## Beaverdam Creek and Unnamed Tributaries Mitigation Plan

Union County North Carolina NC EEP Project Number: D06054-C



Prepared for: NCDENR – EEP 2728 Capital Blvd, Suite 1H 103 Raleigh NC 27604



Submitted: April 28, 2009

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#### **EXECUTIVE SUMMARY**

As discussed in the Restoration Plan for Beaverdam Creek and two associated unnamed tributaries (UT1 and UT2), the mitigation goals and objectives for the project involved restoring stable physical and biological function of the project streams beyond pre-restoration (impaired reach) conditions. Pre-restoration conditions consisted of impaired, channelized, eroding, incised and entrenched stream channels. Nutrient and sediment loading, vegetative denuding and destabilized streambanks associated with hoof shear from uncontrolled cattle access was evident. The specific mitigation goals and objectives proposed and achieved for the project are listed below.

- Stable stream channels with features inherent of ecologically diverse environments, with appropriate streambed features including appropriately spaced pool and riffle sequences, and riparian corridors planted with diversified, indigenous vegetation.
- Superimposed reference reach boundary conditions on the impaired project reaches in the restoration design and construction of improvements.
- Constructed stream channels with the appropriate geometry and gradient to convey bankfull flows while entraining bedload and suspended sediment (wash load) readily available to the streams.
- Created an improved connection between the bankfull channels and their floodprone areas, with stable channel geometries, protective vegetation and jute coir fabric to prevent erosion.
- Minimized future land use impacts to project stream reaches by conveying a perpetual, restrictive conservation easement to the State of North Carolina, including stream corridor protection via livestock exclusion fencing at the surveyed and recorded conservation easement boundaries, with gates at the edge of the riparian corridor on river right and left at reserved conservation easement crossings adjacent to active pasture land.

The restoration of Beaverdam Creek mainstem, UT1 and UT2 met the project goals and objectives set forth in the restoration plan, by providing desired habitat and stability features required to enhance and provide long-term ecologic health for the project reaches. More specifically, the completed restoration project has accomplished the enhancements listed below.

#### Beaverdam Creek Mainstem:

- Reversed the effects of channelization using a Priority Level I restoration approach; restoration increased the width/depth ratio from 9.19 to 18.43.
- Restored natural pattern to the channel alignment, increasing the sinuosity from 1.07 to 1.49, while maintaining a stable relationship between the valley slope and bankfull slope (the bankfull slope was steeper than the valley slope prior to restoration and is now less than the valley slope with the completed restoration). Stable pattern, profile and dimension were restored based on extrapolation from reference reach boundary conditions.
- Stabilized eroding streambanks by providing an appropriately sized channel with stable channel bank slopes built with a combination of embedded stone, topsoil, natural fabrics and hearty vegetative protective cover. The average Bank Height Ratio was decreased from 1.60 to 1.00 (extremely incised to stable).
- Created re-connection between the restored stream channel and the adjacent floodprone area by raising the bankfull channel to the elevation of the adjacent floodplain. The completed restoration increased the average entrenchment ratio from 3.68 to 7.36.
- Created instream aquatic habitat features, including appropriately spaced pool and riffle sequences, and a stable transition of the mainstem reach thalweg to the invert of the downstream culvert carrying Beaverdam Creek under Snyders Store Road.

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• Revegetated the riparian corridor with indigenous canopy, mid-story, shrub and herbaceous ground cover, preserving existing forested riparian corridors where present.

#### **Unnamed Tributary 1 (UT1):**

- Reversed the effects of channelization through a combination of Priority Level I and Priority Level II restoration techniques. The average width/depth ratio of the restored UT1 project reach is 15.02. Stable pattern, profile and dimension were restored based on extrapolation from reference reach boundary conditions.
- Restored natural pattern to the channel alignment, increasing stream channel sinuosity from 1.14 to 1.45.
- Stabilized eroding streambanks by providing appropriately sized channels with stable streambank slopes. The average Bank Height Ratio has been reduced from 1.76 to 1.00 (extremely incised to stable).
- Created re-connection between the restored stream channel and the adjacent floodprone area by a combination of raising the stream bed and/or lowering the adjacent floodplain. The completed restoration increased the average entrenchment ratio from 2.74 to 8.68.
- Created instream aquatic habitat features including appropriately spaced pool and riffle sequences, including a stable transition of the UT1 reach thalweg at its confluence with Beaverdam Creek.
- Revegetated the riparian corridor with indigenous canopy, mid-story, shrub and herbaceous ground cover, preserving existing forested riparian corridors where present.

#### **Unnamed Tributary 2 (UT2):**

- Reversed the effects of channelization through a combination of Priority Level I and Priority Level II restoration techniques. The width/depth ratio of the restored UT2 project reach was increased from 8.32 to 21.00. Stable pattern, profile and dimension were restored based on extrapolation from reference reach boundary conditions.
- Restored natural pattern to the channel alignment, increasing stream channel sinuosity from 1.02 to 1.49
- Stabilized eroding streambanks by providing appropriately sized channels with stable streambank slopes. The average Bank Height Ratio has been reduced from 2.12 to 1.00 (extremely incised to stable).
- Created re-connection between the restored stream channel and the adjacent floodprone area by a combination of raising the stream bed and/or lowering the adjacent floodplain. The completed restoration increased the average entrenchment ratio from 2.74 to 8.68.
- Created instream aquatic habitat features including appropriately spaced pool and riffle sequences, with a stable transition of the UT2 reach thalweg at its confluence with UT1.
- Revegetated the riparian corridor with indigenous canopy, mid-story, shrub and herbaceous ground cover.

The following table summarizes pre-existing and post-restoration stream lengths, mitigation approach and identification of the reaches restored as presented throughout this Mitigation Plan. The original Restoration Plan includes mitigation specific to the Beaverdam Creek mainstem and the two unnamed tributaries. The stream segments and reach identifications used in this table are shown on the As-Built Plan Sheets in **Section 7.0** and on **Figure 2**.

	Pre-Existin	g Conditions/Po	ost-Construction Sun	nmarv	
Project Nu	ımber D06054-C	(Beaverdam C	reek & Unnamed Tr	ibutaries Resto	ration)
Tributary Reach ID	Pre-existing length	Restored Length*	Restoration Level	Credit Ratio	SMUs*
Beaverdam Creek Mainstem	416 lf	460 lf	Priority Level I Restoration	1.0	460
UT1	1,867 lf	2,300 lf	Priority Level I/II Restoration	1.0	2,300
UT2	203 lf	284 lf	Priority Level I/II Restoration	1.0	284
Totals .	2,486 ft	3,044 ft			3,044

<sup>\*</sup>Restored Length excludes permanent conservation easement crossings.

To demonstrate the success of the project, three forms of monitoring will be performed: (1) photo documentation; (2) ecological function assessment; and (3) channel stability measurements. Demonstration of long-term success of channel features will be tested in terms of a minimum exposure to two (2) bankfull events occurring in separate monitoring years. The monitoring shall be performed each year for the 5-year monitoring period. Long-term success criteria will be evaluated by monitoring and documenting the items listed below.

- 1. Channel aggradation or degradation.
- 2. Streambank erosion.
- 3. Presence of in-stream bar deposits.
- 4. Health and survival of indigenous, non-invasive vegetation (80% survival of planted species after 5 years).
- 5. Changes in as-built channel pattern, profile and dimension (should be minimal in comparison to as-built conditions, noting minor changes may represent increases in stability). Maintenance of floodplain connectivity, with respect to dimension, is a key success criteria.

The long-term monitoring of the constructed project includes 3,044 linear feet of longitudinal profiles (the sum of the three project reaches), collection and analysis of particle distributions at each of the eight monumented cross-sections. Eight vegetation monitoring plots with shrub, mid-story and canopy plantings representative of outside meanders, the 50-foot wide riparian buffer, streamside shrubs and floodplain zones will be monitored annually. Two galvanized steel, USGS Type A, 4-foot crest gages have been installed on the project reaches; one crest gage is installed below the confluence of UT2 with UT1 and the second is installed at the confluence of UT1 with Beaverdam Creek mainstem as shown on the As-Built plans in **Section 7.0** to document bankfull and greater flows.

Stream monitoring will be in accordance with the multi-agency, North Carolina Stream Mitigation Guidelines (April 2003) applicable to Priority Level I and Level II Restoration projects, following the template for *Content, Format and Data Requirements for EEP Monitoring Reports, Version 1.2* (November 16, 2006). Vegetation monitoring will be conducted in accordance with *CVS-EEP Protocol for Recording Vegetation, Version 4.0* (Lee, M.T., Peet, RK., Roberts, S.R., Wentworth, T.R. 2006) for Levels 1 and 2 Plot Sampling. Throughout the monitoring period, remedial action will be performed based on agency review of monitoring documents, and decision making between EEP and the provider to ensure the long-term success of the Beaverdam Creek and Unnamed Tributaries Mitigation Project.

<sup>\*\*</sup>Restored Length divided by SMU Credit Ratio

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#### 1.0 PROJECT BACKGROUND

#### 1.1 Project Site Location and Details

The project is located northwest of the intersection of White Store Road (SR 1003) and Snyder Store Road (SR 1945), 3.8 miles south of the town of Wingate, Union County, North Carolina. The site location and vicinity map is presented on **Figure 1**. The project is located on properties owned by Mr. and Mrs. William Earl and Betty H. Parker. The project includes restoration activities along Beaverdam Creek mainstem and two unnamed tributaries, designated UT1 and UT2.

To travel to the site from Monroe, North Carolina, drive east on US-74. Approximately 3.5 miles east of Monroe, make a slight right turn onto US-601 and travel for 4.1 miles. Turn left at Hinson Street/McRorie Road (NC-1952) and travel 0.6 mile then turn right at Old Pageland Monroe Road (NC-1941) and go 0.3 mile. Turn left at Bivens Street/Nash Road (NC-1954) and travel 1.3 miles. Turn right at White Store Road (NC-1003) and go approximately 0.6 mile. Turn left onto Snyder Store Road (NC-1945) and arrive at the site. The Earl and Betty Parker residence is located at 1822 Snyder Store Road, Wingate, NC 28174. As a courtesy to the property owners, please inform Mr. and Mrs. Parker you are conducting at field visit along the restored project stream reaches when conducting a site visit.

The Beaverdam Creek watershed is located within the North Carolina Wetland Restoration Program (NCWRP) targeted USGS 14-digit HUC watershed 03040105081030 (Beaverdam Creek), in the Lower Yadkin River Basin. Beaverdam Creek is a tributary to Lanes Creek, which is tributary to the Rocky River in the Lower Yadkin Pee Dee River Basin. The project stream reaches are mapped on North Carolina Department of Transportation Light Detection and Ranging (LiDAR) coverage of Union County, North Carolina as shown on Figure 2.

The Beaverdam Creek watershed is located in the Piedmont Physiographic Province of south central North Carolina in the Carolina Slate Belt Ecoregion (Draft Level III and Level IV Ecoregions of North Carolina, USEPA, USDA-NRCS & NCDENR, August 17, 2000). Valley Type VIII (Rosgen, 1996) is the most readily identified landform along the mainstem and unnamed tributaries corridors, with subtle terraces positioned laterally along the broad valleys with gentle, down-valley elevation relief in the project vicinity. Alluvial terraces and floodplains are the predominant depositional features in this fluvial geomorphologic system and produce a high sediment supply. As shown on **Figure 2** the first and second order project stream reaches are located in the headwaters of the Beaverdam Creek watershed. Existing valley slopes for the project reaches range from 0.0068 ft/ft to 0.0300 ft/ft with elevations from the upstream watershed boundary to the downstream limits of the project ranging from 640 feet to 571 feet (NAVD 88), with total site vertical relief of 69 feet.

In the project vicinity, bedrock consists of heated and deformed sedimentary and volcanic rock. The Carolina Slate Belt was the site of a series of oceanic volcanic islands about 550 – 650 million years ago. Metamorphic rocks that occur in this region include meta-mudstone and meta-argillite (slate), thin to thickly bedded, bedding planes and axial-planar cleavage common; interbedded with meta-sandstone, meta-conglomerate and meta-volcanic rock. Four formations are recognized in the Union County section of the Carolina Slate Belt – from oldest to youngest, the Uwharrie Formation, Tillery Formation, McManus Formation and Yadkin Formation. Locally, the site is underlain by the McManus Formation, which comprises approximately 11,600 feet, or approximately 70 percent of the Union County section of the Carolina Slate Belt. Thickly bedded, tuffaceous argillite characterizes the McManus Formation, which also contains an appreciable amount of crystal tuff and very fine-grained sandstone.

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The soils along Beaverdam Creek mainstem and along the lower 300-feet reach of UT1 within the project area have been derived from and developed over these metamorphic rock formations and include the Chewacla silt loam, 0 to 2 percent slopes, frequently flooded. This map unit consists mainly of very deep, nearly level, somewhat poorly drained soils developed on floodplains. It is mostly present on broad flats along major streams and rivers and on narrow flats along minor creeks and drainageways. Typically the surface layer is brown silt loam approximately seven inches thick. The subsoil is 45 inches thick. On site, the Chewacla unit is mapped adjacent to the Goldston soils. Where the Chewacla unit occurs adjacent to areas of Goldston soils, small areas of soils encounter bedrock at a depth of less than 60 inches below ground surface. Contrasting inclusions make up about 15 percent of this mapped unit.

The upper reach of UT1 and the entire length of UT2 is mapped Cid channery silt loam, 1 to 5 percent slopes. This map unit consists mainly of moderately deep, moderately well drained and somewhat poorly drained, nearly level and gently sloping Cid and similar soils on flats, on ridges in the uplands, in depressions and in headwater drainageways. Typically, the surface layer is light brownish gray channery silt loam four inches thick. The subsurface layer is a pale yellow channery silt loam 5 inches thick. The subsoil is 18 inches thick. Weathered, fractured bedrock is encountered at a depth of about 27 inches. Hard, fractured bedrock is encountered at a depth of about 32 inches. Permeability is slow in the Cid soil. Available water capacity is low to moderate. The shrink-swell potential is moderate. A seasonal high water table is perched between depths of 1.5 to 2.5 feet below ground surface from December through May. The depth to hard bedrock ranges from 20 to 40 inches. The hazard of erosion is moderate on construction sites if the ground cover is removed. Soils mapping and taxonomic descriptions are from the USDA NRCS, Soil Survey of Union County, North Carolina (USDA NRCS, January 1996).

The drainage area tributary to the downstream limits of the project on Beaverdam Creek mainstem is 0.4910 square miles or 314 acres. UT1 and UT2 have contribution drainage areas of 0.2375 square miles (152 acres) and 0.0765 square miles (49 acres), respectively. The project contribution drainage areas watershed map is presented on **Figure 3**. Drainage areas for the project reaches are summarized in **Table 1**.

TABLE 1	
Drainage Areas	5 · · · · · · · · · · · · · · · · · · ·
Project Number D06054-C (Beaverdam Cree	ek and Unnamed Tributaries)
Reach	Drainage Area (Acres)
Beaverdam Creek Mainstem (downstream project limit)	314
UT1 to Beaverdam Creek*	152
UT2 to Beaverdam Creek*	49
Total	314

\*UT1 and UT2 drainage areas are included in the total contribution drainage area for the Beaverdam Creek stream restoration project. Refer to **Figure 3** for delineation of project sub-watershed drainage areas.

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#### 1.2 Pre-Restoration Existing Conditions

A number of anthropogenic factors had impacted the project stream reaches and riparian corridors, resulting in its unstable deeply incised channel conditions. Pre-restoration land use surrounding the restoration project was active cattle pasture land. Historic stream relocation, channelization and cattle intrusion were the primary causes leading to instability along each of the project reaches. Cattle had unrestricted access to the project stream reaches for watering and, in areas where established riparian canopy corridors exists, cattle accessed the project reaches for shade. The unstable streambanks contributed significant quantities of sediment and nutrient laden runoff from the project stream reaches into the larger Beaverdam Creek and Lanes Creek watersheds due to head cutting and bank destabilization attributed to hoof-shear. **Table 2** provides baseline geomorphologic and hydraulic summaries for regional curve, reference, pre-existing, design and as-built channel dimensions, pattern, profile, substrate, and Rosgen stream type, together with additional reach parameters.

The upper two-thirds of the UT1 reach and the entire UT2 reach had sparse riparian vegetation along their stream corridors. Vegetation along the existing stream corridors was dysfunctional with respect to bank stabilization, nutrient uptake and sediment removal from overland runoff. The approximate lower one-third of the UT1 and Beaverdam Creek mainstem reaches have relatively narrow, pre-existing established hardwood forested riparian corridors. However, these corridors exhibited severe denuding of the understory, shrub and herbaceous ground cover vegetation due to cattle grazing and browsing. Typical species observed within the corridor included *Ulmus alata* (winged elm), *Quercus phellos* (willow oak), *Quercus velutina* (black oak), *Acer negundo* (boxelder), *Asimina triloba* (pawpaw), *Lonicera* species (honeysuckle), *Bignonia capreolata* (crossvine), *Carex* species (sedge), *Mitchella repens* (partridgeberry), and *Geranium* species (wild geranium).

