impacts to the existing wetland areas.
- Pump around from 30+80 to Landsford Road. Complete the channel construction and tie into the existing culvert at Landsford Road.
- Contractor to finish seeding and stabilization of project upstream of Landsford Road.
- 11. Mobilize equipment and materials to lower end of the stream.
- 12. Construct the channel in the dry from station 44+20 to 58+50. Stabilize with seed and matting.
- 13. Construct the permanent crossing at station 46+92.
- 14.Pump around the stream from station 42+90 and divert flow into the newly constructed channel.
- 15. Construct the channel from 42+92 and tie into the newly constructed channel at 44+20.
- 16. Contractor to stockpile materials in only the locations shown on the plans unless otherwise approved by the engineer or owner. Fill abandoned channel as construction proceeds downstream and the stream flow is diverted to the new channel. Seed floodplain, ephemeral pool(s) and wetland enhancement area(s) as final grading is completed.
- 17. Complete re-vegetation of the woody species for the project within the conservation easement as shown on the plans.
- $18. \\ Repair areas used for construction access.$
- Seed and mulch staging areas, stockpile areas, access areas and any remaining non-vegetated areas within the project.

C General Site Completion

- Complete site cleanup and stabilization as called for on the plans and specifications.
- 2. Erosion control devices shall be removed from their respective locations only when the stabilization of the adjacent ground has been established. The removal of the construction entrance will occur when all of the construction equipment has been removed from the project site. Construction entrance stone will only be left on the project site upon the request of the land owner. Upon removal of the entrance the area will be seeded and mulched.
- 3. Obtain Final approvals.
- 4. Complete as-built survey.

PRELIMINARY NOT FOR CONSTRUCTION

ortions of work area. e plans. ccordance e normal

ard Consulting Engineers,
FIRM LICENSE ND C-2619
4805 Green Rd, Sulte 100 (919) 8
Roleigh, NC 27616-2848 FAX (919) 8



601 EAST GENERAL NOTES AND CONSTRUCTION SEQUENCE UNION COUNTY, NORTH CAROLINA

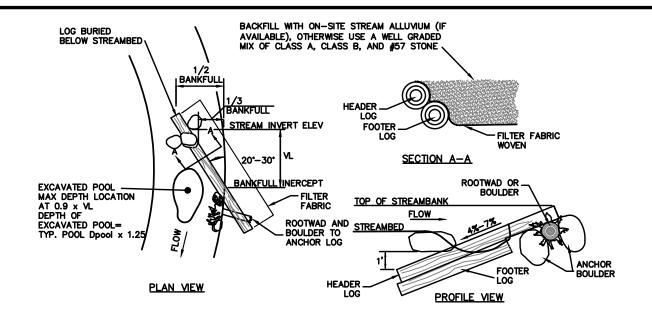
DATE: 5 SEPT 2013
REVISIONS:
PROJECT NAME:
601 East

601 East

WG NAME:
Construction Sequence
CALE:
NTS

MITIGATION PLAN SET

GN1



- HEADER LOG SHALL BE AT LEAST 18" IN DIAMETER AND THE FOOTER LOG AT LEAST 12" IN DIAMETER; RELATIVELY STRAIGHT, HARDWOOD, AND RECENTLY HARVESTED.
- BOULDERS MUST BE AT LEAST 2'X2'X3'.
 SOIL SHOULD BE WELL COMPACTED AROUND BURIED PORTIONS OF LOG.
- 5. SOIL SHOULD BE PLACED BENEATH THE HEADER LOG AND PLACED SO THAT IT LOCKS
 THE HEADER LOG INTO THE BANK.

 5. BOULDERS SHOULD BE PLACED ON TOP OF HEADER LOG FOR ANCHORING.

 6. FILTER FABRIC SHOULD BE NAILED TO THE LOG BELOW THE BACKFILL.

EROSION CONTROL MATTING TO BE LENGTH VARIES SEE PLANS INSTALLED IN EXCAVATED TRENCH AS TAIL LENGTH "C" SHOWN CONTRACTOR TO PACK VOIDS WITH STONE MIX THEN ADD A FINE LAYER OF SOIL TO FILL SMALLER VOIDS AS RIFFLE IS CONSTRUCTED FROM BOTTOM UP STREAM FLOW **PROPOSED** CHANNEL THE RIFFLE TAIL LENGHTS "C" ARE 5' THALWEG MINIMUM. RIFFLE SLOPE PLACE STONE MIX AS SHOWN IN CHART BELOW. CONTRACTORTO UTILIZE EXISTING RIFFLE STONE IN OLD CHANNEL FOR CONSTRUCTION OF NEW RIFFLES WHERE SLOPE 3H:1V SLOPE 3H: 1V RIFFLE

STONE

MIX

TAPER ROCK FROM BOTTOM OF TRENCH TO DEPTH B AT HEAD AND END OF RIFFLE

	F				
STONE MIX	15%	30%	50%	5%	TRENCH DEPTH
CLASS I MIX	#57STONE	CLASS A	CLASS I	SOIL	18"
CLASS II MIX	#57STONE	CLASS B	CLASS II	SOIL	24"

NOTE: CLASS A - RIP RAP 2"-6" AVG 4"
CLASS B - RIP RAP 5"-12" AVG 8" 5"-12" AVG 8" 5"-17" AVG 10"

CLASS I - RIP RAP CLASS II - RIP RAP 9"-23" AVG 14"

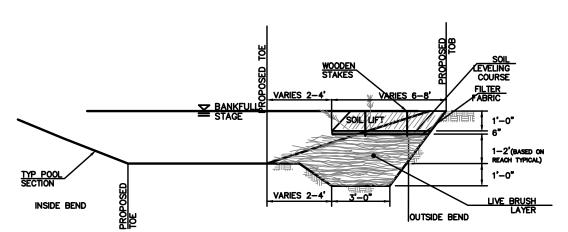
FROSION CONTROL **MATTING** STONE MIX

LONGITUDINAL VIEW

SECTION VIEW "A-A"

SEE VERTICAL ALIGNMENT TABLES FOR CONSTRUCTED RIFFLE LENGTHS, SLOPES, ELEVATIONS AND COORDINATES

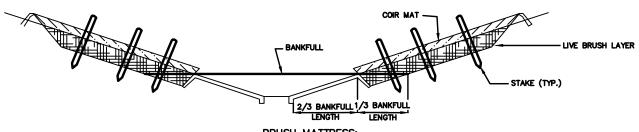
LOG VANE SCALE: NOT TO SCALE



- NOTES:

 1. WRAP SOIL FOR LIFT IN DUAL LAYERS OF WOVEN C-700 FABRIC, SEED AND STRAW FACE & TOP OF LIFT.
- 2. LIVE STAKE VERTICAL FACE & TOP OF LIFT
- 3' SPACING.
 3. PLACE FILTER FABRIC AND SOIL LEVELING COURSE ON TOP OF BRUSH LAYER.

CONSTRUCTED RIFFLE SCALE: NOT TO SCALE



STAKES 3 FT O.C.

COIR ROPE SECURED TO STAKES

BRUSH MATTRESS:
1. BEGIN BRUSH MATTRESS IN UPPER 1/3 OF BANKFULL CHANNEL BOTH SIDES OF THE STREAM.

2. BACKFILL 3" OF ONSITE ALLUVIUM OVER BRUSH LAYER. 3. COVER WITH EROSION CONTROL MAT.

4. STAKE AND TIE DOWN WITH ROPE SECURED TO STAKES.

CROSS SECTION VIEW

MINIMUM OF 20 TO 50 BRANCHES PER SQ. YD. (2.5 IN' MAX DIAMETER)
-6' IN LENGTH

PLAN VIEW

NOTES:

1. BRUSH MATRESS SHOULD
BE INSTALLED DURING
VEGETATION DORMANCY.
2. ONLY USE SPECIES
SPECIFIED UNDER LIVE
STAKES SECTION OF
VEGETATION SELECTION.

TOWARDS THE STREAM WOODEN STAKE SECURE ROPE W/ MIN 3-FT LENGTH **DETAIL**

NOT FOR CONSTRUCTION

PRELIMINARY

BRUSH MATTRESS SCALE: NOT TO SCALE

SCALE: NOT TO SCALE

BRUSH TOE DETAIL

NORTH **EAST** S **DETAIL** 601 COUNTY, NOIN O

CAROLINA

4

Consulting Engineers,

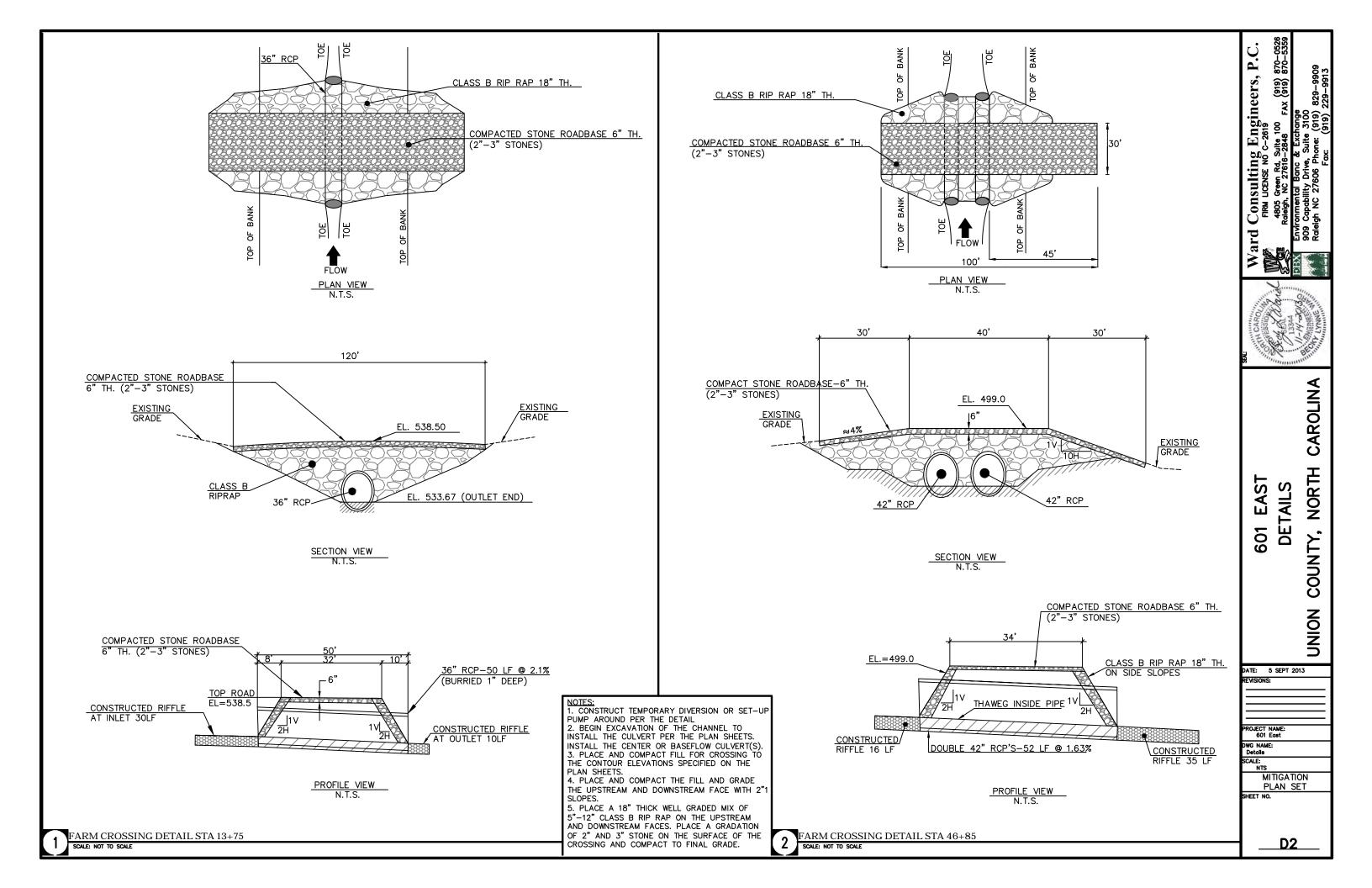
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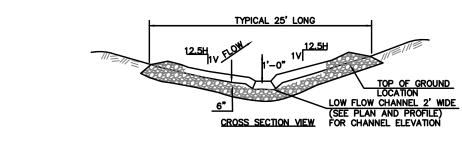
Green Rd, Suite 100 , NC 27616-2848

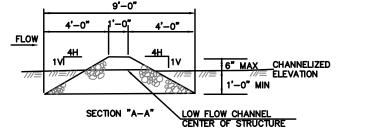
DATE: 5 SEPT 2013 REVISIONS OJECT NAME: 601 East WG NAME: Details NTS

MITIGATION PLAN SET

D1







EPEMERAL CHANNEL ROCK GRADE CONTROL (REACH A)

DESIGN VELOCITY = 4.5 FT/SEC RIP RAP SHOULD NOT EXCEED 3/3 BANKFULL HEIGHT

1. STONE MIX TO CONSIST OF THE FOLLOWING SIZES: 70% 6-8" STONE 20% 2-4" STONE 10% GRAVEL

EPEMERAL CHANNEL ROCK WEIR (REACH A)

STONE AND LOG CONSTRUCTED RIFFLE

SCALE: NOT TO SCALE

FLOW

- CORE FIBERMATTING BANKFULL BOULDERS CLASS II RIP RAP 2/3 BANKFULL HEIGHT MIX CLASS 2"-6" STONE AVG. 4" WITH CLASS II RIP RAP 9" - 23" STONE AVG. 14" EXCAVATED TRENCH

RIFFLE AT CENTER
OF LOGS EROSION CONTROL MATTING INSTALL AT A SLIGHT ANGLE 5-10° RIFFLE STONE MIX
50% CLASS B RIPRAP (5-12") AVG 8"
30% CLASS A (2-6") AVG 4"
15% GRAVEL
5% SOIL FROM PERPENDICULAR (TYP) BOULDER SIZE - CLASS II RIPRAP 12"x18"x24" (MAX) LOG SIZE - 8-12" DIAMETER, LENTH 15' REACH 2, 20' REACH 3 SECTION VIEW A-A MAX SPACING OF LOGS 10" MINIMUM LOGS/STRUCTURE NOTES

1. CONTRACTOR TO UTILIZE
EXISTING RIFFLE STONE IN OLD
CHANNEL FOR CONSTRUCTION
OF NEW RIFFLES WHERE
POSSIBLE FOR BEST BUG AND
LEAF PACK RECRUITMENT AS
WELL AS AESTHETICS.
2. EROSION CONTROL MATTING TO
BE INSTALLED IN EXCAVATED
TRENCH WHERE POSSIBLE. TAIL LENGTH LENGTH VARIES SEE PLANS TAIL LENGTH STREAM FLOW LOGS INCORPORATED **PRELIMINARY** INTO RIFFLE NOT FOR CONSTRUCTION PROFILE VIEW B-B

FLOW NOTES:

1. TOP OF WEIR ELEV 552
TO BE PLACED LEVEL FOR SHEET FLOW.

2. ROCK FACE TO CONSIST OF THE FOLLOWING STONE MIX: FLOW 60% 4-6" STONE 20% 2-4% STONE 20% GRAVEL 6" THICK ROCK LAYER - FLOW _EL. 550 EL. 550 COMPACTED SOIL KEY STONE IN 18"
DEEP US FACE AT TOE FILTER FABRIC

Consulting Engineers, F FIRM LICENSE NO C-2619 4805 Green Rd, Sulte 100 (919) 87 Raleigh, NC 27616-2848 FAX (919) 87 Vironmental Banc & Exchange Ward

CAROLINA

NORTH **EAST DETAILS** 601 COUNTY, NOINO

DATE: 5 SEPT 2013 REVISIONS:

ROJECT NAME: 601 East

WG NAME:

SCALE: NTS MITIGATION PLAN SET

D3

ROCK TOE STABILIZATION

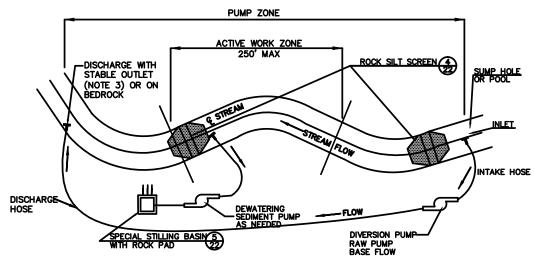
SCALE: NOT TO SCALE

NOTE: 1. SPECIAL STILLING BASIN LOCATION TO BE APPROVED BY THE ENGINEER PRIOR TO INSTALLATION.

