## Payne Dairy Farm Stream Restoration

Executive Summary of Preliminary Design

Alexander County, North Carolina



prepared for



prepared by:



Kimley-Horn and Associates, Inc.

3001 Weston Parkway Cary, North Carolina 27513

> April 2000 011795000

# Jumping Run Creek Payne Dairy Farm Stream Restoration Executive Summary of Preliminary Design Alexander County, North Carolina

Prepared for:
Wetland Restoration Program
North Carolina Department of Environment & Natural Resources

Prepared by:
Kimley-Horn and Associates, Inc.
3001 Weston Parkway
Cary, North Carolina 27513

May2000 011795000

#### **Table of Contents**

		Page No.
1.0	Introduction	1
2.0	Existing Conditions	
2.1	Site Description	
2.2	Stream Condition	2
2.3	Watershed	
3.0	Project Description (Goals and Objectives)	
4.0	Methodology	
4.1	Field Work	
4.2	The Reference Reach	3
4.3	Verification of Regional Curves at Gage Station	4
4.4	Regime Equations	4
4.5	Hydraulic Model	4
4.6	Natural Communities	5
4.7	Sediment Transport Analysis	
5.0	Natural Channel Design	
6.0	Vegetation Plan	
7.0	Fencing Plan	8
8.0	Monitoring Plan	8
9.0	Summary	9

#### Appendix

Appendix A – Morphological Measurement Tables

Appendix B – Reference Reach

Appendix C – NC Rural Piedmont, Regional Curves

Appendix D – Regime Equations Appendix E – HEC-RAS Model, Existing Conditions

Appendix F – Site Photos

## Jumping Run Creek Payne Dairy Farm Stream Restoration Summary of Preliminary Design Alexander County, North Carolina

#### 1.0 Introduction

North Carolina Department of Environment and Natural Resources (NCDENR) - Wetlands Restoration Program (WRP) identified through its search process a site in Alexander County for potential stream restoration. The site is known as the Payne Dairy Farm and currently contains an operating dairy. WRP has purchased a 40.217-acre easement along 7500 feet of Jumping Run and 1300 feet of an unnamed tributary to Jumping Run.

Kimley-Horn and Associates (KHA) has performed the necessary fieldwork and data collection to complete the preliminary design plan for the restoration of Jumping Run located inside this easement. This document is a brief summary of the fieldwork and results, data collection, design procedures, and methodologies that went into the preparation of the preliminary design plans.

#### 2.0 Existing Conditions

#### 2.1 Site Description

This site is located in the Upper Catawba River Basin (Hydrologic Unit # 03050101) in Alexander County, North Carolina. The site is located less than two miles to the southeast of Taylorsville, North Carolina. Refer to Cover Sheet on Preliminary Plan for location maps.

The site contains approximately 7,500 + feet of stream located on two main parcels. The site contains Jumping Run and 1300 ± feet of an unnamed tributary. Jumping Run is classified as a WS-IV stream. The upstream parcel, which contains approximately 4000± feet of Jumping Run, is located north of Henry Road (SR 1614). The downstream parcel, which contains 3500± feet of Jumping Run and the unnamed tributary, is located to the west of Paul Payne Store Road (SR 1605). The segment of Jumping Run Creek between SR 1614 and SR 1605 is not associated with this project. Refer to Sheet 2 of the Preliminary Design Plans for Overall Site Map.

Currently, the majority of the site is active pasture. Cattle have unlimited access to the stream and wetlands on the upstream parcel and very limited access on the downstream parcel. Payne Dairy Farm on the section between SR 1605 and the tributary installed exclusionary fencing in the past year.

#### 2.2 Stream Condition

Large portions of the stream appear to have been straightened and relocated to one side of the valley. This was most likely done to maximize to amount of pasture. The combination of the cattle accessing the stream and the channel straightening has caused the stream to incise. This degradation is most severe on the upstream parcel (north of SR 1614) and on the tributary on the downstream parcel. Jumping Run downstream of SR 1605 is more stable vertically due to the presence of bedrock.

Based on a qualitative assessment and quantitative geomorphic field surveys the upstream reach was classified as an incised 'E' and 'C' stream type with excessive/unstable bank heights. In many places the stream is classified as a 'G' stream type. This classification is based on the Rosgen Morphologic Stream Classification. A complete summary of the Morphologic Description is provided in Appendix A.

#### 2.3 Watershed

The drainage area for Jumping Run is between 0.6 and 2.5 square miles. The majority of the watershed is active pasture and agriculture. However, in recent years there has been in increase in low-density residential development in the watershed. It is believed that residential development will continue based on new lots being subdivided and signs for future subdivisions. However, it was determined that the watershed as a whole would remain "rural" with the continued major land use being agriculture, active pasture and woodland with only a small percentage of low density development. Hydrology and Morphology was predicted based on a future "rural" watershed.

#### 3.0 Project Description (Goals and Objectives)

The project goal was to assess the feasibility of stream restoration and develop preliminary plans. The objective of this project is to restore Jumping Run from an altered/degraded stream corridor,

including adjacent riparian zones and flood prone areas, to its natural or referenced, stable condition. The ultimate goal of the project is to improve water quality, and the natural function of Jumping Run.

#### 4.0 Methodology

#### 4.1 Field Work

KHA performed the following fieldwork to assess the feasibility of restoration and to complete the preliminary design:

- Delineation of 6.38 acres of on-site Wetlands
- Rosgen Level II Classification of Streams
- Detailed Topographic Survey of Easement
- Watershed Condition and Potential Assessment
- Verification of Regional Curves at Gage Site
- Morphologic Survey of Reference Reach
- Natural Communities (Existing, Reference) Assessment

Wetlands on the project site were not identified on the NWI maps but were extensive based on field surveys. All wetlands inside the WRP easement were mapped because they will serve as a constraint for the horizontal location of the stream. The easement purchased by WRP includes all wetlands for preservation. However, the goals of this project did not include wetland creation, restoration or enhancement.

#### 4.2 The Reference Reach

A stable stream in the same watershed as Jumping Run was chosen as a reference to serve as blueprint for the stable dimension, pattern, and profile. Glade Creek just downstream 1000 feet downstream of SR 1604, was used as a reference. Refer to Appendix B for location and Watershed Map. The fieldwork was performed in accordance with the techniques outlined in "Stream Channel Reference Sites: An Illustrated Guide to Field Techniques" and the "Reference Reach Field Book". A summary of the Geomorphic Characterization and Morphological Descriptions and Survey Summary is included in Appendix B. A total station, Digital Terrain Model (DTM) survey was not performed on the reference reach as it was on the project site.

WRP, KHA, and the Alexander County Natural Resource Conservation Service (NRCS), searched for additional sites. However, only the one stable site was identified.

#### 4.3 Verification of Regional Curves at Gage Station

The North Carolina Rural Piedmont Regional Curves were verified at a Gage Station 2142000 at Lower Little River near Hearing Spring. This gage was the closest gage to the project site. The watershed area, discharge, bankfull width, and bankfull depth for the gage site were plotted on each curve to confirm that the curves were valid for this region. The North Carolina Rural Piedmont Regional Curves are provided in Appendix C. The points for Gage Station 2142000 are added to the curves. A detailed morphologic survey was not performed at the gage because the channel was a "G" channel and was not to be used as a reference for design. Based on the gage site, the regional curves are valid for this geographic region and can be used as a basis for design.

#### 4.4 Regime Equations

In developing the preliminary plans for the project site the NC Regional Curves and reference reach information had to be supplemented by regime equations and empirical relations for determining plan dimension. Equations like the Leopold and Wolman (1960) equations were used to calculate and verify plan features such as meander wavelength, radius of curvature, and meander amplitude. These calculations are included in Appendix D.

#### 4.5 Hydraulic Model

HEC-RAS was used to model the existing stream condition. The bankfull flow, 2, 10, 25, 50, and 100-year events were modeled. The bankfull flow was calculated from the NC Rural Piedmont regional curve. The other storm events were calculated using the Rural Regression Equation for the Blue-Ridge Piedmont, NC.

The model gave the designers a better understanding of predicted water surface elevations, water surface profiles, velocities, bank / channel shear stress, and stream power. This information was used to validate the preliminary design of the channel dimensions (i.e. wetted perimeter and hydraulic radius). The existing conditions HEC-RAS model summary tables are included in Appendix E.

The proposed channel will be modeled in detail as a comparison to the existing channel to aid in the final design of stabilization techniques, erosion control materials, and final channel dimension. The model will be completed upon confirmation of the preliminary plans by WRP.

#### 4.6 Natural Communities

Existing natural communities and species were identified through field identification, both adjacent to the stream and at the reference reach site. Additional proposed species were added based on communication with county and state resources, communication with private sector suppliers and contractors, and literature review.

#### 4.7 Sediment Transport Analysis

#### Upstream Segment

Sand and finer materials dominate the bed of the upstream segment. Allowable shear stress criteria are not very useful for design of channels with beds dominated by sands or finer materials. Sand beds are generally in motion at bankfull discharges and their shear stress values are much larger than those indicated by the Shields Criterion. In addition, because the channel on the upstream project segment is being relocated it is anticipated that the particle size distribution of the bed will change from silt/sand to sand/gravel. This was confirmed by looking at the particle distribution upstream of the site. Also, anticipated substrate soil sample was taken by auguring down to the proposed bankfull depth in the flood plain soils. The channel bed upstream, off the Payne property, has sand and gravel dominated bed. The soil auger samples verified the presence of gravel in the proposed new channel location (the current floodplain).

Stream power is the product of bankfull velocity and shear stress. The channel dimensions of the proposed channel matches the channel dimensions of the channel just upstream of the site. Since it is likely that the new channel will have a similar particle size distribution to the channel upstream of the project. Therefore, if the channel dimensions and slope are matched then the stream power will be similar for the proposed channel. If the stream power is similar, the proposed channel will have the same capacity to move the D50 particle as the channel just upstream of the site. During construction, the new channel dimensions will be verified based on the actual particle distribution using Shields Criterion or the Army Corp. Equations.

#### Downstream Segment

The downstream segment is controlled by bedrock. Therefore, a sediment analysis is not appropriate since the entire bed will be mobile during bankfull events.

#### 5.0 Natural Channel Design

The proposed natural channel design takes into account the existing conditions / stability, the cause of the disequilibrium, and the potential and/or morphological character of the natural stable form. This natural stable form was determined based on the methodologies described previously and David Rosgen's paper "A Geomorphic Approach to Restoration of Incised Rivers".

The following is a summary of proposed restoration for each stream segment. Details of the preliminary design contained in attached preliminary plans.

#### Upstream Segment

A Priority 1 restoration is proposed on the upstream segment of Jumping Run, north of SR 1614. Appendix F contains a Description and Summary of Incised River Restoration. 4,325 Feet of existing "G" and incised "E" channel will be converted to 4,419 feet of "C" channel on the original floodplain using a combination of relic channel, existing channel, and new construction. Specific morphological measurements for both the existing and proposed channel can be found in Appendix A.

#### Downstream Segment

The downstream segment is vertically controlled by bedrock. This bedrock has prevented the channel from incising to the same point as the upstream segment. However, the channel dimension and pattern are unstable. Placement of log vane structures in combination with bank stabilization/modification will provide for the minimum meander width ratio for a stable "C" channel. In addition, the in-stream structures will create a low flow channel with a lower width to depth ratio and improve the pool to pool spacing. Specific morphological measurements for both the existing and proposed channel can be found in Appendix A.

#### **Tributary**

A Priority 1 restoration including a culvert removal is proposed on the last 120 feet of the tributary before its confluence with Jumping Run. This will improve the angle of the confluence, and restore an unstable "G" stream type to a stable stream type "C/B" transition

#### Pattern, Dimension, and Structures

Refer to the preliminary plans for proposed stream location / relocation, structures type locations & details, fencing location and details, bank stabilization techniques, and proposed pattern and dimension for both the upstream and downstream segments.

#### 6.0 Vegetation Plan

The preliminary planting scheme has been developed based on the United States Forest Service (USFS) recommendations for riparian buffers. The buffer will consist of three zones from the top of bank to 100 feet from the top of bank. Zone 1 (0 to 20 feet from the top of bank) is the stream bank zone consisting of tree and shrub species typically found along stream banks in the region. Zone 2 (20 to 80 feet from the top of bank) is a forested riparian area consisting of selected tree and shrub species, with varying tolerances of inundation and saturation, to be selectively planted based on microtopography and moisture regime. Zone 3 (80 to 100 feet from the top of bank) is a grass filter strip designed to promote dispersed flow into the forested riparian zone (Zone 2). Zones 1 and 2 will be planted with container and/or bare root seedlings depending on available stock, design plans, climate, and cost. Planting spacing will be determined based on planting type, and will be included in final design plans. It is anticipated that Zone 3 will be seeded using a mix of native species. The entire easement will be planted or preserved. The riparian buffer is shown in plan view. A preliminary species list is also included in the preliminary plan.

In addition to the riparian buffer zones, the final vegetation plan will include planting specifications for stream bank stabilization. This is anticipated to be achieved primarily through live stakes and joint planting, as well as seeding (native species). A typical cross section of the anticipated live stake installation is included in the preliminary plan.

#### 7.0 Fencing Plan

Exclusionary Fencing will be installed along the entire easement. Several stream crossings will be maintained so cattle can move in a controlled manner from one side of the easement to the other. NRCS will work with Payne Dairy to provide alternative water sources for the cattle. The anticipated locations of the fence and crossings are shown in the preliminary plan.

#### 8.0 Monitoring Plan

As-Built Plans will be completed and submitted to the agencies that will document that the intent of the project was implemented in the field. The As-Built Plans will verify the constructed channel is of the design pattern, dimension, and profile.

Biological, geomorphic, and vegetative monitoring will be performed on the proposed constructed stream segment to determine success.

#### Biological Monitoring

Biological monitoring will include monitoring benthic macroinvertebrates per NCDENR's protocol. Biological monitoring will be conducted by and be the responsibility of NCDENR's Wetland 401 Group. The monitoring will consist of preconstruction and post-construction sampling. The current NCDENR standard for monitoring will be used. The NCDENR Wetland 401 Group will determine the biological monitoring procedures and schedule.

#### Geomorphic Monitoring

Geomorphic monitoring will be the responsibility of WRP. Vertical bed stability will be verified using monumented cross-sections and scour chains. The cross-sections will be located in both pool and riffle sections. Scour chains will be installed in appropriate features to verify entrainment size, and scour depths. Lateral bed stability will be verified using monumented cross-sections and bank pins. Existing and departures of a frequency of particle size distribution will be measured using the modified Wolman pebble count

method. The location of the monumented cross-sections, scour chains, bank pins, and pebble count transects will be finalized during construction and shown on the As-Built Plans. Soil Bioengineering success should be monitored. Documentation will occur at pre-established stations each year as well as at specific locations that do not appear to be as successful based on a visual reconnaissance of the corridor.

The morphology of the stream is to be monitored a minimum of once a year for 5 years after construction. It is also recommended to survey the stream after major (>2 year) storm events during this period.

#### Vegetative Buffer Monitoring

Vegetation survival inside the riparian buffer will be documented for a 5-year period through photograph documentation of the entire length of the corridor in which buffers were planted. Documentation will occur at pre-established stations each year as well as at specific locations that do not appear to be as successful based on a visual reconnaissance of the corridor. Vegetation survival of target dominant species will be confirmed.

#### 9.0 Summary

The attached preliminary plans restore Jumping Run and adjacent riparian zones and flood prone areas from a state of disequilibrium to a stable, referenced, natural condition. The preliminary design is based on a geomorphic approach to restoration using Rosgen's Stream Classification System. Use of, historical and existing field indicators, regime equations, and a hydraulic computer model (HEC-RAS) supplemented this methodology.

The attached design restores the geomorphic dimension, pattern and profile of over 5,700 feet of Jumping Run. In addition, the entire 40.2 acre easement will be fenced to exclude the cattle and a vegetative buffer will be planted / preserved along the entire 8,300 linear feet of Jumping Run and unnamed tributaries contained inside the easement.

H:\PN\01179500\Planning Document\Planning.doc

## Appendix A Morphological Measurement Tables



#### Morphological Measurement Table Downstream Of SR 1605

Variables	Existing*	Proposed	NC Rural Piedmont Regional Curves & Regime Eq.	USGS Station** 2142000	Reference Reach
1 Stream Type (Rosgen)	C5/6-1	C5-1	-	G4/5	B4-1c
2 Drainage Area (sq mi)	2.2	2.2	2.2	28.2	1.81 sq miles
3 Bankfull Width (ft.)	25-35	20-24	10-35 (20 avg.)	35	16
4 Bankfull Depth (ft.)	1.7	1.7	1-3 (2 avg.)	4.7	1.7
5 Width / Depth Ratio (ft.)	12.5-17.5	12-14	10	7.6	10
6 Bankfull Cross-Sectional Area (ft 2)	42-60	34-41	18-70(30avg.)	161	24
7 Bankfull Mean Velocity (fps)	3-4.3	4.4-5.6	6	6.4	-
8 Bankfull Discharge (cfs)	180	180	55-450 (180 avg.)	1040	-
9 Bankfull Max Depth (ft.)	2	2.5	-	5.0	4-4.5
10 Width of Floodprone Area (ft.)	125-205	125-205	-	48	30
11 Entrenchment Ratio	4.3-6.1	3-6	>2.2	1.37	1.9
12 Meander Length (ft.)	150	150	224		n/a
13 Ratio of Meander Length to Bankfull Width	5.8-7.1	6.3-7.5	11.2	-	п/а
14 Radius of Curvature (ft.)	30-70	30-70	52	-	n/a
15 Ratio of Radius of Curv. To Bankfull Width	1.3-3	1.25-1.5	2.6	-	n/a
16 Belt Width (ft.)	80	80	73	-	n/a
17 Meander Width Ratio	3.5	3.5	2.6	-	n/a
18 Sinuosity (Stream Length / Valley Length)	1.05	1.05	>1.2	-	1.2
19 Valley Slope (ft/ft)	0.0065	0.0065	-	-	0.012
20 Average Slope (ft/ft)	0.0055	0.0055	-	-	0.0096
21 Pool Slope (ft/ft)	0.002-0.005	0.002-0.005		•	0.007-0.009
22 Ratio of Pool Slope to Avg. Slope	0.4-0.9	0.4-0.9	-		1.1-1.36
23 Maximum Pool Depth (ft.)	2-2.5	2.5-3	-	•	3
24 Ratio of Pool Depth to Avg. Bankfull Depth	1.2-1.5	1.5-2	-	-	1.2 - 1.75
25 Pool Width (ft.)	*	35	-	-	16
26 Ratio of Pool Width to Bankfull Width	*	1.0-1.2	-	-	1.0
27 Pool to Pool Spacing (ft.)	100	100	-	-	70
28 Ratio of Pool Pool Spacing to Bankfull Width	4.3	4.3	5.6	_	4.4
29 Bank HT Ratio (Low Bank / Bankfull) (ft.)	1.3	1.0-1.2	1.0	-	-

<sup>\*</sup> Field indicators in the existing channel were difficult to identify due to heavy disturbance from cattle, severe bank erosion, and overall channel instability.

<sup>\*\*</sup> The USGS Gage was used to verify the accuracy of the NC Rural Piedmont Curves for the Physiogeographic region of the project.

Detail Measurements were not taken because the channel was a "G" channel and was not to be used as a reference.



#### Morphological Measurement Table Upstream of SR 1614 (North Section)

Variables	Existing*	Proposed	NC Rural Piedmont Regional Curves & Regime Eq.	USGS Station** 2142000	Reference Reach
1 Stream Type (Rosgen)	E6, G6, C4/5	C5/4	-	G4/5	B4-1c
2 Drainage Area (sq mi)	1.2	1.2	1,2	28.2	1.81 sq miles
3 Bankfull Width (ft.)	12-21*	12-20avg	12-20	35	16
4 Bankfull Depth (ft.)	1.0-1.8*	1.5-1.8	1.5-1.8	4.7	1.7
5 Width / Depth Ratio (ft.)	7-21*	6.7-13.3	6.7-13	7.6	10
6 Bankfull Cross-Sectional Area (ft 2)	12-24*	18-25	18-25	161	24
7 Bankfull Mean Velocity (fps)	3.1-8.3	3-5.5	3.0-5.5	6.4	-
8 Bankfull Discharge (cfs)	75-100	75-100	75-100	1040	-
9 Bankfull Max Depth (ft.)	1.8	2.5	-	5.0	4-4.5
10 Width of Floodprone Area (ft.)	13-75	120 <u>±</u>		48	30
11 Entrenchment Ratio	1-6	5.6-10	>2.2	1.37	1.9
12 Meander Length (ft.)	50	150	134-180	-	n/a
13 Ratio of Meander Length to Bankfull Width	2.1-4.1	7-13	8.4	-	n/a
14 Radius of Curvature (ft.)	16-45	42-100	42-57	_	n/a
15 Ratio of Radius of Curv. To Bankfull Width	1.3-2.1	3.5-5	3.5	-	n/a
16 Belt Width (ft.)	130	200	42	•	n/a
17 Meander Width Ratio	7.2	12.5	4.3	_	n/a
18 Sinuosity (Stream Length / Valley Length)	1.14	1.4+	>1.4	-	1.2
19 Valley Slope (ft/ft)	0.0092	0.0092		-	0.012
20 Average Slope (ft/ft)	0.0081	0.0066	<u> </u>	-	0.0096
21 Pool Slope (ft/ft)	0.004-0.006	.002005	<u> </u>	-	0.007-0.009
22 Ratio of Pool Slope to Avg. Slope	0.5-0.75	0.2 -0.75		_	1.1-1.36
23 Maximum Pool Depth (ft.)	2-3	5.4	-		3
24 Ratio of Pool Depth to Avg. Bankfull Depth	1.6-2.0	3	-	_	1.2 - 1.75
25 Pool Width (ft.)	•	12-22	13-24	_	16
26 Ratio of Pool Width to Bankfull Width	*	1-1.1	-	-	1.0
27 Pool to Pool Spacing (ft.)	50	45-100		-	70
28 Ratio of Pool Pool Spacing to Bankfull Width	2.4-4.2	2,3-6.3	5.7	-	4.4
29 Bank HT Ratio (Low Bank / Bankfull) (ft.)	1.7-2.2	1.0 - 1.1	1.0	-	-

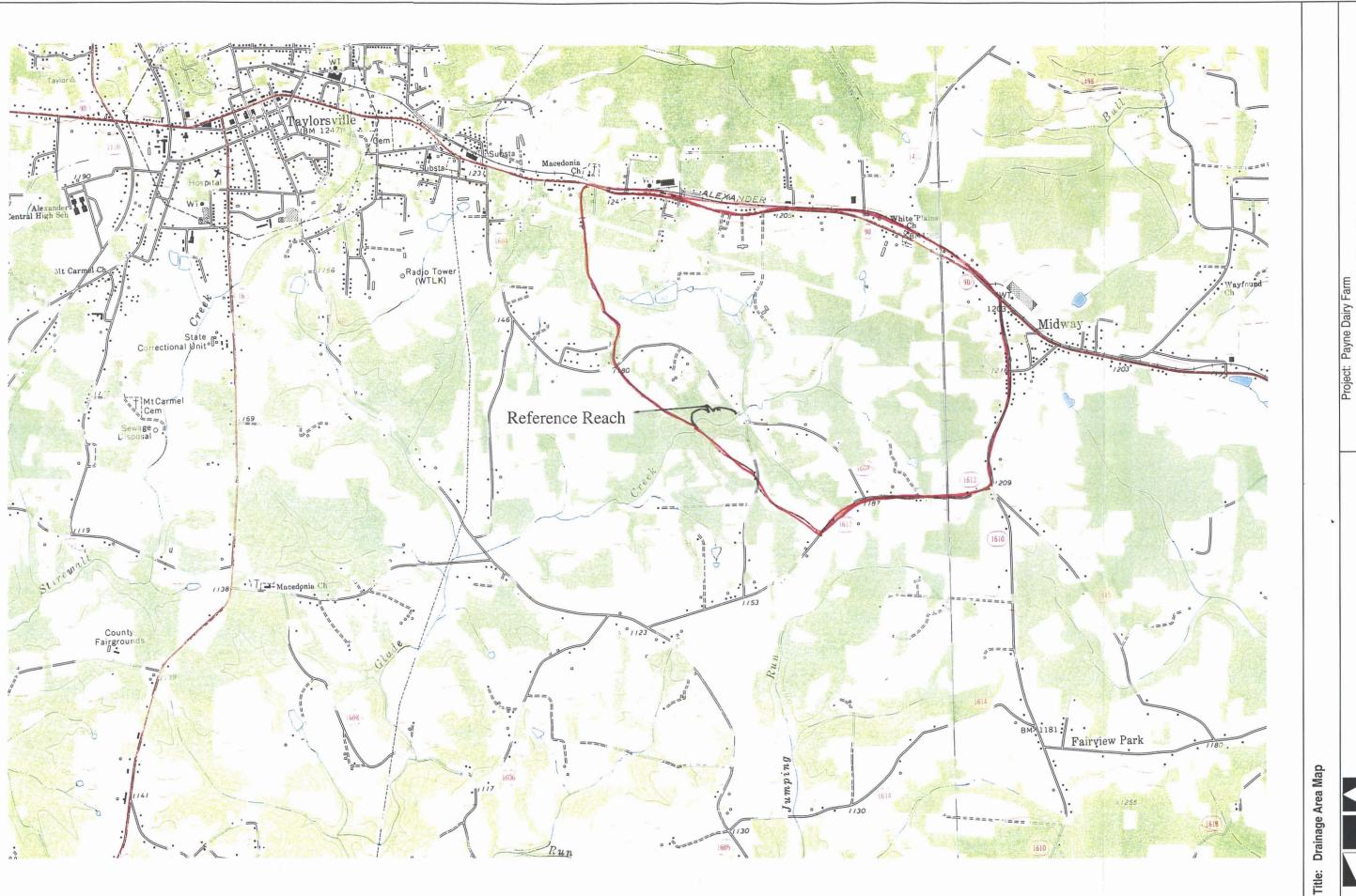
<sup>\*</sup> Field indicators in the existing channel were difficult to identify due to heavy disturbance from cattle, severe bank erosion, and overall channel instability.

<sup>\*\*</sup> The USGS Gage was used to verify the accuracy of the NC Rural Piedmont Curves for the Physiogeographic region of the project.

Detail Measurements were not taken because the channel was a "G" channel and was not to be used as a reference.

Appendix B

Reference Reach



Payne Dairy Farm Reference Reach – Glade Creek Drainage Area Map.

Date: 03/31/2000

Kimley-Horn
And Associates, Inc.
Engineering, Planning and Environmental Consultants

Scale: | Project No. | Exhibit: 1 in. = 200 ft. | 011795000 |



#### STREAM CLASSIFICATION WORKSHEET

Party:	Kimley-		sssociates (V		)	_ Date:	1/14/2000
State:	NC	County:	Alexander	Location:	100	0 ft D/S of Bost	ton Rd. (SR
Stream:	Glade (	Öreek		Drainage A	\rea:	1070 Acres (1	.7 sqmi)
Bankfull I	<b>/leasure</b> Width	ments:	Depth	1.7	W/D	9.4	
	vvidti	10	_ Debui	1.7	. **/**	<del></del>	
Entrenchi	Floodpi or width	one width is of inermed	iate floodplai	at 2x maxim n (10-50 yr.	um depth event)	in bankfull cros	ss-section,
	Bankful		16		ne Width	30	
	Entrend	hment Ration Slight = 2.2		9 ate=1.41-2.2	Entrer	nched = 1.0-1.4	
Sinuosity	(Stream	Length/Va	lley Length)	or (Valley	Slope/Ch	annel Slope):	
	Stream	Length (S <sub>L</sub> )		Valley Slop		0.012	
	Valley l	ength (V <sub>L</sub> )		Channel S	lope (C <sub>s</sub> )	0.00956	
	Sinuosi	ty (S <sub>L</sub> /V <sub>L</sub> )		Sinuosity (	V <sub>s</sub> /C <sub>s</sub> )	1.2552301	
Dominant	Channe	el Soils:					
	Bed Ma				vari	ous	
	Descrip	tion of Soil I	Profiles (from	base of bar	nk to top)		
	Right:	@ Sta 2+2	0 (0-2' 10YR	3/1. 2-2.5'	10YR 3/2.	2.5-3' 10YR 4/	4 w/ 5YR 5/8 incl.
			<b>.</b>	3-5' 7.5YR			
	Left:			Same Co	mpostiion	as Rt.	
	Bank S	ope (Horizo	ntal to Vertica	al) L	1:1.3	_ R	1:1.2
Riparian V	/egetatio	- on:					
	Left Bar % Total % Total	nk: Area (Mass Ht w/ Roots		R R	ight Bank: ht	See	Photo
Water Sur	Water s	urface slope t for a length		ately 20 to 3		ce representing Il channel width	the bankfull stag s:
STREAM	ГҮРЕ	B4-1c	Remarks		Ве	brock present	



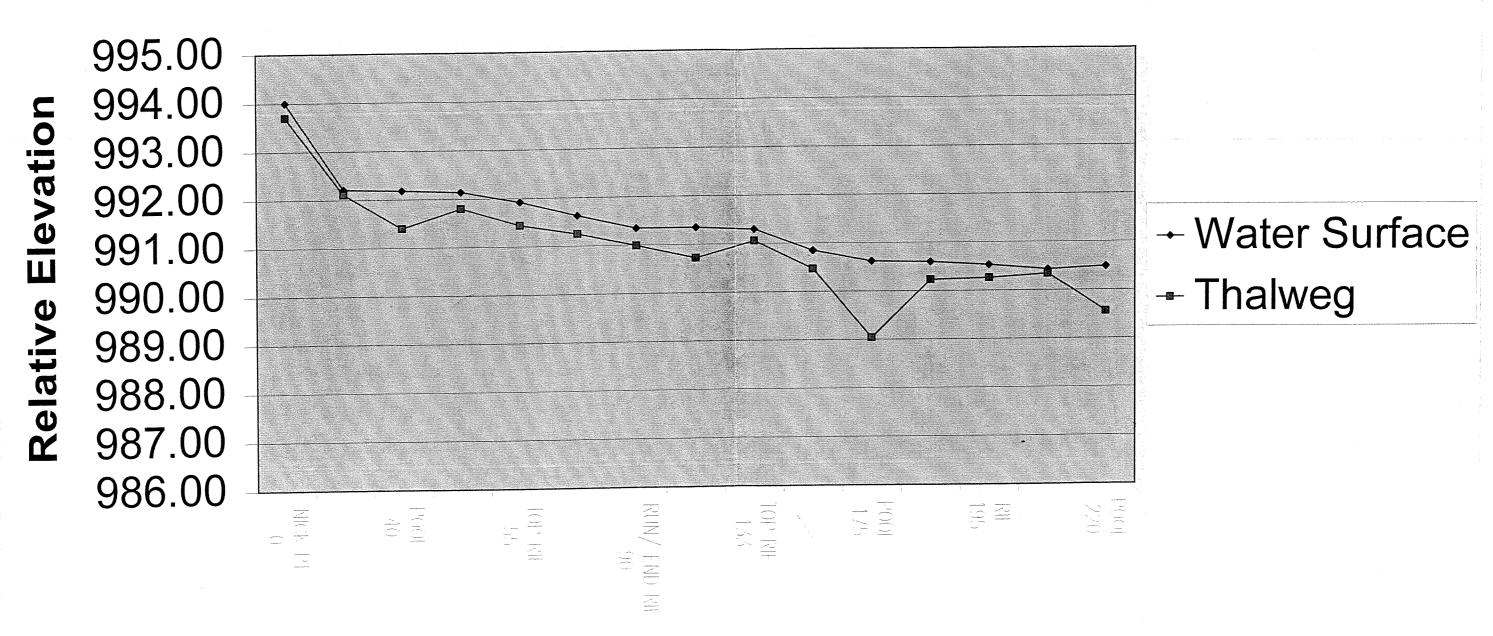
### STREAM CLASSIFICATION WORKSHEET REFERENCE REACH

Party:	Kimley	-Horn and A	sssociates (V	VRW, CWE)		_ Date:	1/14/00
State:	NC	County:	Alexander	Location:		00 ft D/S of Bos	ton Rd. (SR
Stream:	Glade	Creek		Drainage A	\rea:	1070 Acres (1	I.7 sqmi)
Bankfull	Measure	ments:					
	Width	16	_ Depth	1.7	. W/D	9.4	
Entrench	ment Ra	tio (Floodo	rone Width/E	Bankfull wid	ith):		
Littlefieli	Floodp	rone width is	water level a	at 2x maxim	um depth	in bankfull cros	ss-section,
			iate floodplair			00	
		ll Width chment Ratio	<u>16</u>	Floodproi	ne wiatn	30	
	Cittleid	Slight = 2.2		te=1.41-2.2	Entrer	nched = 1.0-1.4	
Sinuosity	(Stream	n Length/Va	llev Length)	or (Valley 9	Slope/Cha	annel Slope):	
	-	Length (S <sub>L</sub> )		Valley Slop		0.012	
	Valley l	Length (V <sub>L</sub> )		Channel S	ope (C <sub>s</sub> )	0.00956	
	Sinuos	ity (S <sub>L</sub> /V <sub>L</sub> )		Sinuosity (	$V_s/C_s)$	1.2552301	
Dominan	t Channe	el Soils:					
Dominian	Bed Ma				vari	ous	
	Descrip	tion of Soil	Profiles (from	base of bar	nk to top)		
	Right:	@ Sta 2+2	0 (0-2' 10YR	3/1, 2-2.5'	10YR 3/2.	2.5-3' 10YR 4/	4 w/ 5YR 5/8 incl.
	J			3-5' 7.5YR			
	Left:			Same Co			
	Bank S	lope (Horizo	ntal to Vertica	al) L	1:1.3	_ R_	1:1.2
Riparian '	Vegetati	on:					
	Left Ba		See Photo	•	ight Bank:	See	e Photo
		Area (Mass		R R			
		l Ht w/ Roots f Actual Ban	s L k Height to Ba		ht		
	riatio o	i / iotaai Daii	it i loigili to D				
Water Su	rface Slo	pe					
	Waters	surface slope	e is the "riffle"	to "riffle" wa	ater surfac	ce representing	the bankfull stage
	gradien	it for a lengti = S			o Dankiui	I channel width	S.
		3=	0.00	,			
STREAM	TYPE	B4-1c	Remarks		B∈	ebrock present	

#### Longitudinal Profile

		WS	TW
Station	Description	ELEV	ELEV
0	NICK PT	994.00	993.70
20	END RIF	992.21	992.11
40	POOL	992.18	991.40
47	NICK PT	992.14	991.80
55	TOP RIF	991.92	991.44
70	RIF	991.63	991.25
90	RUN/ END RIF	991.35	990.99
100	POOL	991.35	990.72
133	TOP RIF	991.30	991.06
150	END RIF	990.85	990.47
175	POOL	990.62	989.04
185	TOP RIF	990.60	990.23
195	RIF	990.53	990.26
205	END RIF	990.43	990.34
220	POOL	990.49	989.56

### **Longitudinal Profile**



**River Station** 



PEBBLE COU	NT	Site REF # ! (Glade Creek)							Site REF # ! (Glade Creek)					
Metric	English	Particle	Count	Tot	%	%	Count	Tot	%	%	Count	Tot	%	%
(mm)	(inches)			#	Tot	Cum		#	Tot	Cum		#	Tot	Cur
<.062	<.002	Silt/Clay		5	6.25	6.25			T	7 3 3 1 1				T
				<del></del>		6.25								<del> </del>
.062-0.25	.00201	Fine Sand			0	6.25				t				<del> </del>
0.255	.01012	Med. Sand		5	6.25	12.5			<b></b>	l				t
.5-1.0	.0204	Coarse Sand			0	12.5			<u> </u>	tI				<del> </del>
1.0-2.0	.0408	Vy Coarse Sand		13	16.25	28.75								<del>                                     </del>
						28.75							<b></b>	$\vdash$
2-8	.0832	Fine Gravel		12	15	43.75							l	<del> </del>
8-16	.3263	Med Gravel		3	3.75	47.5			<b></b>				İ	<del>                                     </del>
16-32	.63-1.26	Coarse Gravel		7	8.75	56.25			<b> </b>				ĺ	<del> </del>
32-64	1.26-2.51	Vy Coarse Gravel		4	5	61.25							<u> </u>	<del>                                     </del>
64-128	2.51-5.0	Small Cobbles		8	10	71.25							<u> </u>	†
128-256	5.0-10.1	Large Cobbles		6	7.5	78.75								<del> </del>
									<b></b>				ļ	<del> </del>
256-512	10.1-10.2	Sm. Boulders											İ	+
512-1024	20.2-40.3	Med Boulders							<b> </b>				İ	+
1024-2048	40.3-80.6	Lg. Boulders							<del>                                     </del>				l	<del> </del>
2048-4096	80.6-161	Vy Lg Boulders							<b> </b>					<del> </del>
		Bed Rock		17	21.25	100							<u> </u>	+

**sum** 80

Project: Payne Dairy Farm Jumping Run Creek Stream Restoration

Date: 2/23/2000

Reference Site: Glade Creek D/S of Bosto Rd.