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#### 2.0 RESTORATION SUMMARY

#### 2.1 Mitigation Goals and Objectives

As discussed in the Restoration Plan for Beaverdam Creek and two associated unnamed tributaries (UT1 and UT2), the mitigation goals and objectives for the project involved restoring stable physical and biological function of the project streams beyond pre-restoration (impaired) conditions. Pre-restoration conditions consisted of channelized, eroding, incised and entrenched stream channels. Nutrient and sediment loading, vegetative denuding and destabilized streambanks associated with hoof shear from uncontrolled cattle access was evident. The specific mitigation goals and objectives proposed and achieved for the project are listed below.

- Stable stream channels with features inherent of ecologically diverse environments, with appropriate streambed features including appropriately spaced pool and riffle sequences, and riparian corridors planted with diversified, indigenous vegetation.
- Superimposed reference reach boundary conditions on the impaired project reaches in the restoration design and construction of improvements.
- Constructed stream channels with the appropriate geometry and gradient to convey bankfull flows while entraining bedload and suspended sediment (wash load) readily available to the streams.
- Created an improved connection between the bankfull channels and floodprone areas, with stable channel geometries, protective vegetation and jute coir fabric to prevent erosion.
- Minimized future land use impacts to project stream reaches by conveying a perpetual, restrictive
  conservation easement to the State of North Carolina, including stream corridor protection via
  livestock exclusion fencing at the surveyed and recorded conservation easement boundaries, with
  gates at the edge of the riparian corridor on river right and left at reserved conservation easement
  crossings adjacent to active pasture land.

The restoration of Beaverdam Creek mainstem, UT1 and UT2 met the project goals and objectives set forth in the restoration plan by providing desired aquatic habitat and stability features required to enhance and provide long-term ecologic health for the project reaches. More specifically, the completed restoration project has accomplished the enhancements listed below.

#### Beaverdam Creek Mainstem:

- Reversed the effects of channelization using a Priority Level I restoration approach; restoration increased the width/depth ratio from 9.19 to 18.43.
- Restored natural pattern to the channel alignment, increasing the sinuosity from 1.07 to 1.49, while maintaining a stable relationship between the valley slope and bankfull slope (the bankfull slope was steeper than the valley slope prior to restoration and is now less than the valley slope with the completed restoration). Stable pattern, profile and dimension were restored based on extrapolation from reference reach boundary conditions.
- Stabilized eroding streambanks by providing an appropriately sized channel with stable channel bank slopes built with a combination of embedded stone, topsoil, natural fabrics and hearty vegetative protective cover. The average Bank Height Ratio was decreased from 1.60 to 1.00 (extremely incised to stable).
- Created re-connection between the restored stream channel and the adjacent floodprone area by raising the bankfull channel to the elevation of the adjacent floodplain. The completed restoration increased the average entrenchment ratio from 3.68 to 7.36.

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- Created instream aquatic habitat features, including appropriately spaced pool and riffle sequences, and a stable transition of the mainstem reach thalweg to the invert of the downstream culvert carrying Beaverdam Creek under Snyders Store Road.
- Revegetated the riparian corridor with indigenous canopy, mid-story, shrub and herbaceous ground cover, preserving existing forested riparian corridors where present.

#### **Unnamed Tributary 1 (UT1):**

- Reversed the effects of channelization through a combination of Priority Level I and Priority Level II restoration techniques. The average width/depth ratio of the restored UT1 project reach is 15.02. Stable pattern, profile and dimension were restored based on extrapolation from reference reach boundary conditions.
- Restored natural pattern to the channel alignment, increasing stream channel sinuosity from 1.14 to 1.45.
- Stabilized eroding streambanks by providing appropriately sized channels with stable streambank slopes. The average Bank Height Ratio has been reduced from 1.76 to 1.00 (extremely incised to stable).
- Created re-connection between the restored stream channel and the adjacent floodprone area by a combination of raising the stream bed and/or lowering the adjacent floodplain. The completed restoration increased the average entrenchment ratio from 2.74 to 8.68.
- Created instream aquatic habitat features including appropriately spaced pool and riffle sequences, including a stable transition of the UT1 reach thalweg at its confluence with Beaverdam: Creek.
- Revegetated the riparian corridor with indigenous canopy, mid-story, shrub and herbaceous ground cover, preserving existing forested riparian corridors where present.

#### **Unnamed Tributary 2 (UT2):**

- Reversed the effects of channelization through a combination of Priority Level I and Priority Level II restoration techniques. The width/depth ratio of the restored UT2 project reach was increased from 8.32 to 21.00. Stable pattern, profile and dimension were restored based on extrapolation from reference reach boundary conditions.
- Restored natural pattern to the channel alignment, increasing stream channel sinuosity from 1.02 to 1.49
- Stabilized eroding streambanks by providing appropriately sized channels with stable streambank slopes. The average Bank Height Ratio has been reduced from 2.12 to 1.00 (extremely incised to stable).
- Created re-connection between the restored stream channel and the adjacent floodprone area by a combination of raising the stream bed and/or lowering the adjacent floodplain. The completed restoration increased the average entrenchment ratio from 2.74 to 8.68.
- Created instream aquatic habitat features including appropriately spaced pool and riffle sequences, with a stable transition of the UT2 reach thalweg at its confluence with UT1.
- Revegetated the riparian corridor with indigenous canopy, mid-story, shrub and herbaceous ground cover.

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#### 2.2 Restoration Approach

#### **Engineering Field Reconnaissance**

EMH&T scientists and engineers mobilized to the site on July 17, 2007 to assess the impaired project reaches. The following sections describe the results of the impaired conditions field assessment. Representative stream profiles ≥ 20 bankfull widths were surveyed using differential leveling techniques on each of the project reaches. Representative riffle and pool cross-sections were surveyed on each reach and riffle and pool streambed particle distributions were collected following standard NC EEP protocols. The following sections discuss, in detail, the results from engineering field reconnaissance, by project stream reach.

#### Beaverdam Creek Mainstem

In its impaired state, the stream's high degree of channel incision, expressed as the ratio of low bank height to maximum bankfull depth, or Bank Height Ratio (BHR range 1.56 - 1.60), low sinuosity (K = 1.08), denuded and destabilized streambanks composed of stratified silty soils, relatively steep profile slope (0.0169 ft/ft, or 89.2 ft/mi) had resulted in a deeply incised, unstable channel with a high erosion potential. The incised, vertical to undercut streambanks, accelerated streambank erosion rates. Utilizing the ratio of near-bank maximum bankfull depth to mean bankfull depth bank erosion hazard index (BEHI) algorithm in RiverMorph® v.4.1.1, it was estimated 21 cubic yards per year (or 28 tons per year) of sediment was being eroded from the unstable, vertical to undercut streambanks along the mainstem impaired reach into the larger Beaverdam Creek watershed. This estimate was calculated using the bank height (2.97 ft) measured at an impaired pool cross-section, located 107 feet upstream from the confluence of UT1 with Beaverdam Creek, and the total mainstem impaired reach length (386 lf), and represents a bank erosion rate of 0.5 ft/yr. BEHI and sediment export, bank erosion rate estimates, together with bank stability evaluation, BHR calculations, with RiverMorph® v.4.1.1 model inputs and results are presented in Appendix 3 in the Beaverdam Creek and Unnamed Tributaries Restoration Plan, EEP Project No. D06054-C (EMH&T, January 16, 2008).

#### UT1

In its impaired state along the lower forested reach, the stream's high degree of channel incision (BHR range 1.41 - 1.76), low sinuosity (K = 1.16), denuded and destabilized streambanks, profile slope (0.0058 ft/ft, or 30.6 ft/mi) had resulted in a deeply incised, unstable channel with high streambank and streambed erosion potential. The incised, vertical to undercut denuded streambanks, accelerated erosion rates. Utilizing the ratio of near-bank maximum bankfull depth to mean bankfull depth BEHI algorithm in RiverMorph® v.4.1.1, it was estimated 67 cubic yards per year (or 87 tons per year) of sediment was being eroded from the unstable streambanks along the forested segment of UT1 impaired reach. This estimate was calculated using the bank height (2.68 ft) measured at an impaired pool cross-section located 212 feet upstream from the confluence of UT1 with Beaverdam Creek mainstem and the lower impaired reach length from the point where the existing channel enters the forested corridor to its confluence with Beaverdam Creek (1351 lf), and represents a bank erosion rate of 0.5 ft/yr. BEHI and sediment export, bank erosion rate estimates, together with bank stability evaluation, BHR calculations, with RiverMorph® v.4.1.1 model inputs and results are presented in **Appendix 3** in the cited project Restoration Plan.

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Upstream of the forested corridor on UT1, pre-existing bank erosion hazard indices were not calculated. This segment of the impaired reach was significantly different from the forested reach. Aggradation was the dominant depositional process as the land use was open pasture land with non-uniform channel geometry, modified by hoof shear together with low profile gradient. In its existing state, the upper UT1 stream segment lacked suitable features for aquatic habitat.

#### UT2

In its impaired state, the stream's high degree of channel incision (BHR range 1.80 – 2.12), low sinuosity (K = 1.01), denuded and destabilized streambanks, relatively steep profile slope (0.0192 ft/ft, or 101.4 ft/mi) had resulted in a deeply incised, unstable stream channel with a high sediment supply. The incised, steep to near vertical denuded streambanks, accelerated erosion rates. Utilizing the ratio of nearbank maximum bankfull depth to mean bankfull depth BEHI algorithm in RiverMorph® v.4.1.1, it is estimated 4 cubic yards per year (or 5 tons per year) of sediment was being eroded from the unstable streambanks along the UT2 impaired reach. This estimate was calculated using the bank height (2.14 ft) measured at an impaired pool cross-section, located 227 feet upstream from the confluence of UT2 with UT1, and the total UT2 impaired reach length (203 lf), and represents a bank erosion rate of 0.25 ft/yr. BEHI and sediment export, bank erosion rate estimates, together with bank stability evaluation, BHR calculations, with RiverMorph® v.4.1.1 model inputs and results are presented in Appendix 3 in the cited project Restoration Plan.

#### **Channel Stability Summary**

Summing the sediment export estimates for each of the project reaches under impaired conditions, the streams had the potential to contribute approximate 92 cubic yards (or 120 tons) of nutrient laden sediment off site into the larger Beaverdam Creek watershed on an annual basis. The rate of erosion, expressed in feet per year per linear foot, was based on estimates from field observations for each of the impaired project reaches and their potential for mass loading of nutrients and sediment due to channel instability from uncontrolled cattle intrusion, agricultural land use and channelization.

The consequence of channelization, cattle intrusion, confinement (lateral containment), incision (vertical containment) major floods, changes in sediment regime, and loss of riparian vegetation are attributed causes and effects for impaired conditions along the project reaches prior to restoration. The effects of these anthropogenic changes were accelerated streambank erosion, channel incision, land loss, aquatic habitat loss, lowering of the water table, land productivity reduction and in-stream and downstream sedimentation and nutrient loading. Weighting each of the mitigation types and categories available against stated projected goals, and based on engineering field reconnaissance and detailed topographic surveys of the impaired project reaches, it was determined only full-scale restoration could achieve stabilization and the establishment of fully functional aquatic and riparian habitat along the impaired project reaches.

#### 2.3 Bankfull Verification

For the project stream reaches, bankfull discharge was evaluated through quantitative analysis of stable reference reach boundary conditions and comparison of predicted bankfull discharge through a stable, surveyed riffle cross-section, located 43 feet upstream from the confluence of Davis Branch with Gourdvine Creek, as shown on **Figure 4**. The contribution drainage area for the Davis Branch Reference Reach is 365.55 acres or 0.5712 square mile. Discharge versus drainage area relationships for the

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reference reach riffle cross-section were compared to *Bankfull Hydraulic Geometry Relationships for North Carolina Streams (Rural Piedmont)* regional curve dataset. Through this analysis, it was determined the rural Piedmont regional curves underestimates bankfull discharge and geometric relationships for project stream reaches.

The Bankfull Hydraulic Geometry Relationships for North Carolina Streams (Rural Piedmont) power function regression equation for bankfull discharge is:

$$Q_{bkf} = 66.57 \times A_w^{0.89} (R^2 = 0.97)$$

where  $Q_{bkf}$  = bankfull discharge (cfs) and  $A_w$  = watershed drainage area (mi<sup>2</sup>). Inputting the Davis Branch Reference Reach drainage area (0.5712 mi<sup>2</sup>) into the power function regression equation yields the following result:

$$Q_{bkf} = 66.57 \times 0.5712^{0.89} = 40.4 \text{ cfs}$$

In an additional effort to validate bankfull discharge for the project reaches, The *Bankfull Hydraulic Geometry Relationships for North Carolina Streams* (Rural Piedmont) dataset was stratified by E stream type using the regional curve data editor in RiverMorph® v.4.1.1. The resulting Log-Pearson Type III distributions and regression analysis from the stratified regional curve dataset yielded the following power function regression equations for bankfull discharge, channel cross-sectional area, mean depth, width, and corresponding coefficient of determination, together with the empirical relationships (predicted values) for the Davis Branch Reference Reach, in bold, where  $A_w = 0.5712 \text{ mi}^2$ .

$$Q_{bkf} = 105.95 \text{ x A}_{w}^{0.6615} (R^2 = 0.97) \ \mathbf{Q}_{bkf} = 73.1 \ \mathbf{cfs}$$

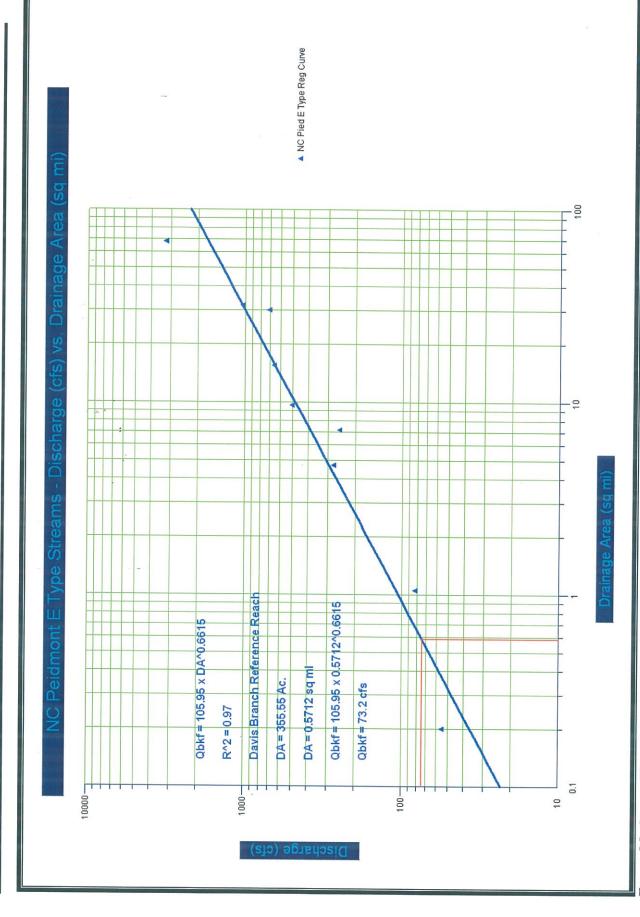
$$A_{bkf} = 21.93 \text{ x } A_w^{0.6748} \text{ (R}^2 = 0.97) \text{ } A_{bkf} = 15.03 \text{ sq ft}$$

$$D_{bkf} = 1.60 \text{ x } A_w^{0.3257} (R^2 = 0.89)$$
  $D_{bkf} = 1.33 \text{ ft}$ 

$$W_{bkf} = 13.67 \text{ x A}_{w}^{0.3496} (R^2 = 0.94) \text{ W}_{bkf} = 11.24 \text{ ft}$$

The calculated discharge, using carefully delineated reference reach drainage area, quantified reference bankfull riffle geometry, profile slope, and bed roughness yielded a bankfull discharge of 77.6 cubic feet per second (cfs). The following Drainage Area versus Discharge, Rural Piedmont Regional Curve, stratified by Rosgen E stream type analysis predicts  $Q_{bkf} = 73.1$  cfs and validates bankfull discharge estimates for the Davis Branch Reference Reach, and subsequently the bankfull discharge estimates for the Beaverdam Creek mainstem, UT1 and UT2 restored project stream reaches.

Since the quantitatively derived bankfull discharge of 77.6 cfs, based on carefully measured field parameters closely matches the stratified Rosgen E stream type Rural Piedmont Regional Curve empirically estimated bankfull discharge, the quantitatively derived bankfull discharge was carried forward into the design, proportionally adjusted for individual project reach drainage areas. Refer to **Tables 2** for reach specific estimates of bankfull discharge and hydraulic geometries from the stratified Rural Piedmont regional curve dataset, reference reach, pre-existing, design and as-built conditions.