2. PROVIDE STABILIZED OUTLET TO DRAIN TOWARDS STREAM.

3. THE SILT BAG SHOULD BE REPLACED AND DISPOSED OF WHEN IT IS 75% FULL OR WHEN IT IS IMPRACTICABLE TO MOVE OR OTHERWISE NOT FILTERING WATER AT A REASONABLE FLOW RATE.

4. THE SILT BAG SHOULD BE REMOVED TO AN UPLAND AREA AND DISPOSED OF WITH OTHER WASTE MATERIAL IN AN AREA PROTECTED BY SEDIMENT AND EROSION CONTROL MEASURES. THE CONTENTS OF THE SILT BAG SHOULD BE DISPOSED OF IN THIS AREA AND THE BAG ITSELF TAKEN OFF-SITE FOR DISPOSAL.



NOTE: 1. WORK AREA TO BE STABILIZED AT THE END OF EACH WORK DAY.

2. ROCK SILT SCREENS REQUIRED FOR PUMP
AROUND OPERATIONS ARE CONSIDERED INCIDENTAL TO PUMPING.

3. STABLE OUTLET TO CONSIST OF ROCK PLACED IN CHANNEL
FOR ENERGY DISSIPATION AND 45°
ELBOW INSTALLATION AT THE END OF THE PIPING SO THAT
THE WATER DISCHARGES VERTICALLY UP IN THE AIR. THE OUTLET WILL
BE APPROVED BY THE DESIGNER PRIOR TO PUMPING.



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CAROLINA NORTH **DETAILS** COUNTY,

EAST 601

DATE: 5 SEPT 2013

NOINO

ROJECT NAME: 601 East

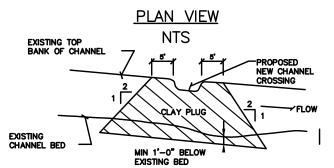
OWG NAME: Details

NTS MITIGATION PLAN SET

<u>D4</u>

SPECIAL STILLING BASIN WITH ROCK PAD

-CLAY PLUG COMPACTED TO 95% STANDARD PROCTOR - EXISTING CHANNEL TO BE FILLED



CLAY PLUG DETAIL (FOR STREAM CROSSING OVER AN EXISTING CHANNEL AT A HIGHER ELEVATION)

USE MINIMUM TOP WIDTH OF 10'
WHERE CHANNEL IS TO THE SIDE OF
THE CLAY PLUG AS SHOWN ON PLANS.

SECTION VIEW A-A NTS

COIR MATS-CHANNEL INSTALLATION

CHECK SLOT AT 25' INITIAL CHANNEL ANCHOR TRENCH INTERMITTENT CHECK SLOT

TYPICAL PUMP AROUND OPERATION

SCALE: NOT TO SCALE

-WOODEN STAKES

TERMINAL SLOPE AND CHANNEL ANCHOR TRENCH

> NOTES: 1. CHECK SLOTS TO BE CONSTRUCTED AT 25' INTERVALS.
> 2. ALL MATTING TO BE SECURED WITH WOODEN STAKES

ACCORDING TO THE SPECIFICATIONS AT 5' INTERVALS. FABRIC OVERLAP WHEN 2 ROWS OF MATERIAL ARE USED SHALL BE PLACED WITH THE UPPER ROW OF MATERIAL PLACED OVER THE LOWER ROW OF MATERIAL.

TRENCH MATTING AT TOP AND BOTTOM OF MAT AS

PRELIMINARY NOT FOR CONSTRUCTION

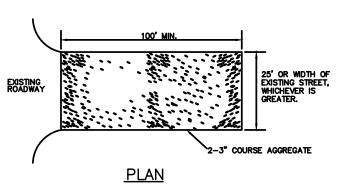
CLAY PLUG SCALE: NOT TO SCALE

REVISIONS

SHOWN IN DETAIL

OVERLAP FABRIC IN DIRECTION OF FLOW WITH MATTING
UPSTREAM ON TOP OF DOWNSTREAM MAT.

MATTING WILL BE INSTALLED ACCORDING TO THE
SPECIFICATIONS.



CROSS SECTION

NEW CONSTRUCTION

GEOTEXTILE FABRIC UNDER STONE

12" MIN.

- NOTES:

 1. GEOTEXTILE FABRIC TO BE ADDED UNDER THE STONE AS SHOWN.

 2. PLACE STONE OVER A STABLE FOUNDATION AT LOCATIONS SHOWN ON THE PLANS.

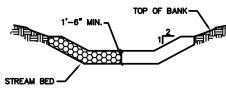
 3. INSTALL PIPE UNDER PAD IF NEEDED TO MAINTAIN PROPER PUBLIC ROAD DRAINAGE.

-STRUCTURAL STONE

CROSS SECTION

USE CLASS B STONE FOR STRUCTURAL STONE AND PAY FOR AT THE CONTRACT UNIT PRICE PER TON STONE FOR EROSION CONTROL, CLASS B. USE NO. 5 OR NO. 57 STONE FOR SEDIMENT CONTROL AND PAY FOR AT THE CONTRACT UNIT PRICE PER TON SEDIMENT CONTROL STONE. CONSTRUCT DAM A MAXIMUM OF 1 FOOT ABOVE NORMAL FLOW DEPTH.

TOP OF BANK ∠BASE OF STREAM → TOP VIEW TOP OF BANK



FRONT VIEW

Ward

CAROLINA

NORTH

COUNTY,

NOINO

EAST

601

DETAILS

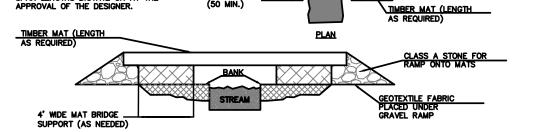
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Raleigh, NC 27616-2848 FAX (919) 87
Vironmental Banc & Exchange

CONSTRUCTION ENTRANCE

EXISTING ROADWAY

SCALE: NOT TO SCALE

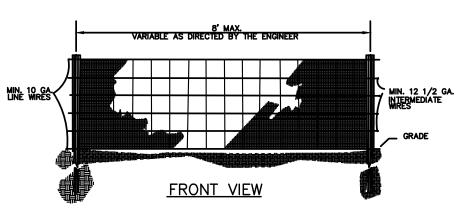
TIMBER MAT TO SUPPORT STREAM CLASS A STONE FOR BANKS (AS NEEDED) NOTES:
1. DEPLOY EROSION CONTROLS AS NEEDED. 2. PERFORM ROUTINE INSPECTION TO INCLUDE REMOVAL OF LOOSE SOIL TRACKED ONTO BRIDGE BY EQUIPMENT AND INSPECTION OF STREAMBANKS FOR STABILITY. 3. MATS SHALL BE POSITIONED TO RETAIN THE NATURAL STREAM CHARACTERISTICS. 4. MATS LAID PERENDICULAR TO THE STREAM CAN BE SUBSTITUTED WITH PRE-FABRICATED BRIDGE STRUCTURES AS SPAN LENGTHS DICTATE OR AT THE APPROVAL OF THE DESIGNER.



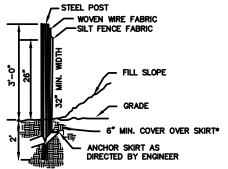
ROCK SILT SCREEN

NOTES:

SCALE: NOT TO SCALE



- USE SILT FENCE ONLY WHEN DRAINAGE AREA DOES NOT EXCEED 1/4 ACRE AND NEVER IN AREAS OF CONCENTRATED FLOW
- FOR REPAIR OF SILT FENCE FAILURES, USE NO. 57 WASHED STONE



SIDE VIEW

PRELIMINARY NOT FOR CONSTRUCTION

BRIDGE MAT DETAIL SCALE: NOT TO SCALE

STANDARD TEMPORARY SILT FENCE

SCALE: NOT TO SCALE

MITIGATION PLAN SET

D5

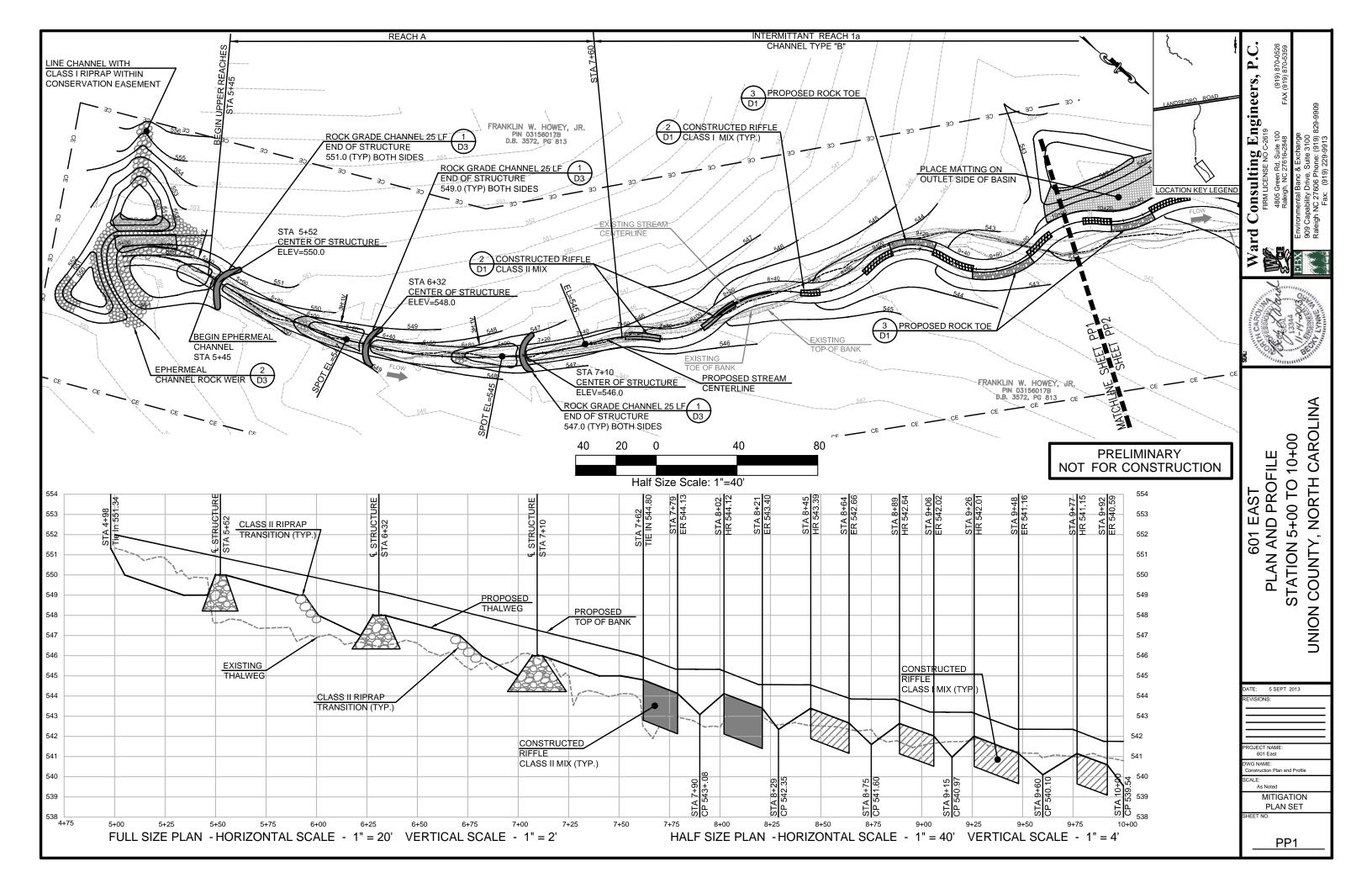
DATE: 5 SEPT 2013

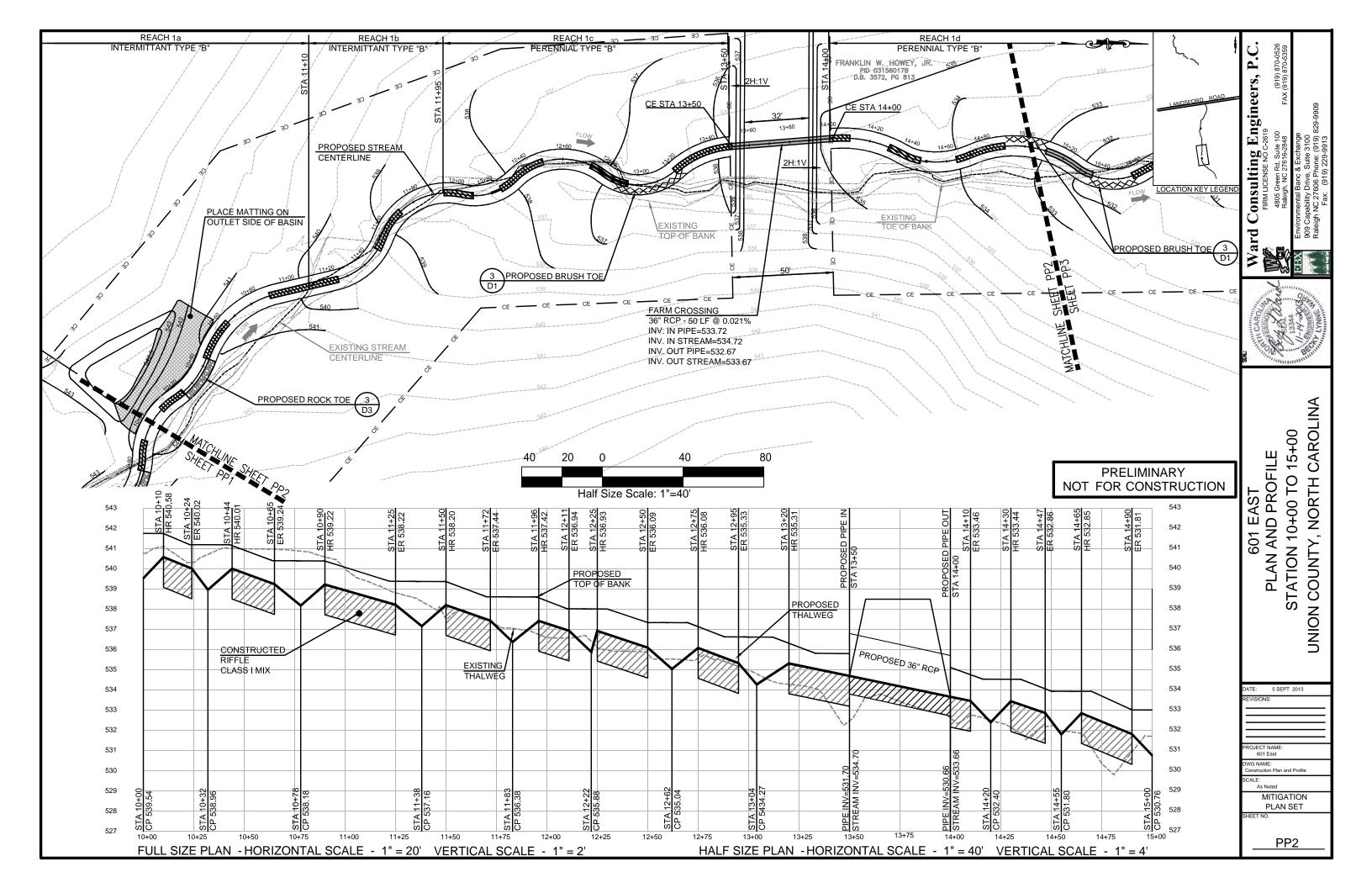
REVISIONS:

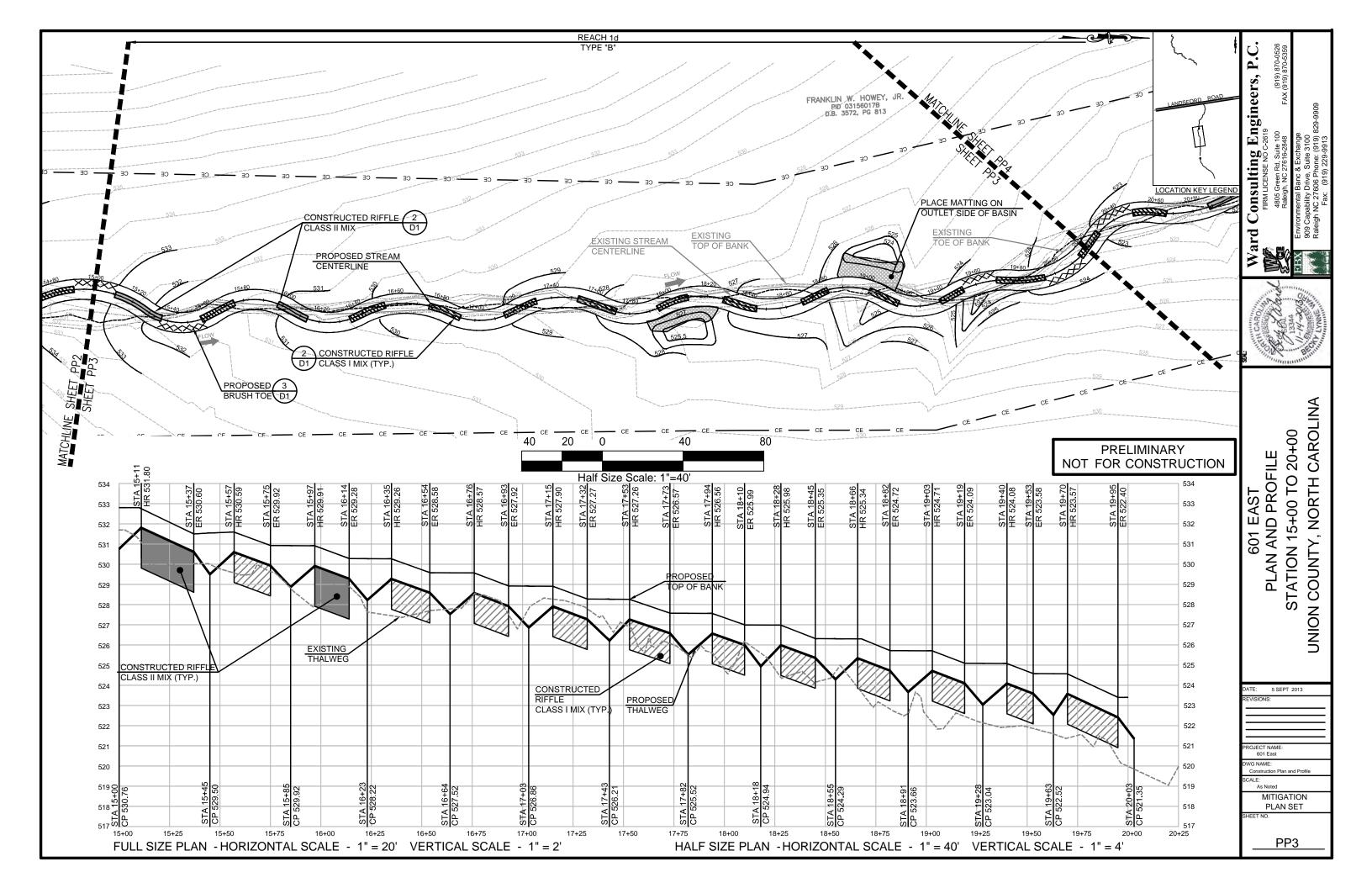
ROJECT NAME: 601 East

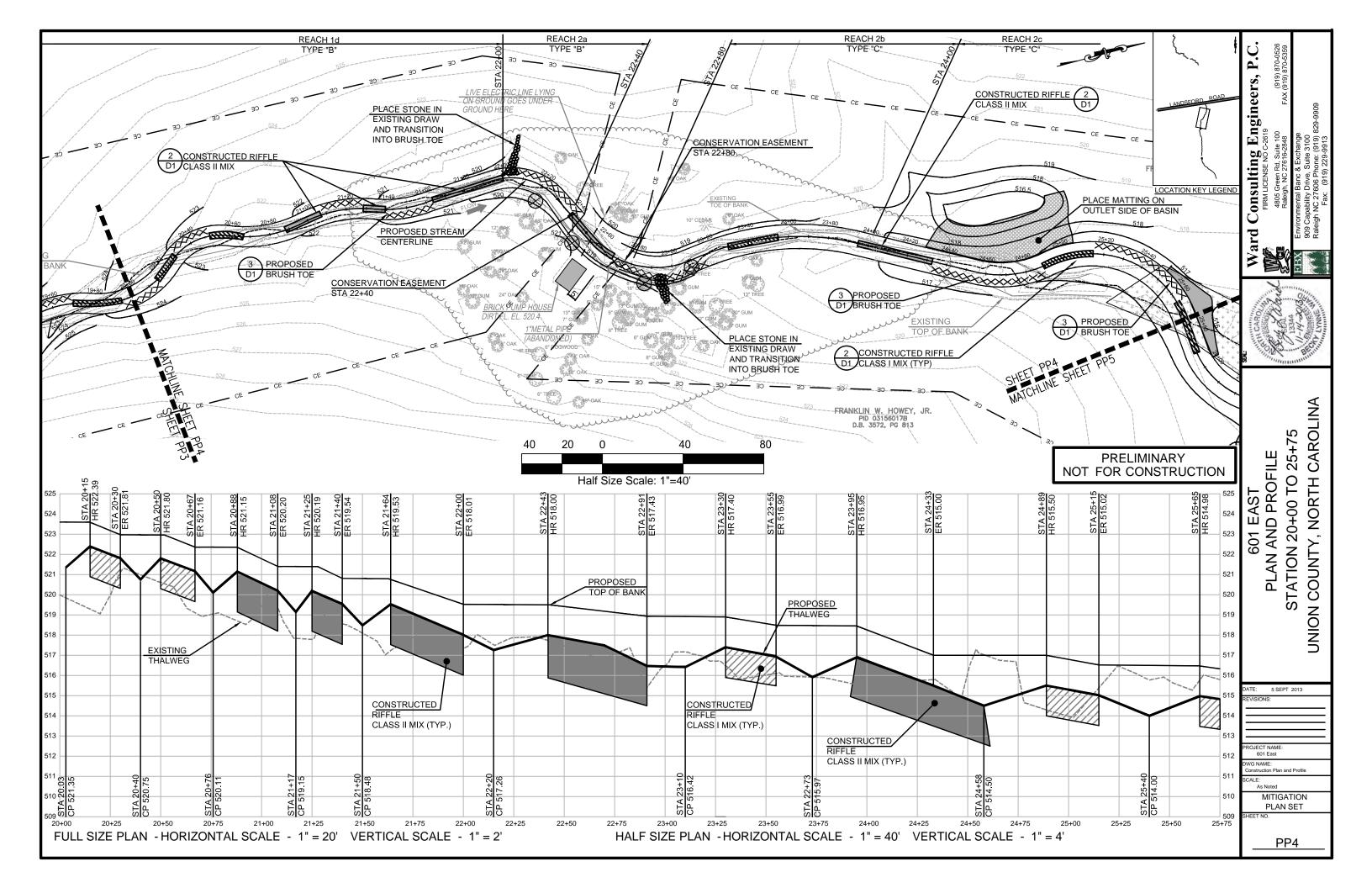
WG NAME: Planting Details

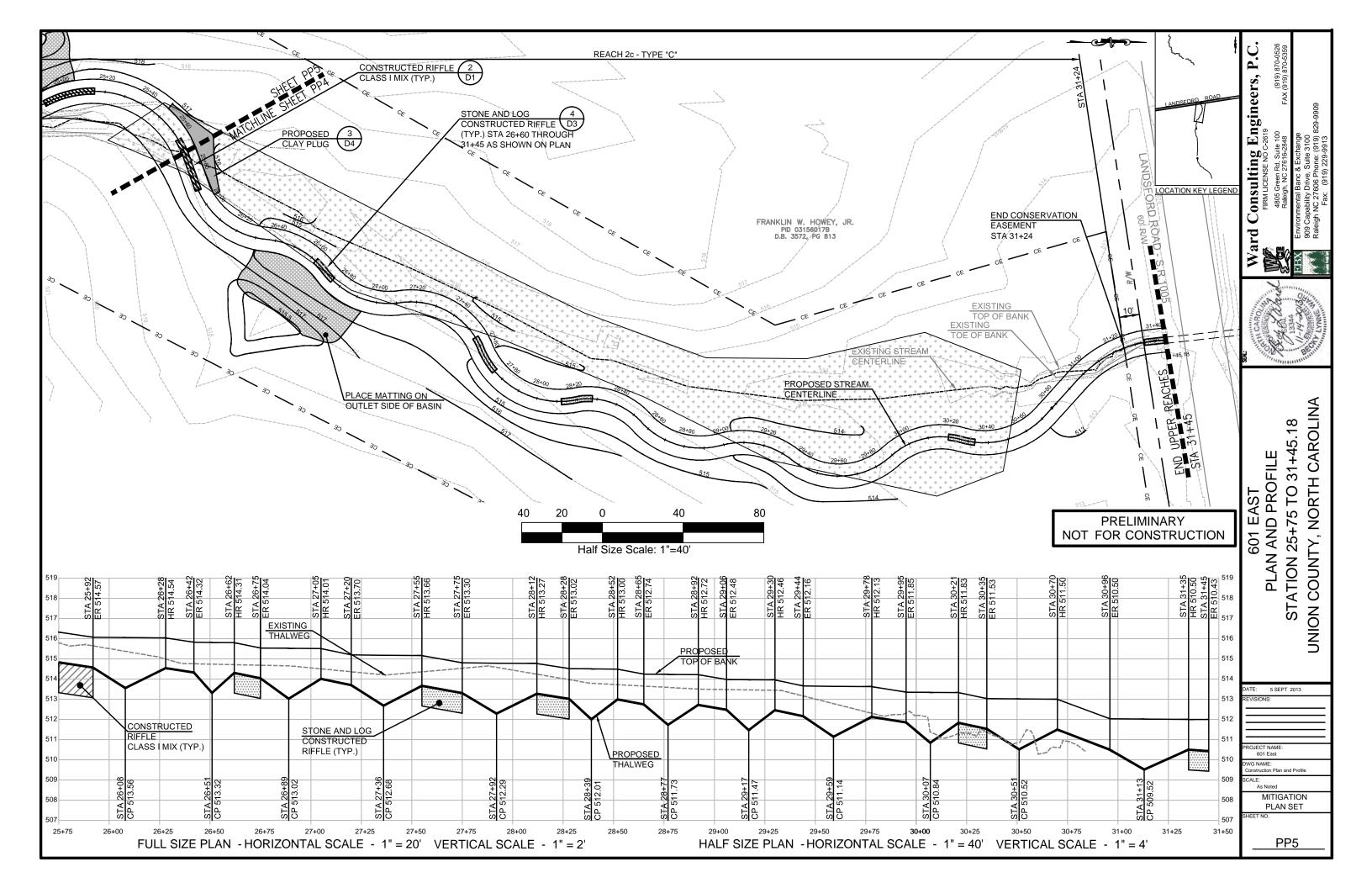
SCALE: NTS

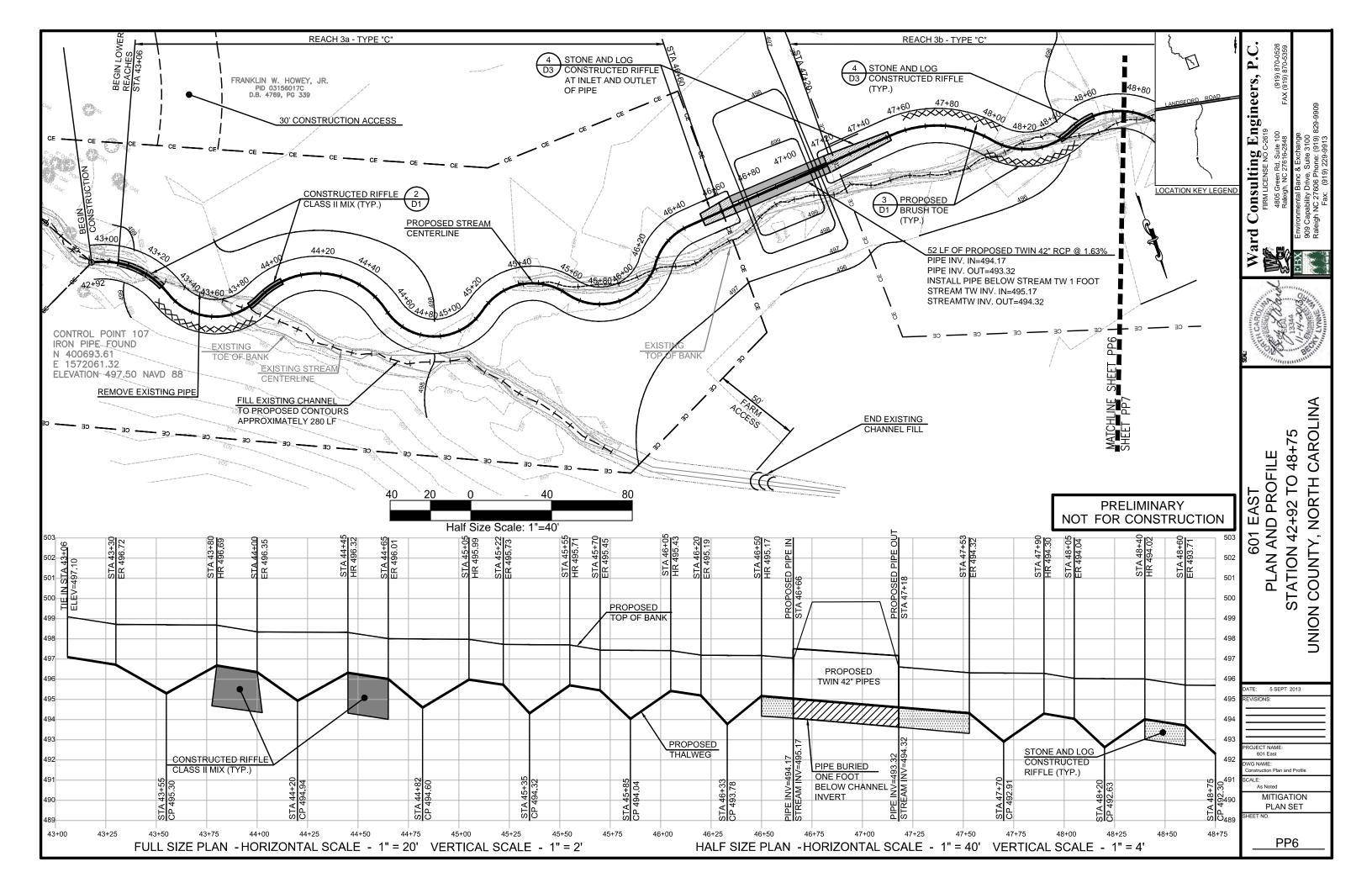


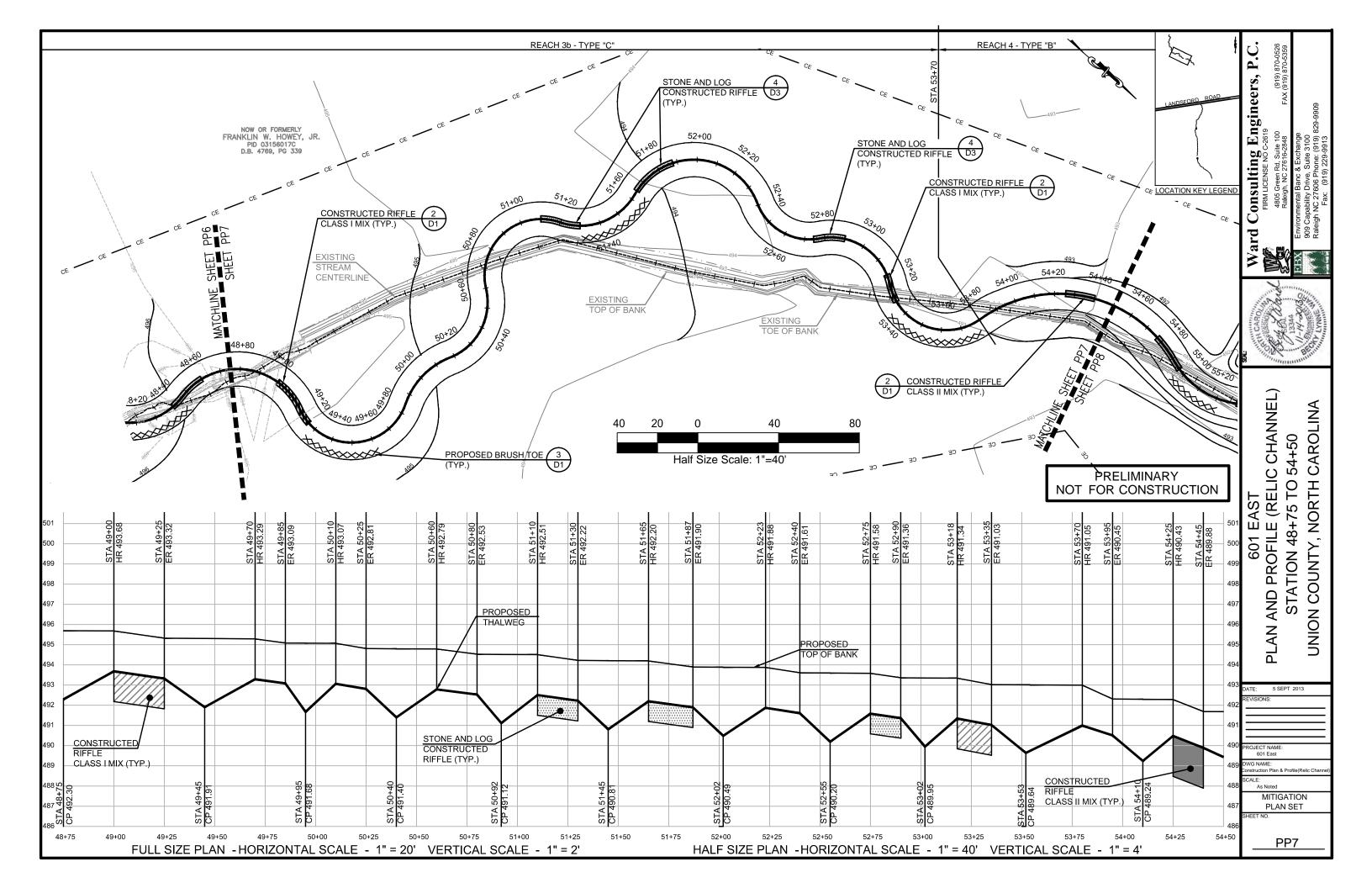


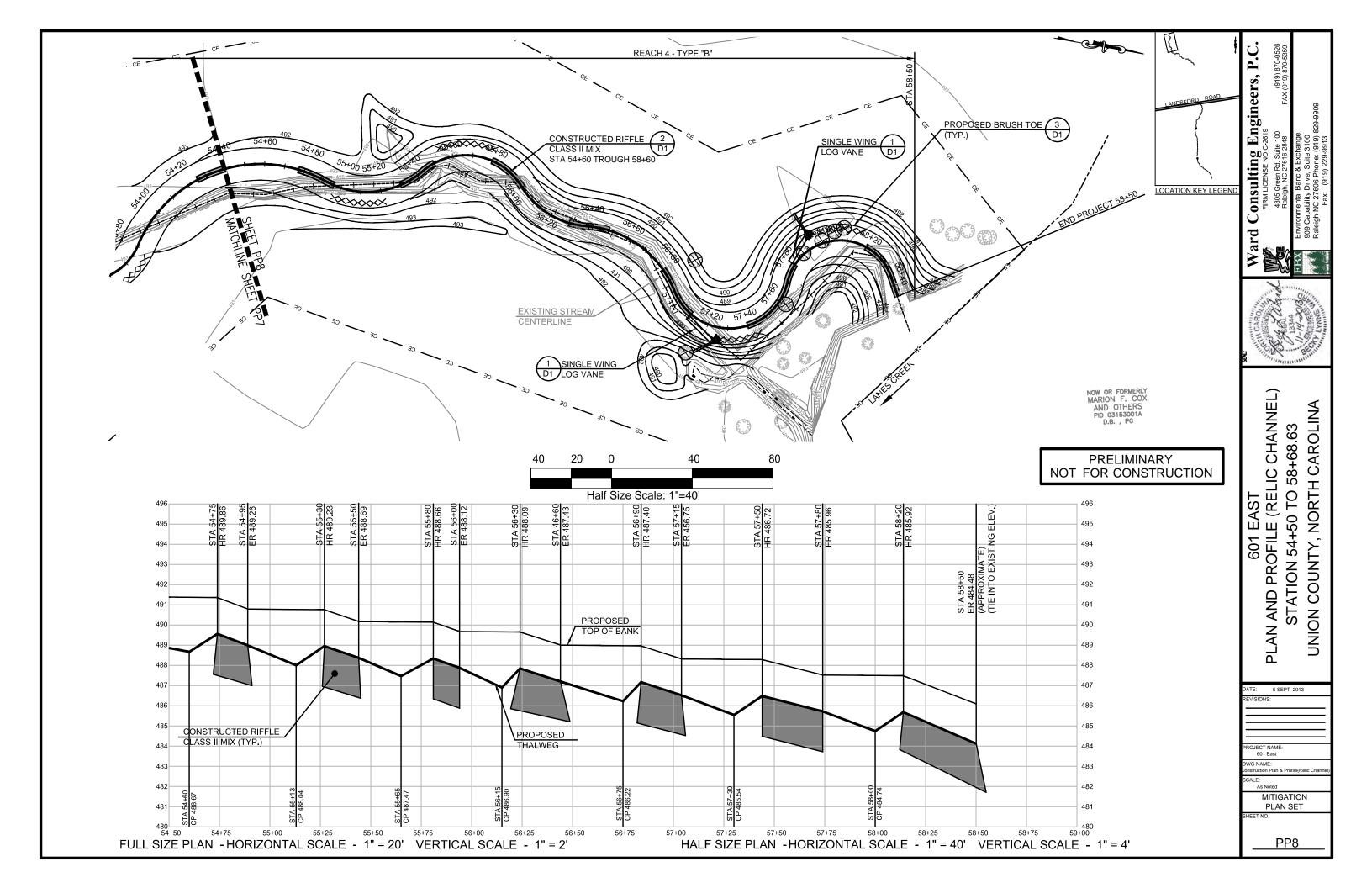




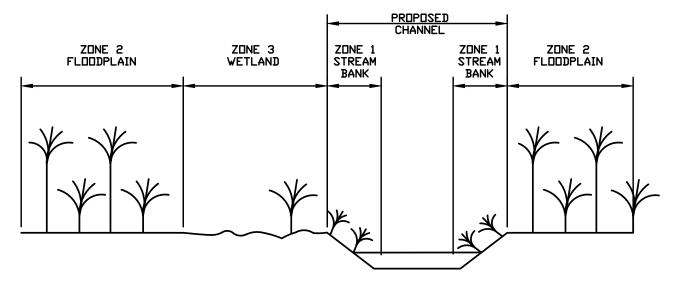








PLAN VIEW



PLANTING ZONE PROFILE SCHEMATIC NOT TO SCALE

Recommended application rate: 20	lbs. per acre	
Species	Common Name	Percent
Agrostis stolonifera	Creeping bentgrass	35
Carex vulpinoidea	Fox sedge	25
Elymus virginicus	Virginia wild rye	
Juncus effusus	Soft Rush	5
Rudbeckia hirta	Black-eyed susan	5
Verbena hastata	Blue vervain	5
	Total:	100
0.3	7 Total Acres	
2	lbs./a cre	
8	Total lbs.	

Recommended application ra	te: 20 lbs. per acre	
Scientific Name	Common Name	Percent
Elymus virginicus	Virginia wild rye	20
Panicum virgatum	Switchgrass	20
Agrostis stolonifera	Creeping bentgrass	15
Coreopsis lanceolata	Coreopsis	10
Panicum clandestinum	Deer tongue	10
Andropogon gerardii	Big bluestem	5
Juncus effusus	Soft rush	5
Polygonum pensylvanicum	Penn. Smartweed	5
Schizachyrium scoparium	Little bluestem	5
Sorghastrum nutans	Indian grass	5
		100
10.37	Total Acres	
20	lbs./acre	
208	Total Ibs.	

- GENERAL NOTES:

 1. TEMPORARY PLANTING WILL OCCUR IMMEDIATELY AFTER CONSTRUCTION TO STABILIZE AREAS OF BARE SOIL. PERMANENT PLANTING AND SEEDINGS SHALL BEGIN IN SEASON OPTIMALY BETWEEN NOVEMBER 15 AND APRIL 15.