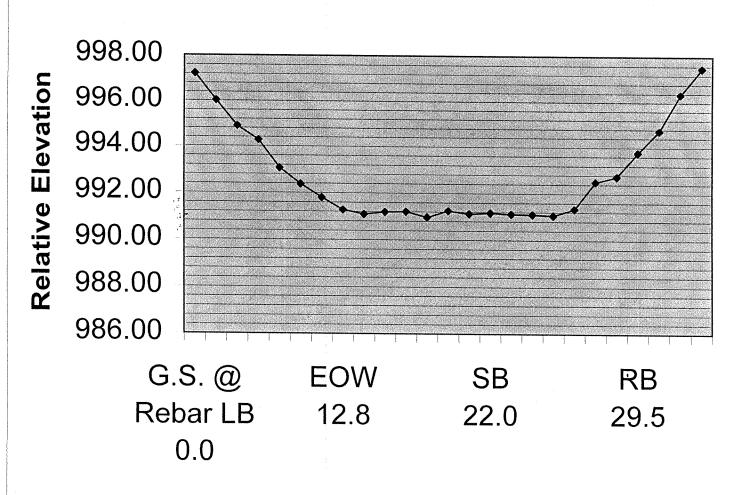
Stream Name: Glade Creek

X-Section @ Approx. STA 1+33 (Riffle)

Station	Description		
0.0	G.S. @ Rebar LB	997.22	
5.0	HT LB	996.02	
8.0	LB	994.88	
9.0	LB	994.27	
11.0	MT LB	993.06	
11.6	LB	992.37	
12.0	LB	991.80	
12.8	EOW	991.28	991.3
12.8	SB	991.09	
15.0	SB	991.19	
17.0	SB	991.20	
18.0	TW	990.97	
19.0	SB	991.24	
20.0	SB	991.12	
22.0	SB	991.17	
24.0	SB	991.11	
25.0	SB	991.10	
26.0	SB	991.06	
27.0	EOW	991.33	991.3
27.5	BF	992.50	
27.8	BF	992.73 -	
29.5	RB	993.77	
31.0	RB	994.72	
32.0	HT RB	996.34	
35.0	HT RB	997.50	

<sup>\*</sup> All elevations are based on a relative BM at X-Section STA +38 (nail in oak tree)

#### X-Section @ Sta 1+33



**Station** 

1000.0 1000.0 Bankfull Width (ft) Bankfull X-Sec. Area (Sq. Ft.) 100.0 100.0 10.0 10.0 0.1 100 1000 10 0.1 10 1000 Watershed Area (sq. mi.) Α Watershed Area (Sq. Ml.) 100.0 10000 Bankfull Depth (ft) 1000 10.0 Discharge (cfs) 100 1.0 0.1 0.1 100 10 1000 0.1 10 100 1000 C D Watershed Area (sq.mi.) Watershed Area (sq. mi.)

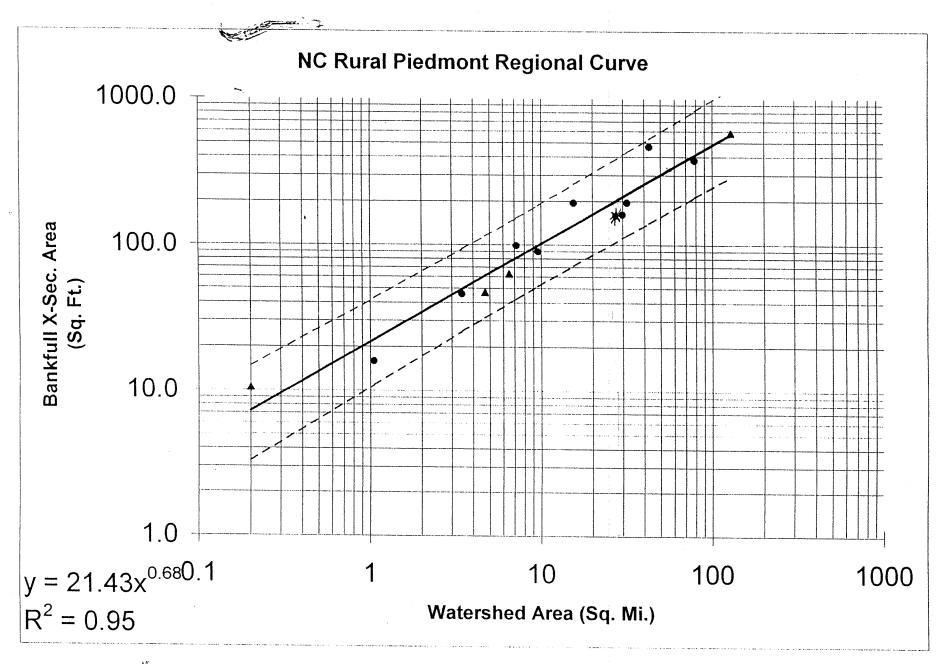
1000 ± alls of SK 1607 Boston Raj

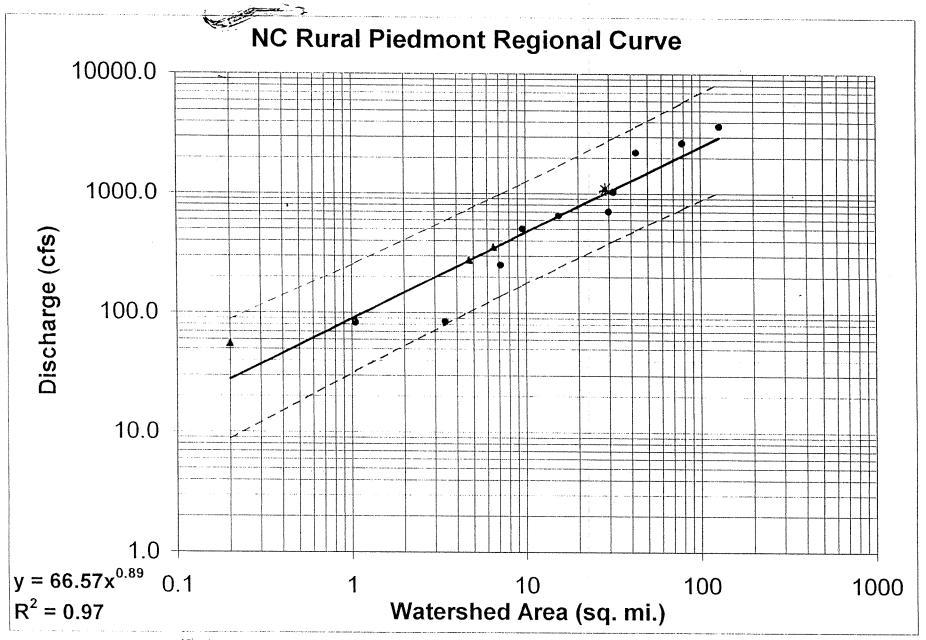
Keach ( 61ade

Figure 2: Bankfull hydraulic geometry relationships for rural Piedmont North Carolina Streams. The four graphs represent:
a) cross sectional area, b) width, c) depth, and d) discharge. The circles represent gage stations and the triangles represent ungaged streams.

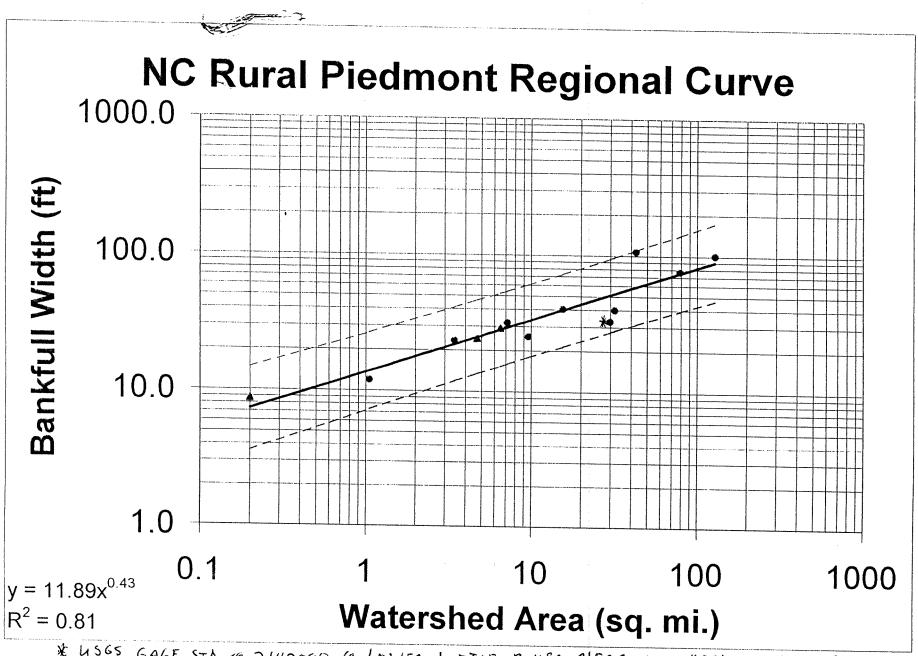
Appendix C

NC Rural Piedmont Regional Curves

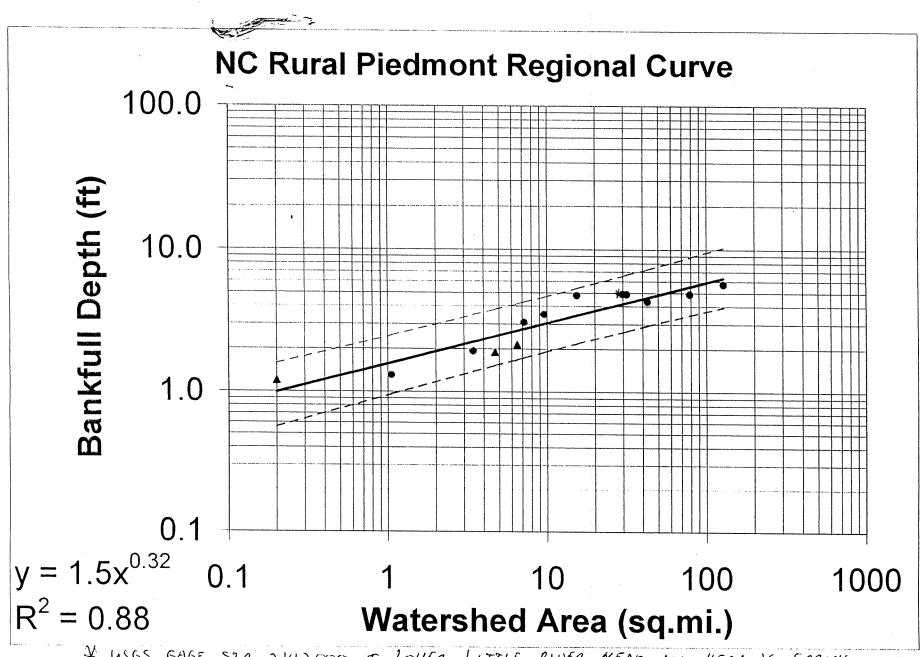




\* WSGS GAGE STA 2142000 (G LOWER LITTLE RIVER NEAR ALL HEALING SPRING



\* USGS GAGE STA & 2142000 & LOWER LITTLE RIVER NEAR ALL HEALING SPRING



\* USGS GAGE STA 2/42000 & LOHER LITTLE RIVER NEAR ALL HEALING SPRING



Stream	Gage Station	Drainage	Stream	Bankfull	Bankfull	Bankfull	Bankfull Mean	Water Surface	Return	Exceedence
Name	ID	Area	Туре	Discharge	Xsec Area	Width	Depth	Slope	Interval	Probability
	7.	(mi2)	(Rosgen)	(cfs)	(ft2)	(ft)	(ft)	(ft/ft)	(Years)	(%)
Sal's Branch	Reference Reach	0.2	E4	55.4	10.4	8.7	1.2	0.0109	n/a	n/a
Humpy Creek	02117030	1.05	E5	83	15.8	12.0	1.3	0.0060	1.7	59
Dutchmans	02123567	3.44	C5	85.1	45.6	23.5	1.9	0.0170	1	100
Mill Creek	Reference Reach	4.7	E4	277	46.7	24.5	1.9	0.0080	n/a	n/a
Upper Mitchell River	Reference Reach	6.5	B4c	356	62.5	29.2	2.1	0.0095	n/a	n/a
Norwood Creek	0214253830	7.18	E5	253.7	98.8	32.0	3.1	0.0008	1.1	91
North Pott's Creek	02121180	9.6	E5	507.2	89.6	25.4	3.5	0.0012	1.7	59
Tick Creek	02101800	15.5	E	655.3	194	40.5	4.8	0.0005	1.3	77
Moon Creek	02075160	29.9	E5	708.8	162	33.0	4.9	0.0015	1.8	56
Long Creek	02144000	31.8	E5	1041	195	40.0	4.9	0.0010	1.4	71
Little Yadkin River	02114450	42.8	G5	2236	469	77.5	6.0	0.0018	1.4	71
Mitchell River	02112360	78.8	C	2681	377	77.0	4.9	0.0030	1.6	63
Fisher River	02113000	128	C3	3687	578	101	5.7	0.0023	1.4	71

Table 1: Hydraulic geometry, survey summary, and flood frequency analyses for gaged and ungaged stream reaches.

Appendix D

Regime Equations

Job Pagno Dairy Subject Man View
Designed by WRW Date Checked by

Sheet No. \_\_\_\_\_\_ of \_\_\_\_\_ Z

Plan View Cales US SEGNIENT

-Leopold & Wolman Equation (1960) to predict Meander Length, Amplitude, & Mean radius of Carvature

- Inpul into Equation is bookfull surface width
- Bankfull Surface Width obtained from Regional
Correct

- Regional Cours Verited W/ Retience Reach

U/S OF TRIB WAKE = 12 Aug [6'-25']

Meander Length =  $L_m = 10.9 \, \text{W}^{101} = 134' \, [67' - 28']$ Amplitude =  $A = 2.7 \, \text{W}^{11} = 42' \, [20' - 93']$ 

Amplitude = A = 2.100 = 92 [20 - 15]redins  $GI = Rc = (\frac{Lm}{4.7})^{1.02} = 30' [15 - 65']$ 

SR 1614 - Trib WAKF = 16'AUG [8-30']

Meanler Length =  $L_n = 10.9 \, \text{W}^{1.01} = 180^{\circ}$ Amplitude =  $A = 2.7 \, \text{W}^{1.1} = 57^{\circ}$ Radius of Carvatur =  $R_c = \left(\frac{L_m}{4.7}\right)^{-2} = 42^{\circ}$ 

\* These #'s Can be used as check (i.e. general rule)



Λ	Λ		Δİ	1	Sheet No of
Job 8071	e Nairy	Subject	11 an	View	 Job No
Designed by	WRW	Date		Checked by	Date

Plan View Cales 10/5 SEGMENT (D/S OF SA 1605)
-Leopold & Wolmon Equation to predict Meander Length, Amplitude, & Mean Radias of Curuch.
- Input into Eq is Bankfull Surface Width
- Bankfull Serface Wilth Obtained from Regional Cues
- Regional Curves Veritied W/ Reference Read / Gage Site
DIS OF SR 1605 Wake = 20 Aug (10-35)
Meander Length = Lm = 10.9 W = 224 (111-395)
$A_{1}, I_{2} = A = 2.7 W'' = 73' (34'-135)$
Redins of $=$ $R_c = \left(\frac{L_m}{4.7}\right)^{1.02} = 52'\left(2\dot{s} - 92'\right)$

Appendix E

HEC-RAS Model Existing Conditions

Upstream Segment Jumping Run North of SR 1614

Vel Chni Flow Area Top Width Frouds # Chi Shear Chan Shear LOB | Shear ROB | Shear Total E.G. Eley E.G. Slope Reach River Sta Q Total Min Ch El W.S. Elev CHI W.S. (lixex) (t) (lb/sq ft) (th/aq:ft) (fi/ft) (11/6) (seq ft) (21) (R/sq ft) (A) (cfs) 0.002342 31.38 30.7 0.42 0.15 0.15 3850 75.00 1096.00 1097.62 1097.11 1097.71 0.21 0.47 0.21 1098.05 0.002784 2.96 40.55 32.77 120.00 Upstream 0.59 0.41 0.41 62,91 3850 275.00 1096.00 1098,56 1097.97 1098.85 0.003902 0.06 0.32 5.01 5.33 0.62 0.51 1098.3 0.004209 82.58 66.70 1098.90 1099.28 385.00 1096.00 Upstream 87.92 0.62 0.56 0.09 0.02 0.30 0.00406 3850 480.00 1096.00 1099.17 1098,64 1099.59 jpetream 0.003602 5.47 133.02 96.76 0,60 0.56 0.14 0.05 0.31 590.00 3850 1096.00 0.08 0.36 0.13 0.02 0.001610 2,39 36,87 48.22 0.02 75.00 1096.00 1097.49 1097.58 Upstream 3800. 0.12 0.26 3.17 59.58 0.44 0.22 0.05 0.05 120.00 1096.00 1097.72 1097.87 0.002293 Jostreem 0.004518 5.27 83.48 88.21 0.65 0.56 0.16 0.19 1098.18 3800 275.00 1096.00 0.79 95.37 0.75 0.26 0.29 0.39 103.81 385.00 1096.00 1098.40 1098.93 0.005744 6.36 7.18 119 73 100 85 0.81 0.98 0.34 0.37 0.49 0.00666 800. 480.00 1098.00 1098.56 106.36 0.61 0.88 1.20 0.44 0.46 1099.53 0.007643 8.02 138.57 3800. Upstream 0.70 15.03 19.55 1.00 0.70 4.99 3750. 75.00 1096.00 1096.93 1096.93 1097.32 0.015446 Upstream 101,63 0.79 0.53 0.12 0.12 0.22 0.008778 4.53 41.72 1097.61 nseriect 3750 120.00 1096.00 1097.32 1097.32 0.87 0.82 0.35 0.27 1097.76 1097.76 1098.18 0.009488 5.97 89.30 116.45 3750 275.00 Upetream 0.010116 115.39 123.45 0.92 1,00 0.48 0.38 0.58 1098.48 3750. 385.00 1096.00 1097.98 1097.98 0.94 0.44 0.67 0.57 480.00 1098.15 1098.71 0.010194 7.26 137.70 129.27 patream 0.98 1.27 0.67 0.50 0.78 7.86 159.97 135.00 1098,95 590.00 1096.00 1098.32 1098.32 0.010608 9.15 10.76 1.57 1.84 1.84 1096,14 0.036399 8.20 3700 75,00 1094.00 1095.09 1095.41 2.15 0.034159 9.20 13,05 12.24 1.57 2.15 120.00 1094.00 1095.43 3700. Jostream 8.09 104.33 1.07 1,40 0.21 0.21 0.42 53.78 0.013193 1097.55 275.00 1094.00 1096,60 1096.91 0.60 1.54 0.29 0.012471 8,70 84.91 109.16 1.06 0.41 1094.00 1096,90 385.00 Jpetream 3700. 113.38 9.16 1.07 0.54 0.36 0.72 0.012197 107.84 1.65 700 480.00 1094.00 1097.10 1097.38 1098.12 0.80 0.011562 9.51 134.80 119.59 1.06 1.72 0.64 0.41 590.00 1094.00 1097.33 Upstream 3700. 0.45 1095.63 0.007075 4.22 17.75 16.94 0.73 0.45 1094.00 75.00 3650. 0.76 0.57 0.57 4.92 18.82 120.00 1094.00 1095.72 1095.47 1096.10 0.007290 0.18 0.12 0.003437 4.68 94,43 111,71 0.57 0.44 0.06 275.00 1094.00 1096.61 Upstream 3650. 0.37 0.08 0.18 0.002443 4.45 142.93 120.64 0.49 0.14 385.00 1094.00 1097.03 1096,68 1097.22 0.002047 4.40 181.11 128.02 0.46 0.35 0.15 0.08 0.18 1094.00 1097.33 3650. 480.00 0.44 0.18 4,41 590.00 1094.00 1097.64 1096.97 1097.82 0.001796 221.99 Upatream 12.20 12,15 1.00 0.95 0.02 0.81 0.014053 6.17 75.00 1093.00 1094.44 1094,44 1095.03 6.29 6.75 25.38 77.25 35,04 0.87 0.89 0,19 0.43 1095.00 0.00999 1093.00 1095.00 3600 120.00 0.58 73.41 0.84 0.97 275.00 1093.00 1096.01 1096.01 1096.53 0.009175 0.04 0.77 0.010078 7.72 98.4 77.68 0.90 1.22 0.64 1096.29 Upstream Upstream 1096.29 3600. 385.00 1093.00 80.83 0.08 0.92 114.61 480.00 1093.00 8.44 1096.49 1098.49 1097.24 0.010766 9.00 135,21 84.69 0.96 1.56 0.91 0.11 1.03 1096.74 Upstream 3600 590.00 1093.00 1096.74 0.18 0.001999 2.86 26.20 16.85 0.40 0.18 1093.71 1092.83 Upstreem 3550 75.00 1091.37 1093.84 27.10 0.45 0.23 0.02 0.20 37.64 1091.37 1093.23 1094.42 0.002397 3.23 Upstream 1094.26 1095,51 0.002627 4.52 71.50 46.14 0.50 0.39 0.10 0.04 0.25 Upstream Upstream 1094.30 3550. 275.00 1091.37 1095.20 0.59 0.34 0.58 0.08 52.81 0.16 1091.3 1094.73 1095.95 0.003485 5.59 85.67 94.86 56.49 0.67 0.76 0.23 0.12 0.45 0.004369 6.51 3550. 480.00 1091,37 1095.65 1095.09 1096.27 0.76 1.02 0.18 0.59 0.32 0.005559 7.57 102.95 59.35 3550. 590.00 1091.3 1095.44 1096.63 Upstream 20.71 0.55 0.27 0.27 75.00 1092.00 1093.52 1093.69 0.004028 3.29 22.77 3500 Upstream 38.66 0.48 0.25 0.02 0.01 0.16 3.31 37.63 0.002731 120.00 275.00 1092.00 1094.11 1094.28 0.08 0,15 1092.00 1095.12 1095.36 0.002119 4.11 101.36 90.41 0.46 0.32 0.08 3500. Upstream 4.91 102.79 0.52 0.44 0.13 0.13 0.20 0.26 petream 3500. 385.00 1092.00 1095.42 1095.75 0.002587 0.18 480.00 1096.02 0.003072 5.58 150.35 110.12 0.57 0.56 0.17 Upstream 3500. 1092.00 1095.61 6.30 0.24 0.33 170.55 117.17 0.62 0.69 0.23 0.003828 590.00 1092.00 1095.79 1096.30 6.05 8.66 0.89 0.88 0.88 0.011756 3450 75.00 1090.65 1092.76 1093.32 0,52 6.31 5.60 1093.41 0.009348 22.70 22.87 0.81 0.88 0.19 1090.65 Upstream 3450. 120.00 92.33 0.67 0.07 0.36 101.39 0.28 0.006473 3450 275.00 1090 65 1094.80 1095.18 0.54 0.13 1095.51 6.90 109.37 109.54 0.84 1,00 0.45 1090.65 1094.96 0.008897 1094.96 Upstream 3450. 385.00 0.18 0.62 7.36 132.53 0.86 480.00 1090,65 1095.16 1095.16 1095.76 0.008942 0.009276 7.91 154.96 120.00 0.88 1.24 0.68 0.24 0.72 1095.35 1095.35 1096,01 Upstream 3450 590.00 1090,65 1092.67 1.03 1091.96 0.013950 6.55 11.45 8.07 0.97 1.03 75.00 1090.00 3400. 1092.01 Upstream 1.28 15.98 9.28 1,01 7.51 1090.00 1092,53 1092.53 1093.41 0.014534 120.00 7.16 7.16 46.24 35,38 0.97 1.14 0.55 0.92 1093.95 1093.95 0.01227 3400 275.00 1090.00 151.50 0.19 0.38 0.88 1.07 0.31 101.96 385.00 1090.00 1094 38 1094.52 1095.06 0.009294 7.76 126.78 159.09 0.91 1.22 0.43 0.28 0.48 0.009881 1094.69 1094.54 3400. 480.00 1090.00 0.58 0.94 166.80 1.36 3400, 590.00 1090.00 1094.71 1094.88 1095.51 0.010234 8.29 154.39 Upetream 4.47 18.52 0.83 0.54 0.54 16.78 0.010154 75.00 1090.00 1091 67 1091.98 Upstream 3350 1091.87 7.04 10.67 17.04 18.66 1.30 1.33 1,33 0.024951 1092.45 Upstream 3350. 120.00 1090.00 1091.68 1.77 25.76 2.85 275.00 1090 00 1092.10 1092.67 1093 87 0.043413 22.81 2.85 Upstream 10.24 37.61 27 45 1.54 2.46 2.46 0.03096 1093.10 1094.20 Upstream Upstream 3350. 385.00 1090.00 1092.57 31.30 2.18 1.39 2.18 48.77 480.00 1092.95 1093.48 1094.46 0.024148 9.84 0.01967 9.64 65.58 59.71 1.28 2.01 0.23 1,29 1094.75 Upstream 3350. 590.00 1090.00 1093.32 1093.82 2.84 26.45 33.50 0.58 0.22 0.22 1091.59 0.004664 Ucstraam 3300 75.00 1090.00 1091.47 41.59 0.44 0.17 1091 40 1092 09 0 002574 2.62 45.81 120.00 1090.00 3300 Upstream 0.001117 2.61 132.70 115.79 0.32 0.14 0.04 0.03 0.08 3300 275.00 1090.00 1093.12 1091.98 1093.22 0.07 385.00 1090.00 1092.3 1093.72 0.000983 2.82 201.37 167.65 0.31 0.15 0.05 0.04 3300. Upetream 3.00 190.54 0.31 0.16 0.06 0.05 0.08 Upstream 3300 480.00 1090.00 1093.92 1092.53 1094.04 0.00095 0.09 0.000950 0.32 0.06 3.20 316.28 204.81 0.18 0.07 Upstream 3300. 590.00 1090.00 1094.22 0.66 11.92 0.83 0.66 75.00 1089.00 1090.80 1090.6 1091.22 0.009204 5 19 14.46 3250. Upstream 13.41 0.96 0.96 6.43 18.66 120.00 1089.00 1091.14 1091.08 1091.78 0.011848 7.24 7.29 1092.21 0.010355 40.89 42.82 0.95 1.11 0.07 0.09 0.60 Upstream 3250. 275.00 1089.00 1092.21 0.40 385.00 1089.00 1092.77 1092.77 1093.54 0.007354 Jpstream 1093.12 0.006344 7.43 112.59 114.81 0.79 1.02 0.21 0.24 0.38 Upetream 3250 480.00 1089.00 1093.12 134.34 0.78 1.07 0.25 0 29 0.41 7.72 149.79 590.00 1093.42 1093.42 1094.19 0.005958 Jostraan 0.76 0.76 1089.00 5.31 75.00 1090.12 1090.12 1090.55 0.014684 6.10 5.98 1091.02 0.013659 19.66 17.23 1.01 0.92 0.92 1090.45 Upetream 3200 120.00 1089.00 1090.45 23.96 0.76 0.75 0.75 45.98 Upstream 3200 275.00 1089.00 1091.76 1091 36 1092.31 0.006748 9.13 42 16 23.09 1.19 1.78 1.78 0.016769 1091.8 3200 385.00 1089.00 1091.59 1092.89 54.36 62.58 1.11 0.73 1092 47 1093 31 0.013861 9.07 1.68 Upstream 9.24 84.73 110.04 1 04 1.65 0.14 0.20 0.55 1093.67 0.011686 590.00 1089.00 1092.39 1092.78