Evans, Mechwart, Hambleton & Tilton, Inc. Engineers, Surveyors, Planners, Scientists

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#### **Channel Morphology**

Landform morphology along the Beaverdam Creek mainstem, UT1 and UT2 reach is Rosgen Valley Type VIII. The pre-restoration channels were a deeply incised E4/1, C4/1 and E4 Rosgen stream types, respectively. The restoration goal to reconnect the project reaches to their adjacent floodplains and reestablish stable pattern, profile and dimension consistent with reference reach boundary conditions was achieved. The as-built Beaverdam Creek mainstem, UT1 and UT2 stream channels are Rosgen C4/1 stream types with areas of bedrock control. Summary morphologic and hydraulic data from the Regional Curves, Davis Branch Reference Reach, Pre-Existing, Design and As-Built conditions for Beaverdam Creek, UT1 and UT2 are presented in **Tables 2**.

Parameter	Reg	gional Cur	rve Data	Davis I	Branch Refere	Beaverdam Cree		Existing Con	dition		Design				
	Min	Max	Mean	Min	Max	Mean	Min	Max	Mean	Min	Max	Median	14:	As-Built	
Dimension								IVIUX	Wican	IVIIII	IVIAX	Median	Min	Max	Median
Drainage Area (mi <sup>2</sup> )			0.5712			0.5712			0.4910			0.4910			0.401
BF Width (ft)			11.24			12.91			7.44			11.20			0.491
Floodprone Width (ft)						50.00			27.40						18.4
BF Cross Sectional Area (ft²)			15.03			15.65			6.05			50.00			135.0
BF Mean Depth (ft)			1.33			1.21			0.03			13.68			18.4
BF Max Depth (ft)			1.55			1.61						1.22			1.0
Width/Depth Ratio			8.45						1.14			1.80			2.3
Entrenchment Ratio			0.43			10.67			9.19			9.18			18.4
Bank Height Ratio						3.87			3.68			4.46			7.3
Wetted Perimeter (ft)			10.00			1.00			1.60			1.00			1.0
Hydraulic Radius (ft)			13.90			13.72			8.05			12.05			19.0
Pattern	No.		1.08			1.14			0.75			1.14			0.9
*Channel Beltwidth (ft)		,		27.00	52.00	20.00									
*Radius of Curvature (ft)				27.80 16.40	53.00 45.30	38.00 29.40			1986			50.00			50.0
*Meander Wavelength (ft)				80.10	116.50	99.20				17.00	28.00	17.00	17.00	28.00	17.0
*Meander Width Ratio				2.15	4.11	2.94				59.01	93.85	72.68	59.01	93.85	72.6
Profile												4.46			2.7
Riffle Length (ft)				12.0	18.5	15.0	41.0	62.0	51.3	11.7	38.7	24.0	14.7	22.9	17
Riffle Slope (ft/ft)				0.0283	0.0799	0.0520	0.0194	0.0328	0.0246	0.0285	0.0939	0.0458	0.0319	0.0720	0.045
Pool Length (ft) Pool Spacing (ft)				12.04	29.09	21.20	17.2	21.9	19.5	16.29	32.40	18.28	16.87	39.62	28.6
Substrate Tool Spacing (II)				33.42	43.70	38.56	67.7	104.9	86.3	28.88	71.06	42.65	29.82	58.36	47.5
D50 (mm)	T					69.2			0.5						
D84 (mm)						140.1			9.5	1. 4		9.5			40
Additional Reach Parameters						110.1		S CALLED STATE	17.2			17.2			162.
Valley Length (ft)						974			387			387			32
Channel Length (ft)						1129			416			463			47
Sinuosity Water Surface Slope (ft/ft)						1.2			1.07			1.20			1.4
BF Slope (ft/ft)						0.0311			0.0300			0.0158			0.010
Rosgen Classification						0.0326 E3/1b**			0.0300			0.0169			0.010
Bankfull Discharge (cfs)			73.1			77.6			E4/1			E4			C4/1
Bankfull Velocity (ft/sec)			49			5.0			66.7			66.7			66.
otes: Blank fields = Historic project documentation ne Where no min/max values is provided, and only * Inclusion will be project specific and determine	cessary	to provide	these data v	vere collecte	dlaamnilad				11.0			4.9			3

Parameter	Regional C	urve Data	Station/Reach: UT1 Sta. 0- Regional Curve Data Davis Branch Reference Reach				Existing Cor	dition	Design				As-Built	
D'	Min Max	Mean	Min	Max	Mean	Min	Max	Mean	Min	Max	Median	Min	Max	Mediar
Dimension										Table 1	Wiedian	171111	IVIAX	Mediai
Drainage Area (mi <sup>2</sup> )		0.5712			0.5712			0.2371			0.2371			0.23
BF Width (ft)		11.24			12.91			11.22			9.00	9.22	13.80	11.
Floodprone Width (ft)					50.00			30.70			50.00	86.55	110.03	98.
BF Cross Sectional Area (ft²)		15.03			15.65			8.42			9.00	7.49		1000-100
BF Mean Depth (ft)		1.33			1.21			0.75			1.00	0.74	10.19	8.
BF Max Depth (ft)					1.61			1.17					0.81	0.
Width/Depth Ratio		8.45			10.67			14.96			1.50	1.64	1.95	1.
Entrenchment Ratio					3.87			2.74			9.00	11.38	18.65	15.0
Bank Height Ratio					1.00			1.76			5.56	7.97	9.39	8.0
Wetted Perimeter (ft)		13.90			13.72		(4)				1.00	1.00	1.00	1.0
Hydraulic Radius (ft)		1.08						14.52			11.00	9.82	14.22	12.
Pattern		1.08			1.14			1.00			0.82	0.72	0.76	0.
*Channel Beltwidth (ft)			27.80	53.00	38.00				-		70.00			
*Radius of Curvature (ft)			16.40	45.30	29.40				17.00	25.00	50.00	12.00		50.
*Meander Wavelength (ft)			80.10	116.50	99.20				÷ 63.29	93.84	20.00 75.00	13.00 63.29	25.00	18.
*Meander Width Ratio			2.15	4.11	2.94			6	03.29	73.04	5.56	03.29	93.84	75.0 4.3
Profile											3.30			4
Riffle Length (ft)	1		12.0	18.5	15.0	47.0	60.0	53.5	10.5	46.1	28.6	7.6	30.2	15
Riffle Slope (ft/ft)			0.0283	0.0799	0.0520	0.0117	0.0185	0.0151	0.0228	0.0957	0.0381	0.0088	0.0702	0.02
Pool Length (ft) Pool Spacing (ft)			12.04	29.09	21.20	24.60	39.40	31.20	18.69	40.99	27.93	22.96	57.82	36.
Substrate			33.42	43.70	38.56	35.40	76.60	54.70	32.70	85.05	54.28	18.07	79.78	50.3
D50 (mm)					69.2									
D84 (mm)					140.1			5.5			5.5	61.4	76.1	68
dditional Reach Parameters					140.1			. 10.1			16.1	143.6	175.5	159
Valley Length (ft)					974	T		1637			1594			160
Channel Length (ft)					1129			1867			2328			162 234
Sinuosity					1.2			1.14			1.46			1.4
Water Surface Slope (ft/ft)					0.0311			0.0051			0.0047			0.004
BF Slope (ft/ft) Rosgen Classification		-			0.0326			0.0058			0.0047			0.004
Bankfull Discharge (cfs)		72.1			E3/1b**			C4/1			E4/1	E4/1	C4/1	C4/1
Bankfull Velocity (ft/sec)		73.1			77.6			32.2			32.2			32
otes: Blank fields = Historic project documentation	naaaaaa	4.9			5.0			3.8			3.6			3

Parameter	Reg	gional Cu	rve Data	Davis B	ranch Refere	Reach: UT2 Sta		xisting Con	dition		Docion			A 70 -11	
	Min	Max	Mean	Min	Max	Mean	Min	Max	Mean	Min	Design	34 1	2.6	As-Built	
Dimension			THE COLUMN	171111	IVIAX	Wican	IVIIII	IVIAX	Iviean	IVIIII	Max	Median	Min	Max	Median
Drainage Area (mi <sup>2</sup> )			0.5712			0.5712			0.0765			0.0765			
BF Width (ft)			11.24			12.91			4.91			0.0765			0.076
Floodprone Width (ft)						50.00			21.24			6.30	1.5		11.5
BF Cross Sectional Area (ft²)			15.03			15.65			2.88			50.00			114.7
BF Mean Depth (ft)			1.33			1.21			0.59			4.30			6.3
BF Max Depth (ft)			1,00			1.61			0.39			0.68			0.5
Width/Depth Ratio			8.45			10.67			8.32			1.00			1.3
Entrenchment Ratio			0.43			3.87						9.26			21.0
Bank Height Ratio						1.00			4.33			7.94			9.9
Wetted Perimeter (ft)			13.90			13.72			2.12			1.00			1.0
Hydraulic Radius (ft)			1.08			1.14			5.70			6.77		to Carter 1	11.9
Pattern			1.00			1.14			0.51			0.63			0.5
*Channel Beltwidth (ft)				27.80	53.00	38.00									
*Radius of Curvature (ft)				16.40	45.30	29.40				10.50		50.00			50.0
*Meander Wavelength (ft)				80.10	116.50	99.20				12.50	16.00	14.50	12:50	16.00	14.5
*Meander Width Ratio				2.15	4.11	2.94				58.08	59.76	58.92	58.08	59.76	58.9
Profile				2.13	4.11	2.94						7.94			4.3
Riffle Length (ft)				12.0	18.5	15.0	22.0	70.4		12.2					
Riffle Slope (ft/ft)				0.0283	0.0799	15.0 0.0520	33.0	72.4	· ).	13.2	27.1	22.7	12.4	23.9	15.
Pool Length (ft)				12.0	29.1	21.2	0.0173	0.0306		0.0258	0.0532	0.0308	0.0115	0.0451	0.021
Pool Spacing (ft)				33.4	43.7		25.0	26.9		19.4	51.1	25.8	23.7	41.0	30.
Substrate				33.4	43.7	38.6			141.2	42.0	64.3	51.9	35.6	70.0	49.
D50 (mm)		T				69.2			= 0						
D84 (mm)									7.8	,		7.8			90.
Additional Reach Parameters						140.1			21.6			21.6			210.
Valley Length (ft)		T				074			200						
Channel Length (ft)						974			200			194			19
Sinuosity						1129			203			282			28-
Water Surface Slope (ft/ft)						1.2			1.02			1.45			1.4
BF Slope-(ft/ft)						0.0311			0.0171			0.0054			0.007
Rosgen Classification						0.0326			0.0192			0.0054			0.006
Bankfull Discharge (cfs)			72.1			E3/1b**			E4			E4			C4/1
			73.1			77.6			10.4			10.4			10.
Bankfull Velocity (ft/sec)  Notes: Blank fields = Historic project documentation			4.9			5.0			3.6			2.4			1.6

= Historic project documentation necessary to provide these data were collected/compiled.

Where no min/max values is provided, and only one value was measured or computed, that value is presented as the mean or median value.

<sup>\*</sup>Inclusion will be project specific and determined primarily by As-built monitoring plan/success criteria

\*\*E3/1b ("E3/1" E stream type channel morphology, large cobble substrate with bedrock control; E3/1"b" bankfull slope greater than 0.02 ft/ft.)

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#### 2.4 As-Built Channel Stability Assessment

#### Beaverdam Creek Mainstem

Under as-built conditions, streambank erosion potential was evaluated using the Vertical Velocity Near-Bank Shear Stress Method algorithm in RiverMorph® v.4.1.1, with bankfull geometries inputs taken individually from the two (2) monumented cross-sections (cross-sections number 7 and 8) on the Beaverdam Creek mainstem reach. Hydraulic slope and percentage of the reach occupied by pools/glides along outside meander bends verses riffles/runs between bends (i.e.,70% pools/glides; 30% riffles/runs) was determined from the as-built mainstem longitudinal profile. The following table proportionally summarizes the estimated sediment loss from streambanks under as-built conditions. Individual BEHI study streambank input assumptions and output data are presented in **Appendix D**.

Table 3a. As-Built Estimated Sediment Loss for Beaverdam Creek Mainstem (Reach Summary)

Study Bank	Proportional Length (l.f.)	Loss (cu yd/yr)	Loss (tons/yr)
Pool XS-7	332.84	0.66	0.86
Riffle XS-8	142.65	0.40	0.52
Totals	475.49	1.06	1.38

Note: Estimated total sediment loss per foot of reach = 0.0029 tons/yr/ft = < 0.02 ft bank loss/year.

#### UT1

Under restored, as-built conditions, the Channel Pattern and/or Depositional Features for Adjustments in Near-Bank Stress algorithm in RiverMorph® v.4.1.1 was applied, using bankfull geometry, hydraulic slope and as-built streambank slopes from the four (4) as-built, monumented cross-sections on UT1. Based on longitudinal profile analysis, the reach is approximately 70 percent pools/glides and 30 percent riffles/runs. Each of the representative, monumented cross-section was selected to proportionally evaluate as-built streambank stability and estimate erosion rates on the UT1 2,345 If restored reach. The model input parameters and estimated streambank erosion rates are presented in **Appendix D** and summarized in the following table:

Table 3b. As-Built Estimated Sediment Loss for Beaverdam Creek UT1 (Reach Summary)

Study Bank	Proportional Length (l.f.)	Loss (cu yd/yr)	Loss (tons/yr)
Riffle XS-3	351.77	0.43	0.56
Pool XS-4	820.79	1.05	1.37
Pool XS-5	820.79	1.34	1.74
Riffle XS-6	351.77	0.43	0.56
Totals	2345.12	3.25	4.23

Note: Estimated total sediment loss per foot of reach = 0.0018 tons/yr/ft = < 0.02 ft bank loss/year.

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#### UT2

Under restored, as-built conditions, the Channel Pattern and/or Depositional Features for Adjustments in Near-Bank Stress algorithm in RiverMorph® v.4.1.1 was applied, using bankfull geometry, hydraulic slope and as-built streambank slopes from the two (2) as-built, monumented cross-sections on UT2. Based on longitudinal profile analysis, the reach is approximately 70 percent pools/glides and 30 percent riffles/runs. Each of the representative, monumented cross-section was selected to proportionally evaluate as-built streambank stability and estimate erosion rates on the UT2 284 If restored reach. The model input parameters and estimated streambank erosion rates are presented in **Appendix D** and summarized in the following table:

Table 3c. As-Built Estimated Sediment Loss for Beaverdam Creek UT2 (Reach Summary)

Study Bank	Proportional Length (l.f.)	Loss (cu yd/yr)	Loss (tons/yr)
Pool XS-1	199.02	0.36	0.47
Riffle XS-2	85.29	0.00	0.00
Totals	284.31	0.36	0.47

Note: Estimated total sediment loss per foot of reach = 0.0017 tons/yr/ft = < 0.015 ft bank loss/year.

### As-Built Channel Stability Summary

Summing the sediment export estimates for each of the restored project reaches, the streams have the potential to export approximate 4.7 cubic yards (or 6.1 tons) of sediment off site into the larger Beaverdam Creek watershed on an annual basis. Under pre-existing, impaired project reach conditions the estimated potential for mass wasting of nutrient laden sediment, attributed to streambank instability associated uncontrolled cattle intrusion, agricultural land use and channelization, was 92 cubic yards (or 120 tons) per year. Table 3.d provides a summary of pre- and post-restoration sediment erosion rates, and represents a 95 percent reduction in streambank erosion rate potential under as-built conditions.

As noted in the restoration plan, upstream of the forested corridor on UT1, streambank erosion rates were not calculated under pre-existing conditions. This segment of the impaired reach was significantly different from the lower forested reach. Aggradation was the dominant depositional process as the land use was open pasture with non-uniform channel geometry modified by hoof shear together with low profile gradient and herbaceous ground cover.

Table 3d. As-Built Estimated Sediment Loss for Beaverdam Creek (Project Summary)

Reach Identification	Pre-Existing Erosion Rate Estimate (tons/yr)	Restored Erosion Rate Estimate (tons/yr)	Net Reduction Post- Remediation Estimate (tons/yr)
Beaverdam Creek	28	1.4	26.6
UT1	87	4.2	62.8
UT2	5	0.5	4.5
Totals	120	6.1	113.9

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The streambank erosion rate summary in **Table 3d** may be somewhat aggressive in that reductions in near-bank shear stress at banks that are protected by erosion control fabrics, rock toe bank protection, and other stream reinforcement measures are not taken into account. Annual surveys at the monumented cross-sections will provide absolute comparisons to the erosion rates summarized in the preceding table and presented in **Appendix D**.

As the revegetated riparian corridors canopy, mid-story, shrub, herbaceous and streamside vegetation matures, intuitively, annual streambank erosion rates should decrease as root mass and density along the restored stream reaches become more pervasive over time.