 2. PRIOR TO PERMANENT PLANTINGS AND SEEDINGS, THE SITE SOILS SHALL BE PREPARED FOR PLANTING. WHERE NEEDED THE SOILS SHOULD BE PLOWED OR RIPPED TO IMPROVE COMPACTED SOILS AND ELIMINATE CHANNELIZED FLOW FROM NON-TARGET AREAS. IF NECESSARY SOILS SHALL BE AMENDED WATLINGTONED TO THE TORSOIL TO FACILITATE VIGOROLIS PLANT GROWTH WITH STORED SITE TOPSOIL TO FACILITATE VIGOROUS PLANT GROWTH.
 - EXOTIC AND INVASIVE PLANTS SHALL BE TREATED AND REMOVED. SUMMARY OF PLANT QUANTITIES CHART SIZE REFERS TO THE SIZE OF THE PLANTS AT INSTALLATION.
 - THE SPACING OF THE PLANTS SHALL BE 3' ON CENTER FOR SMALL PLANTS, WETLAND FORBES, AND ON STREAM BANK ZONES FOR TREES AND SHRUBS. SPACING SHALL BE 10 FEET ALONG ROWS WITH 10 FOOT ROW SPACING. FOR TREES AND SHRUBS PLANTING DENSITY IS TO BE 640 PLANTS /ACRE.
 - PLANTS WILL BE KEPT SHADED AND WELL WATERED TO MAINTAIN HEALTHY,

 - VIGOROUS CONDITION PRIOR TO PLANTING.
 PRERMANENT SEED MIX REQUIRES ADVANCE PRE-ORDER AND SHIPMENT.
 ALL PLANT MATERIAL SHALL CONFORM TO OR EXCEED THE AMERICAN
 STANDARD FOR NURSERY STOCK (LATEST EDITION) AS PUBLISHED BY THE
 - AMERICAN ASSOCIATION OF NURSERYMEN.
 THE SITE SHALL BE PLANTED BY THE ZONES DEPICTED IN THE PLANTING PLAN
 SHEETS WITH SPECIES LISTED IN THE PLANTING TABLES.
 - PLANTING ZONE DESCRIPTIONS:

ZONE 1 - STREAM BANK
THE STREAM BANK ZONE INCLUDED THE STREAM CHANNEL
FROM BASE FLOW TO THE BANKFULL ELEVATION.