Reach	Alver Sta	Q Total	Min Ch El	W.S. Elev	Crtt W.S. (ft)	E.G. Elev	E.G. Slope (fuft)	Vei Chrii (li/s)	Flow Area (sq ff)	Top Width (ft)	Froutie # Chi	Shear Chan (RVsq fl)	Shear LOB (lib/sq ft)	Shear ROB (Ib/sq fi)	Shear Total (ib/eq il)
			4000.00	1090.00	1000.00	1090.04	0.000858	1.50	50.15	48.21	0.25	0.06	ļ		0,06
Upstream Upstream	3150 3150.	75.00 120.00	1088.02 1088.02	1090.00	1089.29 1089.48	1090.75	0.000436	1.42	84.79	50.22	0.19	0.04			0.04
Upstream	3150.	275.00	1088.02	1092.07		1092.11	0.000305	1.63	200.90 244.15	131.46 155.66	0.17	0.05	0.01	0.01	0.03
Upstream Upstream	3150. 3150.	385.00 480.00	1088.02 1088.02	1092.37 1092.59	1090.21	1092.43 1092.67	0.000406	2.02	279.43	171.40			0.02	0.02	0.05
Upstream	3150.	590.00	1088,02	1092.82	1090.64	1092,91	0.000586	2.61	319,93	187.12	0.25	0.12	0.02	0,03	0.06
Upstream	3100.	75.00	1088.00	1089.95		1089.99	0.000838	1.74	43.16	29.45	0.25	0.07			0.07
Upstream	3100	120.00	1088.00	1090,67		1090.73	0.000622	1.83	65.49	32.02	0.23	0.07			0.07
Upstream	3100	275.00 385.00	1088.00	1092.05 1092.35		1092.09	0.000521	1.76	198.70 247.09	151.91 172.34	0.21	0.06	0.00	0.02	0.04
Upstream Upstream	3100,	480.00	1088.00	1092.56		1092.64	0.000708	2,36	285,62	187.33	0.26	0.11	0.01	0.04	0,07
Upstream	3100	590.00	1088.00	1092.78		1092.88	0.000777	2.62	329.38	203.02	0.28	0.13	0.01	0.05	0.08
Upstream	3050.	75.00	1087.00	1089.11	1089.11	1089.82	0.014825	6.76	11.10	7.96	1.01	1.10			1.10
Upstream	3050.	120.00	1087.00	1089.67	1089.67	1090.56	0.014254 0.004694	7.57 6.00	15.85 107.04	9.08 152.27	1.01	1.29 0.69		0.15	1.29 0.20
Upstream Upstream	3050 3050	275.00 385.00	1087.00 1087.00	1091.55 1091.79	1091.55 1091.79	1091.99 1092.30	0.005547	6.78	145.03	157.98		0.88		0.25	0.21
Upstream	3050.	480.00	1087.00	1091.95	1091,95	1092.51	0.006414	7.46	169.28	161.51	0.73	1.03 1.18	0.03	0.34 0.43	0.41
Upetream	3050	590.00	1087.00	1092.13	1092,13	1092.74	0.006945	8.03	200.03	171.91	0.76	1.10	0.03	0.43	0.43
Upstream	3000.	75.00	1085.23	1088.79	1087.08	1088.83	0.000454	1.66	45,13	21.16	0.20	0.06			0.06
Upstream	3000. 3000.	120.00 275.00	1085.23 1085.23	1089.34 1090.34	1087.42 1088.33	1089.41 1090.51	0.000588	2.09 3.29	57.35 101.67	22.92 104.99	0.23 0.33	0.08	0.01	0.02	0.08
Upstream Upstream	3000	385.00	1085.23	1090.61	1088.83	1090.86	0.001489	4,11	134.65	133.86	0.39	0.29	0.03	0.04	0.09
Upstream	3000	480.00	1085.23	1090.78 1090.96	1089.21 1089.61	1091.11	0,001879	4.76 5.42	157.94 184.46	145.64 157.85	0.44	0.39	0.05	0.06	0.13 0.16
Upstream	3000.	590.00	1085.23	1090.98											
Upstream	2950	75.00	1087.00	1088.20	1088.20	1088.72	0.014143 0.013250	5.78 6.58	12.98 18.28	12.63 13.83	1.00	0,86 1,02			0.86 1.02
Upstream	2950. 2950.	120.00 275.00	1087.00 1087.00	1088.60 1089.89	1088.60 1089.89	1089.27 1090.37	0.013250	6.05	87.05	122.57	0,72	0.74		0.17	0.28
Upstream	2950.	385.00	1087.00	1090.19	1090.19	1090.70	0.006263	6.58	127.56	140.91 145.77	0.75 0.77	0.85 0.95		0.27 0.35	0.35 0.43
Upstream Upstream	2950 2950.	480.00 590.00	1087.00 1087.00	1090.38 1090.55	1090,38 1090,55	1090.93 1091.16	0.006574 0.007167	7.02 7.64	155.45 180.38	145.77	0.77	1.10	0.03	0.35	0.43
								7.40	40.40	11.92	1.34	1.39			1,39
Upstream	2900.	75.00 120.00	1085,68 1085,68	1086.66 1086.99	1086.85 1087.25	1087.45 1088.05	0.026790	7.16 8.29	10.48 14.48	12.40	1.35	1.71			1,71
Upstream	2900.	275.00	1085.68	1087.89	1088.52	1089.59	0.022418	10.45	26,33	13.75	1.33	2.34			2.34
Upstream	2900. 2900.	385.00 480.00	1085.68 1085.68	1088,56 1089,00	1089.04 1089.37	1090.02	0.016587 0.012417	9.93 9.70	50.45 76.92	51.37 70.69	1.18 1.05	2.01 1.81	0.11 0.21	0.42	0.98 0.82
Upstream Upstream	2900	590.00	1085.68	1089.42	1089.68	1090.60	0.009770	9.51	113.41	94.27	0.96	1.65	0.31	0.53	0.72
	2650.	75.00	1085.00	1085.96	1086.18	1086,70	0.043995	6,89	10.89	19.88	1.64	1,48			1.48
Upstream Upstream	2850.	120.00	1085.00	1085.96	1086.46	1086.92	0.015265	5.57	21.55	24.40	1,04	0.83			0.83
Upstream	2850.	275.00	1085.00	1086.72	1087.15	1088.14	0.035285	9.57 10.90	28.73 35.31	27.06 29.27	1.64 1.75	2.30 2.86			2.30 2.86
Upstream Upstream	2850. 2850.	385.00 480.00	1085.00 1085.00	1086.95 1087.16	1087.55 1087.86	1088.80	0.038674 0.036542	11.57	41.64	32.86	1.74	3.08		0.15	2.84
Upstream	2850.	590.00	1085.00	1087.39	1088.17	1089.66	0.033335	12.11	51.05	46.32	1.70	3.23		0,34	2.26
Upstream	2900.	75.00	1084.00	1085.54	1084.92	1085.66	0.002248	2.71	27.69	21.61	0.42	0,17			0.17
Upstream	2800.	120.00	1084.00	1086,15	1085.22	1088.28	0.001780	2.88	42.12	27.87	0.39	0.18		0.02	0.16
Upetream Upstream	2800. 2800.	275.00 385.00	1084.00	1087.51 1088.07	1086.00 1086.46	1087.68 1088.28	0.001401	3.36 3.74	96.34 137.16	62.38 88.60	0.37	0.21	0.00	0.05	0.13
Upstream	2800.	480.00	1084.00	1088.43	1086.82	1088.67	0.001350	4.05	170.28	94.95	0.38	0.28	0.05	0.09	0.15
Upstream	2800.	590.00	1084.00	1088.79	1087.22	1089.05	0.001387	4.38	204.85	101.15	0.39	0.32	0.07	0.11	0.17
Upstream	2750	75.00	1083.00	1085.31		1085.48	0.002778	3.24	23.15	15,46	0.47	0.24			0.24
Upstream Upstream	2750. 2750.	120.00 275.00	1083.00 1083.00	1085.92 1087.26		1086,13 1087,54	0.002541	3.62 4.28	33.18 68.96	17.37 52.05	0.46 0.49	0.28 0.36	0.02	0.03	0.28 0.21
Upstream	2750.	385.00	1083.00	1087.82		1088.14	0.002384	4.68	105.34	81.12	0.48	0.40	0.06	0.07	0.19
Updream	2750	480.00	1083.00 1083.00	1088.16 1088.52		1088.53 1088.92	0.002376	5.04 5.36	137.16 174.85	100.08 113.43	0.49 0.50	0.45 0.49	0.09 0.11	0,10	0.20
Upstream	2750.	590.00	1083.00	1006.52		1000.52									
Upstream	2700.	75.00	1083.00	1084.88		1085.25	0.006807	4.88 6,32	15,36 18,99	9.45 11.78	0.68	0.55 0.92			0.55 0.92
	2700. 2700.	120.00 275.00	1083.00	1085.23	1086.37	1085.85 1087.25	0.010969	7.60	41.80	37.63	0.90	1.19	0.21	0.12	0.66
Upstream	2700.	385.00	1083.00	1086.82	1086.82	1087.86	0.009810	8.43 8.28	60.96 92.10	46.72 74.93	0.91	1.38	0.42 0.49	0.25 0.21	0.75 0.55
Upstream Upstream	2700. 2700.	480.00 590.00	1083.00 1083.00	1087.34	1087.34	1088.28 1088.67	0.007474	8.62	122.80	93.17	0,81	1.31	0.56	0.27	0.56
						400.	0.014925	5.26	14.27	17.04	1.01	0.75			0.75
Upstream Upstream	2650. 2650.	75.00 120.00	1083.00 1083.00	1084.34	1084.34	1084.77 1085.22	0.013753	5.26	20.11	18.56	1.01	0.89			0.89
Upstream	2650.	275.00	1083.00	1085,18	1085.54	1086.47	0.023424	9.11	30.20 38.61	21,90 25.11	1,37 1,42	1.93 2.23			1.93 2.23
Upstream Upstream	2650. 2650.	385.00 480.00	1083.00	1085.54 1085.76	1086.03	1087.08 1087.57	0.024272	9.97 10.78	44.51	27.11	1.48	2.55			2.55
Upetream	2650	590.00	1083.00	1086.06	1086.68	1087.99	0.024268	11.16	54,23	54.08	1.46	2.63	0.04	0.08	1.48
Upstream	2600.	75.00	1082.00	1084.04	1083.25	1084.17	0.002064	2.87	31 21	39.45	0.41	0.19	-	0.03	0.10
Upstream	2600.	120.00	1082.00	1084.51	1083.63	1084.66	0.002023	3.27	51.64	47.78	0.42	0.22		0.08	0.13
Upetreem	2600. 2600	275.00 385.00	1082.00 1082.00	1085.66 1086.19	1084.59 1084.97	1085.87 1086.42	0.001890	4.00	115.09	70.14 97.96	0.43	0.30	0.02	0.14	0.19 0.19
Upstream Upstream	2600 2600.	480.00	1082.00	1086.19	1085.23	1086.78	0.002002	4.71	192.37	110.52	0.46	0.39	0.05	0.21	0.21
Upstream	2600.	590.00	1082.00	1086.82	1085.56	1087.12	0.002144	5.16	227.11	125.48	0.48	0.45	0.08	0.25	0.24
Upstream	2550	75.00	1082.00	1083.46	1083.46	1083.93	0.012070	5.64	16.38	20.57	0.94	0.80		0.30	0.57
Upstream	2550.	120.00	1082.00	1084.07		1084.46	0.007230	5.33	30.53 72.10	26.26 52.59	0.75 0.73	0.64 0.79		0.34 0.38	0.49 0.51
	2550. 2550.	275.00 385.00	1082.00	1085.18 1085.70		1085.68	0.006228 0.005984	6.25 6.63	72.10 104.15	52.59 70.28	0.73	0.79		0.38	0.51
Upstream	2550	480.00	1082.00	1086.06		1088,60	0.005774	6.84	134.02	118.93	0.72	0.88	0.02	0.46	0.40
Upstream	2550	590.00	1082.00	1086.43		1086.94	0.005200	6,91	182.13	141.68	0,69	0.87	0.12	0.47	0.41
	2500.	75.00	1081.00	1083.35	1082.53	1083.51	0.002609	3.28	22.87	14.14	0.45	0.24			0.24
Upstream	2500	120.00	1081.00	1083.95		1084.17 1085.39	0.002629	3.74 5.39	32.06 62.30	18.21 45.39	0.47	0 29	0.11		0.29
	2500. 2500.	275.00 385.00	1081.00	1084.95 1085.40		1085.39	0.003622	6.15	100.90	111.84	0.61	0.68	0,13	0.08	0.21
	2500.	480.00	1081.00	1085.86		1086.34	0.003119	6.06	161.20	151.19	0.56	0.63	0.14	0.13	0.20

Reach	Filver Sta	O Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vei Chri	Flow Area	Top Width	Frouds # Chi	Shear Chan	Shear LOB	Shear ROB	Shear Total
Tieraci		(cfs)	(11)	(ft)	(ft)	(ft)	(fi/fi)	(IVs)	(#g #)	(ft) 169,40	0.52	(#t√sq ft) 0.57	(ib/sq fi) 0.17	(lb/sq ft) 0.15	(#b/sq it) 0.21
petream	2500.	590.00	1081.00	1086.31		1086.71	0.002513	5.88	232.94	169.40	0.52	0.57	0.17	0.13	0.21
pstream	2450.	75.00	1081.00	1083.17		1083.37	0.003148	3.59	20.87	12.56	0.49	0.29			0.29
pstream	2450.	120.00	1081.00	1083.74		1084.01	0.003459	4.18 6.20	28.73 63.14	14.73 71.68	0.53 0.67	0.37	0,11	0.13	0.37
pstream pstream	2450. 2450	275.00 385.00	1081.00 1081.00			1085.17 1085.67	0.004967	7.59	83.57	91.26	0.78	1.07	0.19	0.22	0.37
pstream	2450.	480.00	1081.00	1085.01		1086.05	0.008166	8.72	98.23	102,69	0.87	1.39	0.27	0.33	0.48
pstream	2450.	590.00	1081.00	1085.22		1086.41	0.008976	9.56	121.91	119.39	0.93	1.63	0.35	0.42	0,56
petream	2400	75,00	1081.00	1082.42	1082.41	1082.99	0.013950	6.06	12.38	10.67	0.99	0.92			0.92
pstream	2400.	120.00	1081.00	1082.86	1082,86	1083.61	0.013893	6.96	17.25	11.86	1.02	1.13 0.83	0.19	0.08	1.13 0.32
pstream	2400.	275.00 385.00	1081.00	1084.25 1084.60	1084.25 1084.60	1084.83 1085.23	0.006914	6.39 7.01	68.42 101.89	90.47 104.69	0.77	0.96	0.30	0.16	0.41
ostream ostream	2400. 2400	480.00	1081.00	1084.83	1084.83	1085.52	0.006905	7.50	127.89	114.52	0.80	1.06	0,38	0.21	0.47
pstream	2400.	590.00	1081.00	1084.92	1084.92	1085.83	0.008910	8.71	138.59	118.33	0.92	1.41	0.53	0.30	0.64
	2350.	75.00	1080.00	1081.10	1081.10	1081.54	0.014372	5.32	14.09	16.25	1.01	0,76			0.76
petream petream	2350	120.00	1080.00	1081.61	1081.43	1082.04	0.008484	5.27	22.75	17.60	0.82	0.66			0.68
patream	2350.	275.00	1080.00	1083,44	1082.30	1083.76	0.002418	4.62 5.52	68.82 96.19	54.05 89.47	0.48 0.54	0.39	0.05	0.04	0.19
ostream ostream	2350	385.00 480.00	1080.00 1080.00	1083.82 1084.01	1082.79 1083.30	1084.27	0.002521	6.35	114.63	105.24	0.61	0.70	0.13	0.09	0.24
stream	2350	590.00	1080.00	1084.18	1083.85		0.004341	7.23	132,64	109.40	0.68	0.89	0.20	0.15	0.32
				4004.00	4070.00	1081.08	0.000787	1.89	39.69	23.95	0.26	0.08			0.08
stream etream	2300.	75.00 120.00	1079.00 1079.00	1081.02 1081.70	1079.90	1081.08	0.000706	2.11	58.75	26.38	0.25	0.09			0.09
stream	2300	275.00	1079.00	1083.51		1083.60	0.000501	2.42	138.24	103.09		0.10	0.01	0.01	0.04
stream	2300.	385.00	1079.00	1083.94		1084.07 1084.33	0.000618	2.91 3.33	188.48 220.78	132.71	0.26 0.29	0.14 0.18	0.03 0.04	0.02	0.05
stream stream	2300.	480.00 590.00	1079.00 1079.00	1084.18 1084.40		1084.33	0.000749	3.77	253.43	148.48	0.32	0.23	0.06	0.05	0.09
									11.81	9,52	1.00	1.02		ļ	1.02
stream	2250. 2250.	75.00 120.00	1079.00 1079.00	1080.28 1080.75	1080.28 1080.75	1080.91 1081.59	0.015907 0.015574	6.35 7.37	16.28	9.52	1.01	1.27			1.27
stream stream	2250.	275.00	1079.00	1082.08	1082.08	1083.41	0.013944	9.24	30.45	20.34		1.73	0.07	0.04	1.06
stratum	2250	385.00	1079.00		1083.38	1083.95	0.004703	6.88 7.41	132.34 164.58	143.03 149.34	0.59 0.62	0.85 0.97	0.18	0.23	0.26
itream itream	2250. 2250.	480.00 590.00	1079.00 1079.00	1083.60 1083.82	1083.60 1083.82	1084.21 1084.48	0.005484	7.41	197.73	155.56		1.09	0.34	0.38	0.42
50 WHO IS	22.00.	330.00	1070.00												0,18
dream	2200	75.00	1078.70	1080.37	1079.69 1080.01	1080.49 1081.05	0.002215	2.82 3.24	26.59 37.06	19.06 21.24	0.42	0.18 0.23			0.18
stream stream	2200.	120.00 275.00	1078.70 1078.70		1080.01	1081.05	0.002754	4.46	64.43	39.77	0.51	0.39	0.04		0.27
tream	2200.	385.00	1078.70	1080.51	1081.35	1083.19	0.044070	13.14	29.29	19.61	1,89	3.91 3.58			3.91
draam	2200	480.00	1078.70	1080.90	1081.75 1082.48	1083.48 1083.75	0.034663	12.90 12.40	37.21 47.57	21.27 23.21	1.72 1.53	3.58			3.15
tream	2200.	590.00	1078.70	1081.36	1002.40	1003.73	U.UZUTUZ	12.70							
tream	2150.	75.00	1078.00	1079.76		1080.19	0.009011	5.24	14.84	15.47	0.82 0.85	0.66 0.82	0.07		0.51
draam	2150.	120.00	1078.00	1080,19 1081.21	1081.21	1080.74	0.009379	6.02 7.11	23.22 60.65	23.25 68.55		1.02	0.43	0.10	0.44
tream tream	2150. 2150.	275.00 385.00	1078.00 1078.00	1081.64	1081.64	1082.37	0.007428	7.63	96.25	100.29		1,11	0.53		0.44
ream	2150.	480.00	1078.00	1082.02	1082.02	1082.67	0.006097	7.56	141.64 174.22	134.17 139.23	0.76 0.78	1.04	0,53 0.59	0.22	0.40 0.48
Iream	2150	590.00	1078.00	1082.26	1082.28	1082.94	0.006189	8.01	174.22	139.23	0.78	1.14	0.00	0.01	
tream	2100.	75.00	1078.00	1079.67		1079.81	0.002698	2.98	25.19	19.62	0.46	0.21			0.21
ream	2100.	120.00	1078.00	1080.11		1080.30	0.003190	3.48 4.92	34.70 68.40	27.40 63.16	0.51 0.60	0.28 0.49	0,02	0.07	0.25
lream Iream	2100	275.00 385.00	1078,00 1078,00	1080.88 1081.25	1080.31 1080.75	1081.24	0.004039	5.66	95.28	82.34	0.63	0.61	0.15	0.13	0.29
ream	2100.	480.00	1078.00	1081.51	1081.08	1082.05	0.004215	6.19	119.77	101.89	0.66	0.70	0.16 0.20	0.18	0.31
ream	2100.	590.00	1078,00	1081.79	1081.40	1082,40	0.004281	6.65	151.70	124.46	0.67	0.79	0.20	0.21	0.52
tream	2050.	75.00	1077.88	1079.46	<del></del>	1079.63	0.003994	3.29	22.82	20.55	0.55	0.27			0.27
tream	2050.	120.00	1077.86	1079.90		1080.11	0.003869	3.68	33.08	27.48 83.90	0.56 0.56	0.32 0.43	0.04	0.10	0.28
tream	2050. 2050	275.00 385.00	1077.86 1077.86	1080.73		1081.04 1081.49	0.003352	4,64 5,10	88.57 125.58	95.85	0.56	0.49	0.19	0.15	0.26
tream tream	2050.	480.00	1077.86	1081.44		1081.81	0.003176	5.46	154.69	104,22	0.57	0.54	0,24	0.18	0.29
tream	2050.	590.00	1077.86			1082,15	0.003193	5.85	188.56	113.35	0.58	0.60	0.27	0.21	0.33
tream	2000	75.00	1077.00	1078.75	1078.75	1079.24	0.013659	5.74	14.77	16.34	0.99	0.84	0.40		0.72
tream	2000	120.00	1077.00	1079.19	- 1079,19	1079,73	0.013844	6.05	23.15	24.54	1.01	0.91	0.47	0.11	0.77
певл	2000.	275.00	1077.00	1080.09 1080.46	1080.09 1080.48		0.008564	6.87 7.57	62.73 88.67	63.59 78.29	0.87 0.88	0.98 1.12	0.36 0.47	0.11	0.51
ream	2000. 2000	385.00 480.00	1077.00 1077.00	1080.46	1080.46		0.007911	8.01	112.14	89.20	0.88	1.21	0.54	0.25	0.61
ream	2000.	590.00	1077.00		1081.02		0.007706	8.47	138.52	99.99	0.89	1.31	0.61	0.31	0.65
ream	1950.	75.00	1076.00	1078.09	1077.38	1078.19	0.001980	2.61	32.12	26.82	0.40	0.16	0.08		0.14
ream	1950	120.00	1076.00	1078.59	1077.69		0.002121	2.88	47.36	34.55	0,42	0.19	0.12		0.17
tream	1950.	275.00	1078.00		1078.54		0.002056	3.66 3.81	97.55 149.94	77.68 97.88		0.27 0.27	0.09 0.12	0.03	0.16 0.15
meen meen	1950. 1950.	385.00 480.00	1076.00 1076.00		1078.90 1079.25		0.001707	4.19	178.79	105.66		0.31	0.14	0.08	0.18
ream	1950	590.00	1076.00		1079.51	1081.07	0.001656	4.45	218.63	115.56	0.43	0.34	0.16	0.10	0.19
				1077.10	1077.10	1077.05	0.013433	5.66	14.58	16.84	0.97	0.82	0.29		0.68
tream tream	1900. 1900.	75.00 120.00	1076.00		1077.46 1077.85	1077.95 1078.45	0.013433	6.32	21.85	20.35	0.98	0.96	0,46		0.81
nam	1900	275.00	1076.00	1078.77	1078.77	1079.50	0.012000	7.14	47.07	35.99 39.87	0.99 1.18	1.13 1.70	0.59 0.83		0.92
tream	1900. 1900.	385.00 480.00	1076.00 1076.00		1078.95 1079.55	1080.09 1080.45	0.016526	8.89 8.05	54.15 86.18	39.87 62.07	1.18 0.93	1.70	0.83	0.18	0.77
tream tream	1900.	590.00	1076.00	1079.55	1079.86	1080.43	0.008726	8,49		70.52	0.92	1.36	0.61	0.25	0.80
									10.40	16.45	0.84	0.67	0.30		0.58
tream	1850.	75.00	1075.00 1075.00	1076.83 1077.34	1076.70	1077.24	0.009557	5.21 5.50	16.43 25.94	16.43 21.60	0.84	0.67	0.30		0.54
tream tream	1850. 1850.	120.00 275.00	1075.00	1077.34	1077.14		0.012171	7.39	47 72	44.69	1.01	1.19	0.51	0.04	0.78
tream	1850.	385.00	1075.00	1078.62	1078.62	1079.39	0.008743	7.49	78.33	74.55 73.50	0.90 1.16	1.12 1.85	0.51 0.85	0.18 0.26	0.56
tream	1850.	480.00	1075.00 1075.00	1078.58 1078.81	1078.91 1079.18	1079.84	0.014661	9.57	75.26 92.42	73.50 79.21	1.18	2.07	0.85	0.26	1.05
tream	1850.	590.00	1075.00	10.001	107 9, 18	1000 22	0,014000								
tream	1800	75.00	1075.00	1076.88		1076.96	0.001743	2.38	36.99	33.83 57.07	0.37	0.13 0.14	0.07 0.06		0.12 0.10
	1800.	120.00	1075.00	1077.42		1077.51	0.001569	2.53	60.68 129.23	140.64	0.36 0.43	0.14	0.06	0.01	0.10
stream stream	1800.	275.00	1075.00	1078.20	1077.22	1078.36	0.002028	3.46	125.23				0 001	0.071	

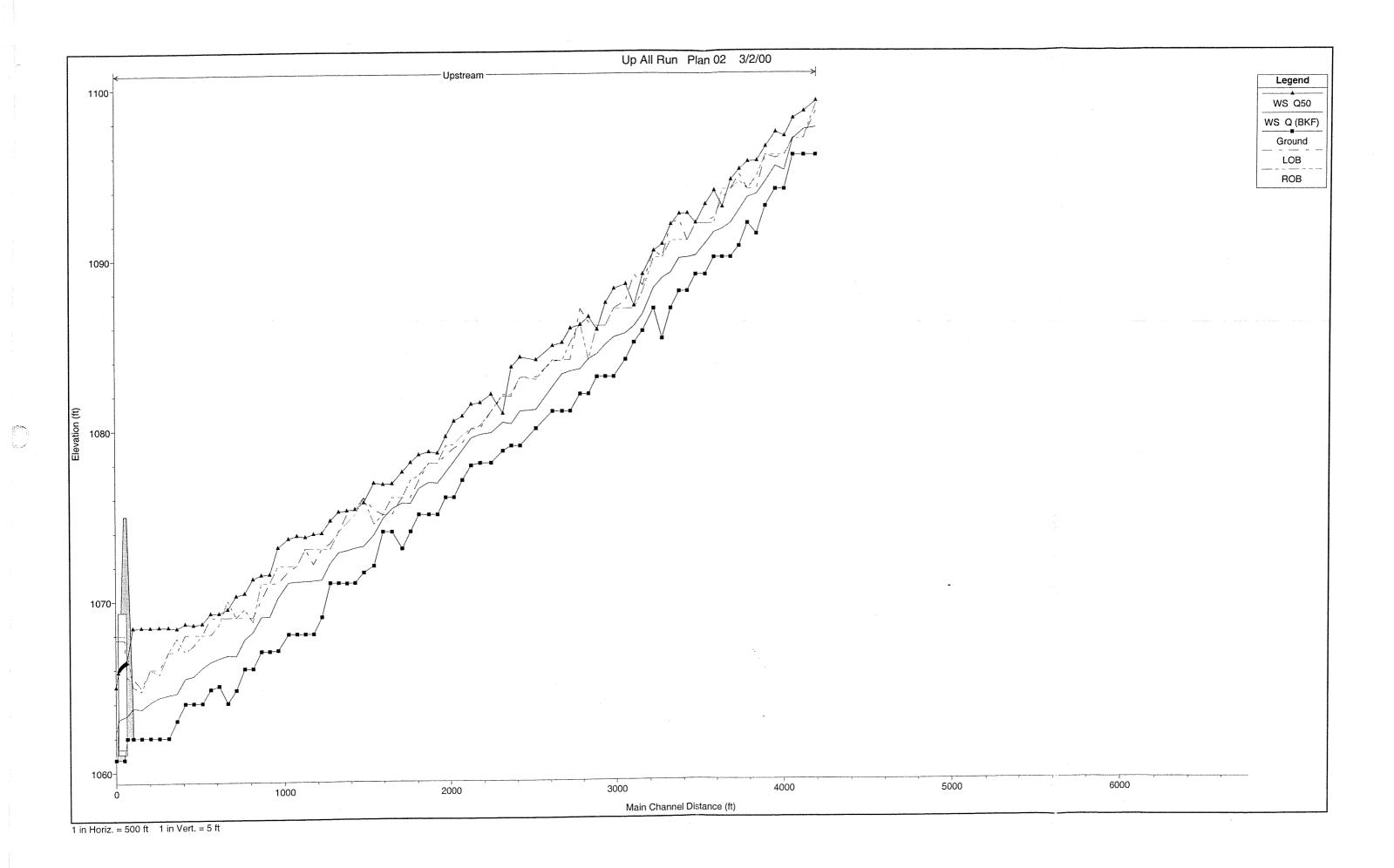
each River Sta	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Stope	Vel Chni	Flow Ama	Top Width	Froude # Chl	Shear Chan	Shear LOB	Shear ROB	Shear Total
	(cfs)	(m)	(ft)	( <b>ft)</b>	_(#)	(f\/ft)	(IVs)	(ii pa)	(P):		(Rñ(11)	(lb/sq lt)	(lb/sq ft)	(it pevdi)
eam 1800.	480.00	1075.00	1078.67	1077.90	1078.90	0.002464	4.40	202.49 237.65		0.49	0.37	0.16	0.05	0.1
eam 1800	590.00	1075.00	1078.87	1078.31	1079.14	0.002041	4,13	207.03	17.5.40		0.70	V.2.		
еат 1750.	75.00	1075.00	1078.52		1076.77	0.006005	3.98	18.84			0,40			0.4
eam 1750.	120.00	1075.00	1077.13		1077.36	0.004158	3.82	37.99		0.58	0.34	0.03	0.04	0:1 0.1
eam 1750 eam 1750.	275.00 385.00	1075.00 1075.00	1078.04 1078.30		1078.23 1078.53	0.002390 0.002706	3.93 4.52	140.59 185.83			0.31	0.13 0.18	0.04	0.1
eam 1750.	480.00	1075.00	1078,49		1078.75	0.002932	4.95	219.88	+		0.46	0.22	0,12	0.2
sara 1750.	590.00	1075.00	1078,68		1078.97	0.003162	5,38	255.54	190.78	0.57	0.53	0.27	0.16	0.2
								44.00		100	101			10
eam 1700	75.00 120.00	1074.00	1075.65 1076.18	1075.65 1076.18	1076.29 1076.97	0,014251	6.42 7.13	11.68 17.52			1.01	0.10		1.0 0.7
eam 1700.	275.00	1074.00	1077.57	1077.57	1078.03	0.004940	6.40	114.83		+	0.77	0.21	0.11	0.2
sam 1700	385.00	1074.00	1077.88	1077.88	1078.33	0.004956	6.84	168.41	182.19		0.85	0.27	0.19	0.2
eam 1700.	480.00	1074.00	1078.04	1078.04	1078.53	0.005503	7.44	198.22	187.90			0.35	0.26	0.3
am 1700.	590.00	1074.00	1078.20	1078.20	1078.74	0.006116	8.08	228.18	193.45	0.75	1.15	0.44	0.34	0.4
am 1650.	75.00	1073.00	1075.68	1074.13	1075.73	0.000539	1.81	46,96	38.71	0.21	0.07	0.01		0.0
m 1650.	120.00	1073.00	1076.09	1074.46	1076.17	0.000768	2.36	66.36	61.23	0.26	0.11	0.02	0.00	0.0
ım 1650.	275.00	1073.00	1076.86	1075.39	1077.03	0.001294	3.65	145.71	140.32	0.35	0.24	0.07	0.03	0.0
m 1650	385.00	1073.00	1077.22	1075.98	1077.43	0.001478	4.18	201.48		0.38	0.30 0.35	0,10 0,13	0.06	0.1
n 1650. n 1650.	480,00 590,00	1073.00 1073.00	1077.48 1077.75	1076,48 1078,90	1077.72 1078.00	0.001611	4.56 4.94	244.39 291.31	172.43 184.52	0.40	0.40	0.16	0.03	0.1
n 1850	390.00	1073.00	1077.73	1079.20	1070.00	0.001750	4,54		75.132					
n 1600.	100.00	1074.00	1075.34	1075.16	1075.61	0.006902	4,19	27.59	43.40	0.72	0.44	0.09		0.2
n 1600.	163.00	1074.00	1075,59	1075.52	1076.01	0.008875	5.36	39.78	57.71	0.84	0.68	0.18		0.3
1 1600	375.00	1074.00	1076.29	1076.29	1076.82	0.007617	6.52 7.48	108.75 142.24	127.08 136.59	0.84	0.88	0.37 0.52	0.18	0.4
1600.	525.00 650.00	1074.00	1076.55	1076.55 1076.81	1077.20	0.008468	7.48	179.60	152.09	0.89	1.16	0.55	0.36	0.5
1600	805.00	1074.00	1077.19	.,,,,,,,,	1077.78	0.006237	7.64	241.33	169.24	0.81	1.06	0.53	0.38	0.5
1550. 1550.	100.00	1074.00	1074.77	1074.77	1075.08	0.014564	4.49	24.29	43.50	0.98	0.59	0.22 0.17		0.5
1550 1550	163,00 375.00	1074.00	1075.03 1075.42	1075.03 1075.59	1075.41 1076.20	0.012978	5.07 7.49	36.72 71.23	64.24 101.81	1,18	1.33	0.17	0.24	0.4
1550.	525.00	1074.00	1076.28	1075.91	1076.63	0.004336	5.35	176,19	145.20	0.65	0.57	0.26	0.15	0.3
1550.	650.00	1074.00	1076.77	1075.99	1077.05	0.002829	4.97	252.14	166.30	0.54	0.48	0.24	0,11	0,2
1 1550	805.00	1074.00	1077.24		1077.50	0.002182	4.87	335.41	184.26	0.49	0.42	0.24	0.12	0.2
1500		4070.00	4070.00	4070.00	1070.00	0.000856	1.59	63.00	53.03	0.26	0.06			0.0
1500	100.00	1072.00	1073.82 1074.38	1072.88 1073.25	1073.66	0.000685	1.73	94.08	58,48	0.24	0.07			0.0
1500.	375.00	1072.00	1075.72	1073.78	1075.79	0.000494	2.06	190.14	84.17	0.22	0.08	0.01	0.02	0.0
1500	525.00	1072.00	1076.41		1076.49	0.000441	2.27	252.49	98.38	0.22	0.09	0.01	0.02	0.0
1500.	650.00	1072.00	1076.85		1076.95	0.000441	2.46	298.24	109,42	0.22	0.10	0.02	0.03	0.0
1500.	805.00	1072.00	1077.30		1077.41	0.000459	2.70	349.21	120.38	0.23	0.12	0.03	0.03	0.0
1450	100.00	1071.61	1073.15	1073.15	1073.68	0.013727	5.82	17.18	16.56	1.01	0.86			8.0
1450	163.00	1071.61	1073.58	1073.58	1074.25	0.012763	6.58	24.75	18.69	1.01	1.02			1.0
1450.	375.00	1071.61	1074.62	1074.62	1075.61	0.011323	8.00	46.87	23.96	1.01	1.32			1,3
1450.	525.00	1071.61	1075.24	1075.24	1076.32	0.010888	8.35	62.91 78.23	29.36 36.60	1.00	1.39			1.3
1450 1450.	650.00 805.00	1071.61	1075.70 1076.14	1075.70	1076.77	0.010747	8.31 8.39	99.33	68.26	0.97	1.37	0.04	0.08	0.8
1450	005,00	1011.01	1070.14	7070.14										
1400.	100.00	1071.00	1073.05	1072.28	1073.19	0.002332	3.02	33.08	22.56	0.44	0.21			0.2
1400	163,00	1071.00	1073.59	1072.69	1073.78	0.002466	3.53	46.24	26.06	0.47	0.26			0.2
1400.	375.00 525.00	1071.00	1074.76	1073.67 1074.19	1075.10 1075.61	0.002787	4.63 5.63	81.07 95.07	33.15 52.32	0.52 0.61	0.41		0.02	0.4
1400.	650.00	1071.00	1075.12	1074.56	1075.96	0.004543	6.46	109.60	103.30	0.68	0.76		0.04	0.3
1400	805.00	1071.00	1074.47	1074.97	1076.44	0.018123	11.28	71,47	31.36	1.31	2.48			2.4
1350.	100,00	1070.98	1072.90		1073.06	0.002721	3.23	30.94 42.70	21.42	0.47	0.24			0.2
1350.	163.00 375.00	1070.98	1073.42 1074.60		1073.64	0.002855	4.85	105.92	112.41	0.54	0.45		0.07	0.1
1350.	525.00	1070.98	1074.99		1075.42	0.003361	5.54	157.39	158.21	0.58	0.56		0.12	0.2
1350.	650.00	1070.98	1075.23		1075.71	0.003493	5.97	198.30	168.58	0.60	0.64	0.02	0.17	0.2
1350.	805.00	1070.98	1075.51	1075.19	1076.02	0.003554	6.38	245.39	173.75	0.62	0.70	0.05	0.23	0.3
1300.	100.00	1071.00	1072.79		1072.93	0.002293	3.03	33.02	22.02	0.44	0.21			0.2
1300.	163,00	1071.00	1073.30		1073.50	0.002542	3.63	44.86	24.47	0.47	0.28			0.2
1300.	375.00	1071.00	1074.51		1074.81	0.002302	4.52	128.59	165.77	0.48	0.38	0.04	0.05	0.1
1300	525.00	1071.00	1074.92		1075.25	0.002324	4,98 5.38	198.61 242.98	176,98 181,44	0.49	0.44	0.07	0.11	0.1
1300. 1300.	650.00 805.00	1071.00	1075.17 1075.44		1075,53	0.002454	5.80	292.60	185.31	0.53	0.56	0.12	0.13	0.2
1300.	003.00	107 1.00	1010.44		1070.00									
1250.	100,00	1071.00	1072.16	1072.16	1072.68	0.013826	5.68	17.62	17.82	1.01	0.83			0.8
1250.	163,00	1071.00	1072.57	1072,57	1073.22	0.012764	8.46	25.22	19.66	1.01	0.99			0.9
1250.	375.00	1071.00	1073.54	1073.54	1074.52	0.010931	8.00 6.88	50.13 142.37	34.67 162.22	1.00 0.72	1.31 0.86	0.07	0.25	0.9
1250. 1250.	525.00 650.00	1071.00	1074.41	1074.65	1075.33	0.005021	7.29	182.91	166.78	0.73	0.94	0.19	0.25	0.3
1250.	805.00	1071.00	1074.90	1074.90	1075.62	0.005216	7.82	224.20	171.31	0.75	1.05	0.24	0.33	0.4
1200.	100.00	1069.00	1071.18	1070.75	1071.43	0.005313	3.99	25.05 44.23	20.69 25.60	0.64	0.39			0.3
1200.	163.00 375.00	1069.00	1072.01	1071.22	1072.22	0.002836	3.69 4.48	88.04	64.45	0.49	0.29	0.02	0.03	0.2
1200.	525.00	1069.00	1073.66	1072.74	1074.09	0.002007	5.33	119.42	102.85	0.56	0.52	0.07	0.06	0.2
1200. 1200.	650.00	1069.00	1073.92	1073.09	1074.44	0.003387	5.90	149.70	131.05	0.59	0.62	0.11	0.10	0.2
1200	805.00	1069.00	1074.23	1073.60	1074.81	0.003494	6.39	197.22	164.84	0,61	0.70	0.14	0.14	0.2
	I					0.004711	2.80	35.75	21.02	0.38	0.17			0.1
1150. 1150.	100.00	1068.00	1071.13		1071.25	0.001710	2.80	35.75 55.36	21.02	0.38	0.17			0.1
1150. 1150.	375.00	1068.00	1073.23		1073.47	0.001578	4.02	114.65	112.57	0.40	0.29	0.06	0.02	0.1
1150.	525.00	1068.00	1073.61		1073.94	0.001946	4.81	162.00	139.45	0.45	0.40	0.10	0.06	0.1
1150,	650.00	1068.00	1073.87		1074 27	0.002181	5.34	201.17	159.16	0.48	0.48	0.13	0.09	0.1
1150.	805.00	1068.00	1074.18		1074 63	0.002311	5.80	253.32	171.68	0.51	0.55	0.16	0.13	0.21
1100.	100.00	1068.00	1071.10		1071.18	0.000833	2.32	43.10	19.13	0.27	0.11			0.11
200000000000000000000000000000000000000			1071.93		1072.04	0.000917	2.69	60.50	22.95	0.29	0.14			0.14
1100.	163.00	1068,00												