#### Reference Reach Data Collection

For Beaverdam Creek, bankfull discharge was determined through a quantitative assessment and analysis of reference reach boundary conditions and comparison of predicted bankfull discharge through a stable riffle cross-section located on Davis Branch, 43 feet upstream from its confluence with Gourdvine Creek. The Davis Branch Reference Reach is located 12.8 miles northeast of the Beaverdam Creek and Unnamed Tributaries Restoration Project. The reference reach is located along the same geologic structural feature, the Troy Anticlinorium (northwest limb near the axial plane of an unnamed syncline), in the same geologic formation, the McManus Formation, is mapped on the same soil series (Chewacla silt loam, Goldston soils and Cid channery silt loam), and is located in the same physiographic province and ecoregion as the Beaverdam Creek project impaired reaches. The reference reach is shown at watershed scale on Figure 4.

A complete Rosgen Level III watershed assessment and analysis of the reference reach conditions was conducted during August 8 and 9, 2006. Due to extremely thick riparian vegetation during August 2006, it was possible to collect profile and cross-section data only along a relatively short length of the stable reach. Approximately 118 linear feet of profile, capturing three pool and four riffle sequences, with one representative riffle and pool cross-section, were surveyed in the field. Geologic structural controls and lithology, fluvial geomorphologic processes, depositional materials, climatic influence, riparian vegetation, deposition-pattern, debris occurrence, meander pattern, channel stability rating, sediment supply, streambed stability and width/depth ratio state were evaluated following Rosgen Level III stream assessment protocols. Visibility was limited in the field to dense vegetative cover along the Davis Branch Reference Reach; therefore, Union County orthoimagery (2/2004) was used to verify stream pattern.

A total of 1129 linear feet of the reach was assessed for each Level III stream state and condition parameter consistent with a Rosgen Level III methodologies. The assessment included GPS data spatial analysis to evaluate channel pattern upstream from the surveyed reach, beyond the point where additional differential level surveying was impracticable and channel pattern could not be discerned from recent aerial imagery.

Calculated bankfull discharge for the surveyed reference reach riffle cross-section, was computed using hydraulic radius, wetted perimeter, channel slope and a relative roughness (u/u\*) method based on the average protrusion height of the steeply dipping bedrock (Rosgen, 1998). Additionally, a particle distribution was collected from the large angular cobble deposited along the reference reach riffle bed.

Reference reach survey data, analysis, classification and geomorphologic summary reports for the Davis Branch Reference Reach are presented in Appendix 3, Beaverdam Creek and Unnamed Tributaries Restoration Plan, NC EEP Project Number: D06054-C (EMH&T, January 16, 2008). The Davis Branch Reference Reach morphologic and hydraulic data are summarized in **Table 2**.

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#### Reference Reach Classification

The reference reach is a Rosgen Valley Type VIII, E3/1b stream type (i.e., E channel morphology, large cobble substrate with strong bedrock control, profile gradient greater than 2 percent). The reference reach is located within a healthy, deciduous hardwood forested riparian corridor. The D84 particle size from the stable riffle particle distribution is 140.1 mm and is consistent with the observed bed thickness and axial splitting planes and observed joint sets in the folded and deformed slate bedrock.

#### Reference Reach Discharge

See Section 3.5 for a comprehensive analysis and of bankfull discharge for the Davis Branch Reference Reach and the Beaverdam Creek and Tributaries project reaches. Regional curve, reference reach, pre-existing, design and as-built bankfull discharge are presented in tabular format in **Table 2**.

#### Channel Morphology

Stream channel morphology data for the Davis Branch reference reach, the Beaverdam Creek mainstem, UT1 and UT2 is presented in tabular format on **Table 2**. The Davis Branch reference reach is a Rosgen Valley Type VIII, E3/1b stream type.

#### **Channel Stability Assessment**

Reference reach channel stability was analyzed using the vertical velocity near-bank stress method algorithm in RiverMorph® v.4.1.1 and reach streambank observations and channel morphology from reference reach Pool Cross-Section 1+83, located on Davis Branch 117 feet upstream from its confluence with Gourdvine Creek. The predicted annual erosion rate estimate was calculated for the entire 1,129 linear feet of stream evaluated as part of the Rosgen Level III reference reach study. Based on reference reach conditions, the predicted sediment loss is 3.23 cubic yards or 4.2 tons per year. This equates to 0.0043 tons/year per foot of reach, or two one hundredths of a foot (0.02 ft) streambank erosion on an annual basis. The near-bank adjective rating (0.35) is very low for the reference reach, indicating extremely stable channel conditions.

#### Vegetation

The Davis Branch reference reach flows through a deciduous hardwood forest area, which provides a wide riparian corridor. The canopy layer is dominated by native tree species including *Plantanus occidentalis* (American sycamore), *Carya* species (hickory), and *Acer negundo* (boxelder). The shrub/sapling and herbaceous understory is extremely thick and provides significant protection against bank erosion. Species such as *Rosa multiflora* (multiflora rose), *Alnus serrulata* (hazel alder), *Bignonia capreolata* (crossvine), *Viola* sp. (violet), and *Convolvulus species* (bindweed) are present within the understory. This healthy, robust vegetation and associated root mass along the reference reach riparian corridor, extending overbank into the channel, is extremely stable and resistant to streambank erosion.

 $\begin{tabular}{ll} \textit{Mitigation Plan-Beaverdam Creek and Unnamed Tributaries} \\ \textit{EEP Contract} ~\#~ D06054-C \end{tabular}$ 

#### 2.5 Restoration Summary

A summary of the restored stream lengths, restoration approach and associated SMU credits are presented in Table 4 below.

Proj	Table 4: Pre-Ex ect Number D060	isting Condition 54-C (Beaverd	ons/Post-Construction am Creek & Tributa	Summary ries Restoration	1)
Tributary Reach ID	Pre-existing length	Restored Length*	Restoration Level	Credit Ratio	SMUs**
Mainstem	416 lf	460 lf	Priority Level I Restoration	1.0	460
UT1	1,867 lf	2300 lf	Priority Level I /II Restoration	1.0	2,300
UT2	203 lf	284 lf	Priority Level I /II Restoration	1.0	284
Totals	2,486 lf	3,044 lf			3,044

<sup>\*</sup>Restored Length excludes permanent conservation easement crossings.

<sup>\*\*</sup>Restored Length divided by SMU Credit Ratio

Mitigation Plan – Beaverdam Creek and Unnamed Tributaries EEP Contract # D06054-C

#### 3.0 MONITORING PLAN

To demonstrate the success of the project, three forms of monitoring will be performed: (1) photo documentation; (2) ecological function assessment; and (3) channel stability measurements. Long-term success criteria will be evaluated by monitoring and documenting the following:

- Channel aggradation or degradation,
- streambank erosion,
- effectiveness of erosion control measures,
- presence of instream bar deposits,
- · health and survival of indigenous, non-invasive vegetation, and
- changes in as-built channel pattern, profile and dimension.

Parameters included in the annual stream monitoring to ensure the success of the restoration activities will include stream channel surveys along longitudinal profiles and monumented cross sections, pebble counts across representative riffle and pool cross-sections, photographs, and vegetation surveys.

The restoration site will be monitored for five consecutive years or until the required success criteria have been met as determined by North Carolina Division of Water Quality (DWQ) and the Wilmington District of the U.S. Army Corps of Engineers (USACE). Channel stability monitoring field surveys, including measurements and photographs, will be performed during June 2009. Planting will occur during the spring of 2009. The planted vegetation will first be monitored during the 2009 growing season, during September. Monitoring will be conducted in accordance with the multi-agency, North Carolina Stream Mitigation Guidelines (April 2003) applicable to Restoration and Enhancement Level I projects and the template Content, Format and Data Requirements for EEP Monitoring Reports, Version 1.2 (11/16/06). Vegetation monitoring will be conducting in accordance with CVS-EEP Protocol for Recording Vegetation, Version 4.2 (Lee, M.T., Peet, RK., Roberts, S.R., Wentworth, T.R. 2008) for Levels 1 and 2 Plot Sampling.

Monitoring reports and discussions of remedial actions will take place with EEP. EEP will review the monitoring documents and make them available to the agencies after the review period. Decision making regarding remediation will be between EEP and WRC and its agents or representatives. Agency interaction will take place through permit requests for maintenance should they become necessary. Agency interaction will take place at the end of the monitoring period.

#### 3.1 Stream Channel Monitoring

Stream channel stability will be physically monitored at eight permanent, monumented cross-sections annually. This includes two cross-sections (1 riffle, 1 pool) on Beaverdam Creek mainstem, four cross-sections (2 riffles, 2 pools) on UT1, as well as two cross-sections (1 riffle, 1 pool) on UT2. Stream stability and pattern will also be evaluated along longitudinal profiles surveyed along the entire length of each restored reach.

Mitigation Plan – Davis Branch and Unnamed Tributary EEP Contract # D06054-C

Photographs will be taken upstream, downstream and across channel at each monumented cross-section at the time of survey. The monumented cross-section locations and longitudinal profiles were surveyed immediately following construction as part of the "as-built" survey and are shown on the As-Built Plan sheets in **Section 7.0**. The As-Built Plan sheets include the dimension, pattern, and profiles of the constructed stream channels. The As-Built condition (Year 0) will be utilized as baseline to compare future monitoring surveys and subsequently to determine channel stability and transition. Year 0 "As-Built" Long-Term Monitoring Profiles are included in **Appendix B**. Year 0 "As-Built" Long-Term Monitoring Cross-Section summary templates and particle distribution summary templates are included in **Appendix C**.

Yearly monitoring will also include pebble counts to evaluate streambed particle distributions. Pebble count data will be collected at each of the eight monumented cross-section locations. The number of particles in standard size classes will be reported each year to assess sediment transport capacity and competency, streambed particle sorting and depositional trends, and stream stability over time. Annual inspection of in-stream structures, which for this project includes only constructed riffles, will also occur to verify proper function and channel stability. Stream channel monitoring surveys will be completed annually for five consecutive years, starting in June 2009 (Year 1), greater than six months post-construction completion. Annual stream profile and cross-section surveys will be compared to the asbuilt conditions stream corridor survey (Year 0, December 2008).

A minimum of two bankfull flow events will be documented during the five year monitoring period, occurring separate monitoring years. Bankfull flow events will be documented utilizing two 4-feet, USGS Type A crest-stage stream gages installed on the project reaches; one crest-gage set at bankfull stage at the confluence of Davis Branch and UT1, and one crest-gage set at bankfull stage near monumented cross-section number four (XS-4) on UT1. Photo-documentation after bankfull flows will be presented in the monitoring reports. The locations of the crest-stage stream gages are shown on the As-Built Plan Sheets in Section 7.0. In the event two bankfull events do not occur during the five-year monitoring period, consultations with the U.S. Army Corps of Engineers, the Division of Water Quality and the resource agencies will be coordinated to determine if further monitoring is necessary to demonstrate success criteria have been achieved.

#### 3.2 Planted Woody Vegetation Monitoring

Woody vegetation planted along the streams on April 8, 2009 will be monitored for five consecutive years. Per the required plots calculation from EEP, a total of eight (8) ten by ten meter square plots (one plot along Davis Branch mainstem, six along UT1 and one along the UT2) have been permanently established. The mainstem plot is five by twenty meters in dimension. Corner markers were permanently installed and one corner surveyed for future reference. The species, density of living stems, and the cause of mortality if identifiable will be recorded for all planted woody species within each plot. Vegetation will be sampled annually and reported each year along with the data collected during the physical monitoring of the project stream reaches. The focus of the vegetative monitoring will be a stem count of planted individuals in the tree and shrub stratum. Data on height and diameter will also be recorded according to the *CVS-EEP* protocol. Percent cover of the plot will be documented via photographic documentation at each vegetative plot. Vegetative problem areas along the project area will be identified, mapped, and documented via photographs. Vegetation monitoring will occur between the months of September and October. Vegetation plots photo documentation is included in Appendix A. Vegetation plot locations are shown on the As-Built Plan Sheets.

Mitigation Plan – Beaverdam Creek and Unnamed Tributaries EEP Contract # D06054-C

#### 3.3 Performance Standards

The performance standards for the restoration project are those mandated in the multi-agency *Stream Mitigation Guidelines* (USACE Wilmington District, et al., April 2003). Performance goals for the site are:

- Minimal or negligible development of instream bar deposits.
- Minimal or negligible change in channel pattern, profile and dimension in comparison to As-Built conditions. Adjustments may occur and some may be indicative of increasing stability, such as moderate reductions in width/depth ratios as a result of slight channel narrowing and natural substrate sorting and shaping of bedform and features
- Maintenance of floodplain connectivity (only reductions or very small increases will be considered acceptable).
- Target density of 320 stems per acre after 3 years and 260 stems per acre after 5 years for planted woody vegetation (represents 80% survival after 5 years).

Subsequent monitoring reports will address the attainment of performance goals. If goals are not be attained, then the monitoring reports will document any remedial actions taken during the monitoring period and the success of these actions.

*Mitigation Plan – Beaverdam Creek and Unnamed Tributaries EEP Contract* # D06054-C

#### 4.0 MAINTENANCE AND CONTINGENCY PLANS

Adaptive management is a systematic process for developing knowledge and continually improving project development by learning from previous projects and their performance outcomes (River Institute, 2004). This project is large in scope and entails many new applications of natural stream channel design methodologies, making an adaptive management approach essential to the success of the project. Rather than following the conventional approach to construction projects where a plan is developed and closely constructed in a rigid and structured format, we will employ a adaptive management strategy in the truest sense. Essentially, we have initiated the initial restoration of the Beaverdam Creek Mainstem, UT1 and UT2 in the context of the data, methodologies and technology currently available. As the project is monitored, we will collect data to verify the streams are evolving in the direction of increased stability and biological diversity. As the data are collected and evaluated, the knowledge gained will be directly integrated into the management and maintenance of the project throughout the monitoring period.

Mitigation Plan – Beaverdam Creek and Unnamed Tributaries EEP Contract # D06054-C

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 $http://www.nceep.net/business/monitoring/Monitoring\_report\_web/pdfs/NCEEP\_Monitoring\_Report\_Template\_Ver\_1\_1\%20\_09\_16\_05.pdf$ 

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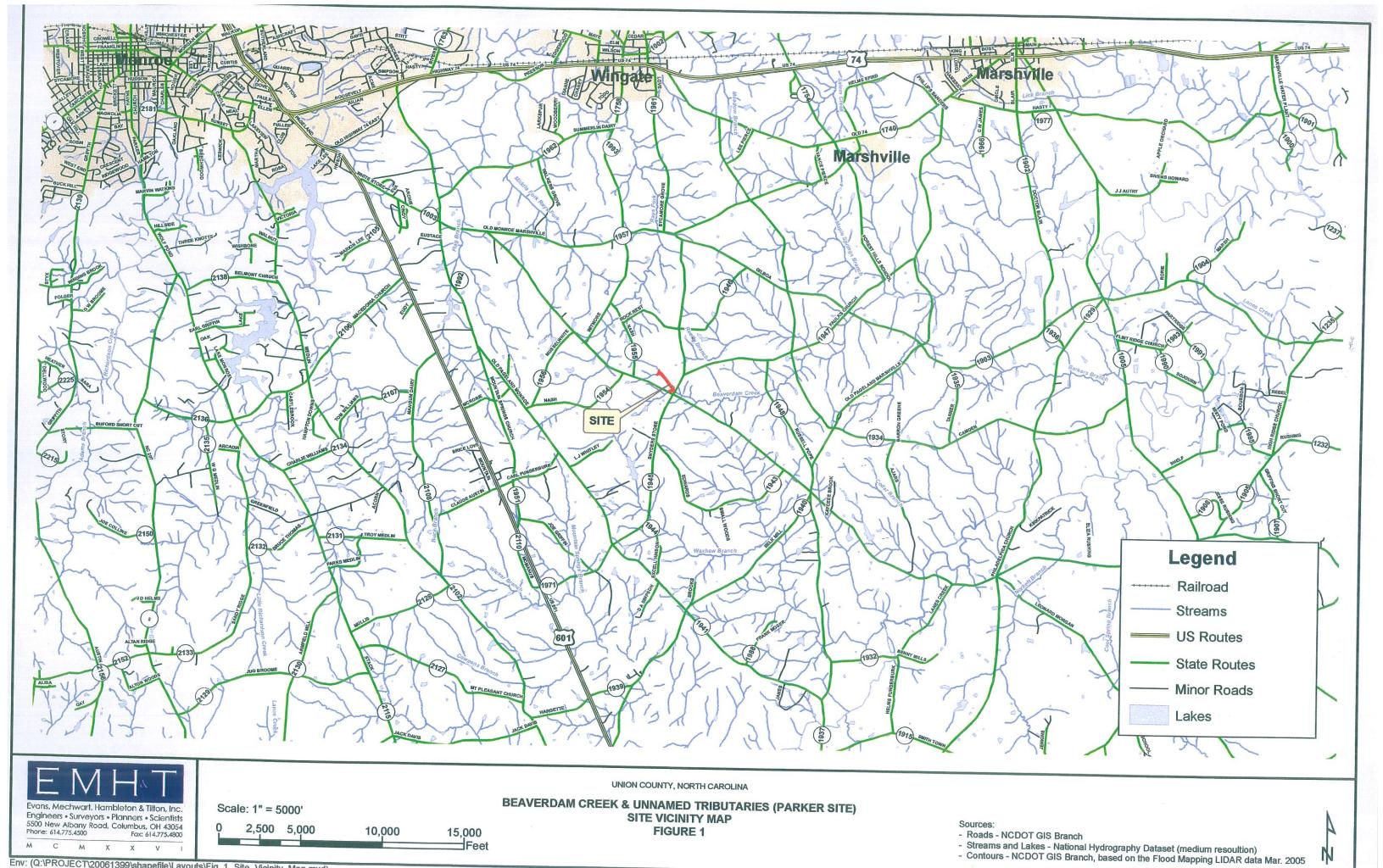
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 $\begin{tabular}{ll} \textit{Mitigation Plan-Beaverdam Creek and Unnamed Tributaries} \\ \textit{EEP Contract} ~\#~ D06054-C \end{tabular}$ 