ZONE 283 - STREAM BUFFER
THE STREAM BUFFER INCLUDES THE AREA FROM THE
BANKFULL ELEVATION TO THE CONSERVATION EASEMENT
LIMIT.

ZONE 4 - WETLAND

THE WETLAND ZONES INCLUDE POCKETS OF ENHANCED EXISTING WETLAND AREAS WITHIN ZONE 2.
ZONE 5- TEMPORARY ACCESS AREA TO BE STABILIZED WITH

TEMPORARY SEED ONLY WITHIN CROP PRODUCTION AREAS.

Plant Table				
Bare Roots	Zon e 1 (Stre amb ank)	Zone 2 (Stream Buffer)	Zone 3 (Strem Buffer)	Zon e 4 (Wetlands)
Black gum (Nyssa sylvatica)		350		
Red Oak (Quercus rubra)		350		
White oak (Quercus alba)		350		
Tuli p poplar (Lirio dendron tuli pifera)		500	400	
River birch (Betula nigra)		300	400	
American persimmon (Diospyros virginiana)		100	100	
TagAl der (Alnus serrulata)		100	100	50
Willow oak (Quercus phellos)		500	250	
Chestnut oak (Quercus mi dhauxii)		500	250	
Ironwood (Carpinus caroliniana)		350	250	
Green Ash (Fraxinus pennsylvanica)			250	
Black Willow (Salix nigra)			250	
Sy camore (Platanus occidentalis)			250	50
Hackberry (Celtis Laevigata)			250	
Buttonbush (Cephalanthus occidentalis)				100
Elderberry (Sambucus canadensis)				100
Bare Root Total =	0	3400	2750	300
Live Stakes				
Black Willow (Salix ni gra)	1000			
Cottonwood	900			
Silky dogwood (Cornus amomum)	1000			
Silky willow (Salix sericea)	600			
Live Stake Total =	3500	0	0	.0



CARDLINA NOTE NORTH 601 EAST ANTING NE COUNTY, UNION

REVISIONS RDJECT NAME: 601 East WG NAME: Planting Notes NTS MITIGATION PLAN SET

DATE: AUG 9 2013

VP1

GENERAL

The vegetation plan for the Newtown Project was developed using a 3 Zone Installation: planting scheme. The planting zones are as follows:

Zone 1- Streambank (1.87 Acres)

Zone 2- Stream Buffer (11.99 Acres Piedmont Aluvial Forest)

Zone 3- Wetland Restoration (3.38 Acres Piedmont Alluvial Forest)

The planting plan zones are shown on the construction plans planting plan sheets. Substitutions of specified plant materials may be made with the approval of the owner and the Designer and shall be compatible with the specified planting scheme. The various species of bare root plants and live broadcast or dropped when wind velocity exceeds 5 mph. Seed is to be stakes specified on the plans is to be at spacing called for on the plans in the appropriate zone.

The planting stock should be grown by restoration nurseries within the same physiographic region (Piedmont) and within 200 miles of the project areas on stream banks shall be protected with coir fiber matting as shown site. The seed sources for the plant material should be obtained from the on the plans. Other seeded areas are to be protected by spreading straw Piedmont, and genetically improved seedlings should be used when available. Plant stock or seed mixes may be obtained from nurseries beyond the 200-mile limit with approval of the Designer. Only the highest other suitable equipment. Alternative seeding methods must be prequality plant material should be planted. The seedlings should have welldeveloped fibrous root systems and healthy buds. Seedling should be packaged and stored prior to planting to protect against damage or extreme temperatures.

if the ground is not frozen, to early spring before growth begins. No planting shall be done when the temperature is below 32 degree F, the soil is frozen, when the sides or bottom of the plant hole are frozen, or when the soil to be used for backfilling is frozen or too wet.

The contractor installing the vegetation on the project site shall have the following qualification/certifications: Certified Landscape Technician, or Certified Plant Professional, or Registered Forester, or Registered Landscape Contractor, or Certified Nurserymen, or otherwise approved by the owner.

Survival of Plantings

The Contractor shall be responsible for maintaining a survival rate of 80% Date of Project Acceptance by the owner. The Date of Project Acceptance is length of 2 to 3 feet, appropriate for driving into the ground. See the Office. The 80% survival rate shall apply additionally to each species planted. The contractor shall incur the cost of replacing any permanent plantings that do not survive through the one-year warranty period. One year after project acceptance, an on-site inspection will be conducted and the Contractor will be directed accordingly on replacement of any mortality.

PERMANENT SEEDING

General:

Permanent seeding will be required in all planting zones specified on the plans and prior to demobilization from the site on all remaining disturbed areas. Contractor shall install temporary cover suitable for that season in conjunction with the permanent seed in all areas as shown on the planting In digging, loading, transporting, unloading, planting or otherwise handling plan to receive permanent seeding as construction and stabilization progresses. Temporary seed mixture and schedule is shown on the Erosion precautions to prevent injury to or drying out of the plant. The live stakes Control Key & Site Access plan sheet EROS 1. Areas fertilized for temporary shall be installed the same day they are prepared. The installation should seeding shall be sufficiently fertilized for permanent seeding; additional fertilizer is not required for permanent seeding. Seed mixes at the rates shown in the tables on Planting Plan VP1 shall be used for seeding. Ideally, tamped into the ground at right angles to the slope and angled species. Soil amendments are shown on VP1.

Materials:

The tables on VP1 list herbaceous, permanent seed mixtures. The contractor shall provide detailed information including but not limited to germination rates, noxious weed seeds and date and location of harvest on seed mix. The designer must approve the seed mix prior to application.

The Contractor is to limit sub-grade and finish grade preparation to areas that will be planted immediately. Preparation areas are to be moistened prior to seeding when soil is dry but care shall be taken not to create muddy conditions. The seedbed shall be non-compacted loose soil. Prepared areas are to be restored if eroded or disturbed after fine grading and before planting. Soil amendments should follow the fertilizer and liming description in the amendment table included on the planting plan.

Seed is to be sown with a spreader of a seeding machine. Seed is not to be 5th Edition, July 2003. evenly distributed by sowing in two directions at right angles to each other. Materials: Wet seed or seed that is moldy or otherwise damaged in transit or storage. Bare root plants are to be planted in the appropriate zone as indicated on is not to be used. After being sown, the seed is to be raked into the top 1/8 the planting plans. The Summary of Plant Quantity table on the planting inch of the topsoil, lightly rolled, and watered with fine spray. Seeded mulch uniformly to form a continuous blanket over the seeded areas (75% coverage = 2 tons/acre). Straw mulch is to be spread by hand, blower or approved by the Designer prior to installation.

LIVE STAKES

General:

Installation should occur during the dormant season, i.e., late fall or winter, Stages required by the Contractor to complete for successful implementation of the planting plan include soil bed preparation, initial planting, plant establishment, and replacement planting. The Contractor shall perform the operations provided for in these specifications in a careful, workmanlike manner that will promote the continued life and healthy growth of all plants in their location. Live stakes shall be handled in means of wet canvas, burlap or straw or by other means acceptable to the accordance with the Pocket guide to Seedling Care and Planting Standards, Designer and appropriate to weather conditions and the length of time the 5th Edition, July 2003 or most recent edition or similar guide with designer roots will remain out of the ground.

Materials

Live stakes are to be planted in the appropriate zone as indicated on the planting plans. The Plant Quantity Summary Table on the planting plan lists the species, minimum stem caliper, plant height/length, and spacing on all permanent plantings for the duration of twelve months following the guidelines. A minimum stake caliper is 0.5 inches to 2 inch diameter with a defined by the Project Acceptance Letter issued by the State Construction standards described in The Pocket Guide to Seedling Care and Planting, July

> Live stakes are to be dormant (cut fall or winter) and gathered locally or purchased form a commercial supplier. Stakes must be freshly cut with side branches removed, but with bark intact (ensure that the bark is not stripped during the cutting, preparation or installation of the stake). Cuttings are to be collected using a saw or sharpened clippers (not an axe).

One end of the live stake must be cut at an angle for insertion into the soil and the other end must be cut square for tamping. Cutting must be kept fresh and moist prior to installation.

plants, the Contractor shall exercise utmost care and use adequate start nearest to the stream and work up the bank/floodplain. Cutting must e installed right side up with the buds pointing upward. Cuttings should be permanent seeding shall occur during the growing season for all listed seed downstream. They are to be tamped into the ground for approximately 4/5 of their length. Cuttings that split or become "mushroomed" must be replaced. Stakes should be installed in a random configuration to prevent gullies and promote a natural effect in the re-vegetated area.

BARE ROOT PLANTS

General:

The work of planting includes planting bed preparation, initial planting. plant establishment, and replacement planting. The Contractor shall perform the operations provided for in these specifications in a careful, workmanlike manner that will promote the continued life and healthy growth of all plants in their location. Seedlings shall be handled in accordance with the Pocket guide to Seedling Care and Planting Standards,

plan lists the species, plant size, spacing guidelines and placement of bare root vegetation. An assortment of bare root plants are required as indicated in this table on the plans

In digging, loading, transporting, unloading, planting or otherwise handling plants, the contractor shall exercise utmost care and use adequate precautions to prevent injury to or drying out of the trunk, branches, or roots: and to prevent freezing of the plant roots. Immediately following delivery to the project, all plants with bare roots, if not promptly planted, shall be heeled-in in constantly moist soil or sawdust in an acceptable manner corresponding to generally accepted horticultural practices.

While plant with bare roots are being transported to and from heeling-in beds, or are being distributed in planting beds, or are awaiting planting after distribution, the Contractor shall protect the plants from drying out by

Installation of bare root vegetation shall be located in designated areas along the stream bank above and below bankfull elevation as described in the plans or a directed by the Designer and in the wetland areas. Soil in the

permit roots to spread out and down without J-rooting. After planting, the soil shall be tamped around the shrub or tree firmly to eliminate air pockets. Straw mulch shall be placed around the base of each plant at least 4-6 inches thick. Straw bails may be torn into segments and placed around the base of each plant.

SHRUB AND TREE TRANSPLANTS

Existing site vegetation may be used to augment plantings. Transplants may only be taken from disturbed areas.

Materials:

Vegetation to be transplanted will be identified by the Contractor and approved by the Designer. Shrub and trees less than 3 inches in diameter shall be salvaged onsite in areas designated for construction access and disturbed areas.

Transplanted vegetation shall be carefully excavated with root balls with intact and surrounding soils. Care shall be taken to prevent damage to limbs or bark. Vegetation shall be transplanted immediately, if possible. Otherwise the vegetation shall be transported to designated stockpile areas and heeled into moist soil or sawdust in an acceptable manner appropriate to weather or seasonal conditions.

Installation of the transplant shall be located in areas approved by the designer. Compacted soils in the transplant area shall be loosened to a depth of at least 1 foot. Transplants shall be replanted to the same depth as they were originally growing. The planting trench or hole shall be deep and wide enough to permit the roots to spread out and down. The plant stem shall remain upright. Soil shall be replaced around the transplanted vegetation and tamped around the shrub or tree firmly to eliminate air pockets, and watered in.

Transplant spacing should be at least 10 ft. x 10 ft. for canopy and 5 ft. x 5 ft. for understory plants.

TOPSOIL

Topsoil will be preserved and spread where necessary to provide a suitable growth medium for vegetation growth. Topsoil will be used throughout the site to reduce the amount of fertilizers and soil amendments needed for vegetation growth.

Spreading:

Uniformly distribute topsoil to a minimum compacted depth of 2 inches on 3:1 slopes and 4 inches on flatter slopes. Do not spread topsoil while it is frozen or muddy, or when the sub-grade is wet or frozen. Compact the topsoil enough to ensure good contact with the underlying soil, but avoid excessive compaction. The volume of topsoil required for application to various depths is included in the chart below.

Volume of Topsoil Required For Application to Various Depths					
Depth (inches)	Cubic Yards Per 1000 Sq. Feet	Cubic Yards Per Acre			
1	3.1	134			
2	6.2	269			
3	9.3	403			
4	12.4	538			
5	15.4	672			
6	18.5	806			

P.C Engineers,

Consulting |



CARDLINA NOTES NORTH 601 EAST ANTING NE COUNTY, NOINO

DATE: AUG 9 2013 SEVISIONS: RDJECT NAME: 601 Eqst WG NAME: Planting Notes MITIGATION PLAN SET

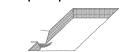
VP2

PLANTING DETAILS

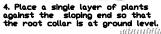
SEEDLING / LINER BAREROOT PLANTING DETAIL

HEALING IN

 Locate a healing—in site in a shady, well protected area. 2. Excavate a flat bottom trench 12' deep and provide



3. Backfill the trench with 2' well rotted sawdust. Place a 2' layer of well rotted sawdust at a sloping angle at one end of the trench.

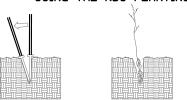




5. Place a 2' layer of well rotted sawdust over the roots maintaining a sloping angle.

6. Repeat layers of plants and sawdust as necessary and water thoroughly.

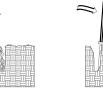
DIBBLE PLANTING METHOD USING THE KBC PLANTING BAR



1. Insert planting bar as shown and pull handle and place seedling at 2. Insert planting bar 2. toward planter toward planter. correct depth.



from seedling.



4. Pull handle of bar 5. Push handle toward planter, firming forward firming soil at bottom.



6. Leave compaction hole open. Water thoroughly.

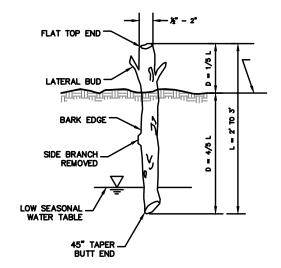
PLANTING NOTES:

PLANTING BAG During planting, seedlings shall be kept in a moist



KBC PLANTING BAR Planting bar shall have a blade with a triangular cross section, and shall be 12' long, 4' wide and 1' thick at center.

RUIT PRUNING All seedlings shall be root pruned, if necessary, so that no roots extend more than 10 inches (10°) below the root collar.