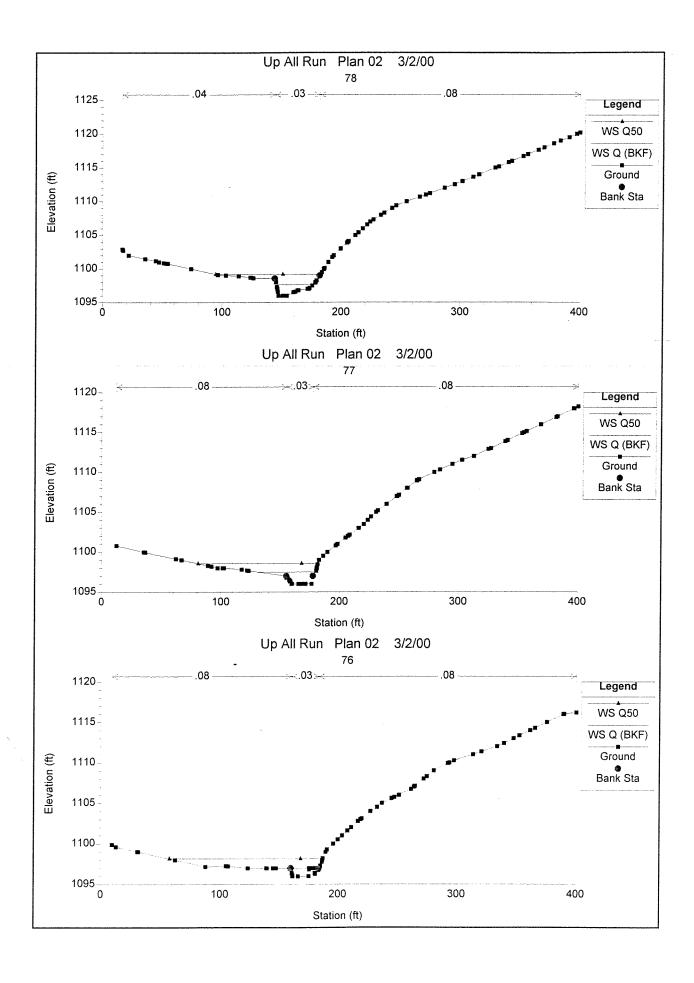
ach	River Sta	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chril (II/s)	Flow Area (sq II)	Top Width	Froude # Chi	Shear Chan (RVsq ft)	Shear LOB (lit/sq ft)	Shear ROB (Ib/sq ft)	Shear To (ib/eq it
	1470	(cfs)	(ft) 1068.00	(ft) 1073.47	(ft)	(株) 1073.84	(II/ft) 0.002092	(IVE) 4.97	145.96	(ft) 131.74	0.46	0.42	0.03	0.06	104.04.11
am am	1100. 1100	525.00 650.00	1068.00	1073.47		1074.15	0.002467	5.61	176.05	140.36	<del> </del>	0.53	0.05	0.10	
	1100.	805.00	1068.00	1073.94		1074.49	0.002840	6,29	212.05	149.51	0.55	0.85	0.08	0.15	
************	1050.	100.00	1068.00	1071.07		1071.14 1072.00	0.000655	2.11	47.38 65.14	20.34 22.74	0.24	0.09			
	1050 1050	163.00 375.00	1068.00 1068.00	1071,90 1073.16		1073.31	0.000776	3.31	215.78	147.02		0.18	0.02	0.05	
3013	1050.	525.00	1068.00	1073.53		1073.72	0.000995	3.97	270.54	155.24	0.33	0.25	0.03	0.08	
em	1050.	650.00	1068.00	1073.77		1074.00	0.001169	4,46	308.85	160.58	0.36	0.31	0.05	0.11	
an	1050	805.00	1068.00	1074.04		1074.32	0.001355	4.98	352.95	166.08	0.39	0.38	0.07	0.15	
	1000	100.00	1068.00	1071.02		1071.11	0,000816	2.31	43.24	18.80	0,27	0.11			
am am	1000. 1000	163.00	1068.00	1071.84		1071.95	0.000010	2.68	60.82	23.44	0.29	0.14	0.00		
am	1000	375.00	1068.00	1073.08		1073.26	0.000992	3.60	181.77	119,10	0.32	0.22	0,06	0.06	
am.	1000.	525.00	1068.00	1073.40		1073.65	0.001350	4.43	220,60	125.47	0.38	0.32	0.10	0.10	
***********	1000.	650.00	1068.00	1073.60		1073.92	0.001670	5.08	245.80	129.30	0.43	0.41	0,13	0.15	
am	1000.	805.00	1068.00	1073.81		1074.22	0.002066	5.83	273.05	133.32	0.46	0.54	0.10	0.20	
am	950.	100.00	1067.05	1070.15	1070.15	1070.90	0.022725	6.95	14.39	9.61	1.00	1.27			
	950	163.00	1067.05	1070.78	1070.76	1071.71	0.022155	7.83	20.81	11.22	1.01	1.51			
am	950.	375.00	1067.05	1072.58	1072.58	1073.09	0.008120	8.54	113.81	125.71	0.65	0.90	0.39	0.30	-
am	950.	525.00	1067.05	1072.87	1072.87	1073,45	0.009361	7.34	152.49 181.92	134.88 140.56	0.70	1.11	0.54	0.49	
am .	950. 950	650.00 805.00	1067.05 1067.05	1073.09 1073.27	1073.09	1073.95	0.010016	8.52	208.68	144.32	0.77	1.46	0.80	0.86	
anı	3,0	505.00	1007.00	1070.27	70.02										
am	900.	100,00	1067.00	1069.04	1068.59	1069.44	0.006440	5.07	19,74	11.34	0.68	0.58			
(1.000 (1	900.	163.00	1067.00	1069.75	1069,17	1070.26	0.006271	5.74	28.41	13.06	0.69 1.43	0.69 3.12			
	900.	375.00	1087.00	1069.92	1070.61	1072.25 1072.79	0.027155	12.25	30.60 66.78	13.50 118.19	1.43	2.00	0.11	0.14	<del></del>
em am	900. 900.	525.00 650.00	1067.00	1071.18	1071.77	1072.79	0.013237	10.29	107.22	128.82	1.02	2.04	0.24	0.37	
	900.	805.00	1067.00	1071.84		1073.32	0.011176	10.79	150.65	135.84	1,00	2.08	0.37	0.56	
	850.	100.00	1067.00	1069.03		1069.19	0,002315	3.28	30.68	17.71	0.44	0.23	0.01		
	850.	163.00	1067.00 1067.00	1069.81	1069.75	1070.01 1071.40	0.001964	3.62 5.19	45.94 91.30	28.39 143.63	0.50	0.48	0.15	0.00	
	850. 850	375.00 525.00	1067.00	1071.33	1070.45	1071.89	0.003407	6.31	139.69	151.46	0.58	0.69	0.21	0.07	
	850.	650.00	1067.00	1071.48	1070.93	1072.20	0.004318	7.29	181.76	154.17	0.66	0.90	0.29	0.13	
	850.	805.00	1067.00	1071.70	1071.70	1072.55	0.004914	8.08	197.60	158.48	0.71	1.09	0.37	0.21	
						4000.00	0.044407	0.00	14.37	9.74	1.01	1,13			
	800	100.00	1066.00	1068.15 1068.75	1068.15 1068.75	1068.90 1069.73	0.014127 0.013517	6,96 7.92	20.57	10.70	1.01	1.13			
**********	800. 800.	163.00 375.00	1066.00	1070.42	1070.42	1071.18	0.005840	7.80	104.23	102.30	0.73	1.08	0.26	0.26	
	800.	525.00	1066.00	1070.90	1070.90	1071.65	0.005629	8.33	160,58	129.36	0.73	1.18	0.33	0.35	
	800	650.00	1066,00	1071.25	1071.25	1071.98	0.005198	8.47	210.66	148.78	0.71	1.19	0.32	0.40	
um .	800.	805.00	1066.00	1071.51	1071.51	1072.26	0.005602	9.13	248.61	153.65	0.75	1.35	0.36	0.52	
	ne.	100,00	1066.00	1067.73	1067.60	1068.16	0.009640	5.25	19.06	16.41	0.86	0,67			
	750. 750	163.00	1066.00	1068.48	1068.03	1068.87	0.005461	5.01	32.55	19.33	0.68	0.55			
	750.	375.00	1066.00	1070.01	1069.11	1070.46	0.003223	5.50	90.76	97.50	0.57	0.55	0.10	0.06	
m	750.	525.00	1066.00	1070.23	1069.94	1070.93	0.004875	6.95	113.66	113.64	0.69	0.86	0,18	0.12	
	750.	650.00	1068.00	1070.41	1070.39	1071.29	0.005568	7,89	135.95 155.45	127.14 137.57	0.76 0.86	1.08	0.25	0.19	
un .	750	805.00	1066.00	1070.56	1070.77	1071.70	0.007009	9.11	133.43	107.07	0.00				
un.	700.	100.00	1064.75	1066,75	1066,75	1067.53	0.014570	7.12	14.05	9.06	1.01	1.18			
	700.	163.00	1064.75	1067.39	1067.39	1068.40	0.013987	8.04	20.28	10.25	1,01	1.40			
	700	375.00	1064,75	1069.58	1069.58	1070.24	0.005158	6.97	103.92	127.48	0.65	0.88	0.09	0.17	
	700.	525.00	1064.75	1069.99	1069.99	1070.68	0.005287	7.59	160.51 201.50	148.22 162.61	0.67 0.69	1.01	0.16	0.29	
	700.	650.00	1064.75	1070.28	1070.26 1070.51	1070.96 1071.27	0.005465	8.06 8.65	245.14	177.02	0.72	1.26	0.26	0.46	
m	700.	805.00	1064.75	1070.51	1070.31	10/1.2/	0.003020								
m	650.	100,00	1064.00	1066.78	1065.83	1068.97	0.002342	3,49	28.66	14.62	0.44	0.26			
n	650.	163.00	1064.00	1067.34	1068.34	1067.62	0.002895	4.33	42.32	31.61	0.50	0.37	0.06		
	650.	375.00	1064.00	1068.86	1067.73	1069.23	0.002819	5.14 6.42	98.43 133.20	44.47 157.82	0.51 0.62	0.48	0.23	0.04	
	650.	525.00 650.00	1064.00	1069,19 1069,48	1068.33 1068.75	1069.75	0.004024	6.86	182.51	176.12	0.64	0.82	0.31	0.11	
	650.	805.00	1064.00	1069.84	1069.61	1070.43	0.004068	7.06	248.52	195.16	0.63	0.85	0.34	0.19	
	600.	100.00	1065.00	1066.62		1066.82	0.003575	3.65	27.40	18.87 19.92	0.53 0.54	0.31			
	600.	163.00	1065.00	1067.18		1067.46	0.003415 0.003490	4.25 5.14	38.37 83.15	19.92 98.92	0.54	0.38		0.03	
	600. 600.	375.00 525.00	1065.00	1068.65		1069.06	0.003490	6.13	118.70	119.23	0.64	0.70		0.11	
	600	650.00	1065.00	1069.24		1069.87	0.004549	6.65	157.14	155.43	0,67	0.80	0.05	0.16	
	600.	805.00	1065.00	1069.60		1070.22	0.004160	6.84	215.65	171,43	0.65	0.81	0.09	0.23	
								0.74	26.92	19.96	0.56	0.32			
	550.	100,00	1064.81	1066.42 1067.02		1068.63	0.004099	3.71 4.15	39.31	21.30	0.54	0.37			
	550. 550.	163.00 375.00	1064.81	1068.61		1068.89	0.002077	4.44	138.94	131.08	0.44	0.36		0.08	
	550.	525.00	1064.81	1068.97		1069.31	0.002496	5.14	186.62	137.74	0.49	0.47		0.14	
m !	550.	650.00	1064.81	1069.24		1069.62	0.002673	5.51	230.30	164.57	0.52	0.53	0.04	0.19	
m l	550.	805.00	1064.81	1069.60		1069.98	0.002569	5.76	290.81	174.86	0.52	0.56	0.08	0.23	
n s	500	100.00	1064.00	1066.08		1066.40	0.004800	4.54	22.03	12.54	0.60	0.46			
	500. 500.	100.00	1064.00	1066.40		1067.00	0.0048001	8,24	26.11	13.23	0.78	0.83			
	500	375.00	1064.00	1068.07	1068.07	1068.69	0.006379	6.48	87.05	128.14	0.74	0.84	0.01	0.13	
	500.	525.00	1064.00	1068.46	1068,46	1069.10	0.006008	6.97	139.31	139.75	0.74	0.92	0.09	0.26	
m !	500.	650.00	1064.00	1068,66	1068.66	1069.38	0.006573	7.62	167.08	145.58	0.78	1.07	0.13	0.35	
m E	500.	805.00	1064.00	1069.43		1069.84	0.003184	6.20	293.20	176.63	0.57	0.66	0.14	0.30	
	***	100.00	1064.00	1000 00	1065,55	1066.01	0.012718	5.18	19.29	21.28	0.96	0.71			
	450.	100.00	1064.00	1065.59	1000.55	1066.01	0.012718	5.22	31.22	25.55	0.83	0.65			
	450. 450.	375.00	1064.00	1065.09	1066.79	1067.92	0.003379	4.85	102.03	116.85	0.57	0.46		0.07	
	150.	525.00	1064.00	1068.22	1067.49	1068.52	0.002345	4.71	189.14	157.84	0.49	0 40	0.02	0.12	
m 4	150.	650.00	1064.00	1068.58	1067.81	1068.87	0.002128	4.86	250.83	182.42	0.48	0.41	0.05	0.14	
m 4	150.	805.00	1064.00	1069.51		1069.68	0.001023	3.99	443.29	229.73	0.35	0.26	0.06	0.11	
	100	100.00	1064.00	1065.46		1065.61	0.003757	3.06	32.70	32.12	0.53	0.24			
n  4				1000.401	I		V. W. 1	0.00	00			0.20			

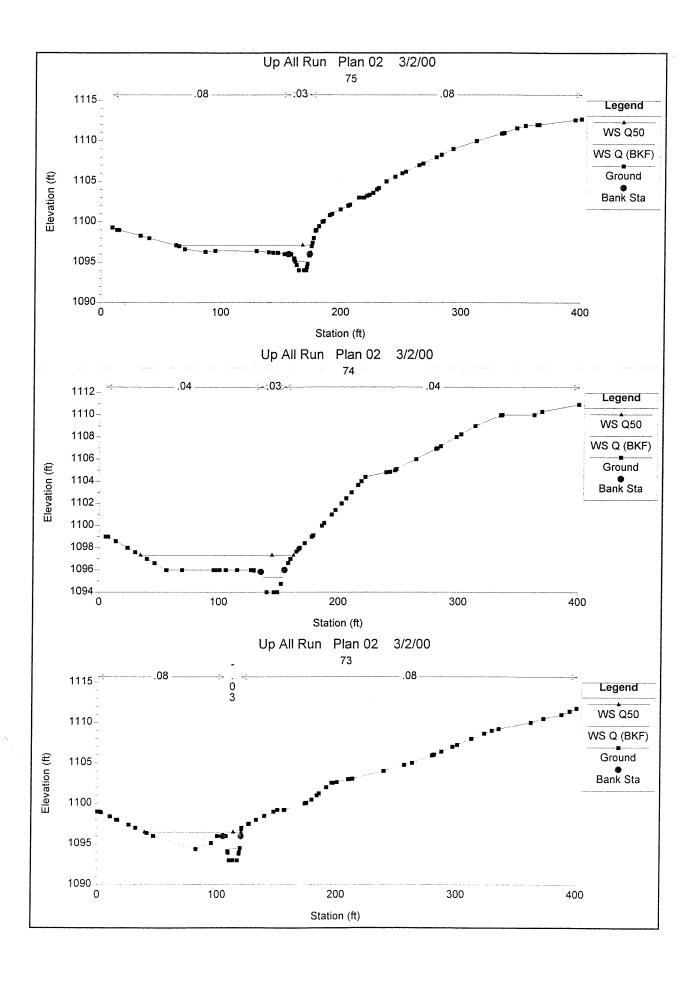
Reach	River Sta	Q Total	Min Ch El	W.S. Elev	Crt W.S.	E.G. Eley	E.G. Slope	Vel Chni	Flow Area	Top Width	Frouds # Chi	Shear Chan	Shear LOB	Shear ROB	Shear Total
		(cfs)	(ff)	(ft)	(#)	(ft)	(lvh)	(IVs)	(# pa)	(3)		(It pevdi)	(lib/eq fi)	(lb/sq ft)	(It pe/dl)
Upetream	400.	375.00		1067.66		1067,77	0.000909	2.76	193.43	168.88	0.30	0.14		0.03	0.0
Upstream	400.	525.00		1068.29		1068.40	0.000723	2.81	313.84	215.68	0.28	0.14	0.01	0.05	0.0
Upstream	400.	650.00		1068.65		1068.76	0.000688	2.95	394.60	233.54	0.28	0.15	0.02	0.06	0.0
Upstream	400	805.00		1069.55		1069.62	0,000385	2.57	620.04	264.41	0.22	0.10	0.02	0.05	0.0
- p	1		1,5-1,5-1												
Upetream	350.	100,00	1063.00	1064.60	1064.60	1065.24	0.013520	6.40	15.62	12.45	1.01	0.99			0.9
Upstream	350.	163.00		1065.13	1065.13	1065,93	0.012679	7.21	22.61	14.22	1.01	1.16			1,1
Upstream	350	375.00		1066.38	1066.38	1067.56	0.011384	8.72	43.03	18.46	1.01	1.51			1.5
Upetream	350.	525,00		1067.59	1067.59	1068.26	0.005281	6.94	134.59	172.13	0.71	88.0	0.14	0.15	0.1
Upstream	350.	650,00		1068,38		1068.68	0.002281	5.25	297.53	226,38	0.49	0.47	0.12	0.16	0.
Upstream	350.	805.00	1063.00	1069.47		1069.59	0.000833	3.78	566.29	264.70	0.31	0.22	0.07	0.11	0.
100	1														
Upstream	300.	100.00	1062.00	1064.50	1063,79	1064.74	0.003357	3.91	25.58	14.74	0.52	0.33			0.
Upstream	300.	163.00		1065.11	1064.29	1065.44	0.003698	4.65	35.08	16.51	0.56	0.44			0.
Upstream	300.	375.00		1066.52	1065.55	1067,01	0.003772	5.77	94.65	102.24	0.59	0.62		0.10	0.:
Upstream	300	525.00	1062.00	1067.57	1068.64	1067.80	0.001664	4,51	275.79	235.15	0.41	0.35	0.05	0.12	0.
Jostream	300.	650.00	1062.00	1068.45		1068.56	0.000760	3.50	498.75	264.13	0.28	0.19	0.06	0.09	0.
Jostraam	300.	805.00	1062.00	1069.48		1069.54	0.000384	2.84	780.67	282.54	0.21	0.12	0.05	0.07	0.
Jostream	250	100.00	1062.00	1064.38		1064.56	0.002642	3.60	27.81	15.07	0.47	0.28			0.
Joetream	250.	163.00	1062.00	1064.95		1065.25	0.003115	4.41	36.96	16.42	0.52	0.39			0.
Jostream	250.	375.00	1062.00	1068,37		1066.81	0.002953	5.54	120.76	209.17	0.53	0.54	0.03	0.07	0.
Jostream	250.	525.00	1062.00	1067.58		1067.71	0.000851	3.65	403.38	249.20	0.30	0.21	0.06	0.08	0.
Jostream	250	650.00		1068.45		1068.52	0.000455	3.00	628.18	267.04	0.23	0.14	0.05	0.07	0.
Jpetream	250	805.00	1062.00	1069.48		1069.52	0.000264	2.56	912.23	285.08	0.18	0.09	0.04	0.05	0.0
Jpstream	200.	100.00	1062,00	1064,09		1064.36	0.005608	4.15	24.09	18.98	0.65	0.41			0.4
petream	205	163.00	1062,00	1084.78		1065.05	0.004035	4.16	39.17	24.13	0.58	0.38			0.3
petream	200.	375,00	1062.00	1066.43		1068,63	0.001623	3.91	180.68	189.90	0.40	0.28	0.05	0.07	0.0
ipatniam .	200.	525.00	1062.00	1067.57		1067.68	0.000614	2.98	415.35	221.28	0.26	0.15	0.08	0.06	0.0
pstream	200.	650.00	1062.00	1068.44		1068.50	0.000368	2,62	618.96	246.24	0.21	0.11	0.05	0.05	0.
Jpstream	200	805.00	1062.00	1069.47		1069.51	0.000229	2.34	884.71	269.30	0.17	0.08	0.04	0.04	0.
Jpelmam	150.	100.00	1062.00	1063.68		1064.04	0.006386	4.83	20.68	13.82	0.70	0.54			0.
Jostream	150.	163.00	1062.00	1084.33		1064.77	0.006378	5.34	30.61	18.81	0.71	0.62		0.03	0.5
Jpetream	150	375.00	1062.00	1066.42		1066.54	0.001013	3,39	270.62	205.08	0.32	0.20	0.06	0.08	0.0
lpetream	150.	525.00	1062.00	1067.56		1067.62	0.000432	2.68	518.28	225.67	0.22	0.11	0.05	0.06	0.0
lpatniam	150.	650.00	1062.00	1068.43		1068.48	0.000279	2.42	719.10	240.65 254.52	0.18	0.09	0.05	0.05	0.0
petream	150.	805.00	1062.00	1069.46		1069.50	0.000187	2.22	973.58	234.32	0.13	0.07	0.04	0.04	- 0,1
	ļ							1.96	50.97	47.35	0.33	0,10	<del>-</del>		0.
Jostneam	100.	100.00		1063,76	1063.11	1063.82	0.001439	1.83	89.27	52.39	0.25	0.07			0.1
jpstream	100.	163,00	1062.00	1064.53	1063.36	1064.58		1.77	224.01	88,89	0.17	0.05	0.01	0.01	0,1
patreem	100.	375.00	1062.00	1068.45	1063.93	1066.49	0.000278	1.80	337.50	120.42	0.17	0.05	0.01	0.01	0.0
Jostream	100	525.00	1062.00	1067.56	1064.25	1067.61	0.000193	1.82	454.87	157.21	0.13	0.05	0.01	0.01	0,1
Jostream	100.	650.00		1068.42	1064.49 1064.77	1068.47 1069.49	0.000154	1.79	651,96	203.48	0.13	0.04	0.01	0.01	0.0
Jostowan	100.	805.00	1062.00	1069.44	1004.77	1009.49	0.000118	1,75	031.30	200.40	0.10	0.04			
	ļ														
Apstream	40	Culvert													
	<u> </u>				4000 11	1000 70	0.008004	4.86	20,59	17.01	0.78	0.57			0.
ipelrown	0.	100.00	1060.74	1062.35	1062.14	1062.72	0.008004	5,70	28.61	18.41	0.781	0.73			0.
pstream	0.	163.00	1060.74	1062.80	1062.57	1063.31 1064.76	0.008002	7.33	51,19	22.25	0.85	1.06			1,
henemi	0.	375.00	1060.74	1063.92	1063.63		0.008007	7.33	65.74	25.08	0.87	1.21			1.
Jpetream	0.	525.00 650.00	1060.74 1060.74	1064.54	1064.25 1064.69	1065.53	0.008006	8.43	77.06	27.06	0.88	1.21			1.3
Jostosam	0.														

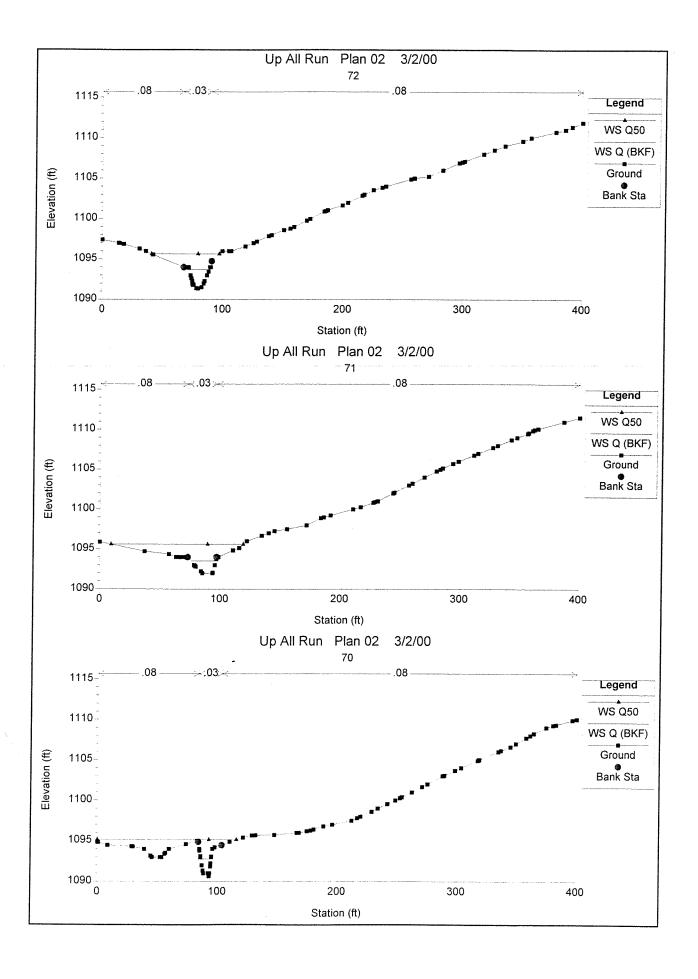
-

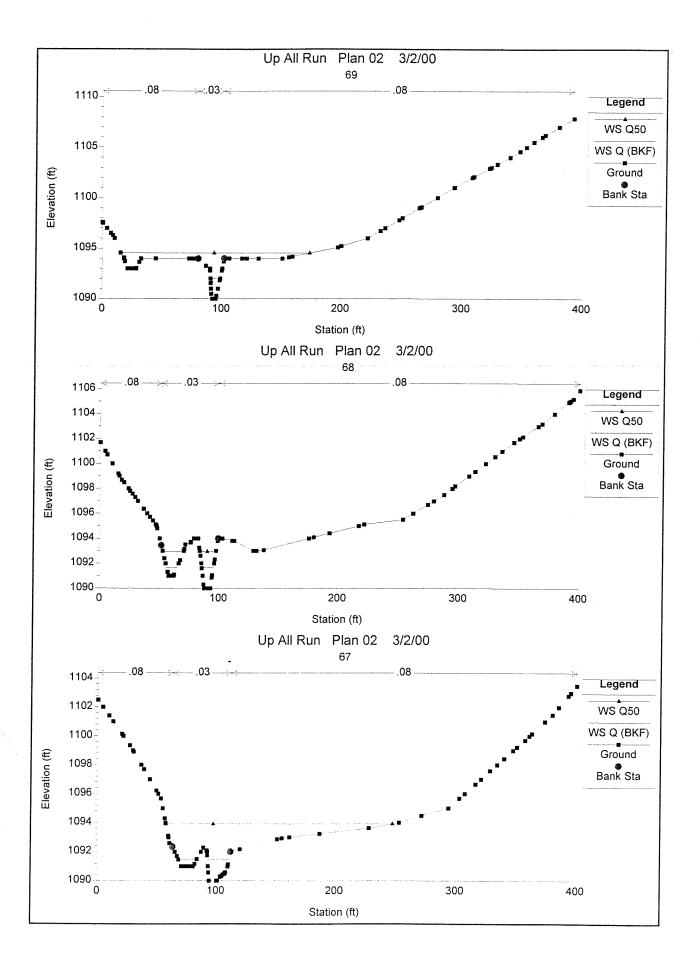
7:

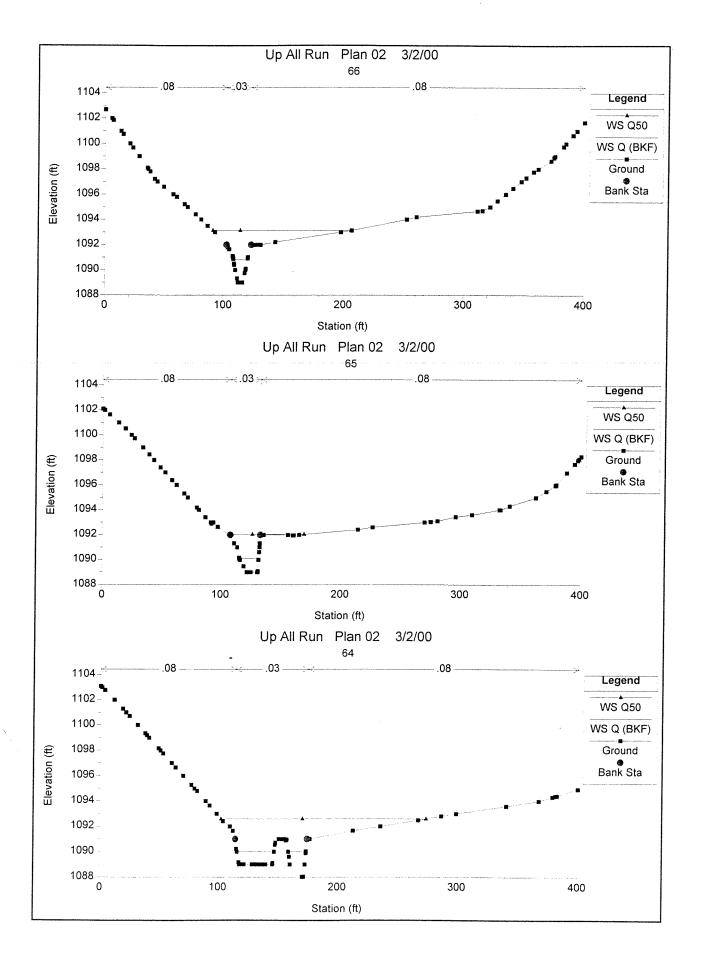


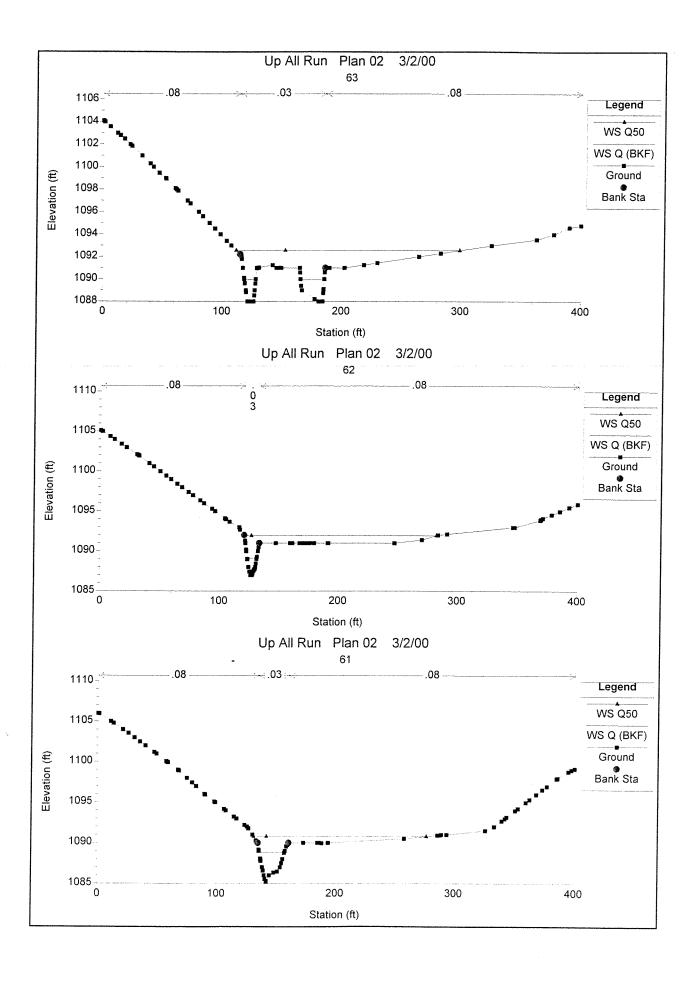


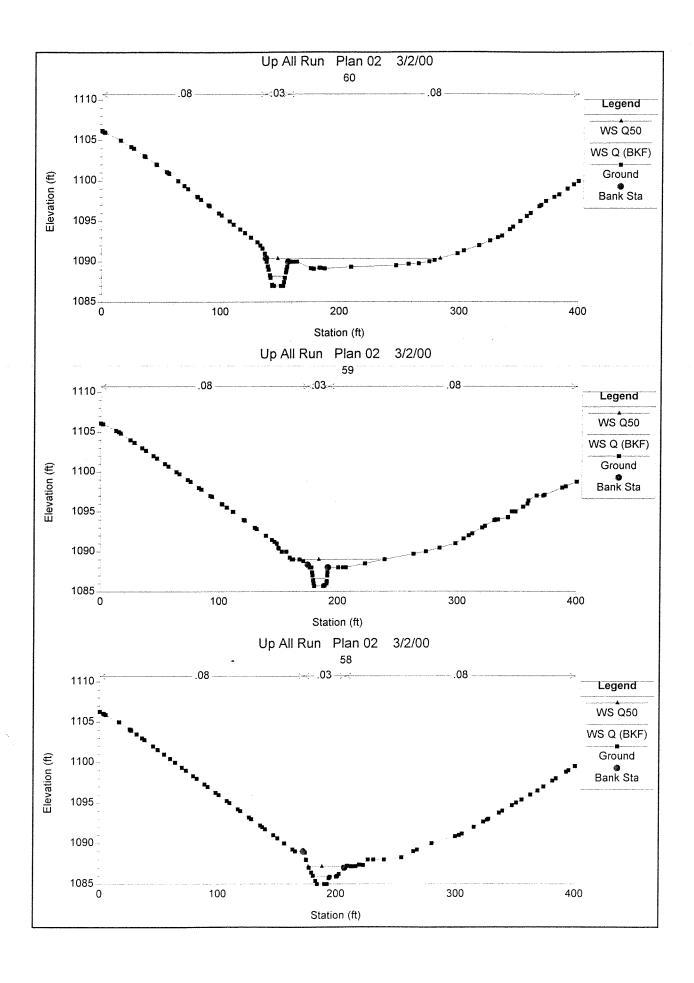


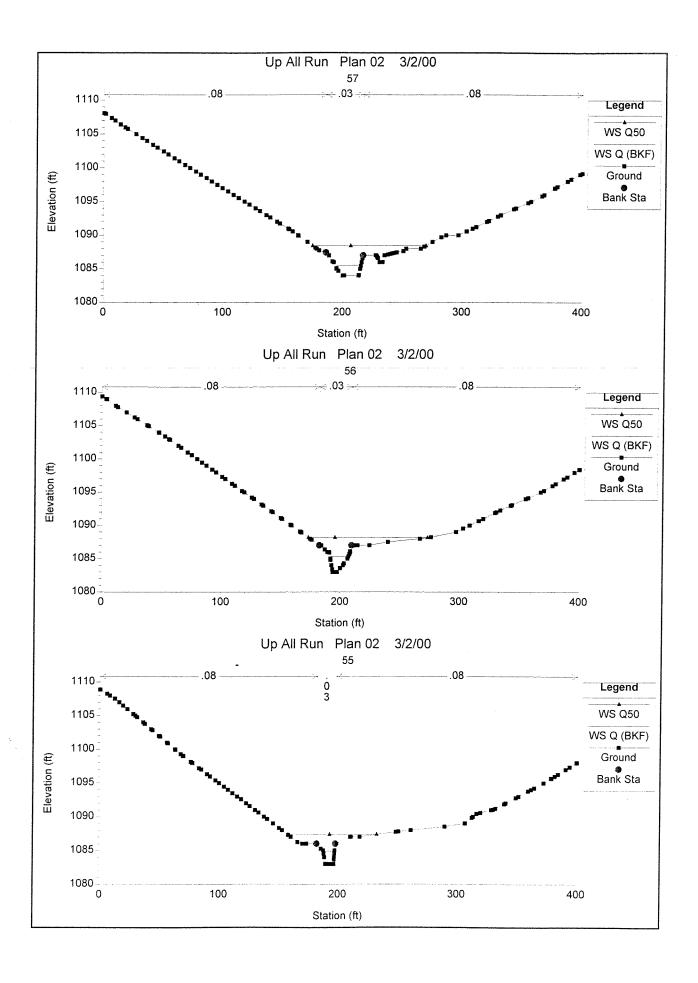


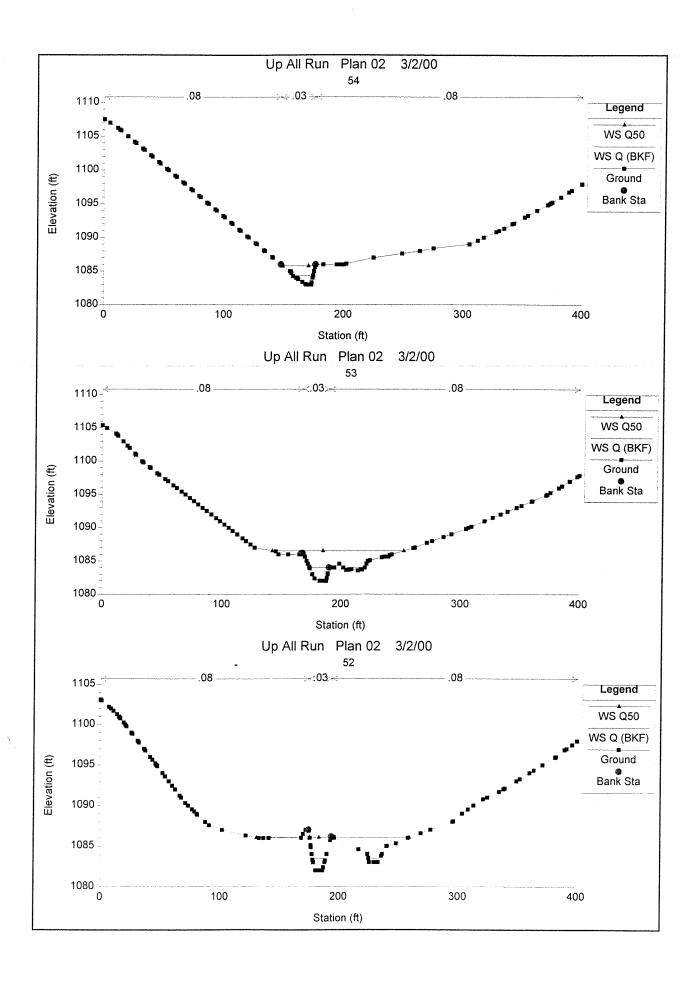


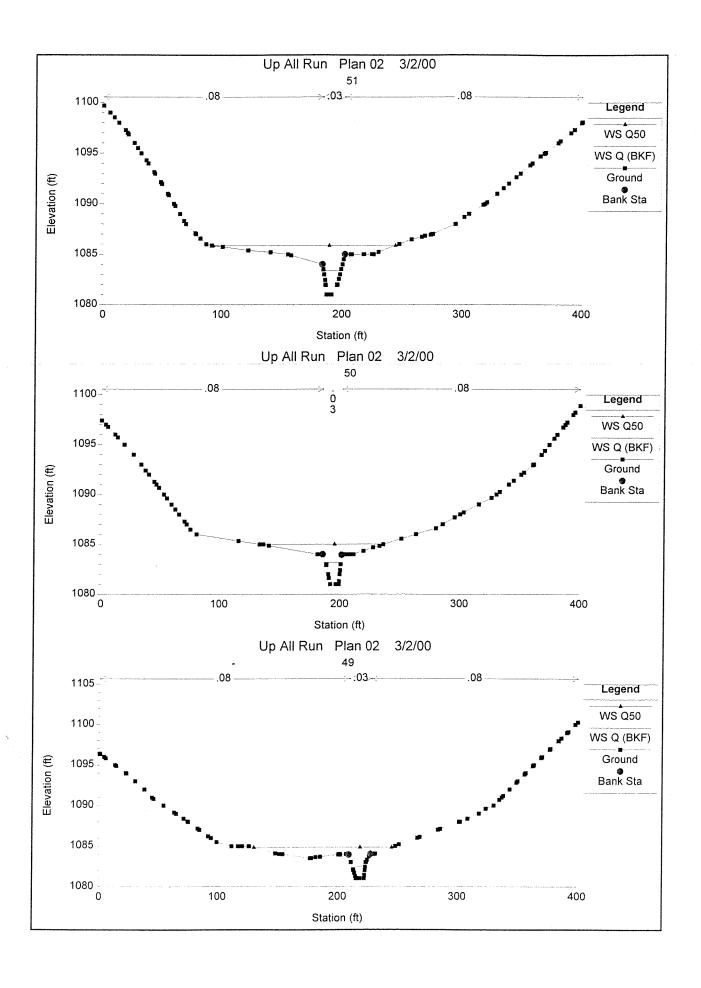


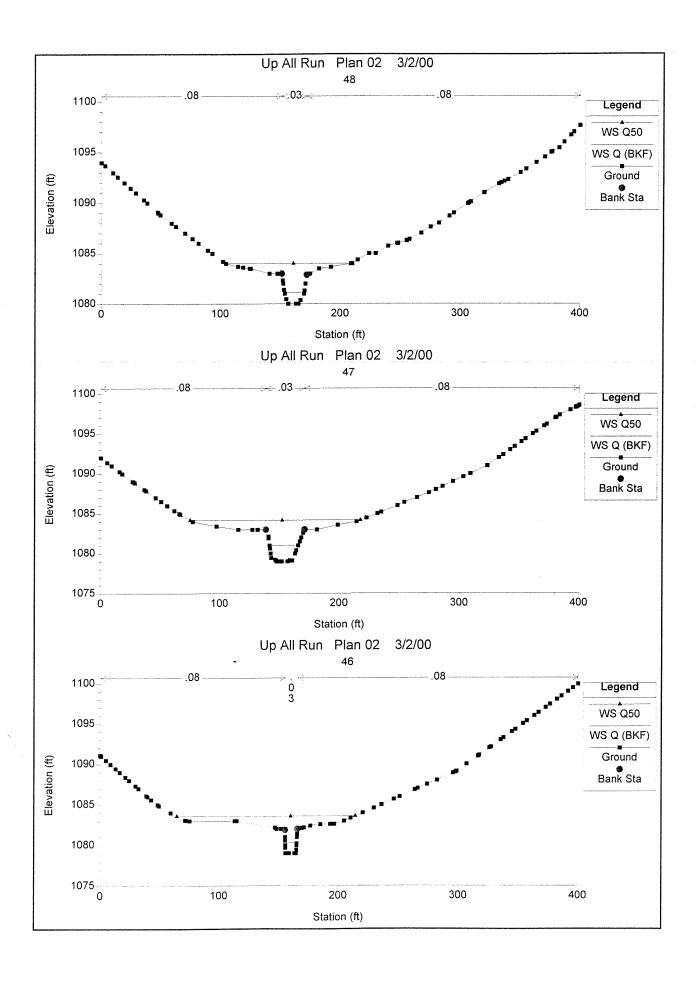


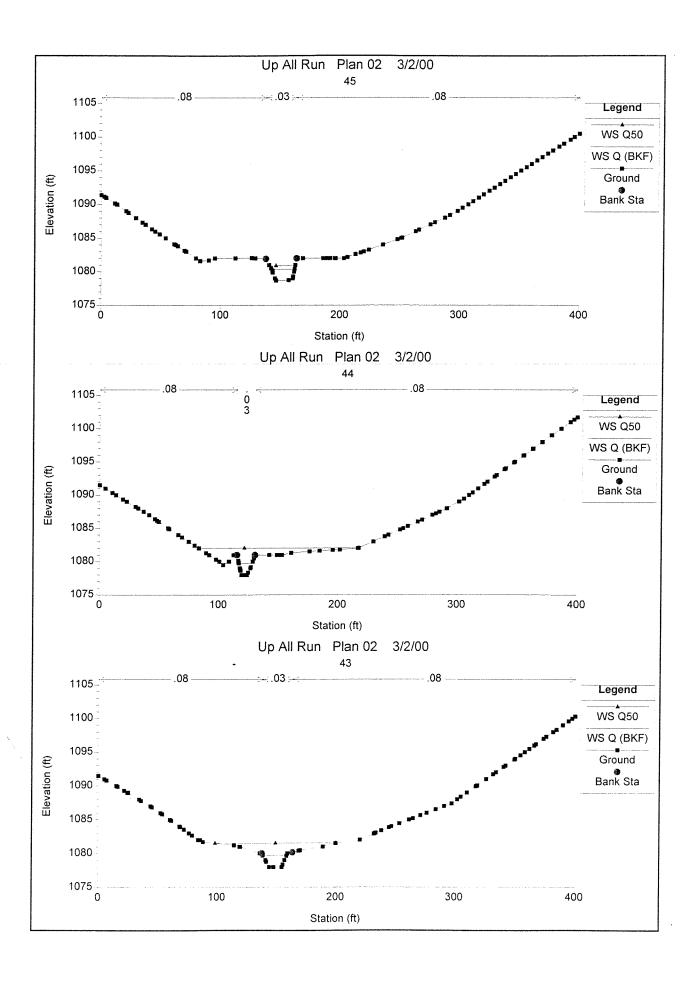


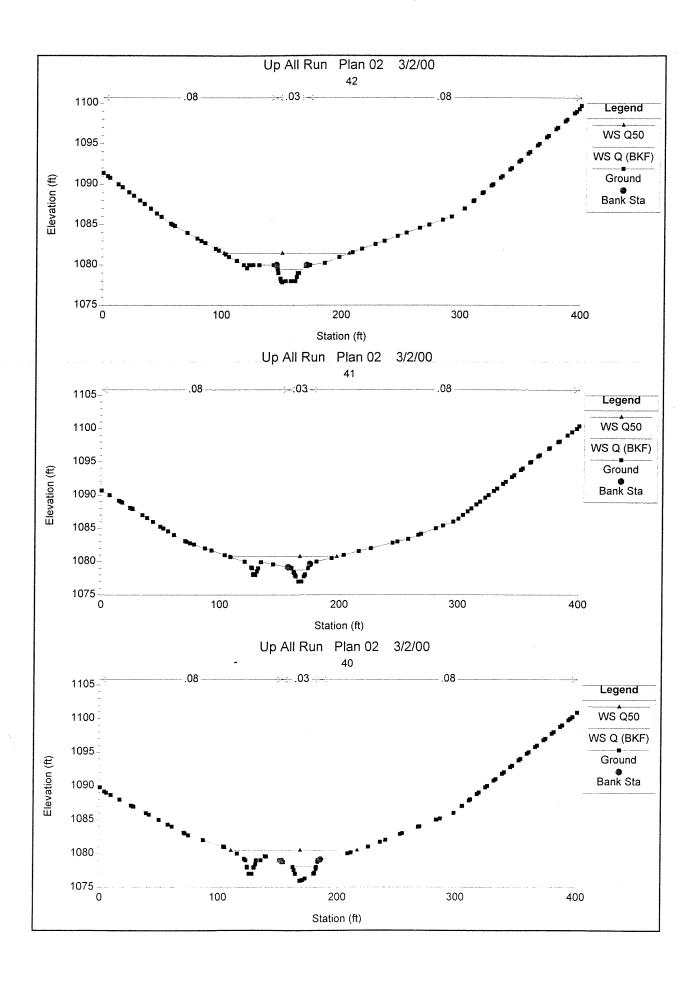


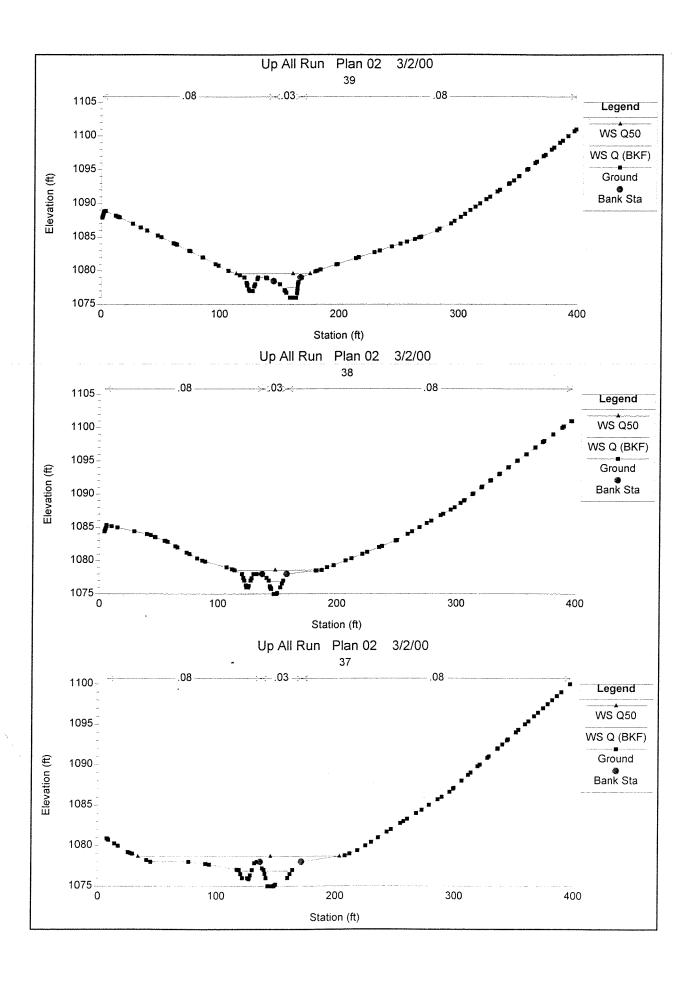


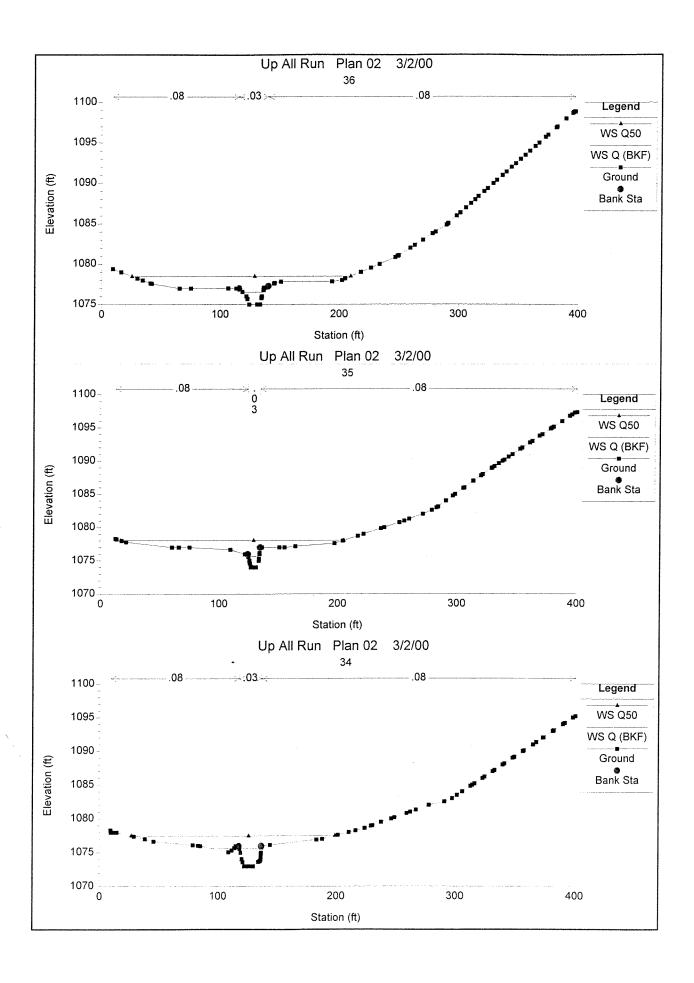


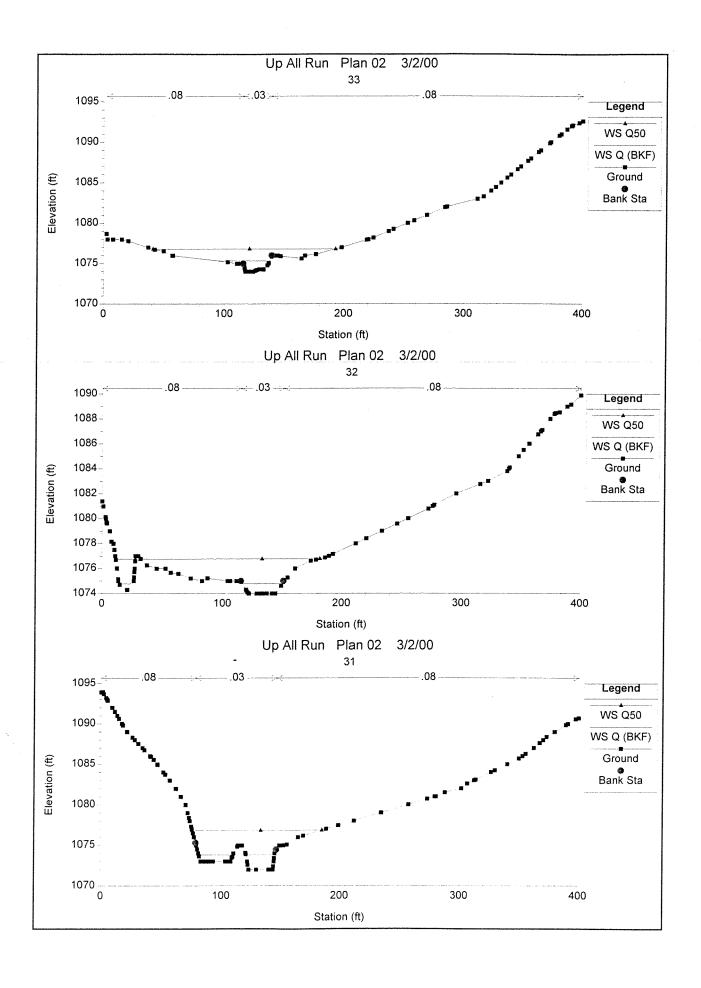


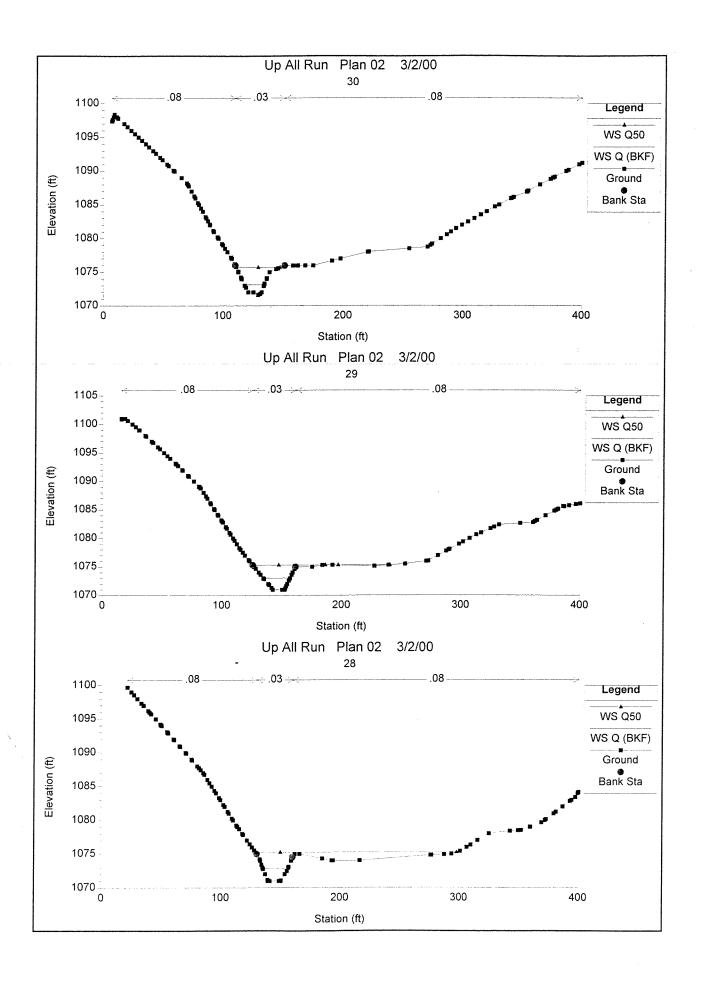


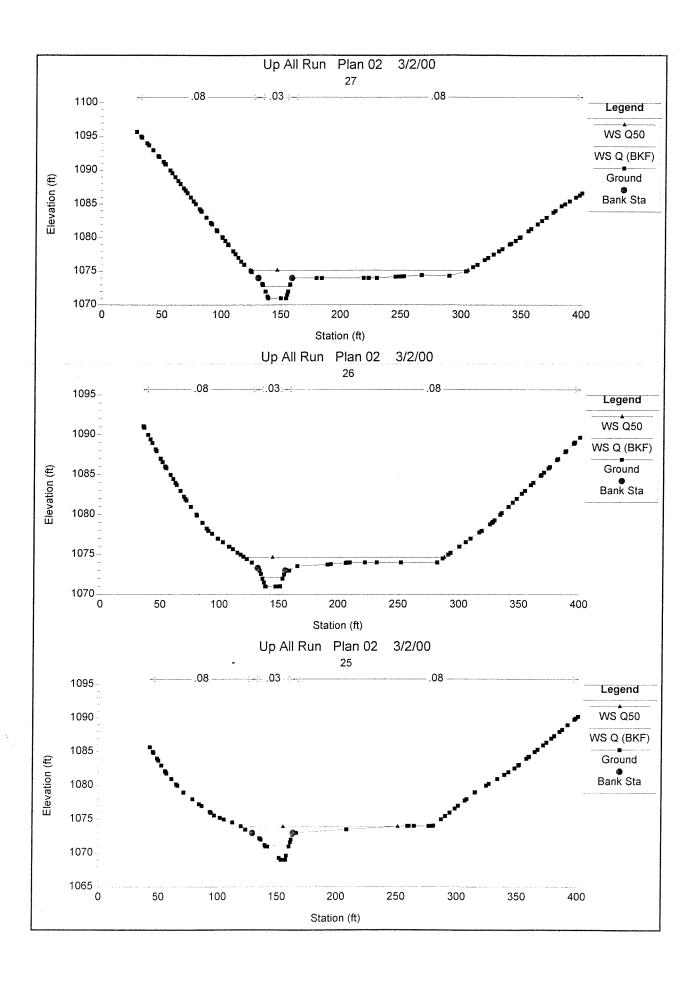


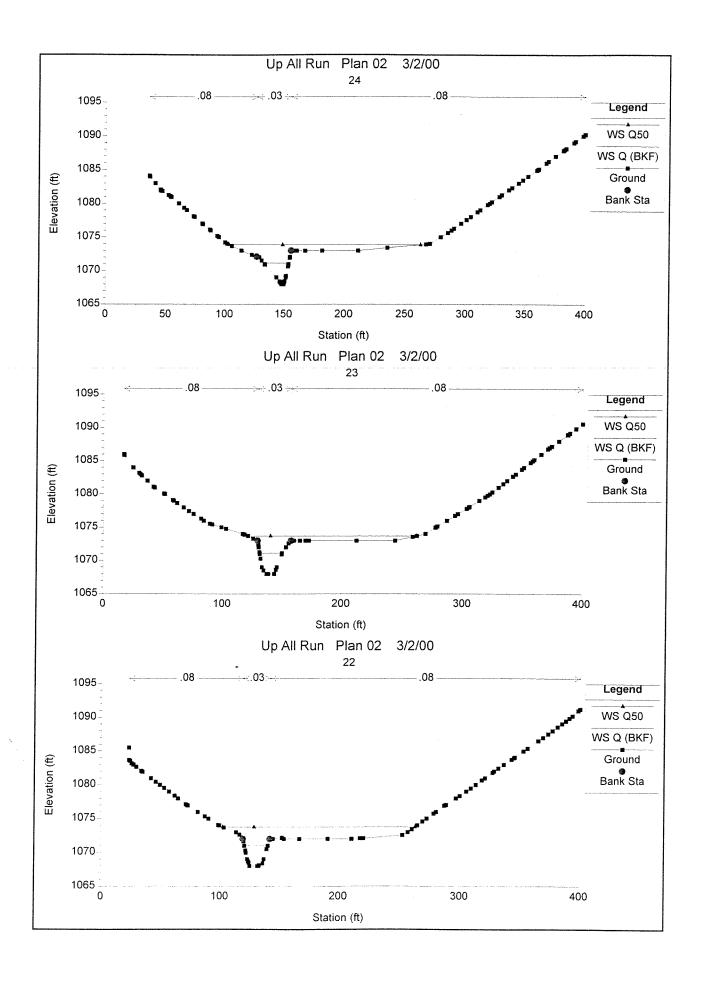


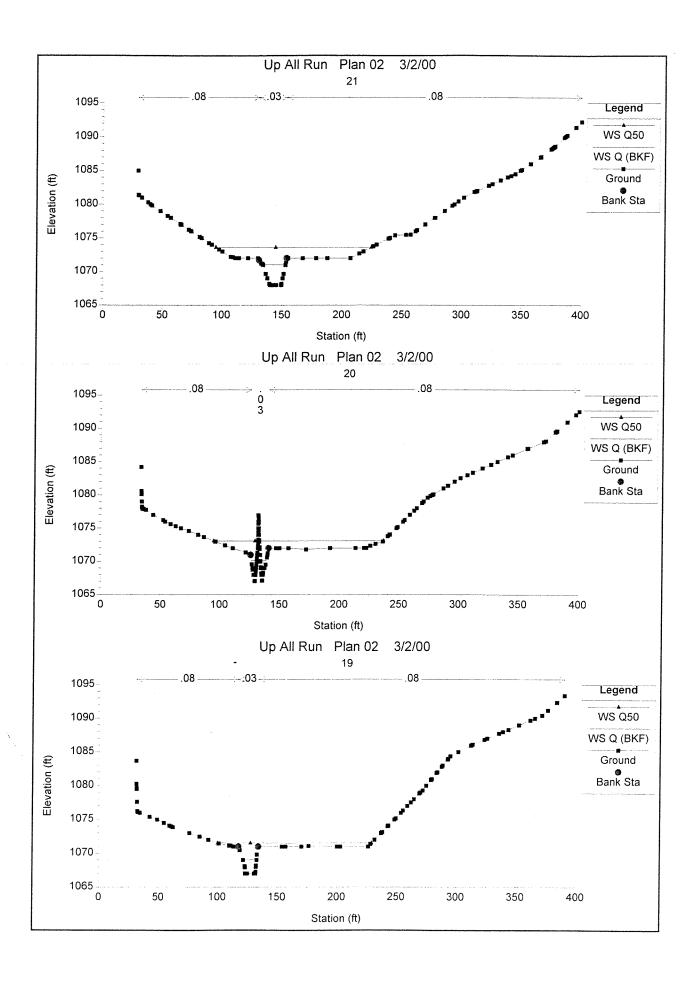


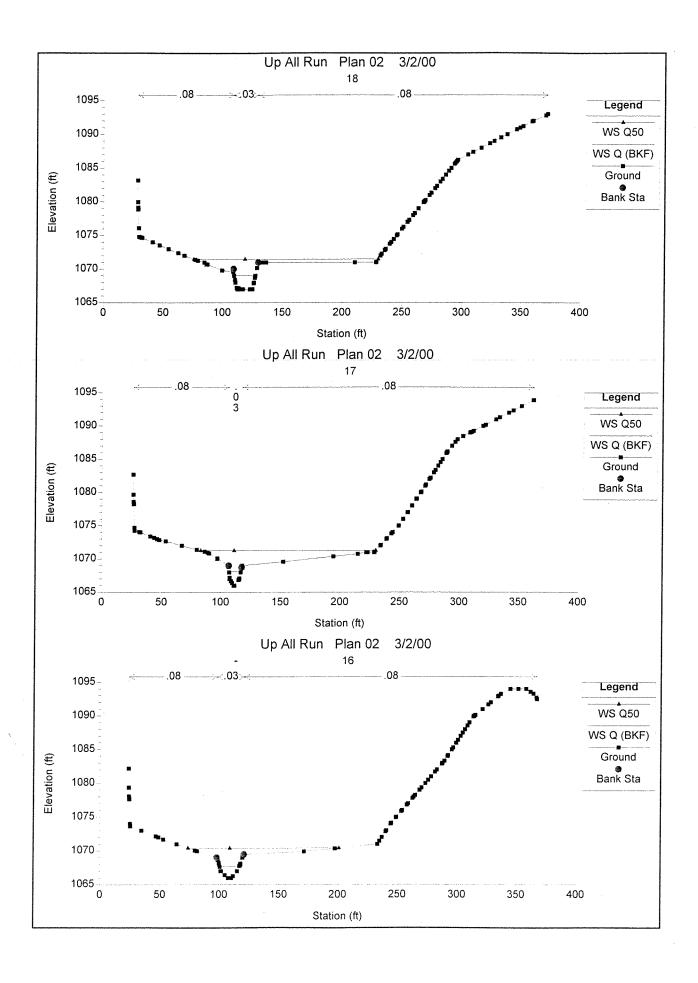


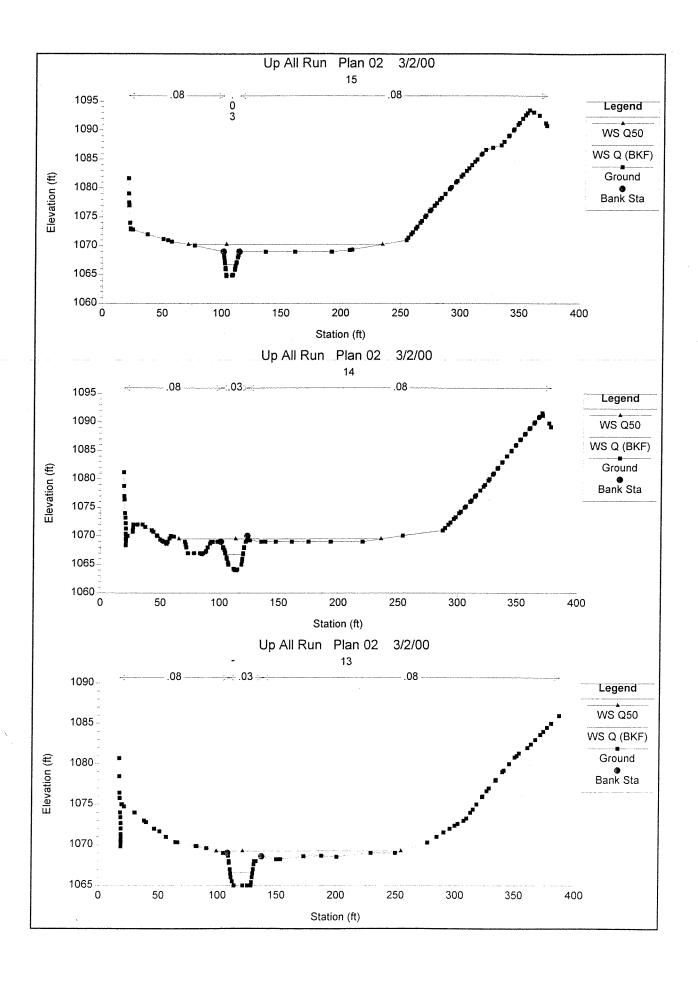


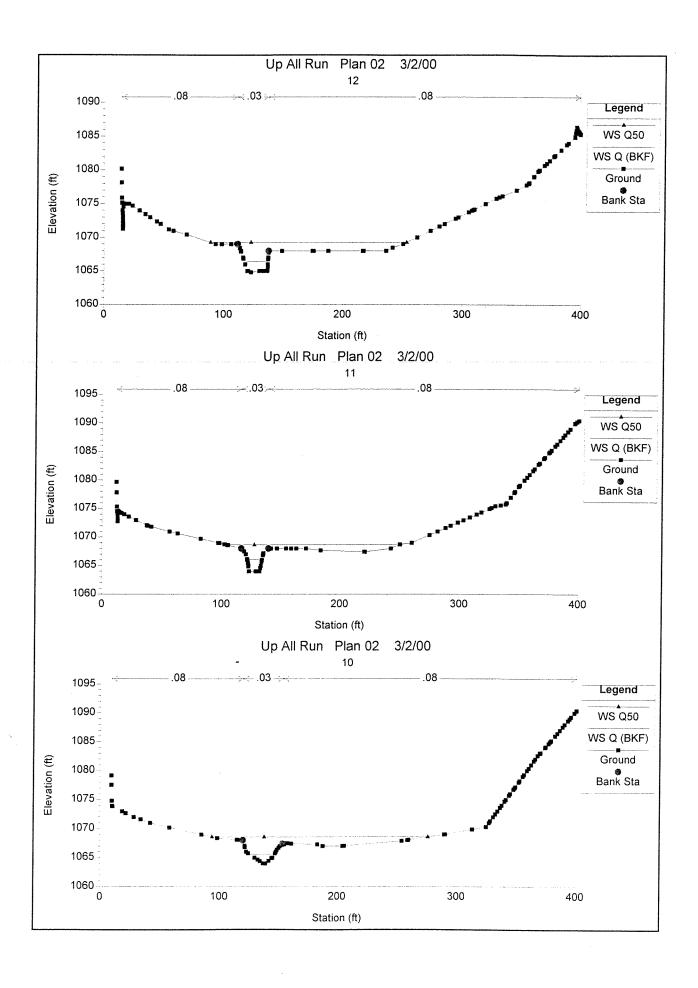


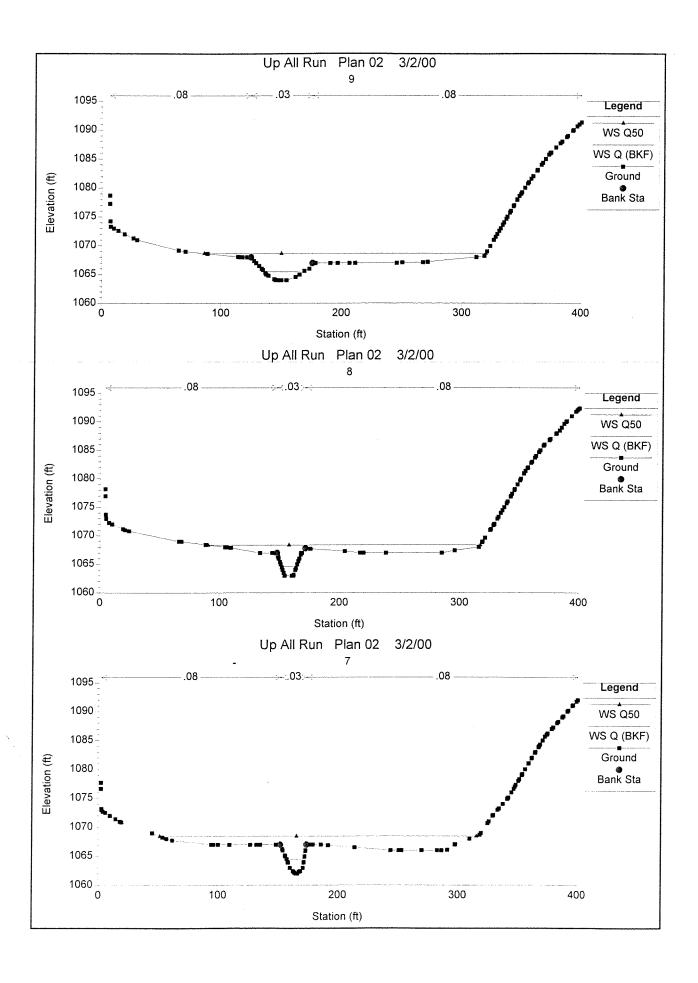


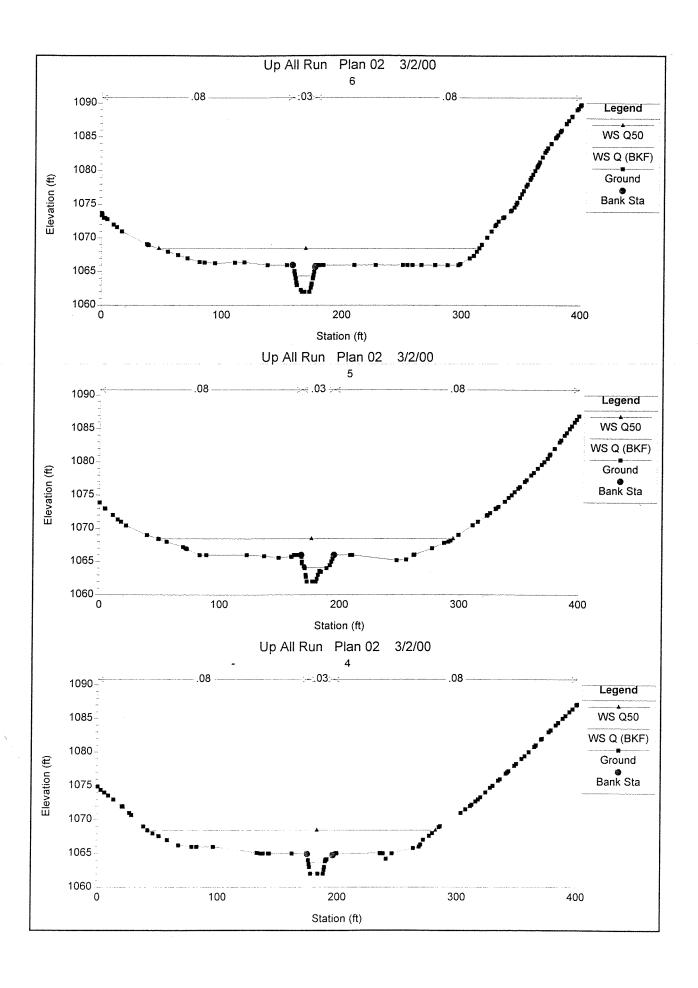


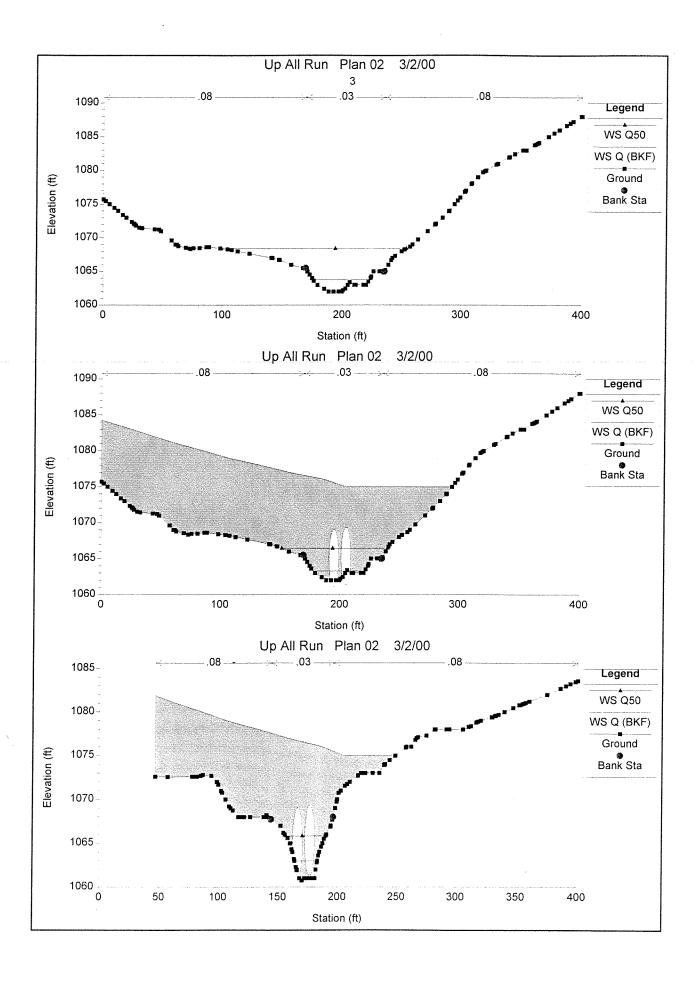


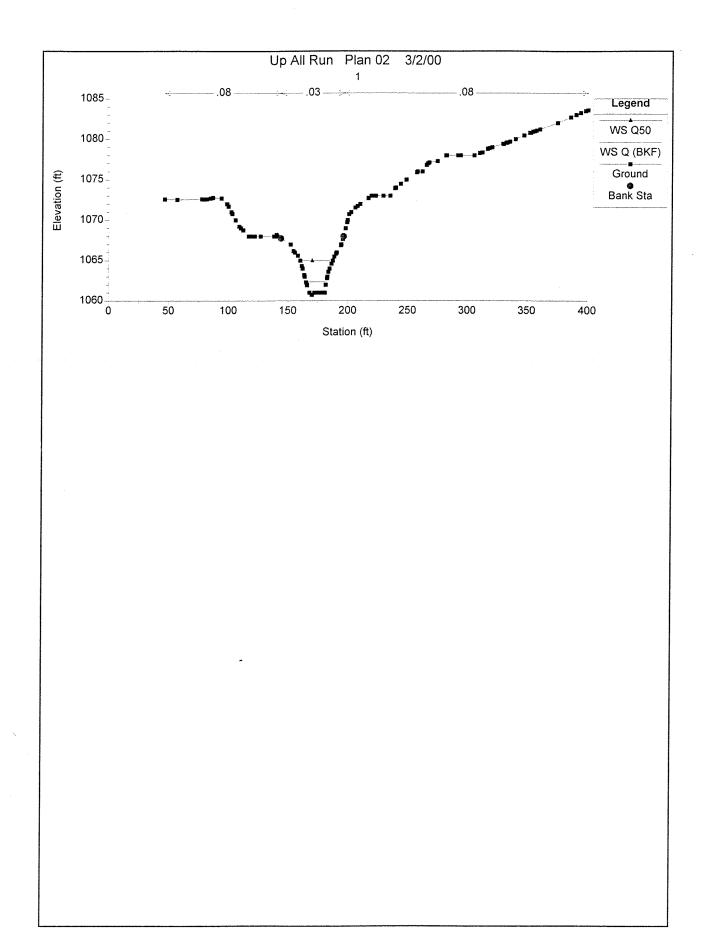












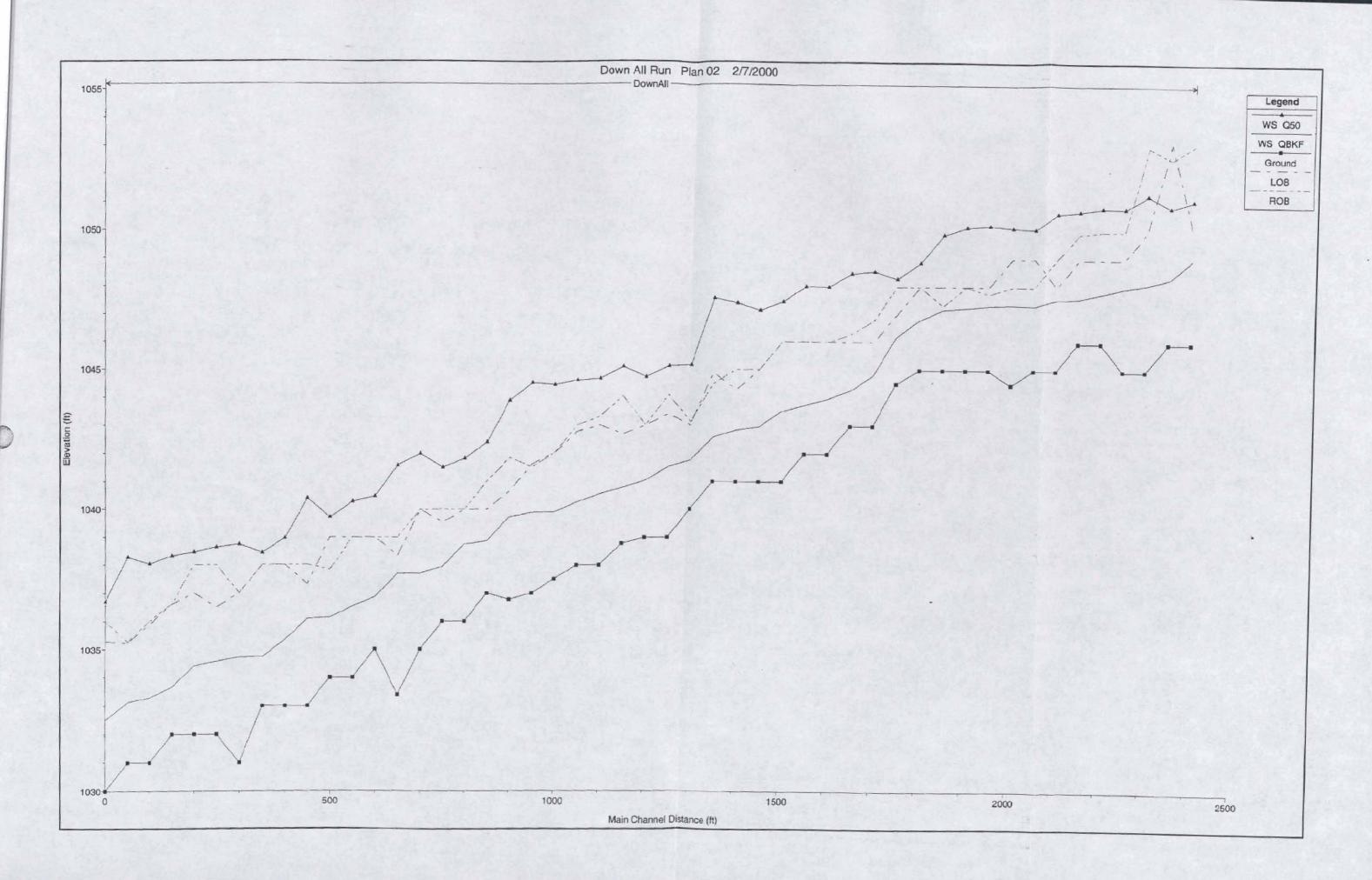
Downstream Segment Jumping Run East of SR 1605

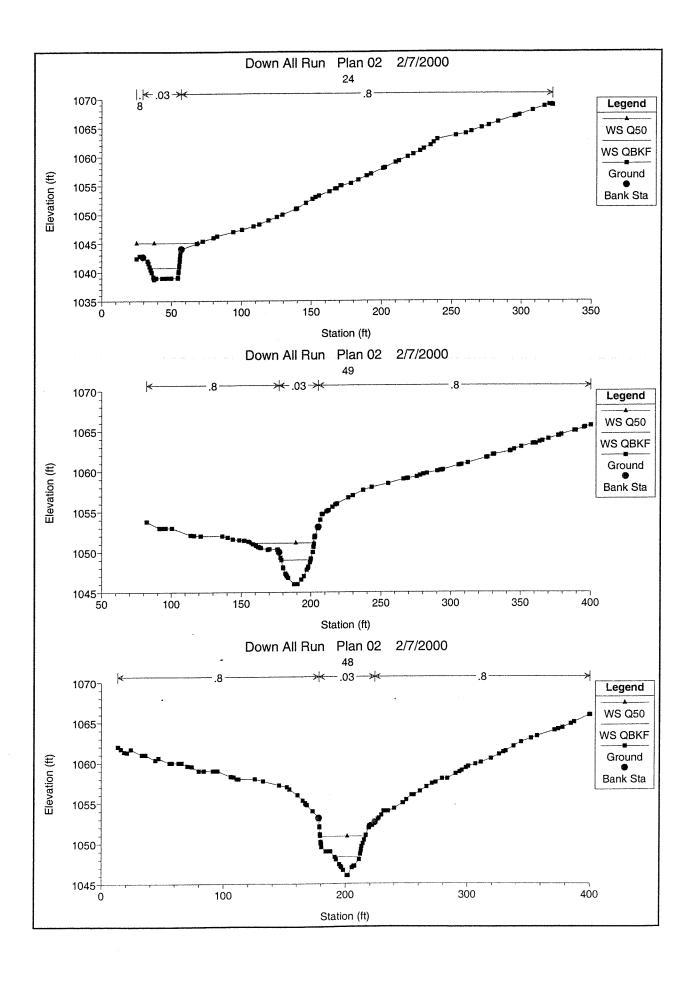
Part   100	HEC-RAS PI	an: Plan 01 R	iver: Jumping C	reek Reach: I	OownAll W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chal	Flow Area	Top Width	Froucie # Chi	Shear Chan	Shear LOB	Shear ROB	Shear Total
			(cfs)			(ft)					The state of the s				(it perdit)	
Section   March   Ma											<del></del>			<del>+</del>		
Company   Comp				~												0.65
Company   Comp						1050.54	1052.14									0.96
Company   Comp		•						<del>,</del>							<b></b>	
Part   Part	DOWNAM	2400.	1193./3	1046.00	1051.58	1051.58	1053.60	0.009207	11.42	121.15	37.02	0.55	2.14	0.42		1
Company   Comp	DownAll	2350	160.00	1046.00	1048.32	1048.32	1048.95	0.013079								0.98
The color   The																1.13
Company   Comp																1.53
Company   Comp									·							1.67
Section   Color   Co	DownAll	2350.	1193.73	1046.00	1051.29	1051.29	1052.86	0.009876	10.04	118.86	38.08	1.00	1.80			1.80
Section   Color   Co	Desam AN	2200	160.00	1045.00	1049 10		1048 15	0.000418	170	94.29	42.55	0.20	0.06			0.06
Description   1982   1982   1983   1984   1985																0.08
Company   Comp	DownAll	***************														0.14
Section   1982									<del></del>							
Company   Comp																0.14
Description   Color																
Section   1985																
Part   Part						-								0.07		0.30
Description   Process	Personal Property Company	<b>*************************************</b>														0.24
Common   C																
Decision   1985   1986   198	S.VBird		1133.73	1040,00	1031.32		1002.02	0.002000						5.29		
Dennist   1986															<u> </u>	0.30
Demin														0.09		0.29
Demind   2000										271.92	147.79	0.48	0.41	0.15		0.24
Commit   150	DownAll	2200.	973.78	1046.00	1050.84		1051.24									0.26
Descript   1985	Down All	2200.	1193.73	1046.00	1051.38		1051.84	0.001832	5.49	442.25	175.87	0.47	0.48	0.22	0.07	0.29
Demin	DownAll	2150	160.00	1046.00	1047.60		1047.79	0.003566								0.29
Demontal   1756   778.72   1040.00   1050.00																0.28
Demind   1565						<u></u>						<del> </del>			0.01	
Demail   1986   1987   1986   1987   1986   1987																0.26
Demonth   2000   264.09   1065.00   1064.01   1065.00   1064.01   1065.00   1064.01   1065.00	DownAll		1193.73	1046.00	1051.25		1051.74	0.001887	5.71	477.01	192.79	0.48	0.51	0.24	0.08	0.29
Demonth   2000   264.09   1065.00   1064.01   1065.00   1064.01   1065.00   1064.01   1065.00	Davin 44	nano.	100.00	1045.00	1047 55		1047.66	0.001442	271	58 97	32.84	0.36	0.16			0.16
Demin   2000														0.01		0.08
Demontal 2000							1049.75									0.17
Demonth   2000																
Demontal   2000																0.29
Demin No.   1965   286.50   196.50   1047.80   1047.80   1048.10   1049.10			7,120.0													
Demin   2005   586.20   1646.00   1646.00   1646.00   1646.00   1696.01   1696.01   1696.02   1696.00																0.32
DownAr   2000														0.17	0.12	
DownAI   2000									6.76	266.31	166.54	0.64	0.78	0.28	0.22	0.38
DemMA   2000   150.00   104.4   1047.35   1047.44   0.000720   2.31   89.32   28.01   0.26   0.10   0.10   0.10																. 0.46
DownAl   2000   248.00   1044.49   1047.92   1048.05   0.000941   2.00   8570   29.91   0.30   0.15   0.15   0.15	DownAll	2050.	1193,73	1045,00	1050.49		1051.48	0.004089	8.12	420.25	191,00	0.69	1.05	0.47	0.37	0.50
Demonal   1900   594.23   1044.49   1049.12   1049.45   1059.05	DownAll	2000.	160.00	1044.49	1047.35		1047.44	0.000720								0.10