6.0 FIGURES



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**LEGEND** 

PROP. BANKFULL

PROP. CONSERVATION EASEMENT

Evans, Mechwart, Hambleton & Tilton, Inc. Evans, Mecriwan, Hambieron & Illion, Inc. Engineers • Surveyors • Planners • Scientists 5500 New Albany Road, Columbus, OH 43054 Phone: 614.775.4500 Fax: 614.775.4800

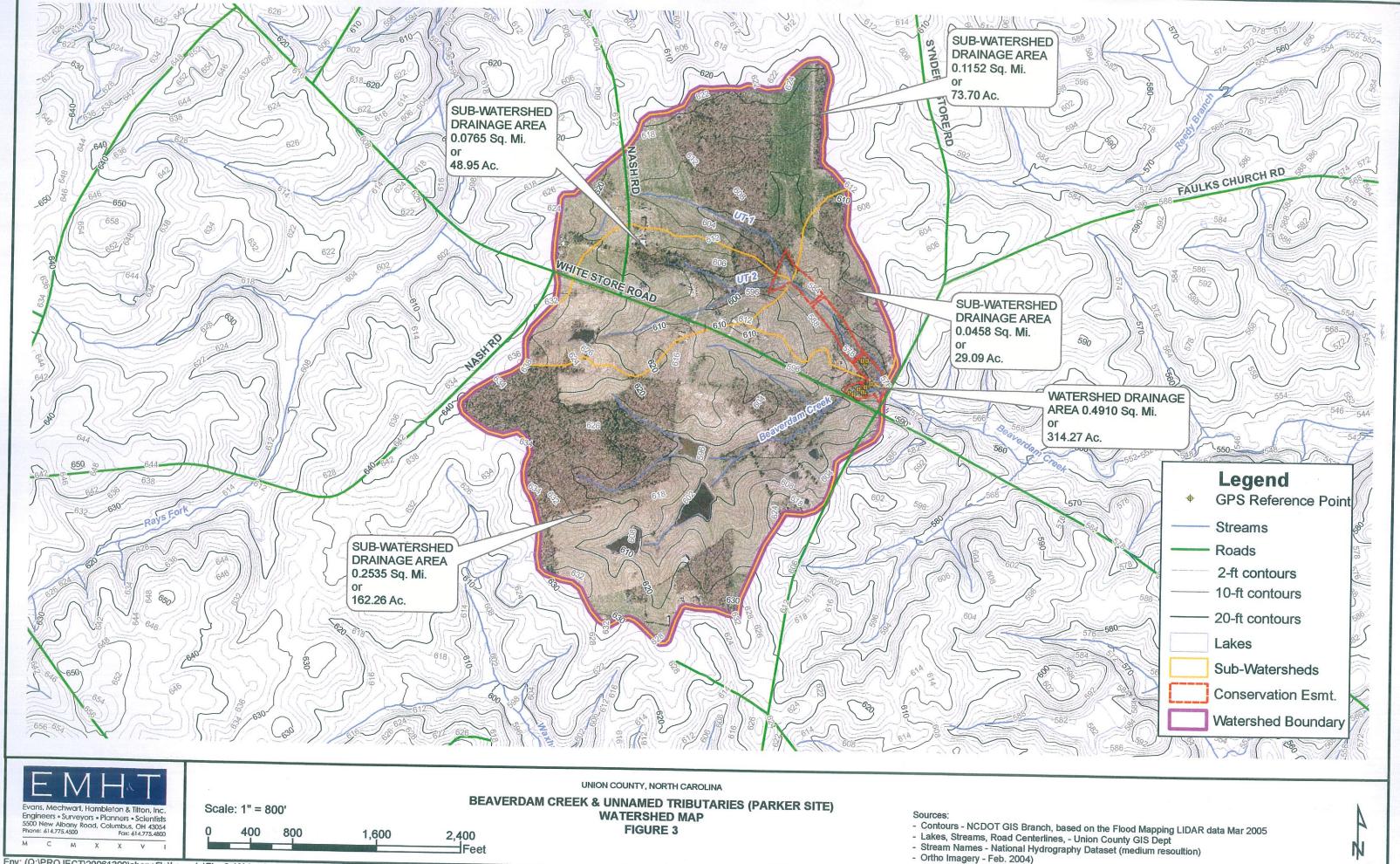
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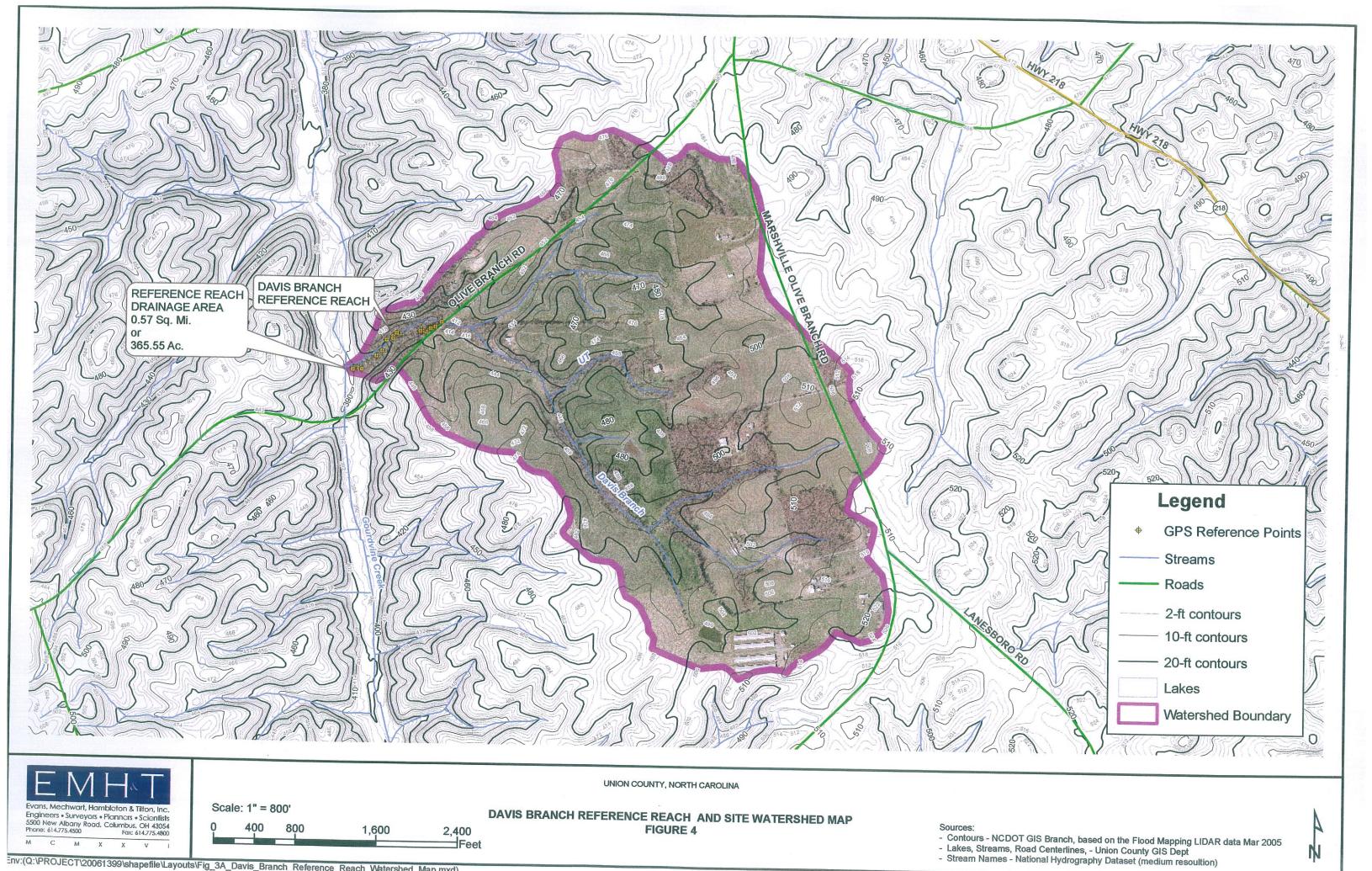
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Scale: 1" = 200' 100 200 800 UNION COUNTY, NORTH CAROLINA

# BEAVERDAM CREEK & UNNAMED TRIBUTARIES (PARKER SITE) STREAM REACHES MAP FIGURE 2

- Contours NCDOT GIS Branch, based on the Flood Mapping LIDAR data Mar 2005 Ortho Imagery Feb. 2004





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Mitigation Plan – Beaverdam Creek and Unnamed Tributaries EEP Contract # D06054-C

7.0 AS-BUILT PLAN SHEETS

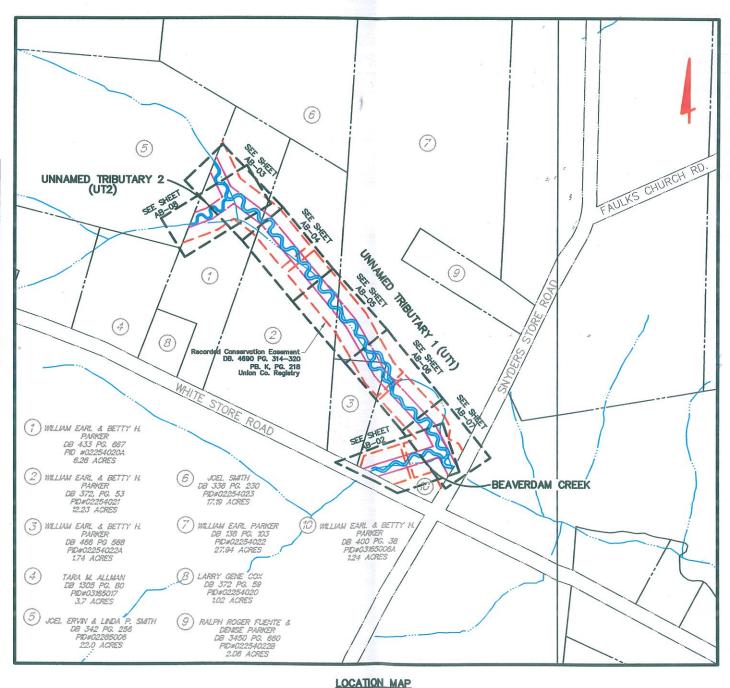
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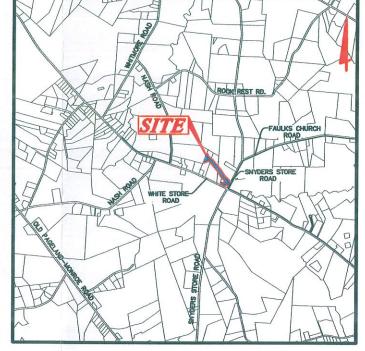
## **BEAVERDAM CREEK AND UNNAMED TRIBUTARIES** NC EEP PROJECT NO. D06054-C 2009

Project Num	Pre-Existin nber D06054-0	g Conditions C (Beaverdan	/Post—Construction Creek & Unnamed	Summary 1 Tributaries R	estoration)
ributary ach ID	Pre-existing Length	Restored Length *	Restoration Level	Credit Ratio	SMUs**
Beaverdam Creek Mainstem	416 lf.	460 lf.	Priority Level I Restoration	1.0	460
UT1	1,867 If.	2,300 lf.	Priority Level I/II Restoration	1.0	2,300
UT2	203 If.	284 If.	Priority Level I/II Restoration	1.0	284
Totals	2,486 If.	3,044 If.			3,044

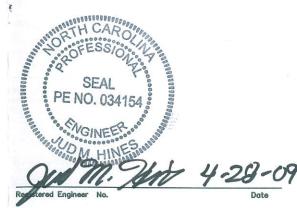
\* Restored Length excludes permanent Conservation Easement crossings.

\*\* Restored Length divided by SMU Credit Ratio.