GROUND SURFACE

يم

LAUG Engineers, I LOST NO C-2619
5. Green Rd, Suite 100
7. NC 27616-2848
FAUTH Drive. Exchallity Drive. C

Consulting FIRM LICENSE NO

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CAROLINA

DETAIL

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PLANTIN

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601

NORTH

COUNTY,

NOINO

REFORESTATION DETAIL

SCALE: NOT TO SCALE

WOVEN COIR FIBER MAT ESTABLISHED PLANT SHOWN FOR INFORMATION ONLY PLANTING TO TOP 30" LIVE CUTTING (DORMANT) OF RIP RAP (TYP) EXISTING GROUND NOTE: INSTALL LONG STRAW

LIVE STAKE DETAIL

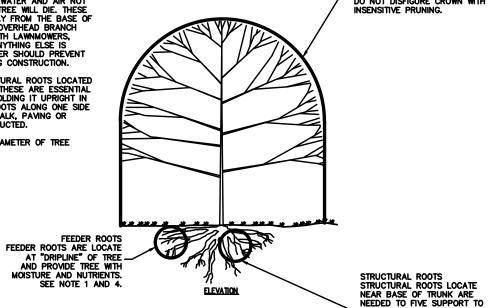
SCALE: NOT TO SCALE

IREE PROTECTION DURING CONSTRUCTION

1. DO NOT COMPACT SOIL BENEATH TREES. NO VEHICLE
SHALL BE ALLOWED TO PARK UNDER TREES. NO HEAVY MATERIALS SHALL BE STORED BENEATH TREES.
RESULTS OF COMPACTION CAUSE WATER AND AIR NOT RESULTS OF COMPACTION CAUSE WATER AND AIR NOT TO REACH THE ROOTS AND THE TREE WILL DIE. THESE FEEDING ROOTS OCCUR WELL AWAY FROM THE BASE OF THE TREE TO THE EDGE OF THE OVERHEAD BRANCH CANOPY. DAMAGING THE BARK WITH LAWNMOWERS, CONSTRUCTION EQUIPMENT, OR ANYTHING ELSE IS PROHIBITED. A PROTECTIVE BARRIER SHOULD PREVENT DAMAGE FROM OCCURRING DURING CONSTRUCTION.

2. NO CUTTING OF LARGE STRUCTURAL ROOTS LOCATED NEAR THE BASE OF THE TRUNK. THESE ARE ESSENTIAL IN SUPPORTING THE TREE AND HOLDING IT UPRIGHT IN HIGH WINDS. REMOVAL OF THE ROOTS ALONG ONE SIDE IS OFTEN DONE BECAUSE OF A WALK, PAVING OR BUILDING WHICH IS BEING CONSTRUCTED.

3. AVOID CUT AND FILL WITHIN DIAMETER OF TREE CROWN DURING EXCAVATION.



CROWN OF TREE IS NEEDED FOR LEAF GROWTH TO PRODUCE OXYGEN, FILTER THE AIR, REDUCE WIND, SOFTEN NOISE, AND PROVIDE BEAUTIFUL APPEARANCE. DO NOT DISFIGURE CROWN WITH INSENSITIVE PRUNING.

DATE: 9 AUG 2013

REVISIONS

ROJECT NAME: 601 East

WG NAME: Planting Details CALE: NTS

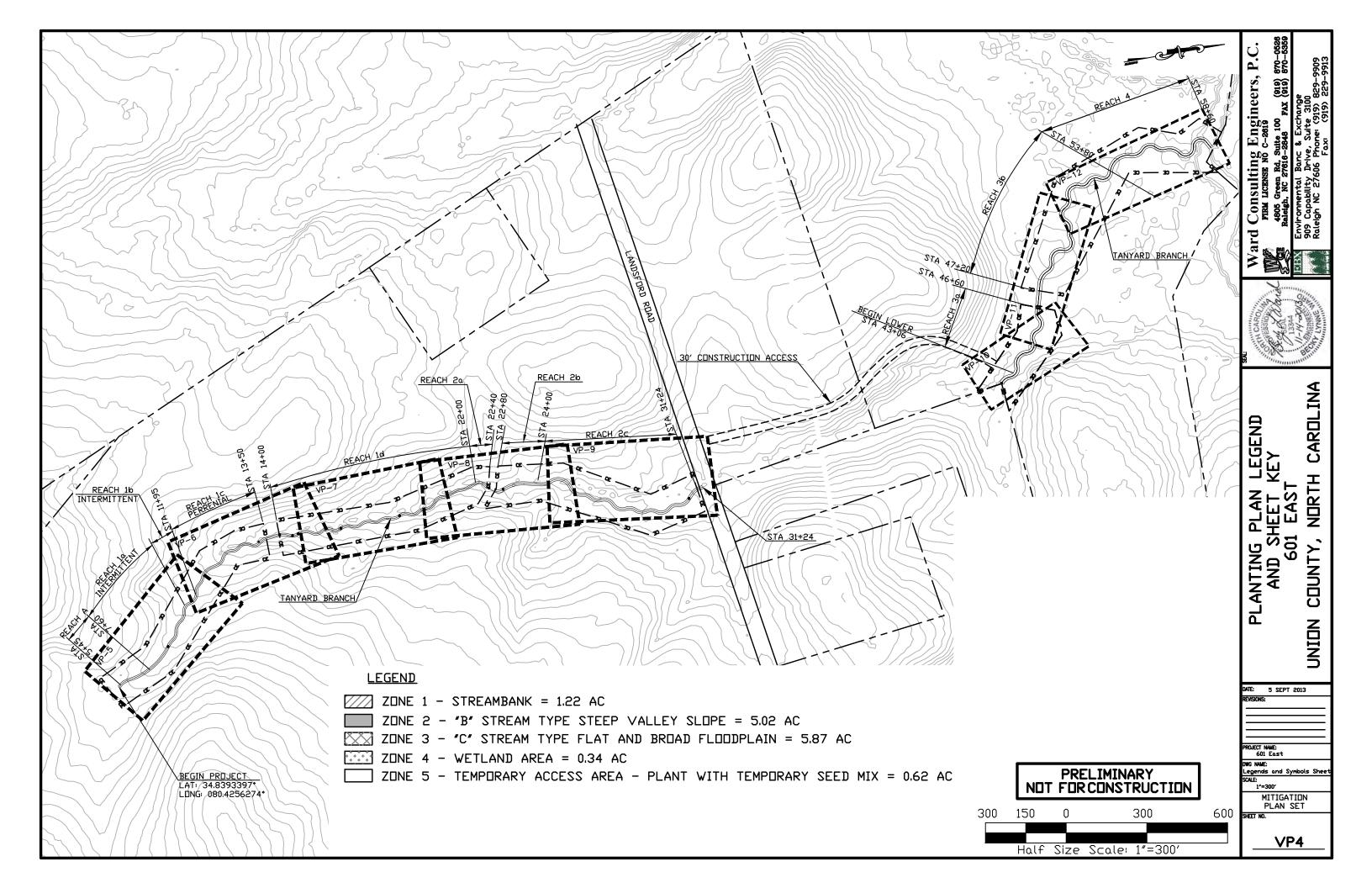
MITIGATION PLAN SET

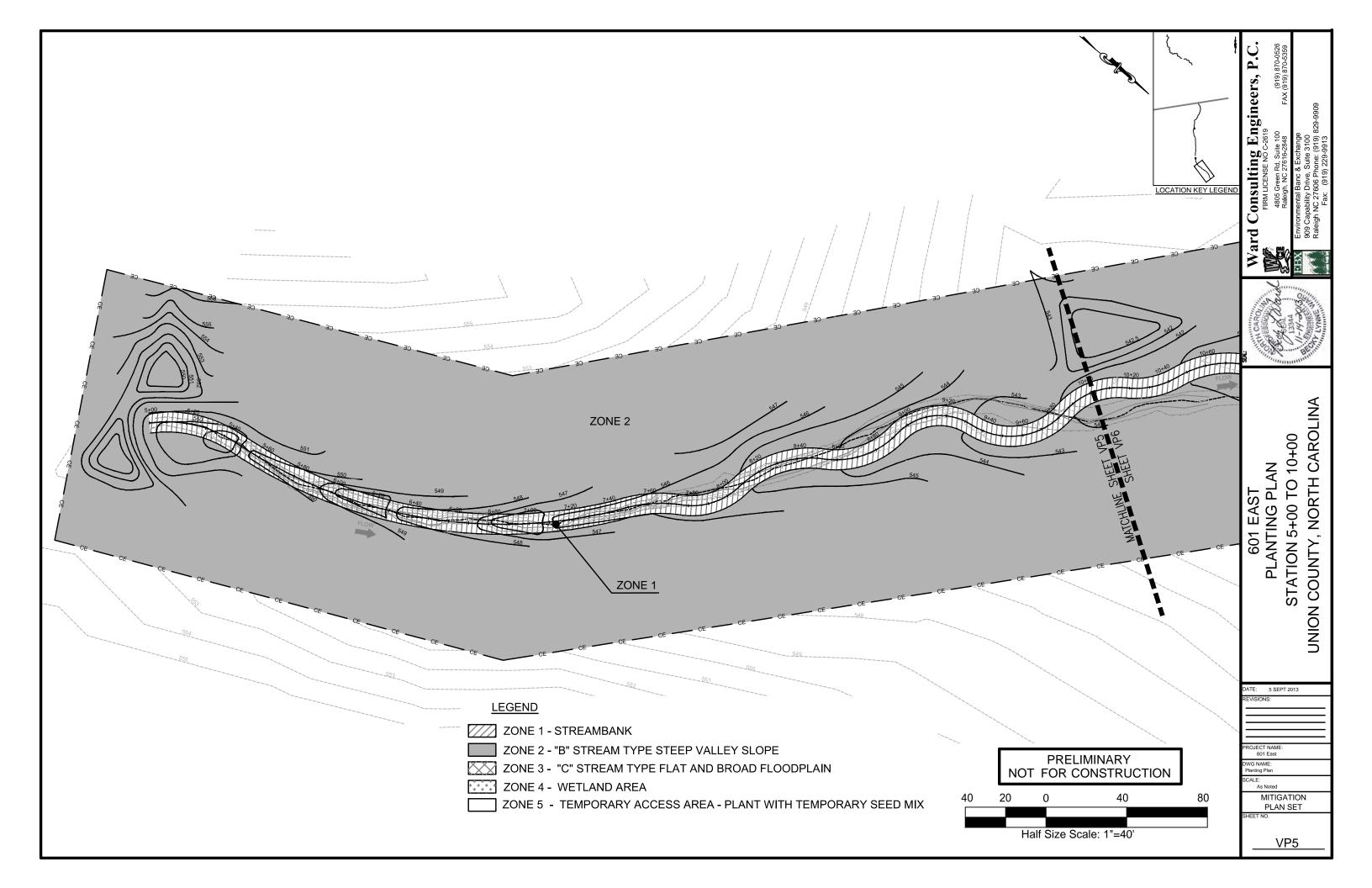
SEE NOTE 2 AND NOTE 4.

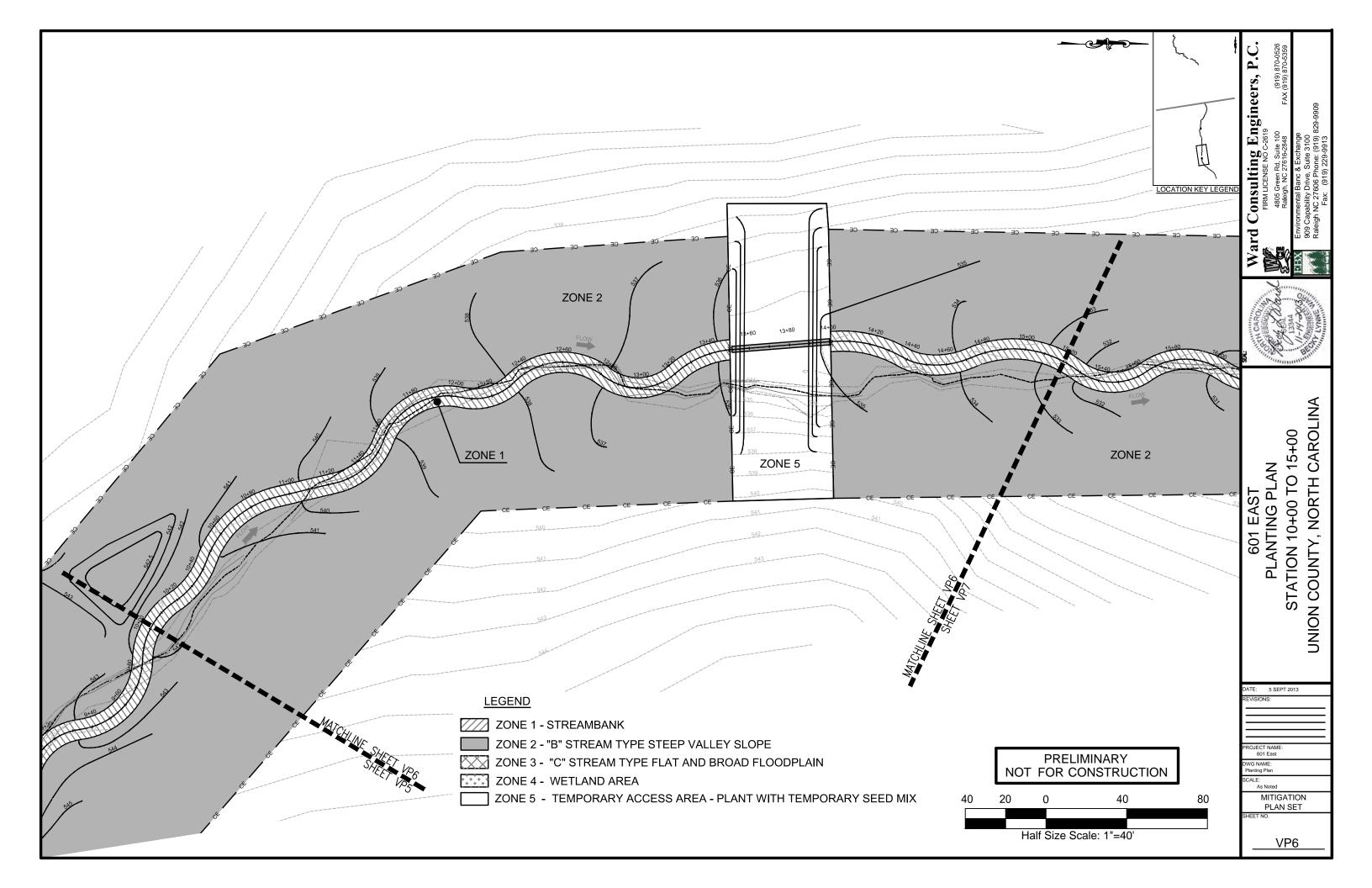
ENTIRE TREE. IF REMOVED, TREE CAN FALL AND DAMAGE