								<del>-</del>						0.00	0.00	0.15
DownAir   1900   973.79   1944.49   1950.11   1950.67   0.002098   9.11   424.17   292.38   0.49   0.58   0.21   0.19   0.27   0.29   0.34   0.35   0.35   0.34   0.35   0.35   0.34   0.35															~~~~~~~~~~~	
DownAl   1900   1904500   1904500   1904732   1904739   0.0000385   2.16   74.211   388.59   0.27   0.10   0.10   0.10										424.17		0.49	0.58	0.21	0.19	0.27
Desirical   1980   248.30   1045.00   1047.89   1047.99   0.000948   2.53   98.16   45.27   0.30   0.13   0.00   0.12	DownAll	2000,	1193.73	1044.49	1050.55		1051.24	0.002323	6.82	516.74	219.33	0.52	0.70	0.27	0.25	0.34
DownAI   1950   248.50   1045.00   1047.89   1047.99   0.000946   2.53   98.16   45.27   0.30   0.31   0.00   0.12	DownAll	1950	160.00	1045 00	1047.32		1047.39	0.000835	2.16	74.21	38.59	0.27	0.10			0.10
DeverAl   1950									2.53	98.16	45.27	0.30	0.13		0.00	0.12
Description   1980   973.76   1045.00   1050.16   1050.52   0.001281   4.71   527.03   240.20   0.39   0.35   0.14   0.10   0.17						T										0.10
DeverAll   1900   19373   1045 00   1045 00   1045 00   1047 24   1047 34   0.001299   2.50   64.07   38.02   0.34   0.13   0.13   0.13												· · · · · · · · · · · · · · · · · · ·				0.14
DownAR   1900   248.30   1045.00   1047.81   1047.93   0.001412   2.83   87.63   45.83   0.36   0.17     0.17																
DownAR   1900   248.30   1045.00   1047.81   1047.93   0.001412   2.83   87.63   45.83   0.36   0.17     0.17	D 4#	1000			****		1047.04	0.001000	0.50	64.07	20 00	0.34	0 12			n 12
DownAll   1900   584.23   1045.00   1049.06   1049.27   0.001328   3.74   290.19   210.15   0.38   0.25   0.08   0.05   0.11																
DownAR   1900	DownAll	1900	564.23	1045.00	1049.06		1049.27	0.001326	3.74	290.19	210.15	0.38	0.25			0.11
DownAll   1900   1193.73   1045.00   1050.60   1050.99   0.001431   5.11   664.45   266.03   0.42   0.40   0.20   0.13   0.22																
DownAl   1550,   160 00   1045 00   1047 18   1047 28   0.001239   2.52   83.44   35.59   0.33   0.13   0.13																0.18
DownAll   1850   248.30   1045.00   1047.73   1047.86   0.001265   2.97   85.71   44.97   0.35   0.17   0.02   0.15			1100.10	10.10.00	1000.00											
DownAR   1850   584.23   1045.00   1048.90   1049.19   0.001588   4.35   263.99   205.18   0.42   0.32   0.08   0.08   0.13															0.00	
DownAR   1850   782.72   1045.00   1049.44   1049.84   0.001812   5.15   380.58   229.84   0.45   0.43   0.14   0.12   0.19														0.08		
DownAR   1850   1193.73   1045.00   1059.28   1059.88   0.002125   6.35   589.11   258.21   0.51   0.62   0.26   0.21   0.30												0.46		0.14		0.19
DownAN   1800   160.00   1045.00   1046.80   1047.14   0.005076   4.65   34.38   21.52   0.65   0.48   0.																
DownAN   1800   248.30   1045.00   1047.18   1047.70   0.007328   5.79   42.89   25.55   0.79   0.73     0.73     0.73     0.73     0.73   0.73   0.73   0.73   0.73   0.73   0.74   1800   564.23   1045.00   1048.09   1048.09   1048.97   0.010917   7.56   118.76   138.28   0.99   1.70   0.31   0.58   0.52   0.79   0.74	DownAll	1850.	1193.73	1045.00	1050.28		1050.88	0.002125	6.35	589.11	258.21	0.51	0.62	0.26	0.21	0.30
DownAr   1900   248.30   1045.00   1047.18   1047.70   0.007326   5.79   4.289   25.55   0.79   0.73     0.73     0.75	DownAll	1800.	160.00	1045.00	1046.80		1047.14	0.005076								
DownAl   1800   782.72   1045.00   1048.54   1048.54   1049.60   0.009951   8.35   183.82   153.84   0.98   1.36   0.52   0.17   0.74	DownAll	1800,	248.30	1045.00	1047.18									T		
DownAl   1800   973.78   1045.00   1048.86   1048.86   1050.09   0.009722   9.02   235.68   184.18   0.99   1.52   0.67   0.28   0.86															0.17	
DownAl   1750   1044 52   1046 20   1046 83   1047 50   1048 80   1047 50   1048 80   1049 104															~~~~~~~~~	
DownAl   1750   248.30   1044.52   1048.63   1046.63   1047.22   0.012335   6.24   62.59   89.76   0.99   0.93   0.31   0.53		~~~~~														
DownAl   1750   248.30   1044.52   1048.63   1046.63   1047.22   0.012335   6.24   62.59   89.76   0.99   0.93   0.31   0.53			100.00	10::55	1010.00	1040.00	1040 70	0.013154	5.00	70.81	54 22	1.00	Λ 9.0	0.10		0.46
DOWNAR   1750,   564.23   1044.52   1047.50   1047.50   1048.38   0.010941   7.65   165.81   134.73   0.99   1.23   0.67   0.83																
DownAl 1750 973.78 1044.52 1049.28 1048.28 1049.48 0.010238 9.03 276.90 151.99 1.01 1.55 1.03 0.09 1.16	DownAll	1750.	564.23	1044.52	1047.50	1047.50	1048.38	0.010941				0.99				
30.00 (0.00)															0.00	
						1046.28										