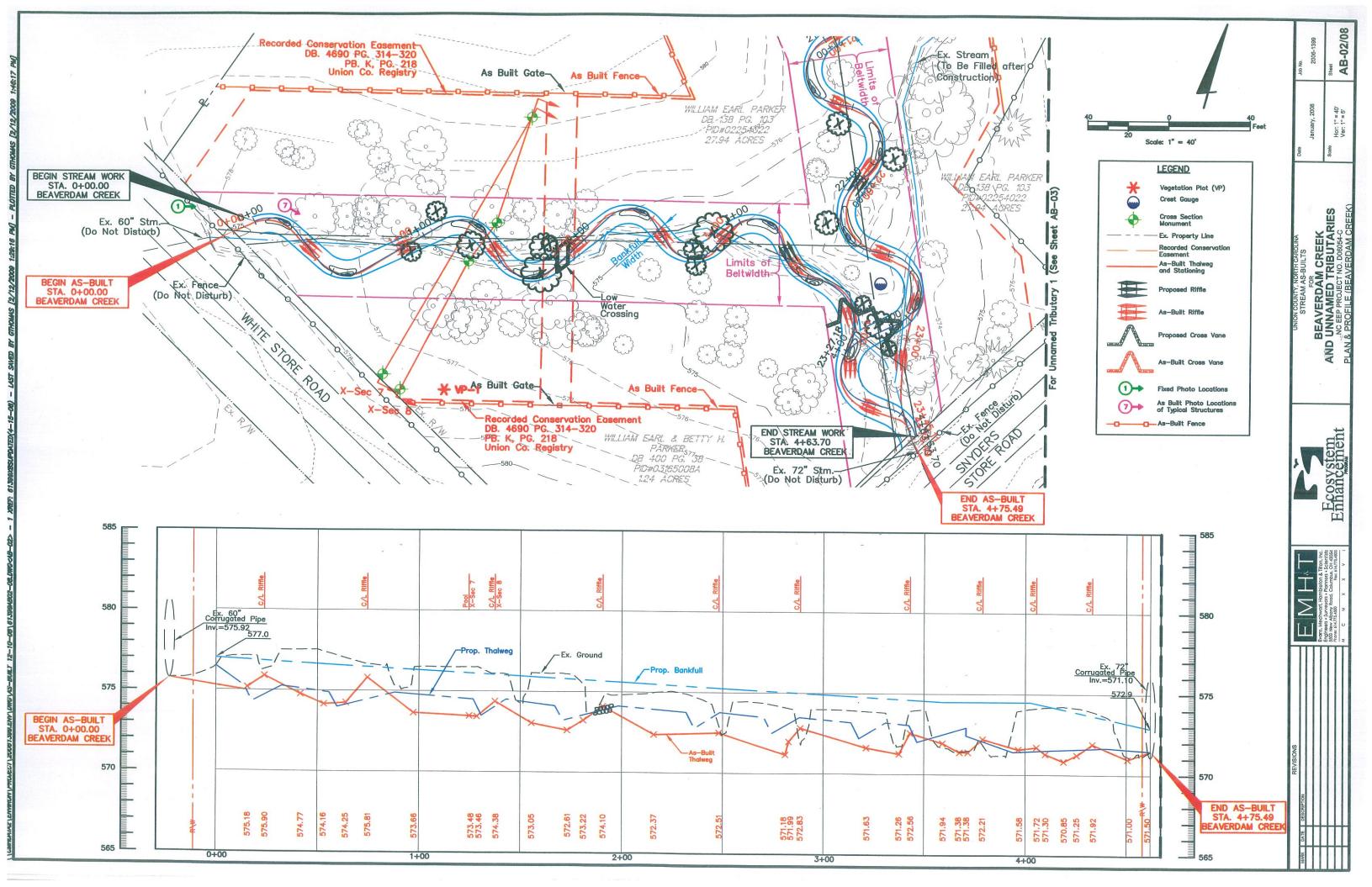


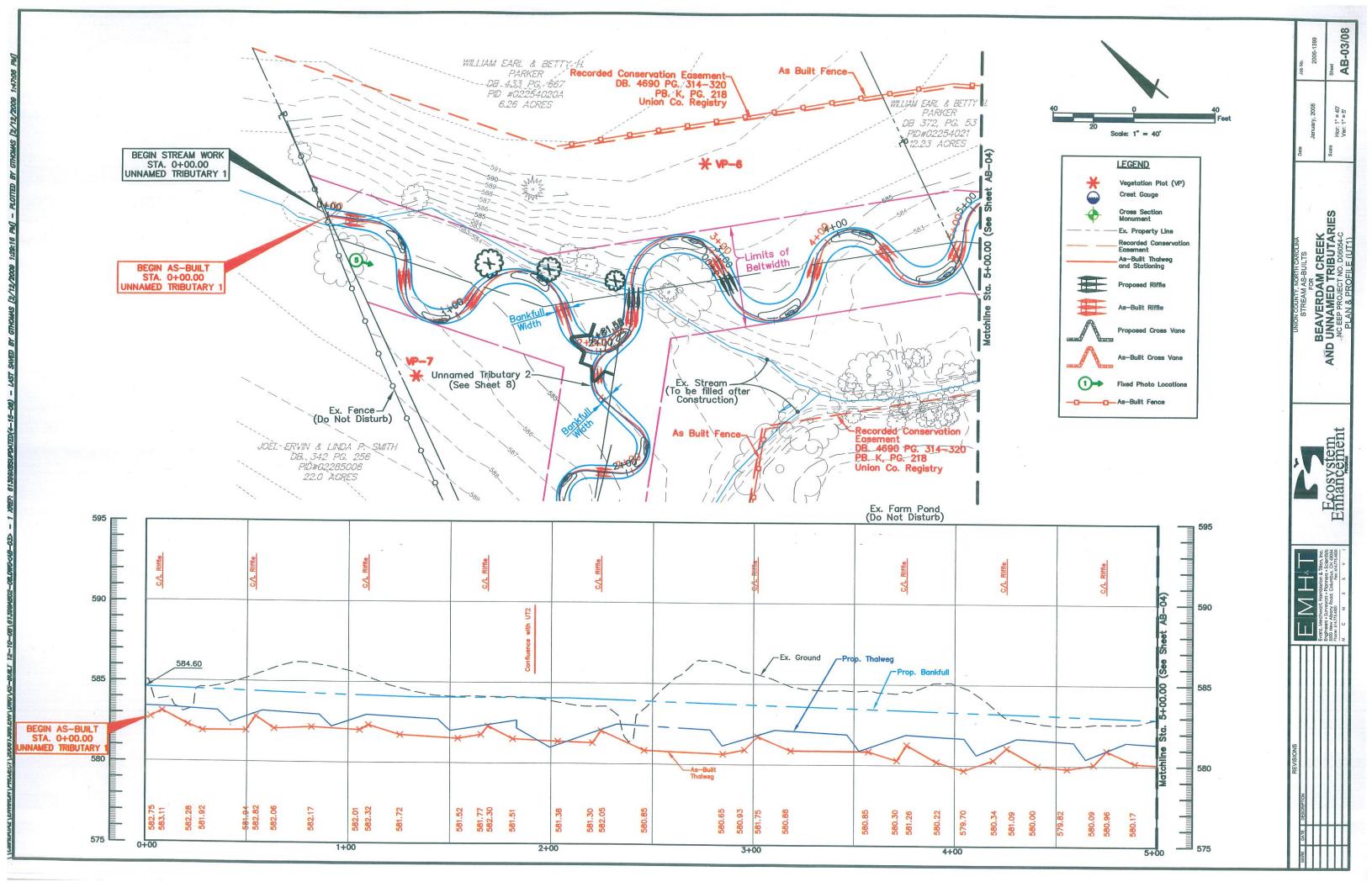


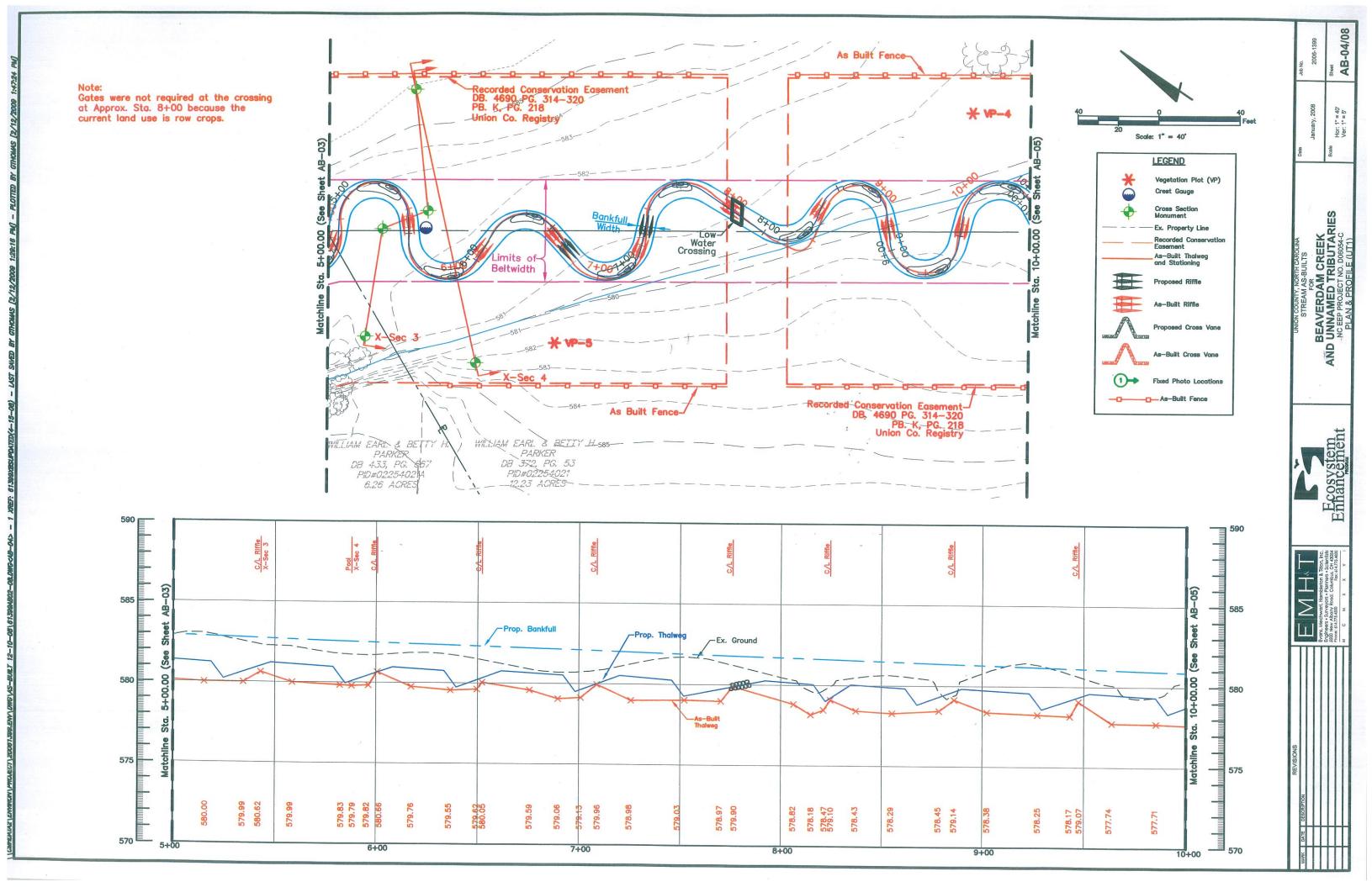
BEAVERDAM CREEK
AND UNNAMED TRIBUTARIES
NC EEP PROJECT NO. D00054-C

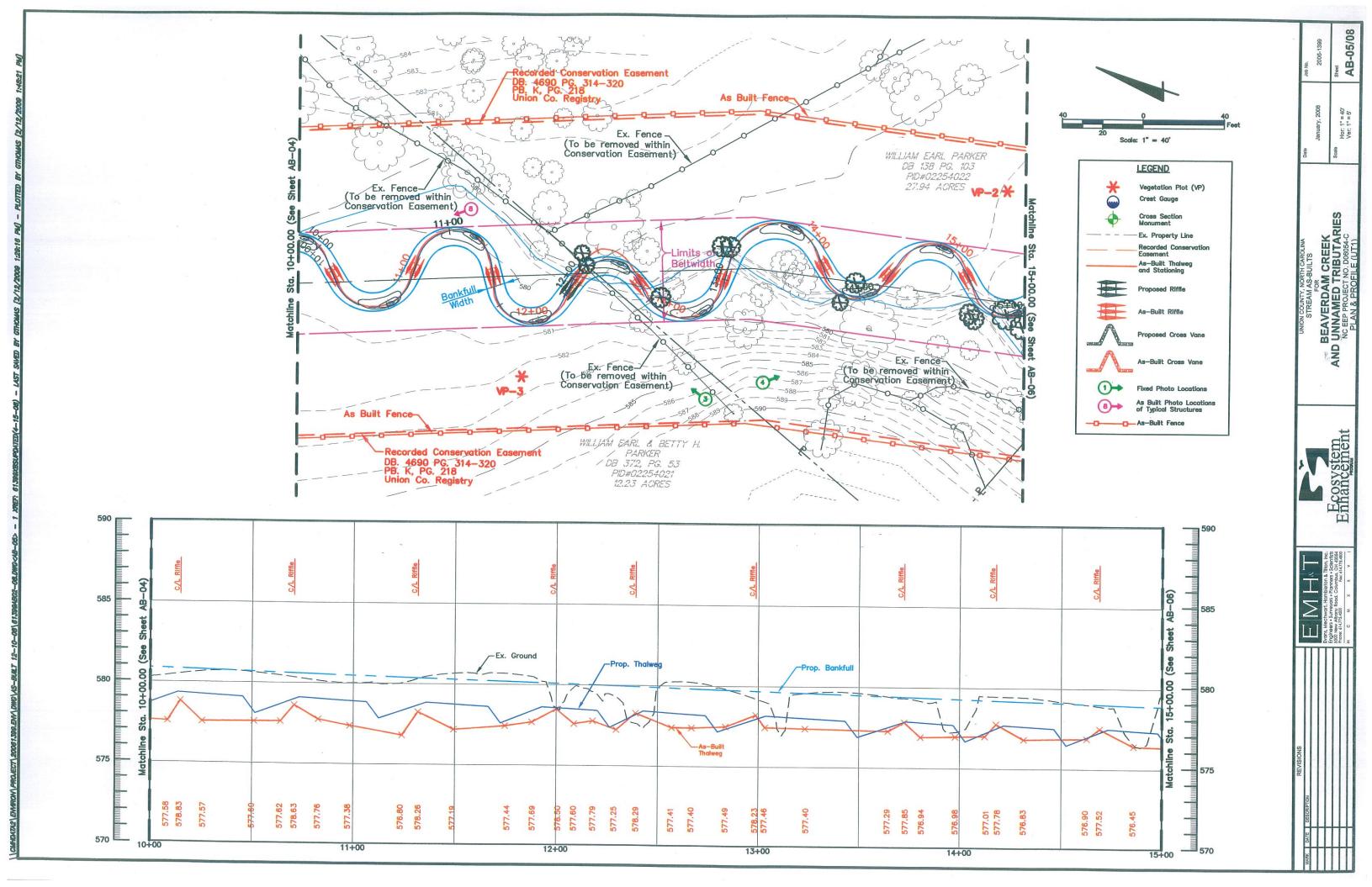


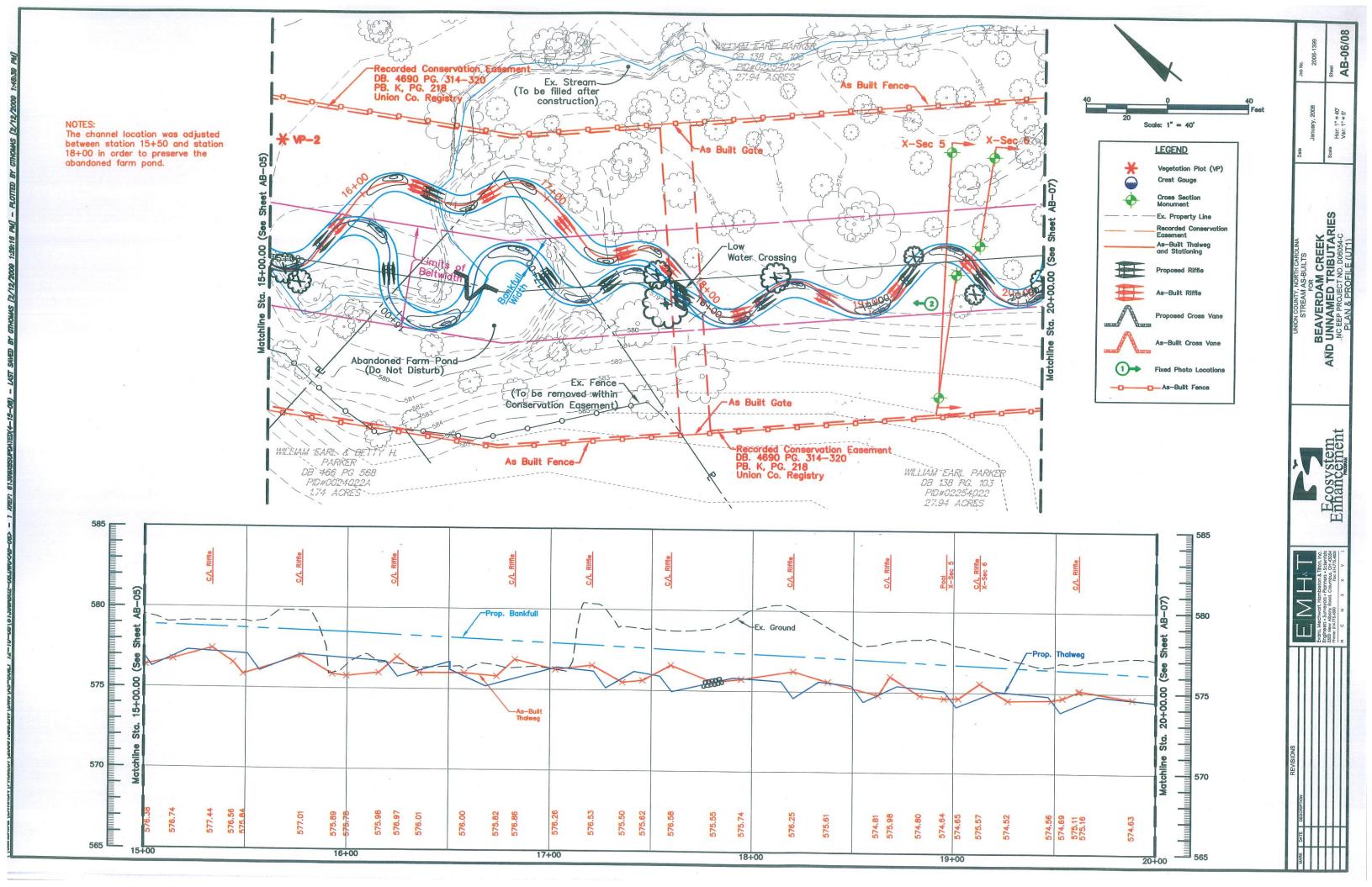


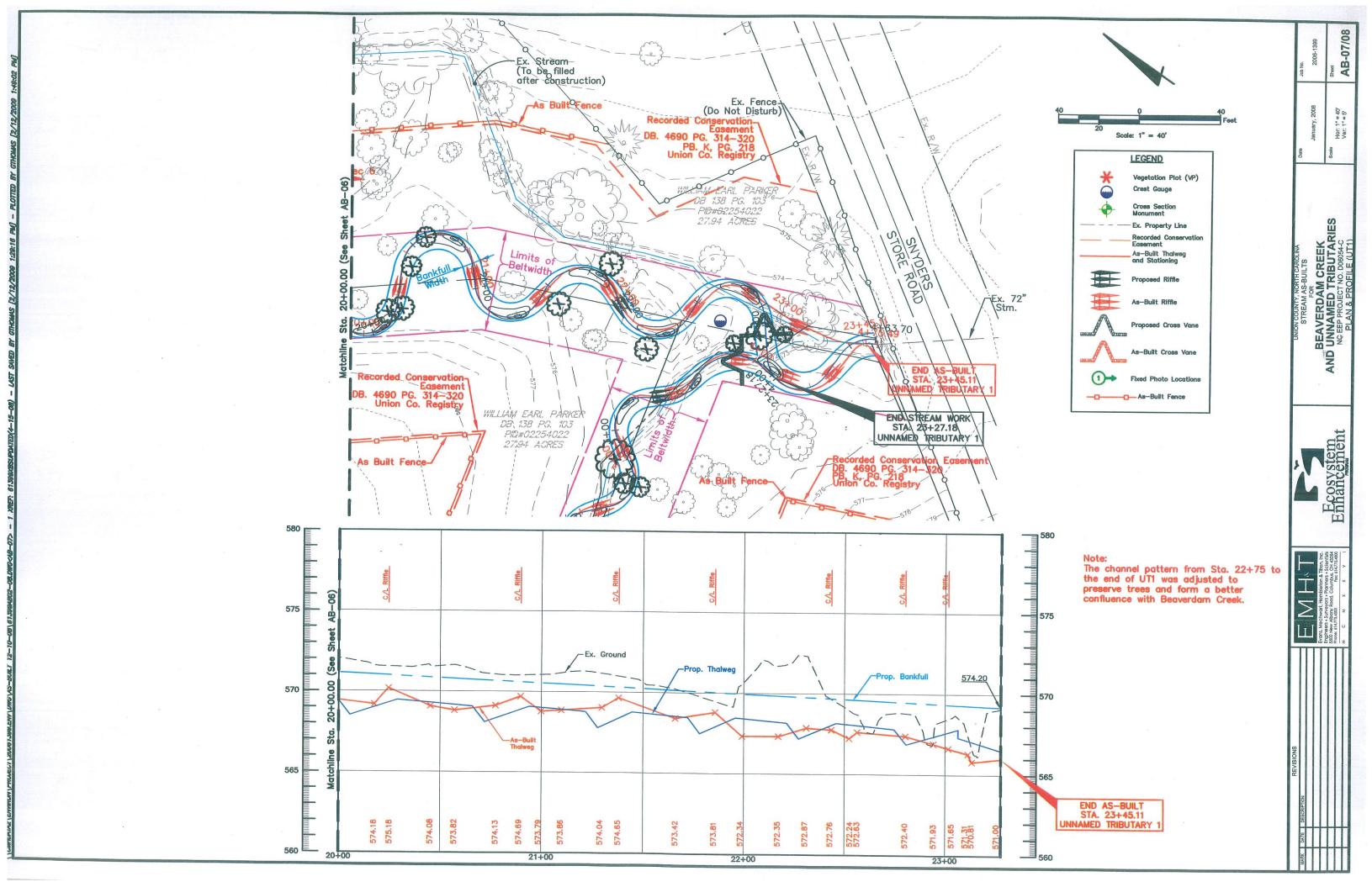


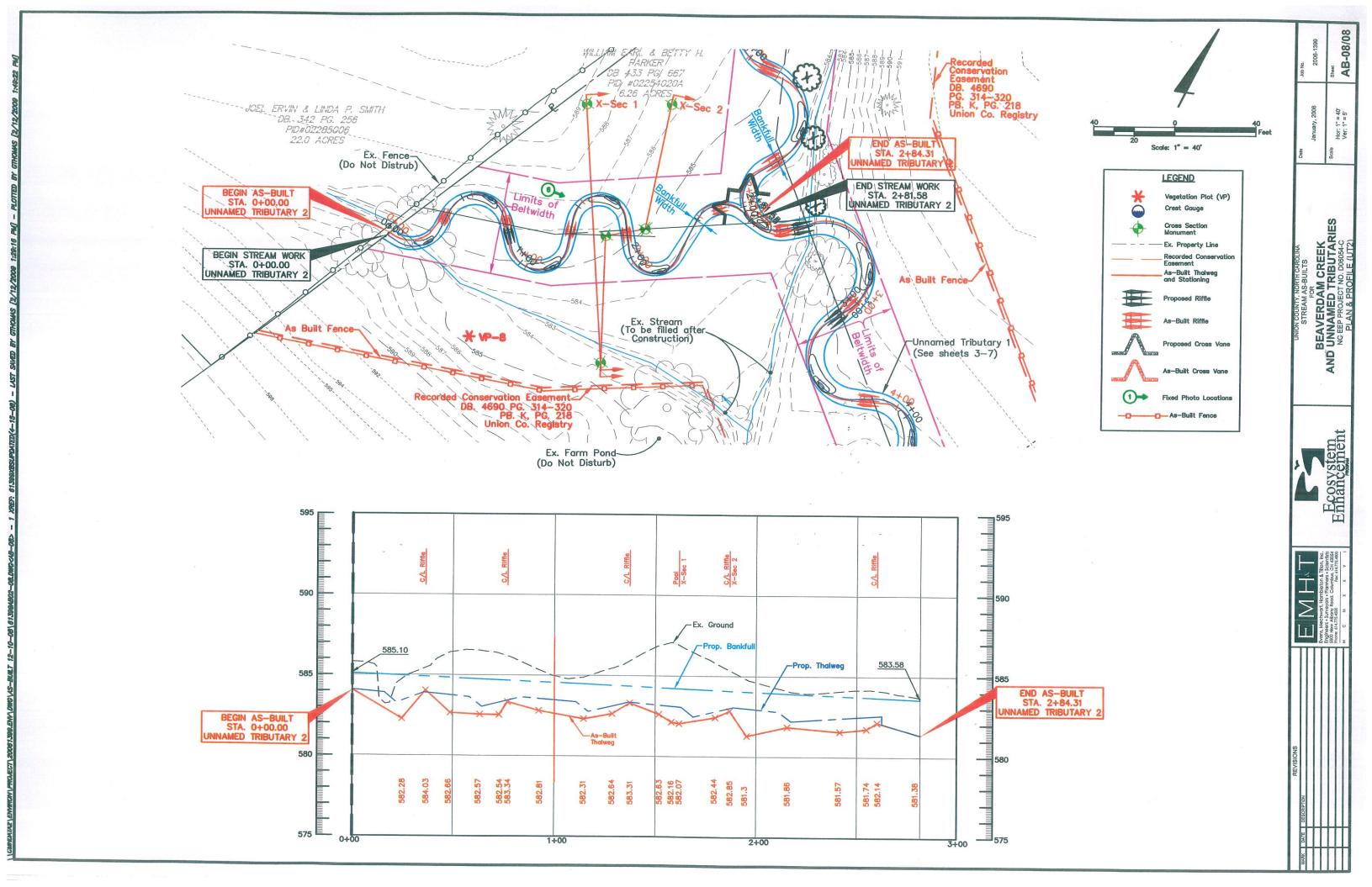












#### ECOSYSTEM ENHANCEMENT PROGRAM

 $\begin{tabular}{ll} \textit{Mitigation Plan-Beaverdam Creek and Unnamed Tributaries} \\ \textit{EEP Contract} ~\#~ D06054-C \end{tabular}$ 

### Appendix A

**Beaverdam Creek Mainstem and Unnamed Tributaries** 

Fixed Station As-Built Photographic Documentation





Photograph 1
Fixed Station 1. Overview of Beaverdam
Creek, looking downstream.



Photograph 3
Fixed Station 3. Overview of valley along UT1, looking upstream near station 13+00.



Photograph 2
Fixed Station 2. Overview of UT1, looking upstream near station 19+00.



Photograph 4
Fixed Station 4. Overview of valley along UT1, looking downstream near station 13+00.



Photograph 5
Fixed Station 5. Overview of UT1, looking downstream from upstream project limits.



Photograph 6