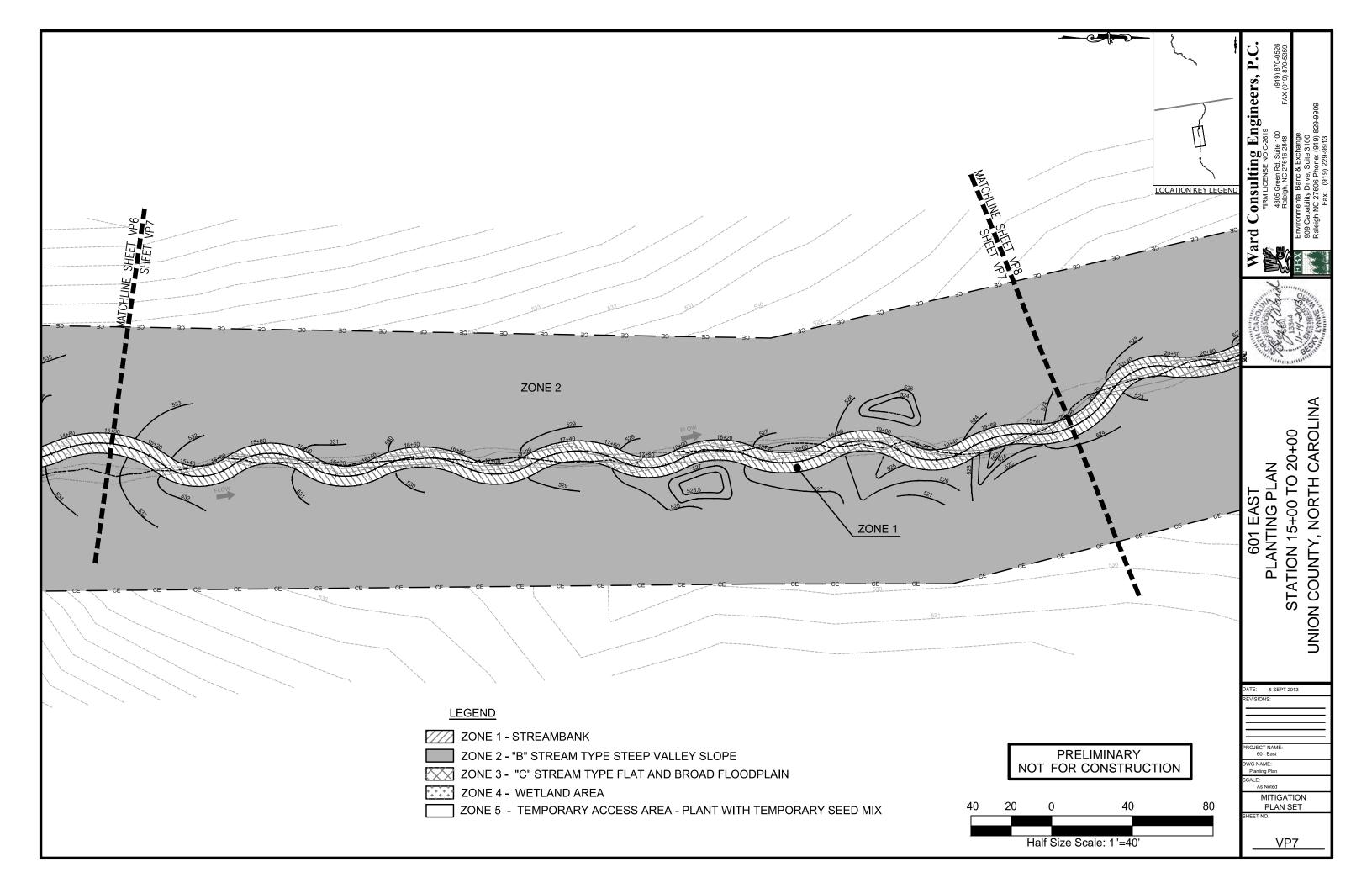
VP3

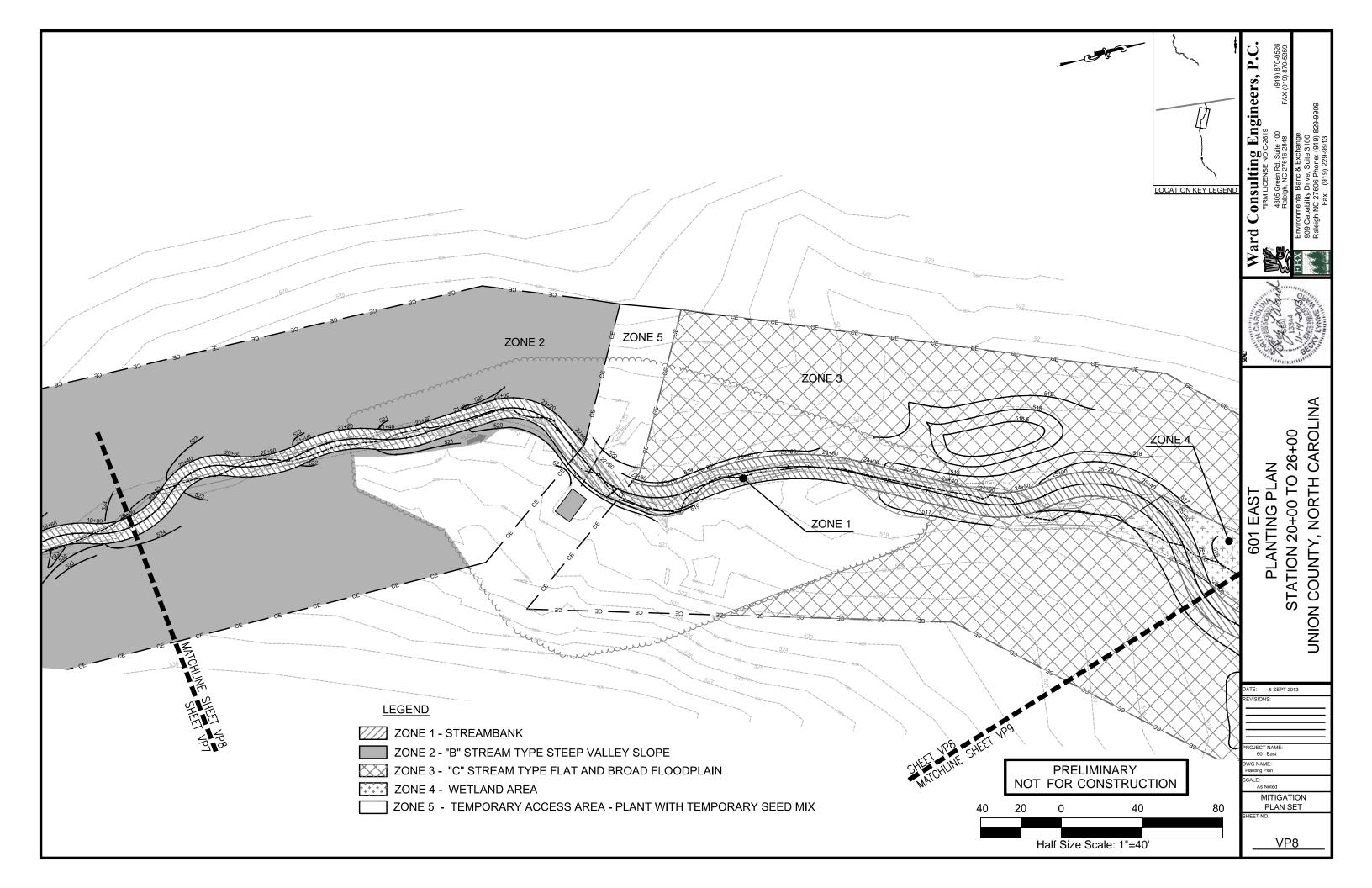
METHOD OF TREE PROTECTION DURING CONSTRUCTION SCALE: NOT TO SCALE

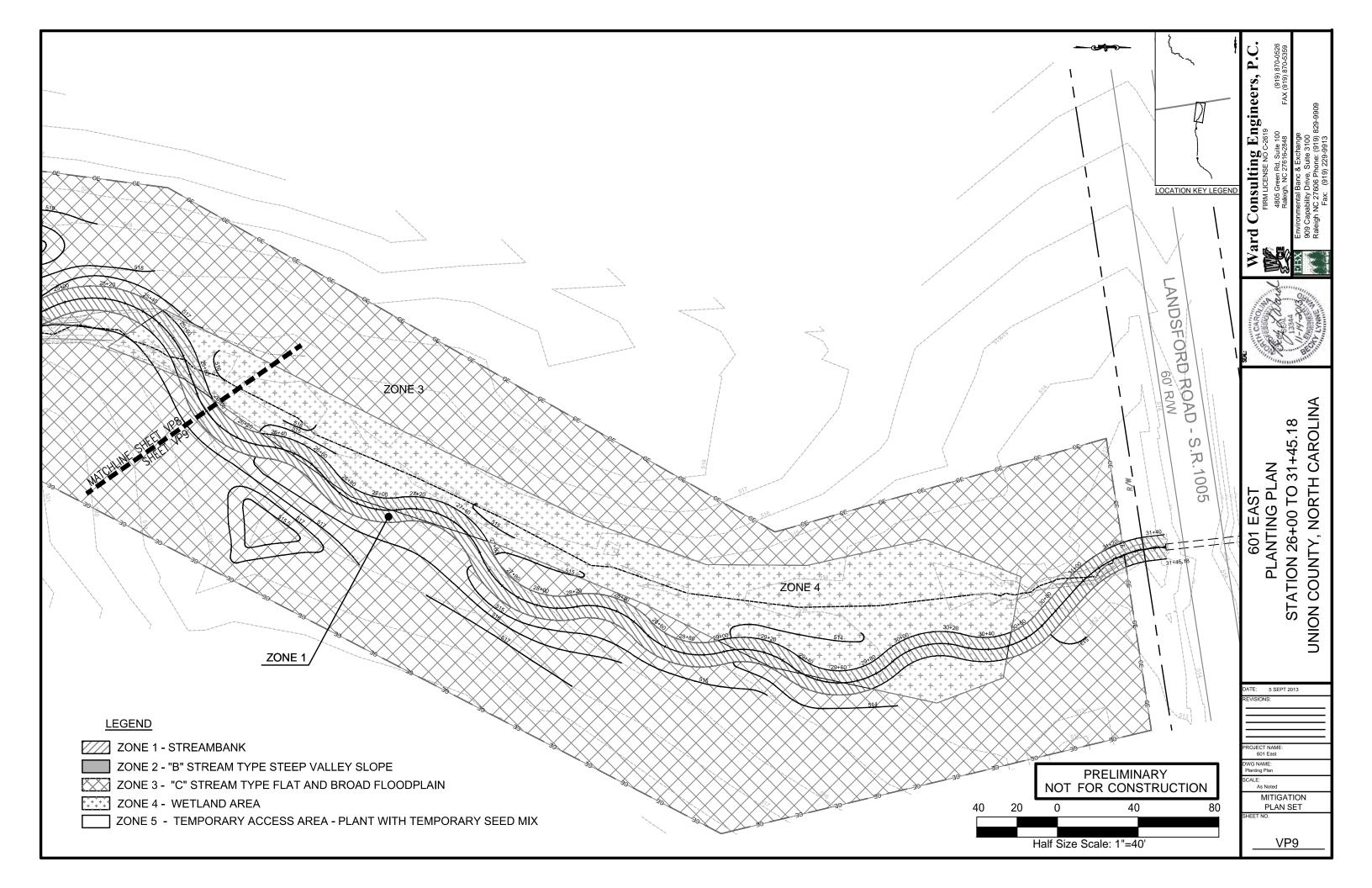


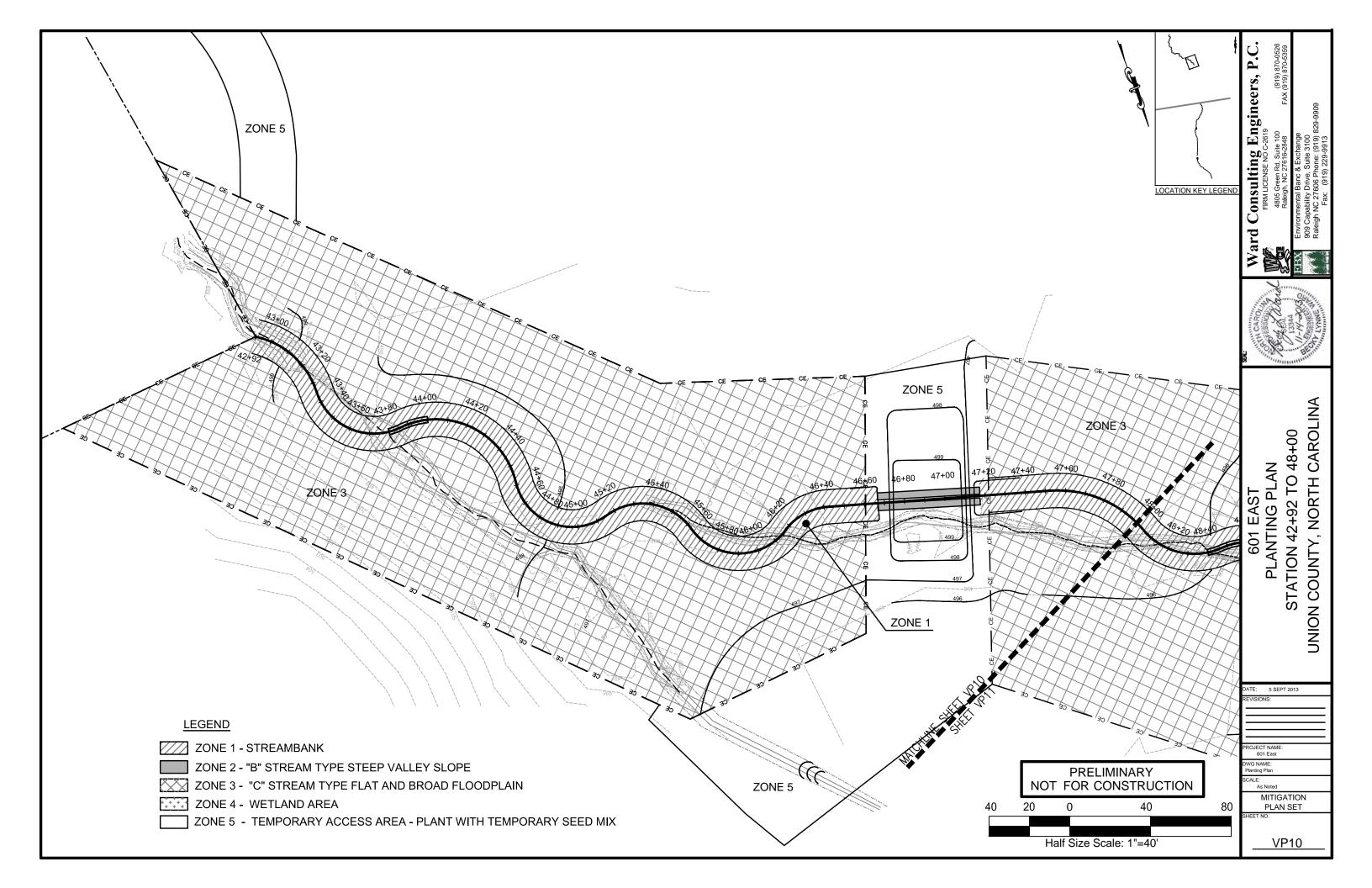