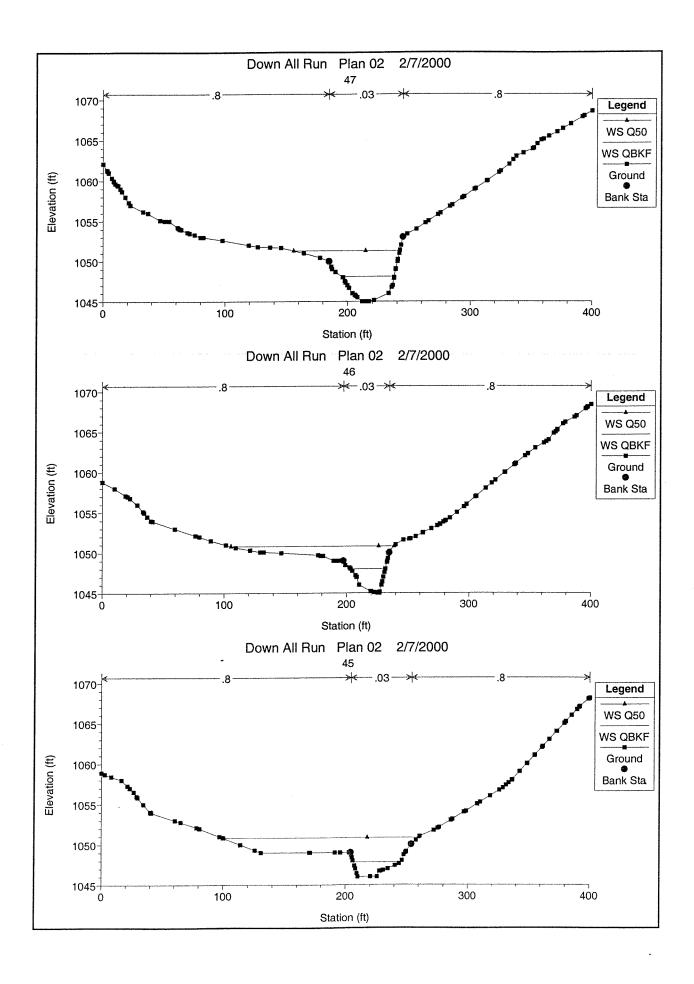
UE C F	AC Dia	Dian O Total	Min Ch El	W.S. Elev	Tonws	CEG Flev	E.G. Slope	Vel Chris	(Contin	Top Width	Froude # Chi	Shear Chan	Shear LOB	Shear ROB	Shear Total
	(876) 586	(cfs)	(ft)	(ft)	(ft)	(ft)	(N/ft)	(ft/s)	(sqft)	(ft)	1,000	(it petdit)	(fb/eq ft)	(It petdi)	(lb/sq fi)
DownAll	1700.	160.00	1043.00	1044.8	1 1044.69	1045.31	0,009831	5.65	28.31	22.43	0.89	0.76	3		0.76
DownAll	1700.	248.30	1043.00	1045.2	6 1045.19	1045.84	0.010972	6.16	45.75	5 58.27	0.94	0,89	0,13		0.53
DownAll DownAll	1700. 1700.	564.23 782.72				1047.37 1048.28	0,003767	5.68					0.28	0.07	0.37
DownAll	1700.	973.78	1043.00	1048.5	4	1049.05	0.002101	5.87	481.52	177.39	0.50	0.55	0.32	0.08	0.35
DownAll	1700.	1193.73	1043.00	1049.4	0	1049.92	0.001677	5.93	644.71	197.21	0,46	0.52	0.32	0.11	0.34
DownAll	1850.	160,00					0.011571								0.79
DownAll DownAll	1650. 1650.	248.30 584.23				1045.39 1047.20	0.006721	5.49 5.33	45.20 240.89			0.66		0.03	0.66 0.26
DownAll	1650	782.72	1043.00	1047.6	9	1048.15	0.002120	5.62	397.13	184.48	0.49	0.51	0.24	0.05	0.28
DownAll DownAll	1650 1850	973.78 1193.73				1048.94 1049.83	0.001775	5.78 5.91	548.02 739.11				0.28	0.08	0.29 0.29
													0.51	0.03	0.23
DownAll DownAll	1600	180,00 276.46				1044.36 1045.08	0.005614	5.11 5.84	35.20 47.37			0.57			0.57 0.68
DownAll	1800.	625.68	1042.00	1046.2	7	1046,99	0.004423	6.90	231.69	189.99	0.66	0.84	0.22	0.28	0.33
DownAll DownAll	1600	866.60 1078.16	1042.00			1047.98 1048.80	0.003609	7.31 7.52	418.93 588.47			0.87	0.35 0.45	0.41	0.43
DownAll	1600.	1319.22	1042.00			1049,70	0.002581	7.69	803.76			0.86		0.38	0.51
DownAll	1550.	180.00	1042.00	1043.74		1044.08	0.005049	4.65	38.73	24.20	0.65	0,48			0.48
DownAll	1550	276.46	1042.00	1044.42	2	1044.80	0.003934	4.97	55.68		0.59	0.50			0.46
DownAll DownAll	1550. 1550.	625.68 866.60	1042.00 1042.00	1048.25		1048.76 1047.77	0.002783 0.002363	5.78 6.22	223.05 390.03	168.79 186.88	<del> </del>	0.57	0,15	0.09	0.22
DownAll	1550.	1078,16	1042.00	1048.00	)	1048.61	0.002068	6.47	548.85	209.30	0.49	0.61 0.63	0.26 0.33	0.13 0.14	0.30 0.33
DownAll	1550.	1319.22	1042.00	1048.90	-	1049.54	0.001781	6.67	756.32	239.70	0.47	0,63	0.38	0.17	0.34
DownAll	1500.	180.00	1041.00	1043.52		1043.85	0.003937	4.87	38.55	19.29		0.45			0.45
DownAll DownAll	1500. 1500	276.46 625.68	1041.00 1041.00	1044.14		1044.59 1046.55	0.004090	5.43 7.20	50.89	20.44 105.67	0.61	0.57 0.89	- 0.17		0.57
DownAll	1500.	866.60	1041.00	1045.76	·	1046.55	0.004482	7.92	255.02	152.82	0.66	1,02	0.17	0.08	0.35 0.42
DownAll	1500; 1500	1078.16 1319.22	1041.00 1041.00	1047.44 1048.36		1048.44 1049.38	0.003623 0.003065	8.20 8.39	387.35 555.36	172.86 191.45	0.63 0.59	1.03 1.02	0.46	0,17	0.49
	1,00	1519.22	1041.00	1048.36		1049.38	J.503065	6.39	333.36		0.59	1,02	0.56	0.24	0.54
DownAll DownAll	1450	180.00 276.46	1041.00 1041.00	1042.98 1043.47		1043.55 1044.27	0.008641	6.16 7.18	29.22 38.49	17.57 18.95	0,84 0,89	0.83 1.07			0.83
Down All	1450.	276.48 625.68	1041.00	1043.47	+	1044.27	0.009135	7.18 8.65	38.49 78.79	18.95 117.63	0.89 0.86	1.07	0.03	0.02	1.07 0.31
DownAll DownAll	1450 1450	866.60	1041.00	1046.19 1047.13		1047.33	0.005104 0.003910	8.64 8.63	226.16 367.47	143.40	0.74	1,21	0.38	0.20	0.49
DownAll	1450.	1078,16 1319.22	1041.00 1041.00	1047.13	·	1048.24 1049.22	0.003910	8.70	531.90	158.66 174.64	0.67 0.62	1.14	0.51	0.28	0.55
D	1.00	400.00		4040.04		404040	2 22 1522	4.50	00.70	00.07					
DownAll DownAll	1400	180.00 276.46	1041.00	1042.84	<del> </del>	1043.16	0.004529	4.53 5.12	39.73 54.03	22.97 26.23	0,61 0,63	0.45			0.45
DownAll	1400.	625.68	1041.00	1045.31		1045.82	0.002783	5.77	183.84	115.73	0.53	0.57	0.18	0.05	0.27
DownAll DownAll	1400	866.60 1078.16	1041.00	1046.45 1047.38		1046.99 1047.95	0.002081	5,98 6,16	326.80 462.64	135.85 155.96	0.48 0.45	0.56	0.28	0.12	0.30
DownAll	1400.	1319.22	1041.00	1048.37		1048.96	0.001500	6.35	623.53	168.77	0.43	0.56	0.36	0.19	0.33
DownAll	1350.	180,00	1041.00	1042.57		1042.90	0.006035	4.59	39.22	29.55	0.70	0.49			0.49
DownAll	1350	276.46	1041.00	1043.29		1043.59	0.003929	4.48	62.47	38.57	0.59	0.42	0.03		0.39
DownAll DownAll	1350. 1350.	625.68 866.60	1041.00	1045.40		1045.64	0.001408	3.96 3.96	226.68 369.04	112.92 124.47	0.39	0,27 0.25	0.10 0.13	0.03	0.17
DownAll	1350.	1078,16	1041.00	1047.55		1047.80	0.000730	4.03	492.60	133.74	0.31	0.24	0.14	0.07	0.16
DownAll	1350	1319.22	1041.00	1048.56		1048,82	0.000610	4.13	632.08	143.81	0.29	0.24	0.15	0,08	0.16
DownAll	1300.	180.00	1040.00	1041.74		1042.46	0.011326	6.78	26.54	16.19	0.93	1.03			1.03
DownAll DownAll	1300	276.46 625.68	1040.00	1042.36	1043.70	1043.24	0.010005	7.53 9.85	36.71 67.56	16.86 26.53	0,90	1.17	0.37	0.21	1.17
DownAll	1300.	866.60	1040.00	1044.52	1044.52	1046.55	0.010201	11.44	87.13	32.96	0.99	2.20	0.58	0.41	1.46
DownAll DownAll	1300.	1078.16 1319.22	1040.00 1040.00	1045.15 1045.85	1045.15 1045.85	1047.50 1048.50	0.009777	12.32	110.02 141.86	40.51 50.60	1.00	2.44	0.68	0.55 0.67	1.45 1.43
					.5.5,03								9.73	V.67	
DownAll DownAll	1250. 1250.	180.00 276.46	1039.00	1041.51 1042.10		1042.00 1042.79	0.005707	5.61 6.64	32.10 41.66	15.54 16.85	0.69	0.65 0.87	F		0.65 0.87
DownAll	1250.	625.68	1039.00	1043.60		1044.85	0.008220	8.95	69.93	21.34	0.87	1.44			1.44
DownAll DownAll	1250	866.60 1078.16	1039.00	1044.42 1045.10	1044.64	1045.92	0.008189	9.81	88.70 107.42	24.88	0.88	1.65		0.09	1.55
DownAll	1250.	1319.22	1039.00	1045.84	1045.26	1047.69	0.007149	10.91	134.97	42.61	0.84	1.88		0.32	1.24
DownAll	1200	180.00	1039.00	1041.02		1041.64	0.008826	6.31	28.51	16.52	0.85	0.87			0.86
DownAll	1200.	278.46	1039.00	1041.55		1042.39	0.009325	7.35	37.68	18.03	0.89	1.11	0.03		1,04
Down All Down All	1200. 1200.	625.68 866.60	1039.00	1043.24 1044.06		1044.44	0.007526	8.78 9.78	73.27 98.05	28.03	0.85	1.37	0.09	0.06	0.98
DownAll	1200	1078.16	1039.00	1044.72		1048.42	0.006517	10.45	120.72	35.76	0.84	1.72	0.37	0.34	1.10
DownAll	1200	1319.22	1039.00	1045.45		1047.36	0.006076	11.09	150.72	48.40	0.83	1.85	0.46	0.31	0.99
DownAll	1150,	180.00	1038.78	1040.77		1041.20	0.006652	5.30	33.97	20.82	0.73	0.62			0.62
DownAll DownAll	1150 1150	276.46 625.68	1038.78	1041.43		1041.94	0.005437	5.74 6.49	48.20 99.53	22.06 31.62	0.68	0.67 0.73	0.13		0.67 0.64
Jown All	1150.	866.60	1038.78	1044.31		1045.09	0.003425	7.07	130.41	35.55	0.59	0.73	0.13	0.03	0.64
DownAll DownAll	1150. 1150	1078.18 1319.22	1038.78 1038.78	1045.08 1045.91		1045.95 1046.87	0.003094	7.48 7.88	161.18 201.88	44.32 54.21	0.58 0.57	0.86 0.91	0.29	0.10	0.61
			1030.78								0.57	0,91	0.32	0.16	0.57
Down Aff	2200	180.00	1038.00	1040.55		1040.92	0.004214	4.92 5.78	36.60 47.83	17.33	0.60	0.50			0.50
	1100.		1038.00	1041.17		1041.69	0.004582	7.37	84.93	18.59 24.04	0.64	0.65			0.65 0.95
DownAll DownAll	1100. 1100.	276.46 625.68	1038.00	1042.93											
DownAll DownAll DownAll	1100. 1100 1100	625.68 866.60	1038.00 1038.00	1043.89		1044.87	0.004664	7.93	109.50	26.21	0.68	1.04		0.06	1.02
DownAlf DownAlf DownAlf DownAlf	1100. 1100	625.68	1038.00				0.004664 0.004289 0.004015	7.93 8.35 8.78	109.50 130.97 160.92	26.21 30.10 43.96	0.68 0.66	1.11		0.11	0.97
DownAll DownAll DownAll DownAll DownAll	1100 1100 1100 1100 1100	625.68 866.60 1078.16 1319.22	1038.00 1038.00 1038.00 1038.00	1043.89 1044.66 1045.49		1044.87 1045.75 1046.68	0.004289	8.35 8.78	130.97 160.92	30.10 43.96	0,66 0.64	1.11			0.97 0.79
DownAll DownAll DownAll DownAll DownAll	1100, 1100 1100, 1100,	625.68 866.60 1078.16	1038.00 1038.00 1038.00	1043.89 1044.66		1044.87 1045.75	0.004289	8.35	130.97	30.10	0,66	1.11		0.11	0.97 0.79 0.59
DownAll DownAll DownAll DownAll DownAll	1100, 1100 1100, 1100, 1100, 1100,	625.68 866.60 1078.16 1319.22	1038.00 1038.00 1038.00 1038.00	1043.89 1044.66 1045.49 1040.24		1044.87 1045.75 1046.68	0.004289 0.004015 0.005560	8.35 8.78 5.27	130.97 160.92 34.13	30.10 43.96 18.67	0,66 0.64 0.69	1.11 1.17	0.08	0.11	0.97 0.79

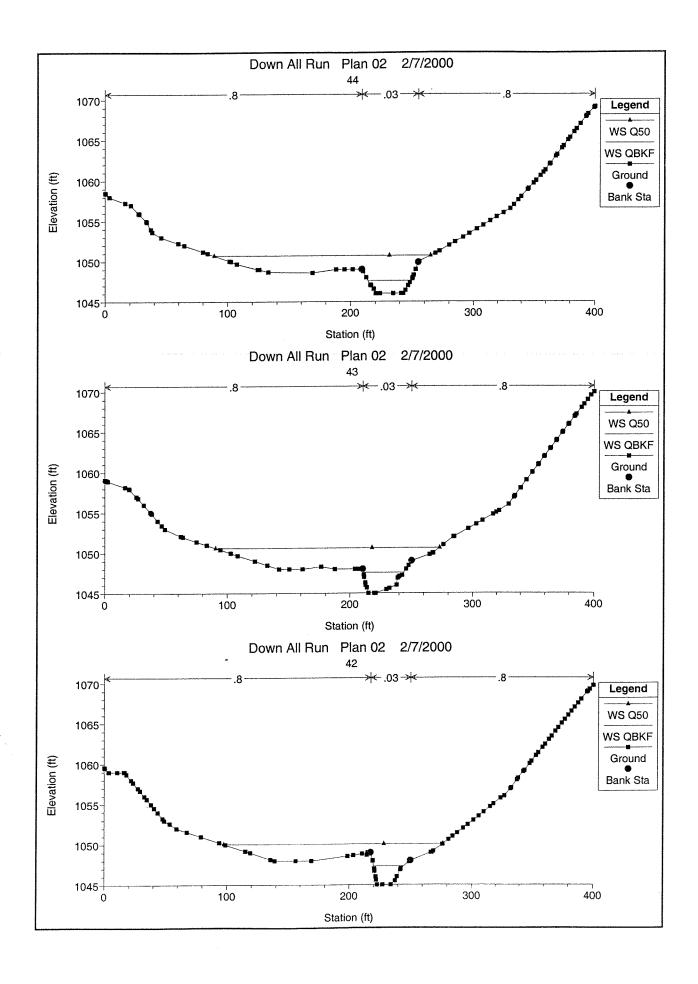
HEC DAG	Diag: Diag	Min Ch El	عنيابي	pina Cr	صيب الم	E.G. Slope		Captie	June of June 1	Froude # Chi	Shear Chan	Shear LOB	Shear ROB	Shear Total
Reach Riv	ver Sta C Total (cfs)	(8)	W.S. Elev (ft)	(10)	(ft)	(19/11)	(ft/s)	(sq ft)	(ft)		(if pe(di)	(lib/eq fr)	(flipe(dli)	(fb/sq ft)
DownAll 1050	1319	22 1038.0	0 1045.44		1046.46	0.002789	8.15	220.82	74.25	0.58	0.96	0.08	0.21	0.48
DownAll 1000	180	00 1037.5	0 1039.89		1040.37	0.006399	5.55	32.41	17.89	0.73	0.66			0.66
DownAll 1000					1041.18	0.005403		45.92 91.05				0.07	0.00	0.72
DownAll 1000 DownAll 1000					1043.30	0.004436		140.53				0.07	0.06	0.86
DownAll 1000	1078.	16 1037.5	1044.42		1045.36	0.003088		196.92		<del></del>		0.09	0.22	0.46
DownAll 1906	1319	22 1037.5	1045.30		1048.32	0.002778	8.18	272.02	96.28	0,58	0.96	0.08	0.27	0.46
DownAll 950	180	00 1037.0	1039.88		1040.12	0.002355	3.91	46.06	20.65	0,46	0.30			0.30
DownAil 950	276			+	1040.93	0,002341	4.44	62.24			<del></del>			0.37
DownAll 950.  DownAll 950.	625. 866.				1043.06 1044.23	0.002210	5.58 6.14	118.30 175.29					0.04	0.37
DownAll 950	1078	<del> </del>	1044,49		1045.18	0.002010	6.56	244.97	94.98	0.47	0.64		0.15	0.31
DownAll 950.	1319.	22 1037.00	1045.38		1046.12	0.001964	6,96	340.01	118.58	0.46	0.69		0.20	0.33
DownAll 900.	180.	00 1036.7	1039.72		1039.99	0.002553	4.15	43.42	17.75	0.47	0.34			0.34
DownAll 900	276.		-		1040.80	0.002861	4.91 6.83	57.74 106,64			0.45	0.06	0.02	0.39
DownAll 900.  DownAll 900.	625. 866.				1042.90 1044.07	0.003294	7.79	148.12	<del> </del>		0.93	0.29 0.42	0.02	0.57
DownAll 900	1078.	16 1036.77	1043.88		1044,98	0.003290	8.49	208.28		0.60	<del></del>	0.50	0.18	0.41
DownAll 900	1319.	22 1036.77	1044.68		1045.94	0,003255	9.14	294.27	121.15	0.61	1.18	0.57	0.25	0.46
DownAll 850.	180,	00 1037.00	1038.88	1038.88	1039.69	0.012720	7.24	24.87	15.45					1.17
DownAll 850 DownAll 850	276. 625.			1039.45 1040.94	1040.47 1042.55	0.012094	8.13 10.17	34.00 68.84	16.80 27.09	1.01	1.38 1.87	0.56		1.38
DownAll 850	868			1040,94	1042,55	0.009966	11.34	90.85			2.16	0.87	0.22	1.49
DownAll 850.	1078.	16 1037.00	1042.39	1042.39	1044.62	0.009061	12.02	123.62			2.30	1.04	0.24	1.00
DownAll 850.	1319	22 1037.00	1043.05	1043.05	1045.57	0.008581	12.79	170.72	77.09	0.98	2.49	1.18	0.48	1.10
DownAll 800.	180.				1039.13	0.003981	4.91	36.65	16.83	0.59	0,49			0.49
DownAll 800. DownAll 800.	276. 625.				1039.92 1041.89	0.004359	5,76 8.17	48.04 96.02	18.29 49.21	0.63	0.64 1.13	0.27	0.14	0.64
DownAll 506	868.				1042.91	0.006504	9.87	125, 16	55.94		1.58	0.53	0.30	0.85
DownAll 800	1078.			1042.17	1043.75 1044.67	0.007518	11.24 12.38	148.36 181.44	61.07 67.64	0.90 0.94	1.99 2.33	0.76 1.01	0.44 0.60	1.06
DownAll 800.	1319	22 1036.00	1042.32	1042.17	1044.67	0.007969	12.30	101,44	67.54	0.94	2.33	1.01	0,60	1.24
DownAll 750	180.0			1037.95	1038.76	0.012579	7.21	24.95	15.61	1.01	1,16			1.16
DownAll 750. DownAll 750.	276. 625.			1038.52 1040.05	1039.53	0.011913	8.05 9.63	34.32 75.58	17.26 63.74	1.01	1.35 1.70	0.38	0.03	1.35
DownAll 750	866.0		+	1040.78	1042.52	0.008742	10.44	131.86	78.39	0.95	1.85	0.70	0.38	0.87
DownAll 750	1078.				1043.33	0.007827	10.99 11.58	185.97 248.00	88.04 96.94	0.93 0.91	1.94 2.05	0.88	0.58	0.98
DownAll 750.	1319.2	22 1036.00	1042.16		1044.19	0.007162	11.30	240.00	30,34	0.91	2.05	1.03	0.72	1.09
DownAll 700.	180.0				1038.08	0.004460	4.92	36,57	18,40	0.62	0.51			0.51
DownAll 700 DownAll 700	276.4 625.6				1038.91	0.003959	5.40 6.58	51,23 121,17	20.13 82.95	0.60 0.64	0.56	0.08	0.14	0.56 0.35
DownAll 700.	866.6				1041.99	0.003297	6.99	208.23	99.01	0.59	0.79	0.23	0.24	0.41
DownAll 700 DownAll 700	1078.				1042.80	0.002980	7.38 7.80	285.72 375.50	111.71 125.00	0.58 0.57	0.84 0.89	0.30	0.31	0.45
DownAll 700	1319.2	1035.00	1042.73		1043.65	0.002702	7.00	373.30	125.00	0.57	0.03	0.37	0.36	0.49
DownAll 850.	180.0			1038.01	1037.90	0.001597	3.66	49.13	16.49	0.37	0.25			0.25
DownAll 650 DownAll 650	276.4 625.6	<del></del>		1036.63	1038.73	0.002180	4.45 6.48	62.10 143.01	20.07 100.45	0.44 0.52	0.36	0.11	0.09	0.36 0.23
DownAll 650.	866.6		1040.95		1041.82	0.002939	7.55	238.18	120.48	0.56	0.88	0.26	0.21	0.34
DownAll 850. DownAll 850.	1078.1			1040.58	1042.62 1043.46	0.003157	8.38 9.24	313.95 394.36	126.86 134.10	0.59 0.62	1.03	0.37	0.33	0.46 0,59
2000	1515.2	2 1033.33	1042.70	1040.50	10-70-40	0.00000		501.00	101.75	0.02				0,00
DownAll 600	180.0			1036.85	1037.67	0.012872	7.24 8.08	24.86	15,44 17,06	1.01	1,18			1.18
DownAll 800. DownAll 800.	276.4 625.6			1037.43	1038.44	0.008127	8.97	34.20 77.48	64.12	0.88	1.37	0.12	0.07	1.37 0.58
DownAll 600	866.6			1039.74	1041.52	0.008007	10.14	144.03	129.67	0.90	1.73	0.45	0.23	0.54
DownAlf 600. DownAlf 600.	1078.1			1040.99	1042.31	0.008108	11.06	214.40 297.18	145.89 158.49	0.93 0.94	1.98	0.68	0.43	0.72 0.91
			19.10.00											
DownAll 550 DownAll 550	180.0 276.4			<u>-</u>	1037.05	0,006137	5.81 6.69	30.98 41.30	14.97 16.20	0.71	0,70			0.70 0.88
XownAll 550.	625.6		1037.19	1038.34	1040.06	0.006359	8.47	74.16	32.18	0.82	1.29		0.01	0.88
XownAll 550.	866.6	0 1034.00		1039.30	1041.08	0.006991	9.47	153.05	128.35	0.83	1.51	0.30	0.25	0.50
JownAll 550 JownAll 550	1078.1		1040.26 1040.86		1041.86	0.006888	10.25 10.93	231.31 329.35	150.05 170.51	0.84 0.84	1.69	0.51 0.71	0.41	0.64 0.78
ovenAll 500.	180.0 276.4		1036.12 1036.69		1036.70	0.007674	6.12 7.25	29.41 38.14	15.02 15.60	0.77	0.80			0.80 1.06
Jown All 500	625.6		1038.49	1038.14	1039.67	0.008193	8.76	98.21	85, 19	0.85	1,40		0.22	0.56
kownAll 500.	866.6		1039.20		1040.69	0.008257 0.008457	9.87 10.80	173.95 248.74	140.22 160.72	0.87	1.67	0.10 0.36	0.44	0.62 0.79
kownAll 500. kownAll 500	1078.1	-	1039.70 1040.19	1040.19	1041.46	0.008457	11.77	333.57	181.02	0.90	2.21	0.36	0.79	0.79
ownAll 450, ownAll 450.	180.0 276.4	~	1036.08 1036.85		1036.34 1037.12	0.004011	4.08	44.07 65.83	27.52 28.99	0.57	0.37			0.37
ownAll 450	625.6	8 1033.00	1038.90		1039.27	0.001684	4.89	199.94	149.35	0.42	0.39	0.08	0.06	. 0.14
ownAll 450.	866.6		1039.75		1040.22	0.001697	5.55 6.07	365.24 496.68	206.24	0.43	0.48 0.55	0.15 0.20	0.13	0.18 0.25
kownAli 450. kownAli 450.	1078.1 1319.2		1040.38 1040.98		1040.93	0.001737	6.64	623.80	214.88	0.45	0.63	0.24	0.19	0.25
ownAll 400.	180.0 276.4		1035.33	1035.71	1036.01	0.009096	6.59 8.24	27.32 33.57	14.94 15.48	0.86	1.39			0.94 1.39
ownAll 400.	625.6	1033.00	1037.51	1037.51	1038.98	0.011229	9.74	64.22	21.88	1.00	1.77			1.77
ownAt 400	866 6		1038.39	1038.39	1039.94	0.009917	10.04	124.17	141.56 206.90	0.97	1.80	0.23	0.20	0.53
lownAll 400.	1078.1		1038.96	1038.96	1040.65	0.008772	10.39	395.39	216.70	0.94	1.87	0.50	0.36	0.58 0.74
ownAll 350.	180.00 276.40		1034.73	1034.73	1035.45	0.013224	6.84 7.82	26.30 35.36	18.41 18.88	1.01	1.09			1.09
							8.94	70.02	20.47	0.85	1,44			
ownAll 350. ownAll 350.	625.68	1033.00	1036.97		1038.21	0.008223	9.94	87.16	21.00	0.86	1.70			1.44

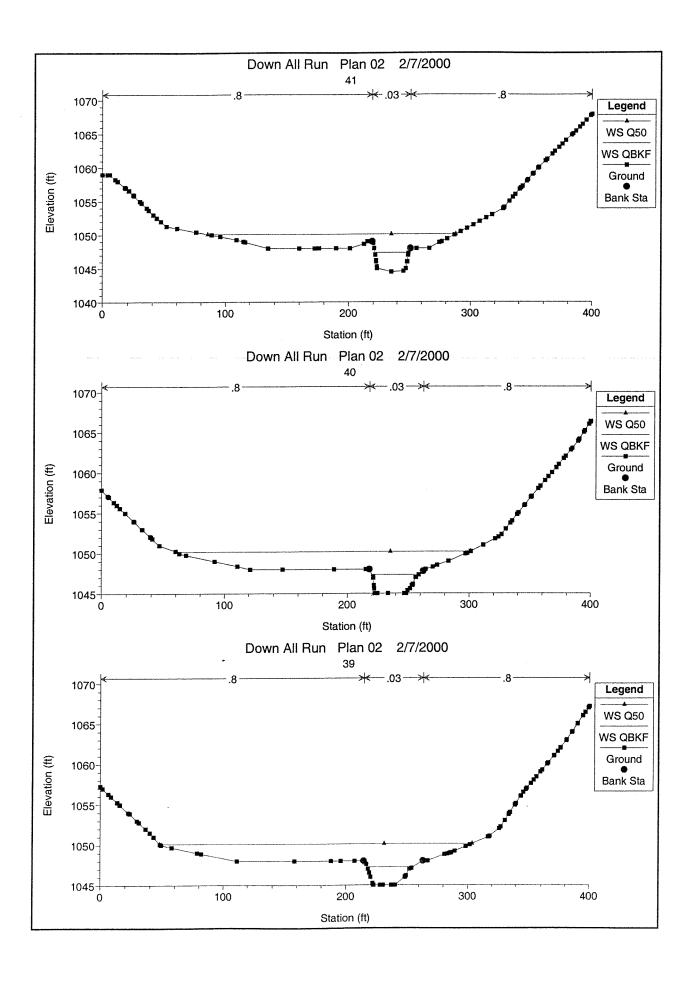
Fleach	A.C. Dion River Sta	Q Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chi	Shear Chan	Shear LOB	Shear ROB	Shear Total
	1	(cfs)	(8)	(ft)	(ft)	(ff)	(IVII)	(ft/s)	(#q ft)	(ft)		(fb/sq ft)	(ityleq ft)	(Bb/sq ft)	(fb/sq ft)
Dawn All	350	1078.16	1033.00	1038.44	1038.12	1040.18	0.007998	10.63	181.62	201.32	0.86	1.88	0.22	0.22	0.4
DownAll	350	1319.22	1033.00	1039.24		1041.03	0.006859	10.90	344.57	209.06	0.81	1.85	0.49	0.52	0.6
DownAll	300.	180.00	1031.00	1034.71		1034.97	0.002754	4,12	43.71	19.61	0.49	0.34			0.3
DownAll	300	276.48	1031.00	1035.33		1035.71	0.003069	4.91	56.28	20.52	0.52	0,46			0.4
DownAll	300	625.68	1031.00	1037.12		1037.79	0.003413	8.57	95,21	23.76	0.57	0.73			0.7
DownAll	300.	866.60	1031.00	1038.02	1036.44	1038.88	0.003376	7,48	166.28	206.94	0,59	0.88	0.06	0.06	0.1
DownAll	300.	1078.16	1031.00	1038.74	1037.04	1039.71	0.003239	7.99	317.23	210.81	0.59	0.96	0.18	0.20	0.3
DownAil	300:	1319.22	1031.00	1039.53		1040.59	0.003038	8.43	484.87	214.87	0.58	1.03	0.29	0.33	0.4
	1									05.70	2.40	2.05			
DownAll	250.	180.00	1032.00	1034.57		1034.83	0.002758	4.14	48.34	25.73	0,48 0.53	0.35	0.11		0.2
DownAll	250.	276.46	1032.00	1035.16		1035.55	0.003229	5.02 8.74	64.92 130.94	31.24 44.46	0.53	0.48	0.19 0.40	0.02	0.5
DownAll	250.	625.68	1032.00	1036.91		1037.60	0.003793	7.39	245.03	164.20	0.62	0,78	0,40	0.28	0.3
DownAll DownAll	250 250.	866.60	1032.00	1037.85		1038.69	0.003897	7.66	408.55	216.59	0.59	0.90	0.49	0.18	0.3
****************	250.	1078.16	1032.00	1038.64 1039.48		1040.39	0.003403	7.88	591.88	217.92	0.57	0.92	0.52	0.38	0,4
DownAll	230.	1319.22	1032.00	1039.40		1040.35	0.002.547	7.00	331.00	211.02	0.37	0.52	0.02		
DownAll	200	180.00	1032.00	1034.40		1034.68	0.003139	4.26	42.26	19.91	0.52	0.37			0.3
DownAll	200	276.46	1032.00	1034.97		1035.38	0.003652	5.14	53.76	20.93	0.57	0.51			0.5
DownAll	200.	625.68	1032.00	1036.71		1037.41	0.003871	6.72	93.13	24.27	0,60	0.78			0.7
Xown All	200.	866.60	1032.00	1037,66		1038.50	0.003687	7.36	205.62	185.01	0.60	0.88	0.15	0.12	0.2
Down All	200	1078.16	1032.00	1038.46		1039.35	0.003274	7.66	376.48	224.83	0.58	0.91	0.27	0.24	0.3
Javen All	200.	1319.22	1032.00	1039.33		1040.25	0.002848	7.88	572.83	228.30	0.55	0.92	0.36	0.36	0.4
DownAll	150.	180.00	1032.00	1033.66	1033.66	1034.36	0.012772	6.70	26.85	19.45	1.01	1.04			1.04
Joven All	150.	276.46	1032.00	1034.21	1034.13	1035.05	0.010532	7.32	37.76	20,19	0.94	1.14			1.11
lownAll	150.	625.68	1032,00	1036.34	1035.50	1037.18	0.005073	7.33	88.51	71.22	0.70	0.95		0.02	0,35
DownAll	150.	866.60	1032.00	1037.46		1038.31	0.003720	7.47	286,90	240.23	0.62	0.90	0.14	0.18	0.27
XownAll	150.	1078.16	1032.00	1038.34		1039.18	0.002999	7.56	500.75	248.53	0.58	0.87	0.25	0.30	0.36
NownAll .	150	1319.22	1032.00	1039.24		1040,10	0,002527	7.70	729.43	256.50	0.54	0.86	0.32	0.38	0.43
XxwnAlf	100.	180.00	1031.00	1033.29		1033.77	0.006049	5.56	32.37	16.91	0.71	0,65			0.65
)ownAll	100.	276.46	1031.00	1034.03		1034.61	0.005264	6.08 7.21	45.45 96.93	18.14 108.75	0.68	0.72	0.03	0.03	0.72
ownAll	100	625.68	1031.00	1036.14	1034.89	1036.94	0.004123	7.78	286.11	218.81	0.60	0.95	0.03	0.03	0.28
JownAll JownAll	100.	866.60 1078.16	1031.00	1037.20		1039.01	0.0033441	8.13	474.76	232.83	0.58	0.98	0.23	0.13	0.39
XownAli	100.	1319.22	1031.00	1038.04		1039.94	0.002856	8.45	686.11	248.71	0.57	1.02	0.42	0.42	0.48
ANTIAN	100	1319.22	1031.00	1030,92		1035.54	0.0020301	0.40	000.11	240.11	0.37	1.02	U.72	0.42	
ownAll	50.	180.00	1031.00	1033.12		1033.47	0.004544	4.73	38.03	20.75	0.62	0.48			0.48
DOWNAE	50	276.46	1031.00	1033.12		1034.33	0.003472	4.81	57.49	24.80	0,56	0.48			0.46
own All	50.	625.68	1031.00	1036.30		1036,69	0.001766	4.98	169.86	119.05	0.43	0.41	0.05	0.06	0.15
ownAll	50.	868.60	1031.00	1037.43		1037,87	0.001465	5.33	320.31	145.88	0.41	0.43	0.06	0.13	0,19
own All	50.	1078,16	1031.00	1038.28		1038.77	0.001345	5,65	459.88	180.29	0.40	0.46	0.06	0.15	0.2
own All	50	1319.22	1031.00	1039.17		1039.70	0.001249	5.96	634.20	211.26	0.40	0.49	0.06	0.18	0.23
lown All	0	180.00	1030.00	1032.51	1032.15	1033.14	0.008002	6.40	28.13	13.46	0.78	0.87			0.87
ownAll	0.	276.46	1030.00	1033,21	1032.78	1034.03	0.008009	7.27	38.04	14.55	0.79	1.05			1.05
ownAll	o.	625.68	1030.00	1035.19	1034.53	1038.44	0.008006	8.96	69.80	18.60	0.82	1,44			1.44
емпА#	0.	866.60	1030.00	1036.08	1035.56	1037.61	0.008002	9.94	91.48	56.18	0.84	1.68	0.22	0.04	0.73
own All	0	1078.16	1030.00	1036.68	1036.24	1038.50	0.008009	10.84	130.64	75.07	0.86	1.91	0.44	0.27	0.80
own All	o.	1319.22	1030.00	1037.30	1036.90	1039.42	0.008007	11.72	184.87	103.01	0.87	2.15	0.62	0.42	0.84