Fixed Station 6. Overview of UT2, looking downstream.



Photograph 7
Example Structure. Riffle at Station 0+32 on Beaverdam Creek, looking downstream.



Photograph 8
Example Structure. Riffle at Station 10+73
on UT1, looking upstream.



Vegetation Plot No. 1 5 m x 20 m. Beaverdam Creek Mainstem Station 0+75, looking downstream.



Vegetation Plot No. 3
10 m x 10 m. UT1 Station 11+50, looking downstream.



Vegetation Plot No. 2 10 m x 10 m. UT1 Station 15+50, looking downstream.



Vegetation Plot No. 4
10 m x 10 m. UT1 Station 10+00, looking downstream.



Vegetation Plot No. 5
10 m x 10 m. UT1 Station 6+50, looking downstream.



Vegetation Plot No. 6
10 m x 10 m. UT1 Station 3+50, looking downstream.



Vegetation Plot No. 7
10 m x 10 m. UT1 Station 1+50, looking downstream.



Vegetation Plot No. 8
10 m x 10 m. UT2 Station 0+50, looking downstream.

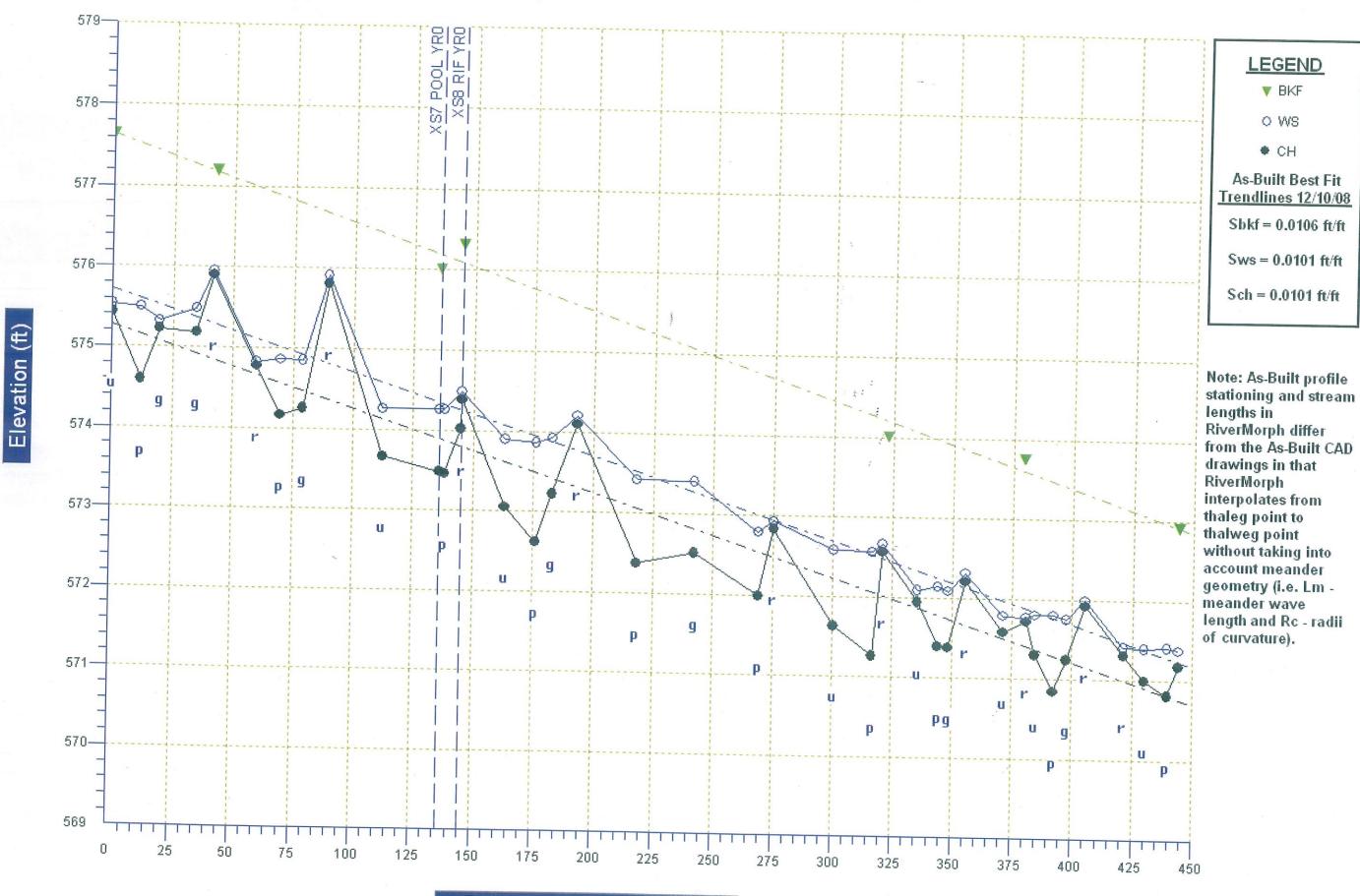
#### ECOSYSTEM ENHANCEMENT PROGRAM

 $\begin{tabular}{ll} \textit{Mitigation Plan-Beaverdam Creek and Unnamed Tributaries} \\ \textit{EEP Contract} ~\#~ D06054-C \end{tabular}$ 

### Appendix B

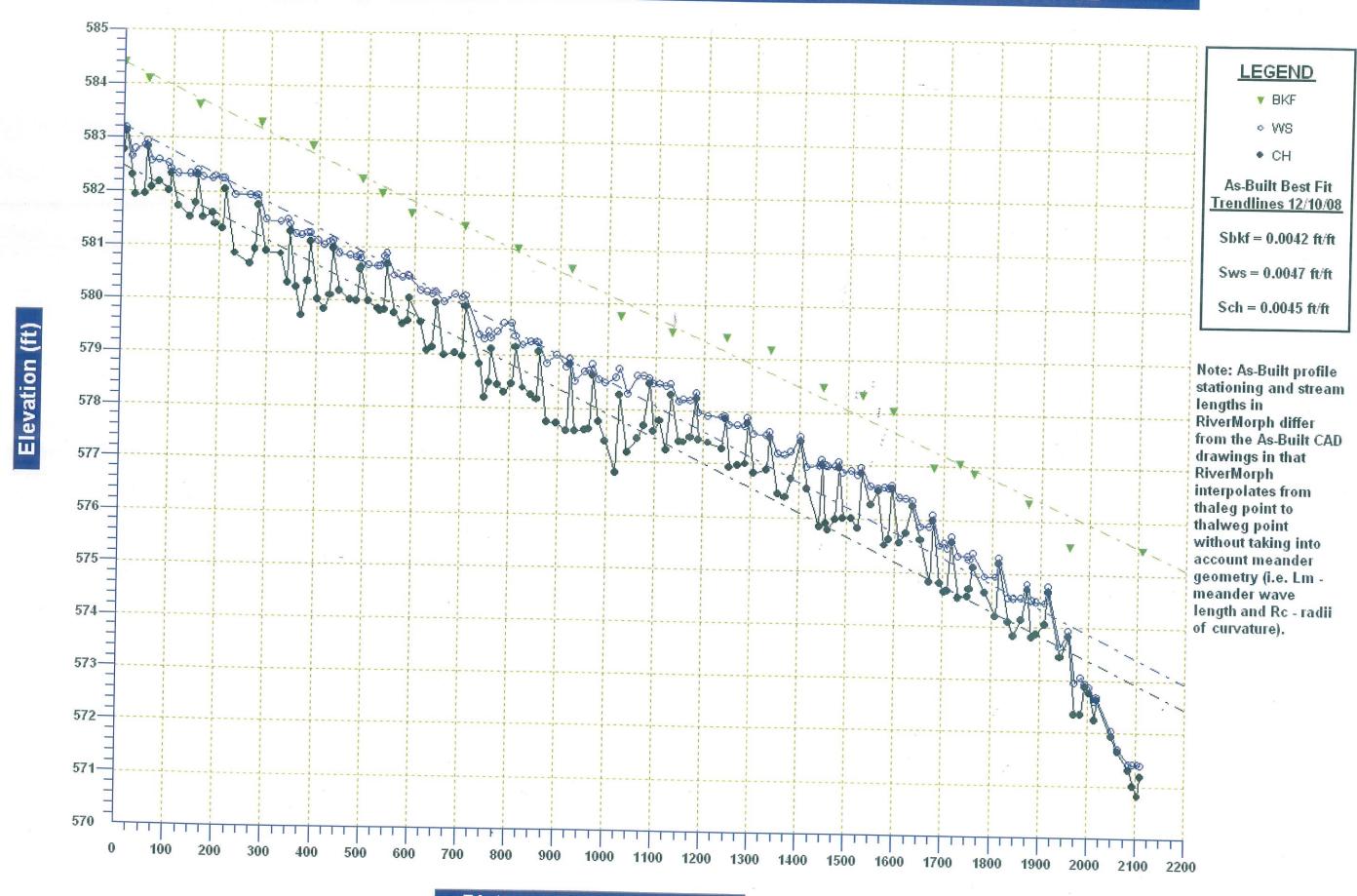
**As-Built Long-Term Monitoring Profiles** 