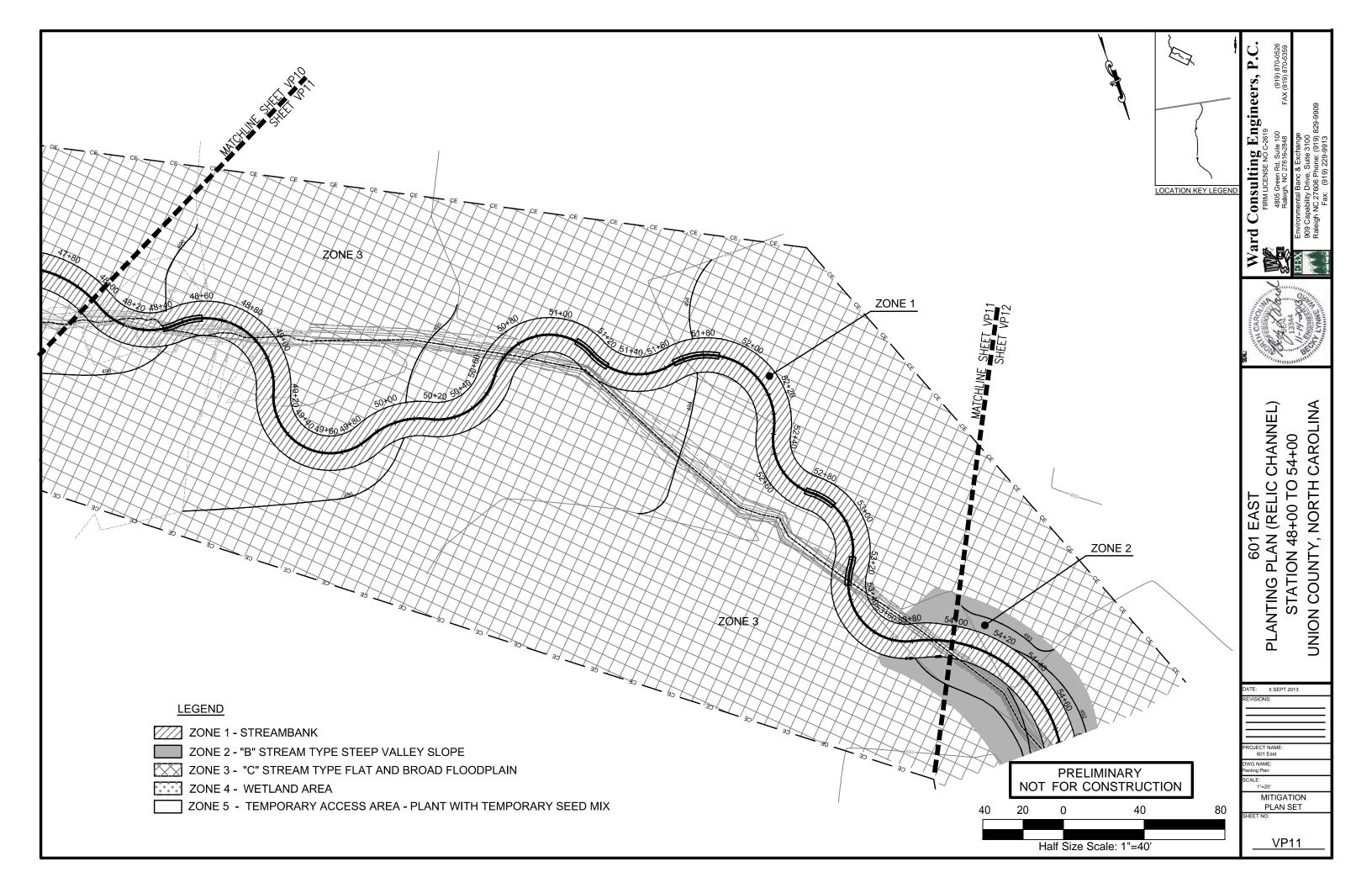


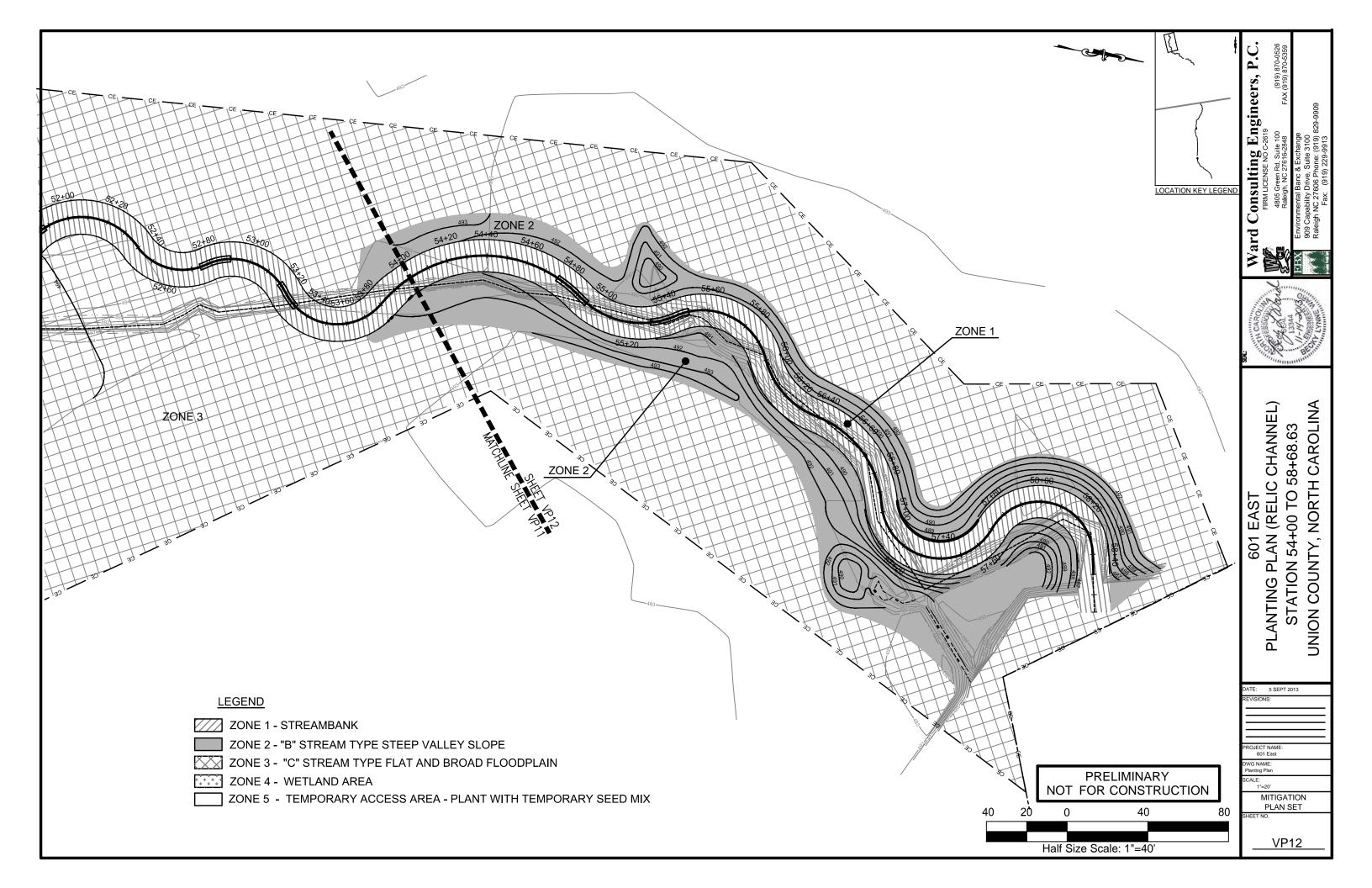


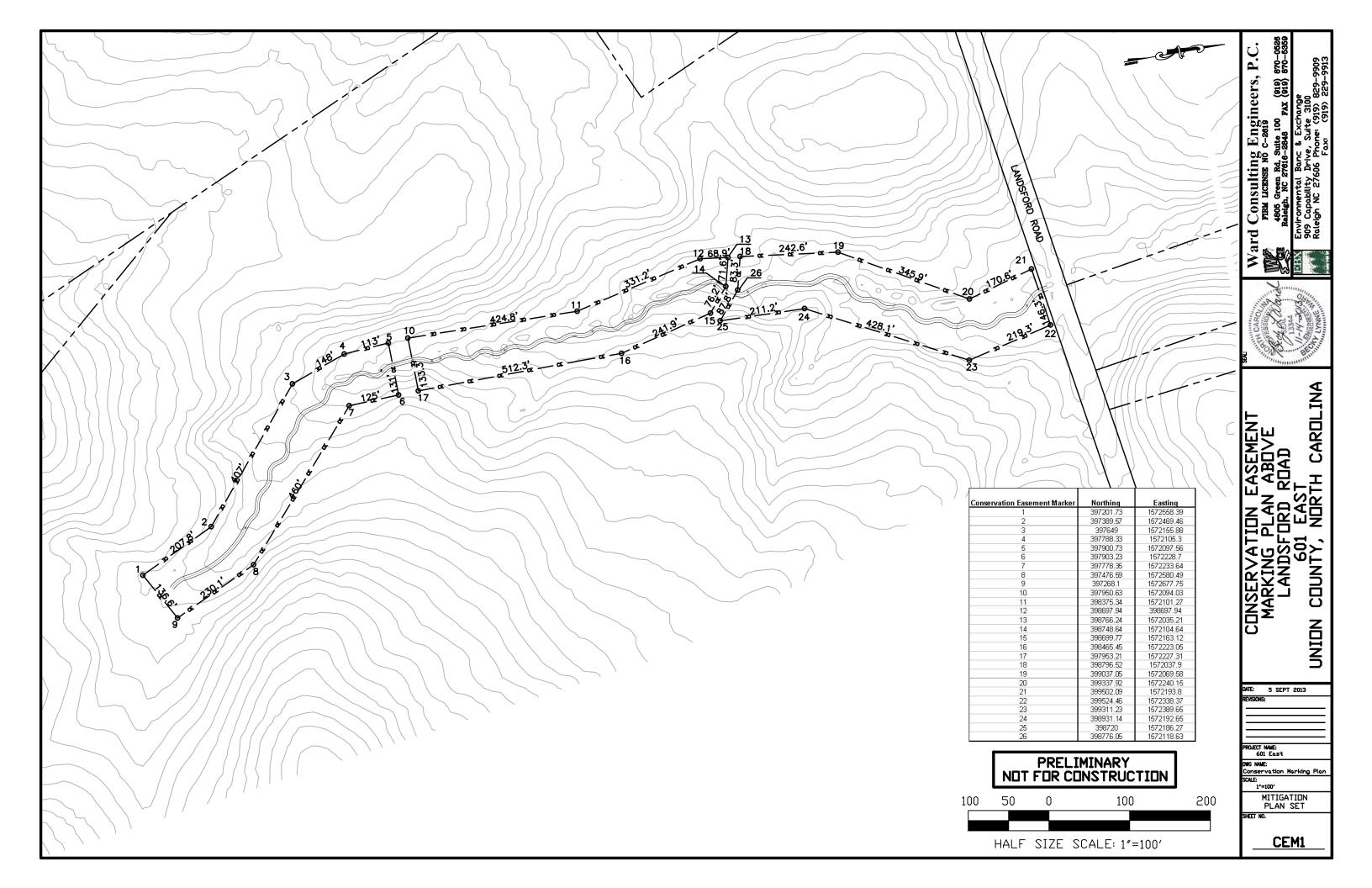


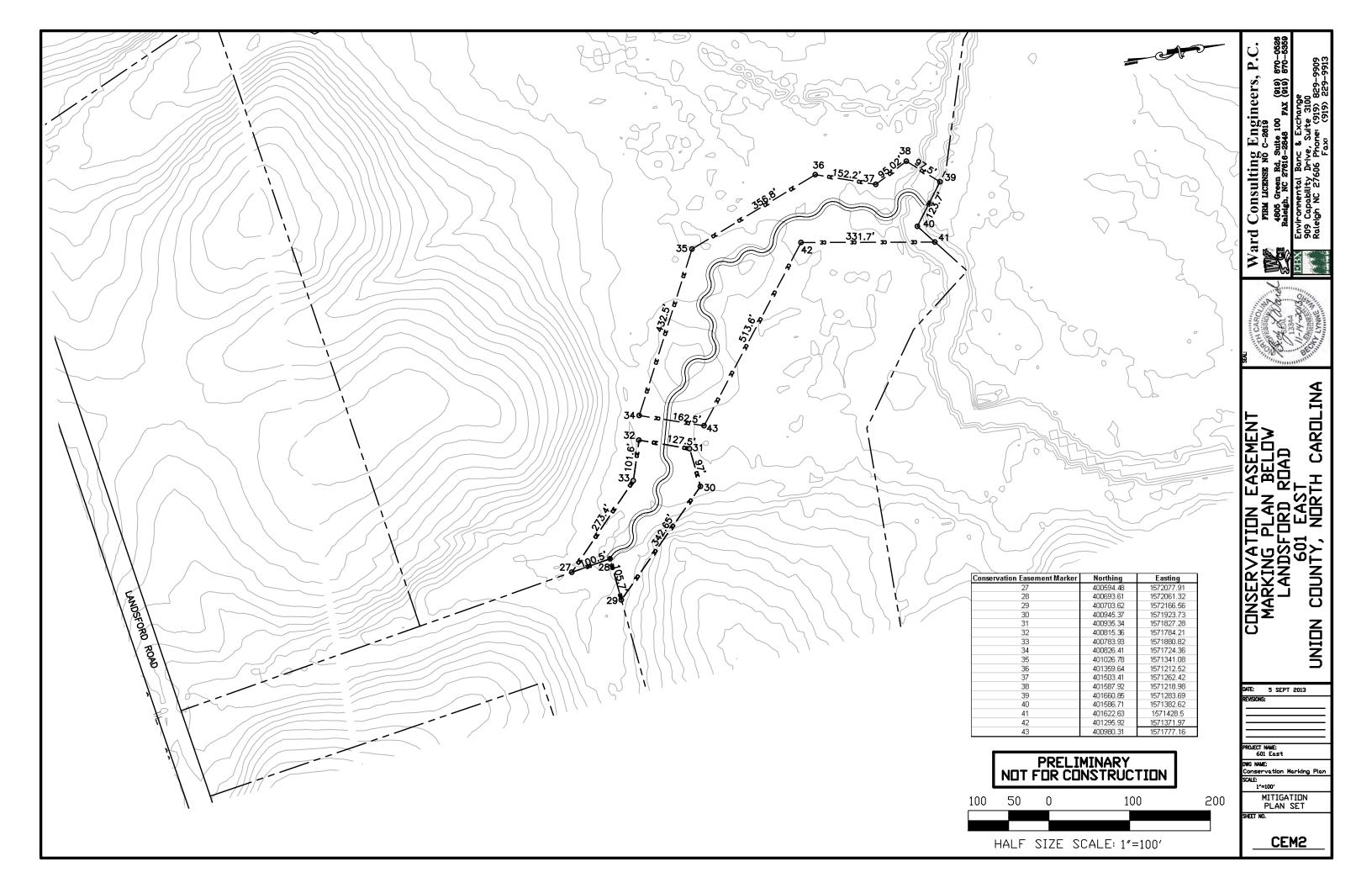












Appendix E. Preliminary Monitoring Plans