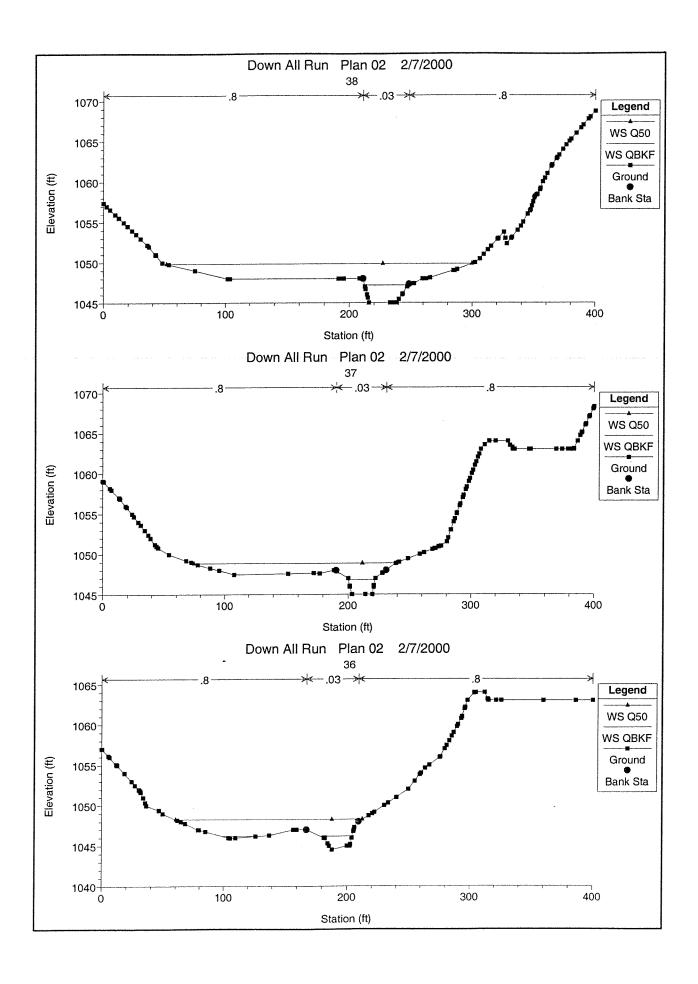


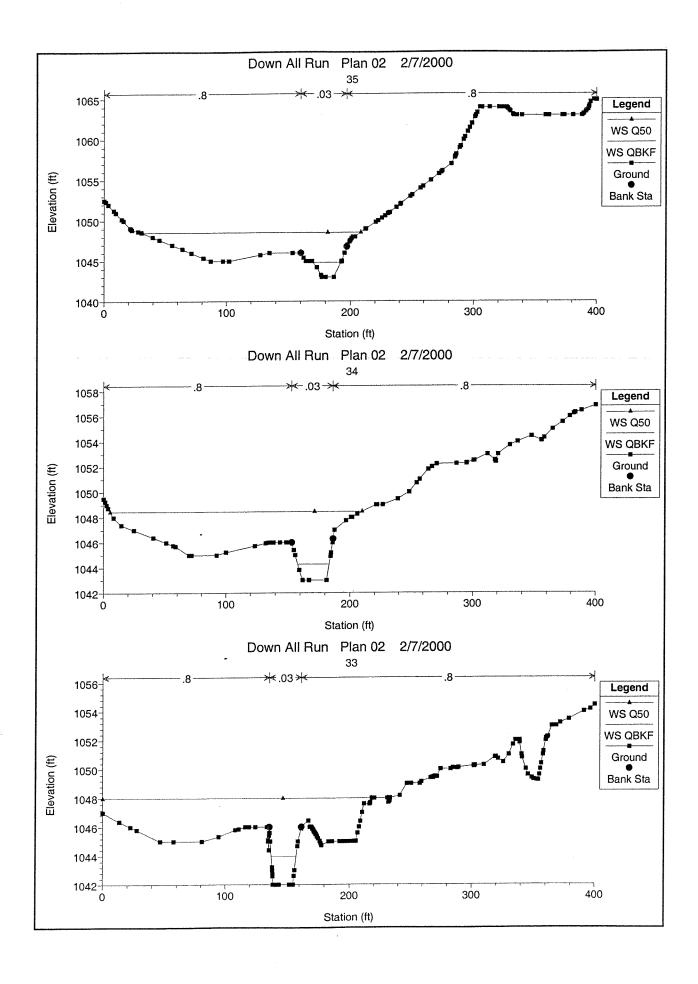


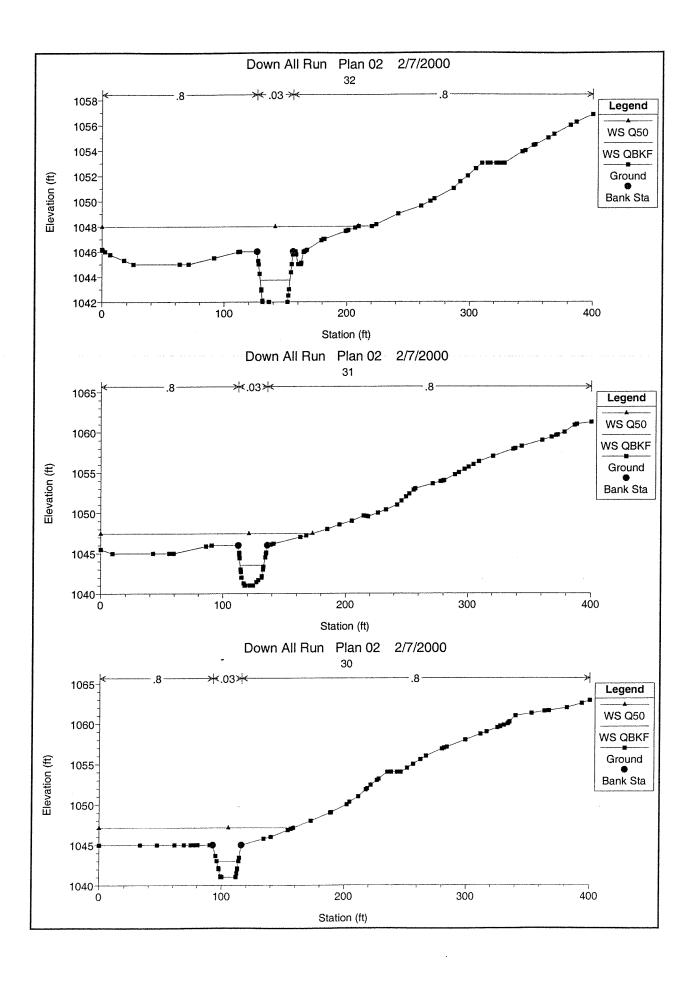


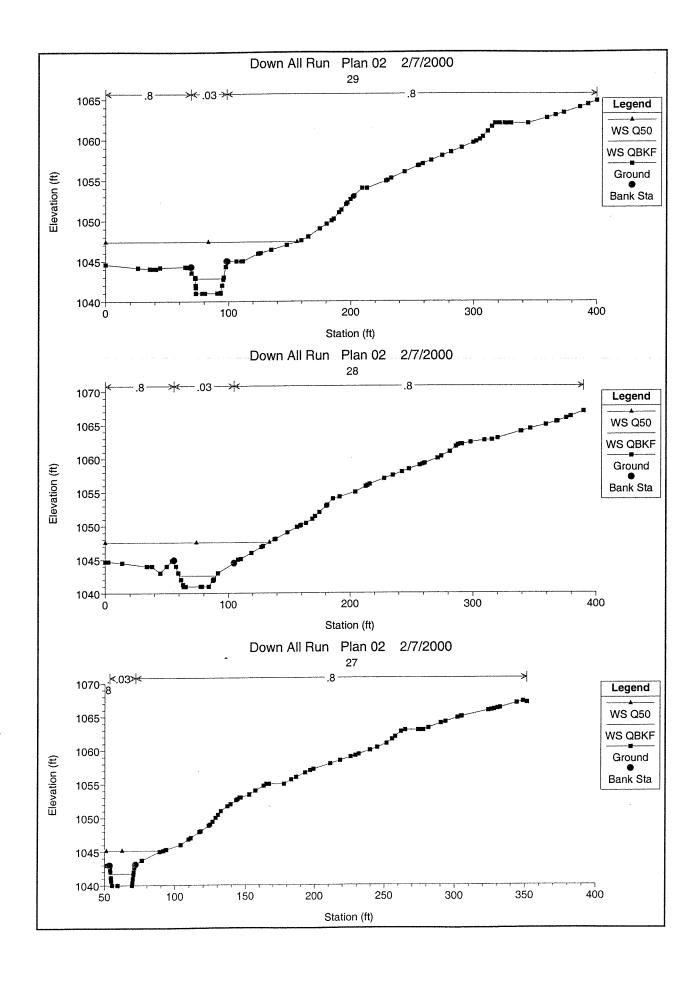


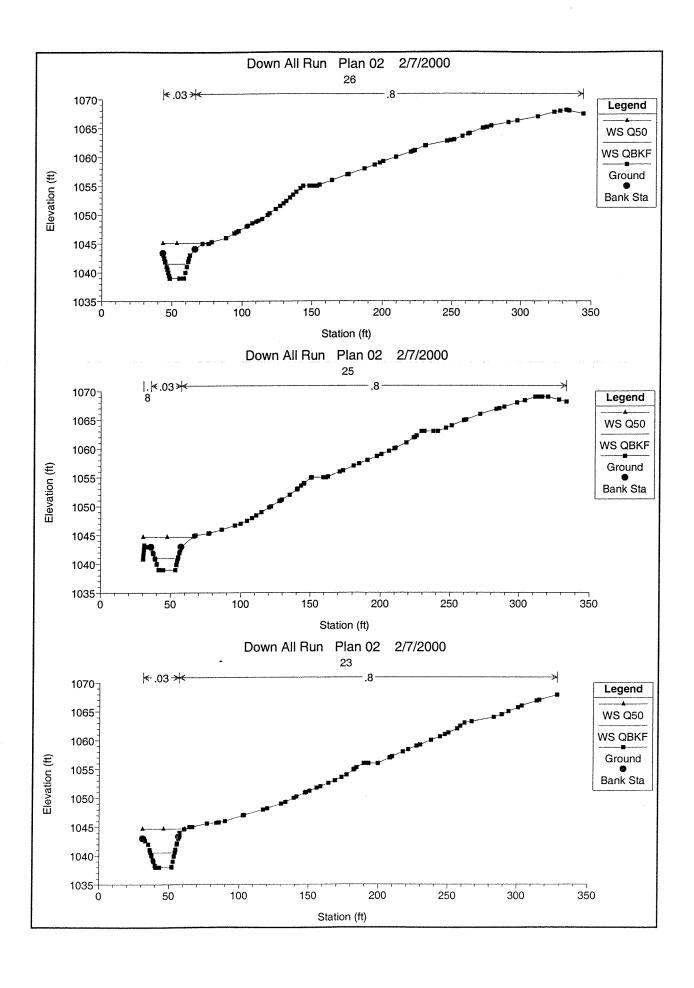


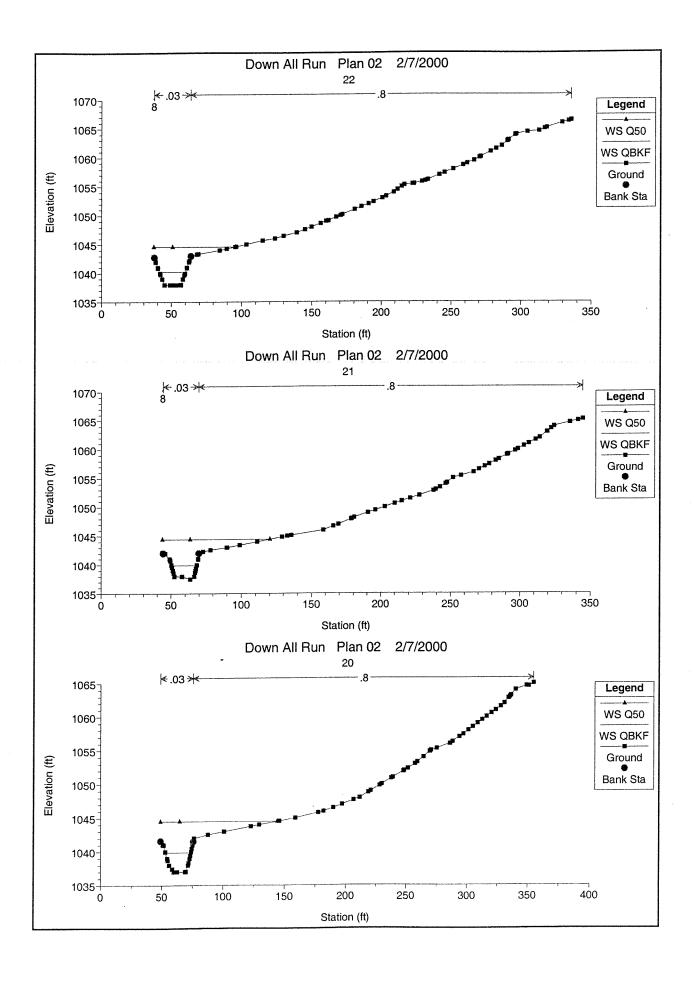


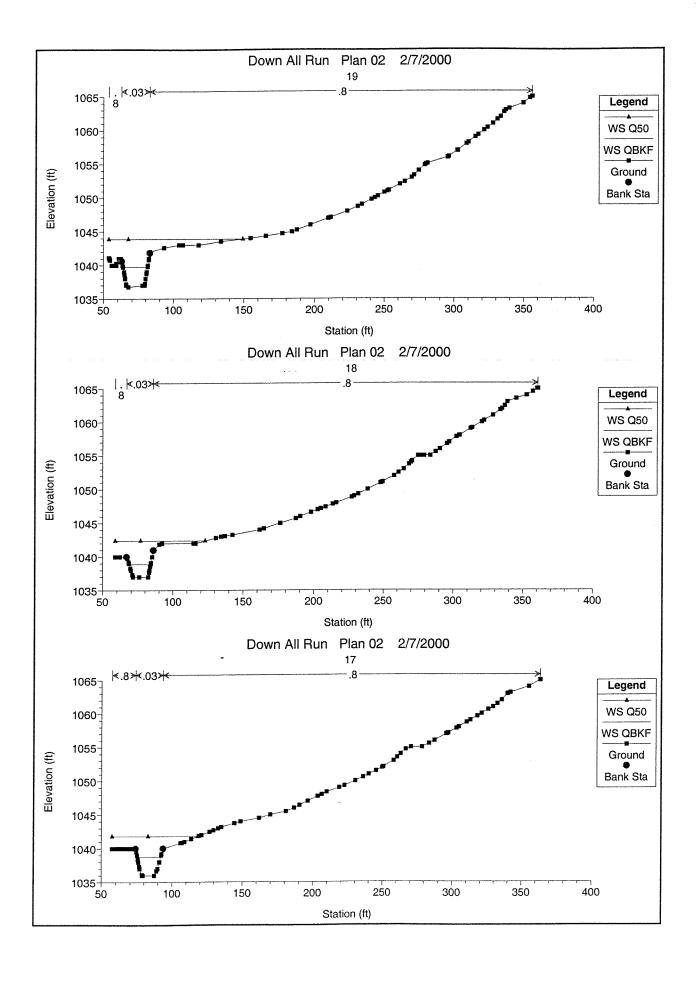


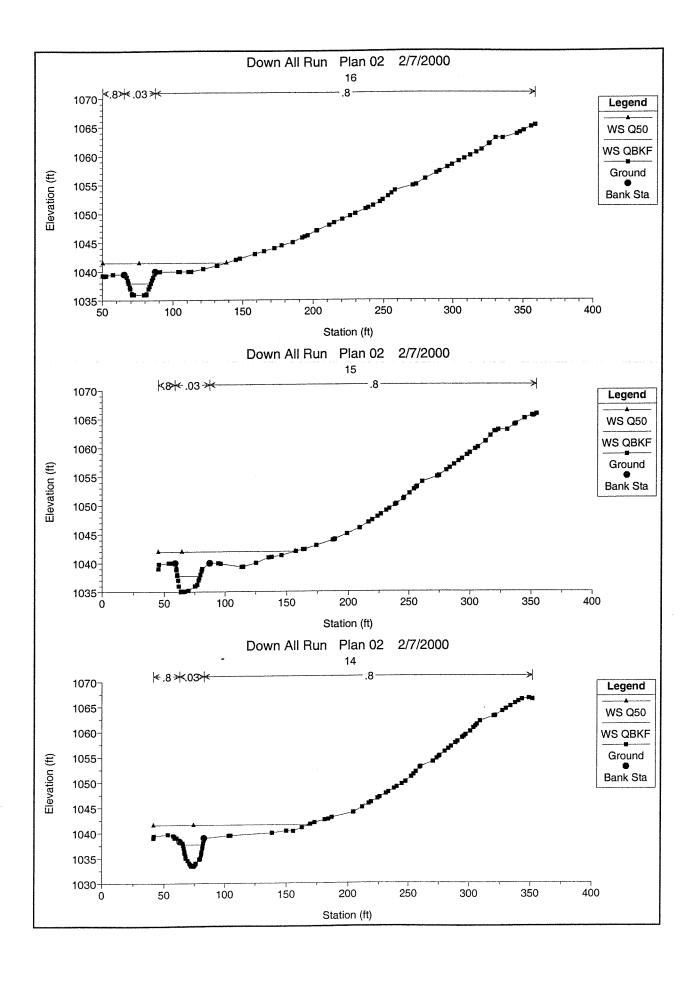


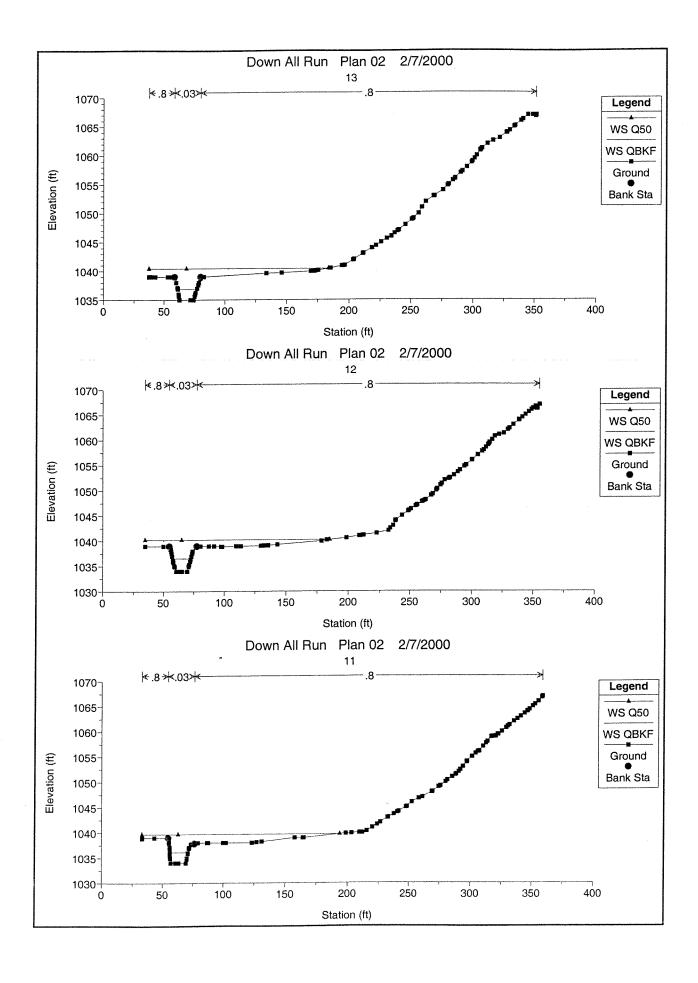


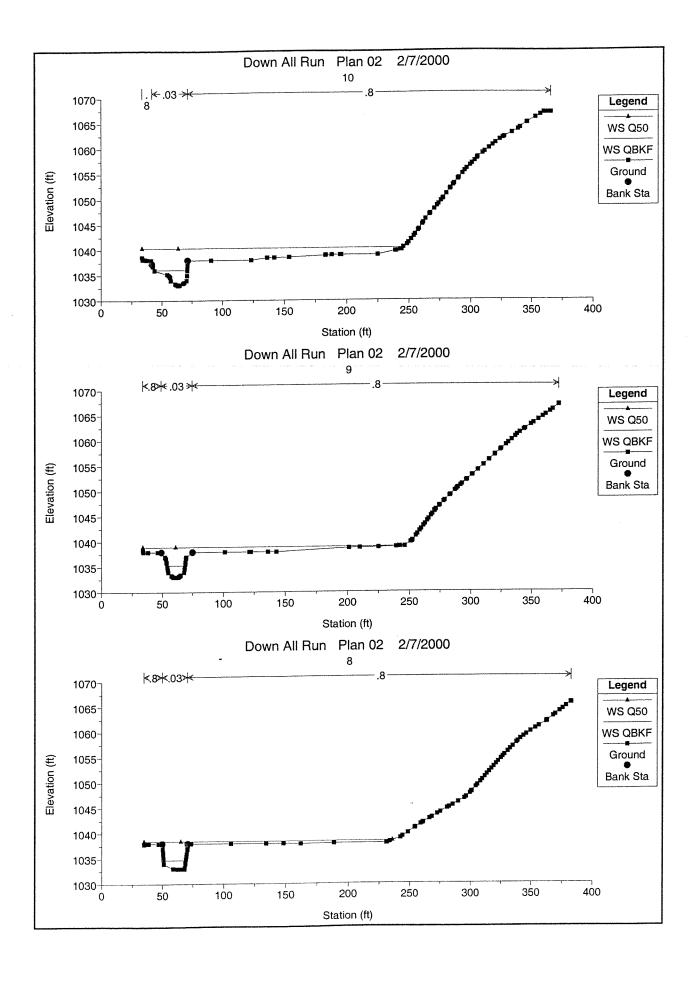


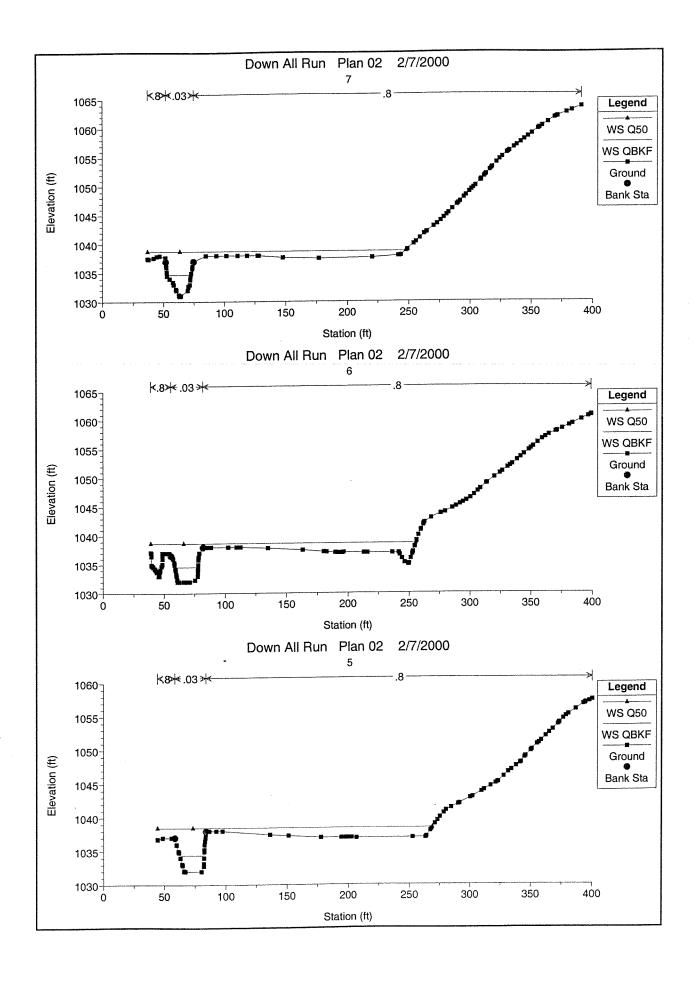


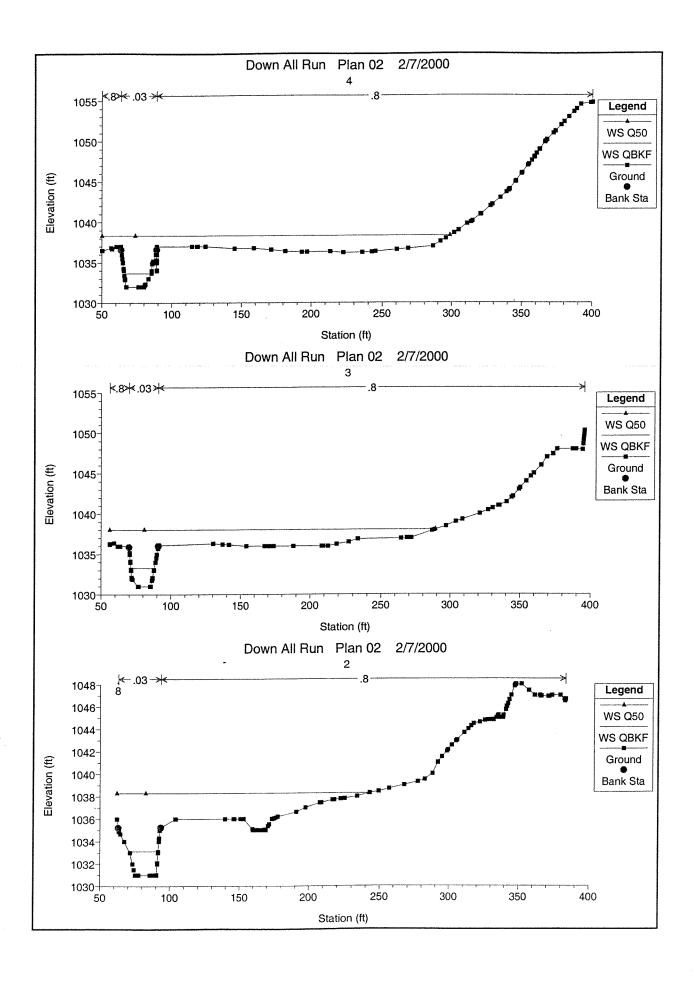


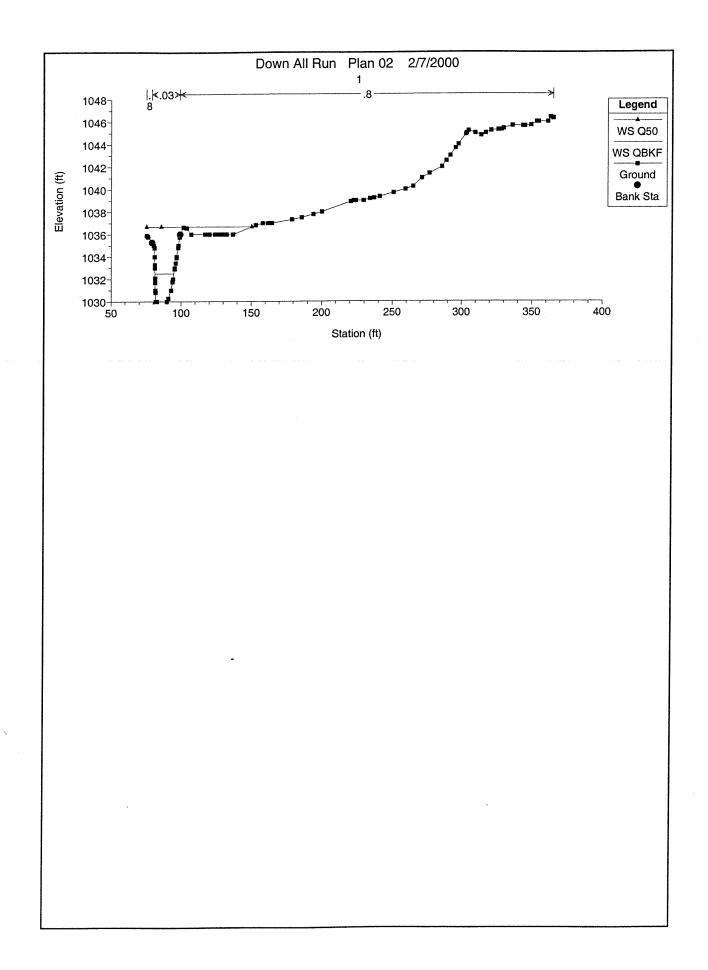












Appendix F

Site Photos

Reference Reach Glade Creek



Title: Reference Reach Glade Creek

Prepared by: Wil Welhelm.

Job Number: 011795000

Sheet 1 of 4



#1 -Looking downstream at STA 0+00



Title: Reference Reach Glade Creek

Prepared by: Wil Welhelm.

Job Number: 011795000

Sheet 2 of 4



#2 - Looking upstream at STA 2+25



Title: Reference Reach Glade Creek

Prepared by: Wil Welhelm.

Job Number: 011795000

Sheet 3 of 4



#3 – Looking downstream at STA 1+30



Title: Reference Reach Glade Creek

Prepared by: Wil Welhelm.

Job Number: 011795000

Sheet 4 of 4



#4 - Looking upstream at STA 1+30

Upstream Segment Jumping Run North of SR 1614



Title: Upstream Segment - Jumping Run Job Number:

Prepared by: Will Wilhelm.

Job Number: 011795000

Sheet 1 of 4



#1 - Cattle have unlimited access to stream



#2 - Cattle in stream with vertical banks and no riparian vegetation.



Title: Upstream Segment - Jumping Run

Prepared by: Will Wilhelm.

Job Number: 011795000

Sheet 2 of 4



#3 – Typical banks with cattle disturbance (foreground) and vertical undermined banks (background)



#4 - Cattle crossing upstream of SR1614 - looking upstream



Title: Upstream Segment - Jumping Run Job Number:

Prepared by: Will Wilhelm.

Job Number: 011795000

Sheet 3 of 4



#5 - Chanalized section of stream. Relic channel background.



#6 - Bank disturbance from cattle (typical).



itle: Upstream Segment - Jumping Run Job Number:

Prepared by: Will Wilhelm.

Job Number: 011795000

Sheet 4 of 4



#7-Single row of trees upstream of SR1614.

Downstream Segment Jumping Run East of SR 1605



Title: Downstream Segment - Jumping Rundob Number:

011795000

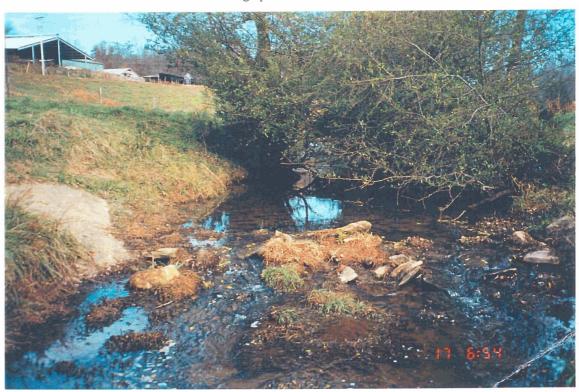
Prepared by: Will Wilhelm.

Sheet 1

of 3



#1 - Looking upstream at SR 1605



#2 – Looking upstream – bedrock present.

Kimley-Horn and Associates, Inc.

Project: Payne Dairy Farm

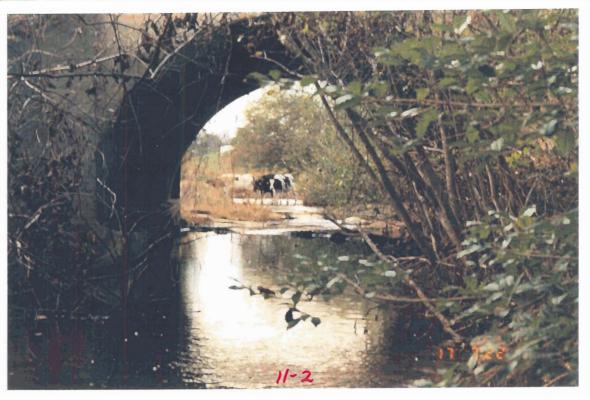
Title:

Downstream Segment - Jumping Rundob Number:

Prepared by: Will Wilhelm.

Sheet 2

011795000 of 3



#3 – Cattle crossing just downstream of SR 1605. Looking downstream through culvert under SR 1605.



#4 – Bank erosion (typical)

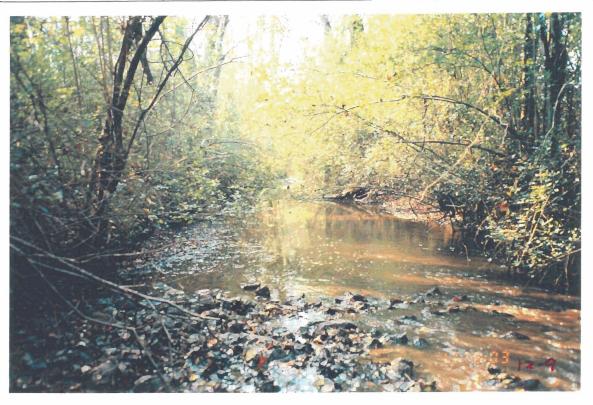


Downstream Segment - Jumping Runlob Number:

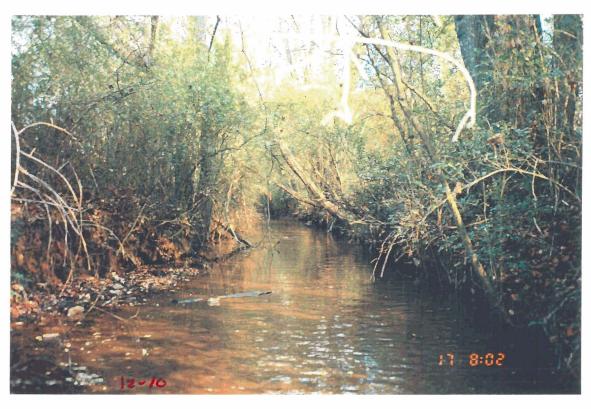
011795000 of 3

Sheet 3

Prepared by: Will Wilhelm.



#5 – Jumping Run downstream of proposed restoration (view 1).



#6 – Jumping Run downstream of proposed restoration (view 2).