### Beaverdam Mainstem As-Built Profile -12/10/2008



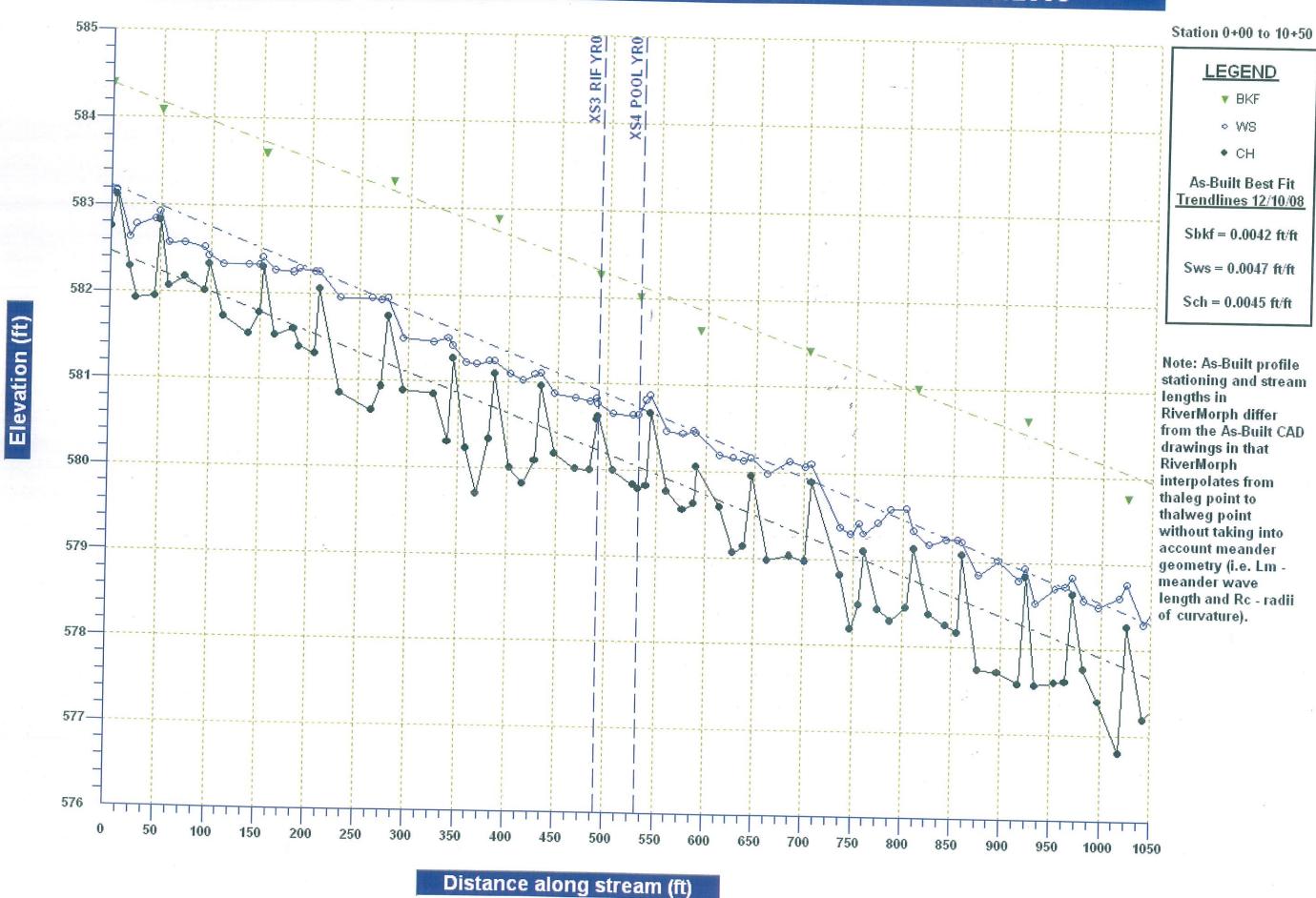
Distance along stream (ft)

# Beaverdam Creek - Unnamed Tributary 1 As-Built Profile - 12/10/2008

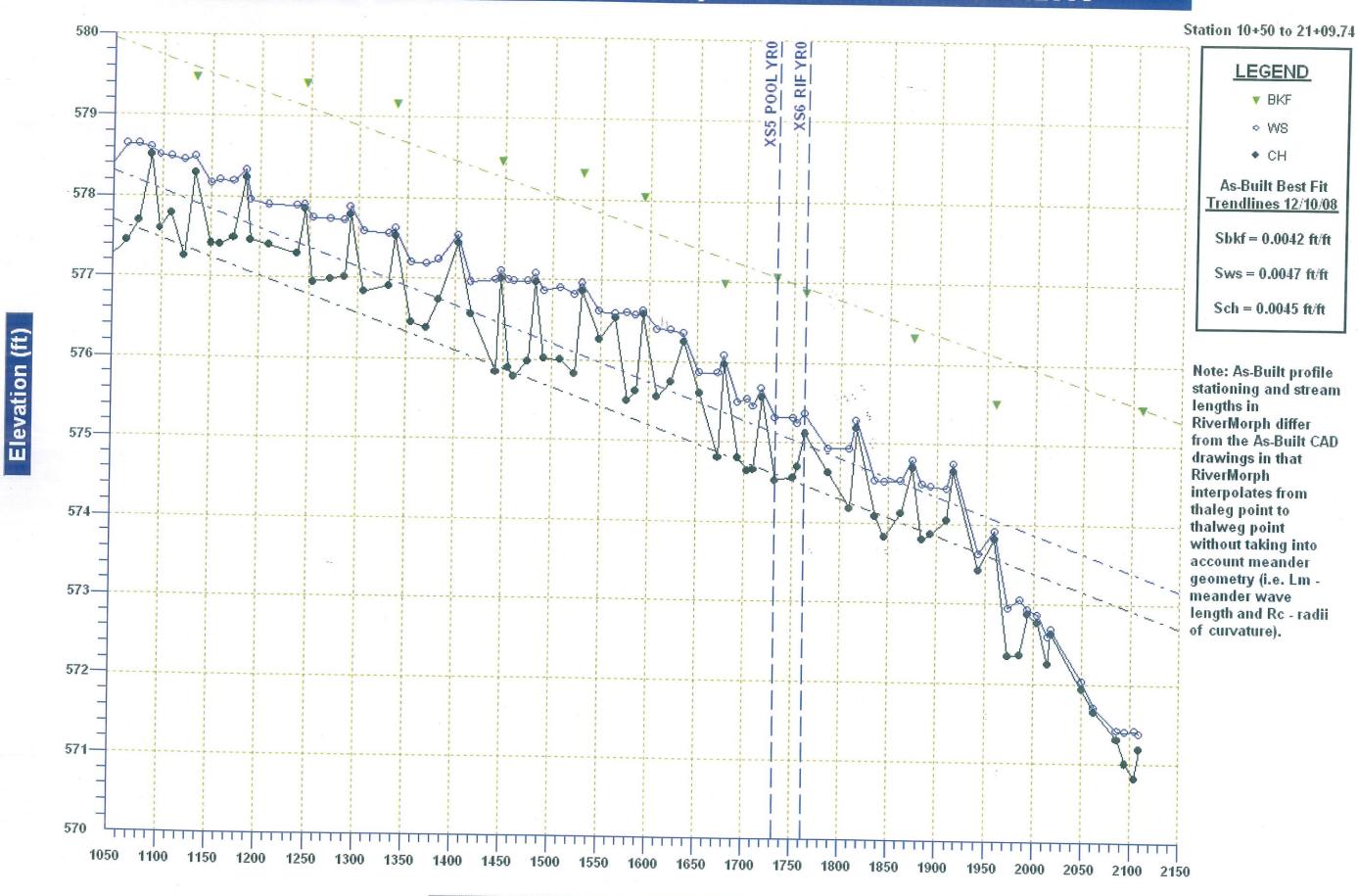


Distance along stream (ft)

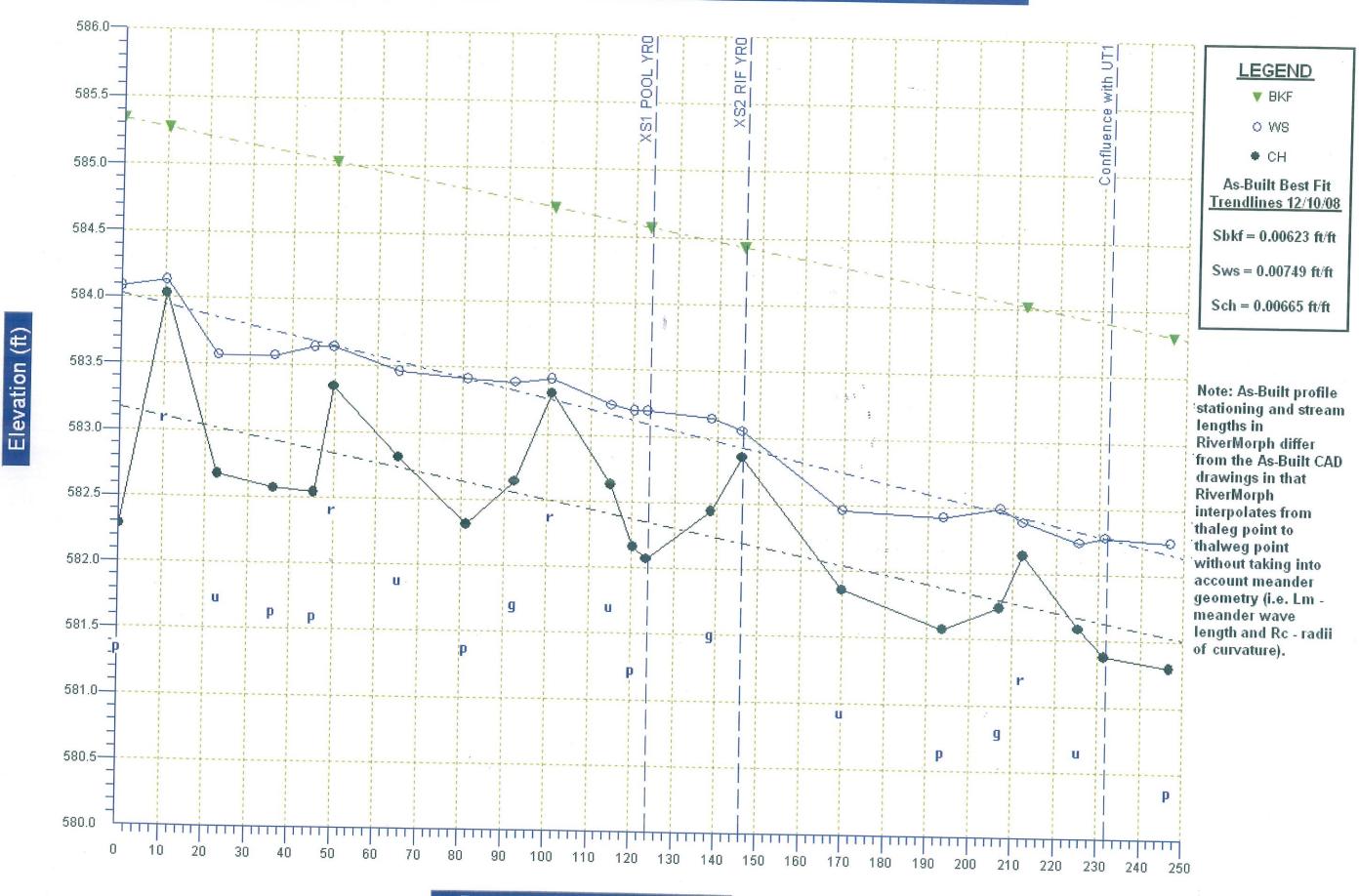
## Beaverdam Creek - Unnamed Tributary 1 As-Built Profile - 12/10/2008



## Beaverdam Creek - Unnamed Tributary 1 As-Built Profile - 12/10/2008



### Beaverdam Creek - UT2 As-Built Profile - 12/10/2008



Distance along stream (ft)

### ECOSYSTEM ENHANCEMENT PROGRAM

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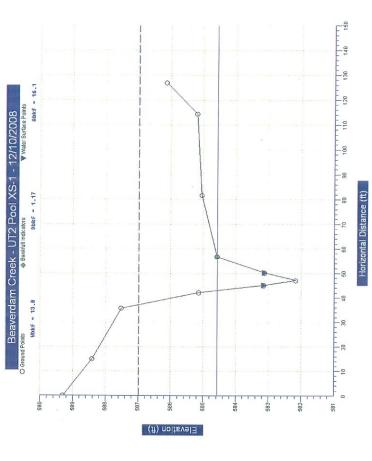
### Appendix C

As-Built Long-Term Monitoring Cross-Section Summary Templates and Particle Distribution Summary Templates

Cummory Data				PROJECT	PROJECT Beaverdam Creek
All dimensions in feet					D06054-C
					0-YEAR
Bankfull Area	$16.15  \mathrm{ft}^2$		TASK	Cross-Section	
Bankfull Width	13.77 ft		REACH	UT2	
Mean Depth	1.17 ft		DATE	12/10/08	
Maximum Depth	2.41 ft	***			
Width/Depth Ratio	11.77		,		
Entrenchment Ratio	6.52		C	SECTION:	_
Classification	E4/1		Honevetein	CEATIDE	
			Emhancement	real ure:	F00I





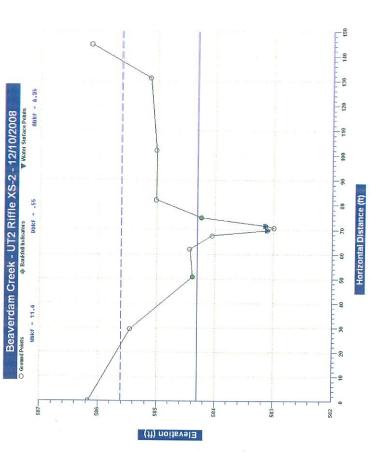




Summary Data				PROJECT	Beaverdam Creek
All dimensions in feet.					D06054-C
					0-YEAR
Bankfull Area	6.35 ft <sup>2</sup>		TASK	Cross-Section	
Bankfull Width	11.55 ft		REACH	UT2	
Mean Depth	0.55 ft		DATE	12/10/08	
Maximum Depth	1.31 ft	*	5	12/10/00	
Width/Depth Ratio	21		,		
Entrenchment Ratio	9.94			CROSS SECTION:	2
Classification	C4/1			SECTIONS	
			Liniancemen	FEATURE:	Riffle





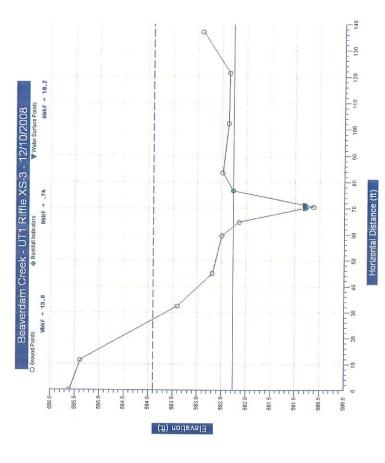




Summary Data				PROJECT	Beaverdam Creek
All dimensions in feet.					D06054-C
					0-YEAR
Bankfull Area	10.19 ft <sup>2</sup>	2	TASK	Cross-Section	
Bankfull Width	13.8 ft		REACH	LTI	
Mean Depth	0.74 ft		DATE	19/10/08	
Maximum Depth	1.64 ft	7		000	
Width/Depth Ratio	18.65	<i>*</i>	,		
Entrenchment Ratio	7.97			CROSS	က
Classification	C4/1		Froeverem	CEOTION.	
			Filliancement	realone:	КІШЕ





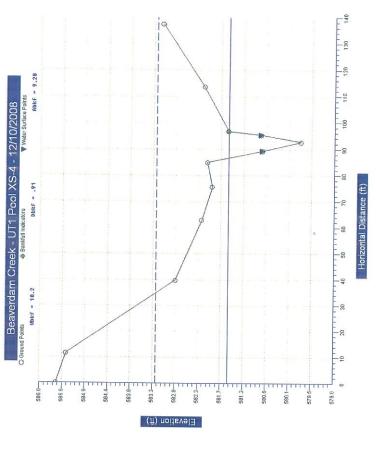




4					PROJECT	Beaverdam Creek	Creek
Summary Data							
All dimensions in feet.						D06054-C	
						0-YEAR	
Bankfull Area	$9.28 \text{ ft}^2$			TASK	Cross-Section		
Bankfull Width	10.22 ft			REACH	E		
Mean Depth	0.91 ft		ير	DATE	20/10/05		
Maximum Depth	1.72 ft			3120	12/10/06		
Width/Depth Ratio	11.23		 ==	,			
Entrenchment Ratio	10.05	æ.		V	CROSS	4	
Classification	E4/1				SECTION.		_
				DESTRUCTION OF THE PROPERTY OF	FEATURE:	Pool	





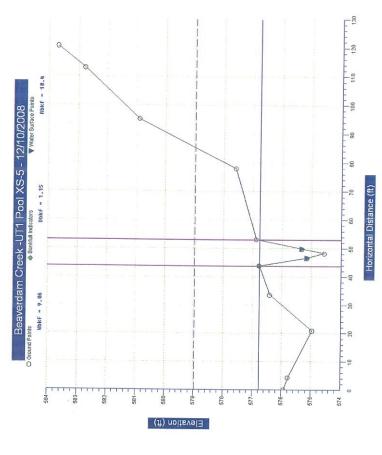




Summary Data				PROJECT	Beaverdam Creek
All dimensions in feet.					D06054-C
					0-YEAR
Bankfull Area	10.44 ft <sup>2</sup>		TASK	Cross-Section	
Bankfull Width	9.06 ft		REACH	Ē	
Mean Depth	1.15 ft		T T V	10/10/10	
Maximum Depth	2.21 ft	**	5	12/10/08	
Width/Depth Ratio	7.88	# .5			
Entrenchment Ratio	9.41			CROSS SECTION:	5
Classification	F4/1		t	SECTION:	-
			Enhancemen	FEATURE:	Pool

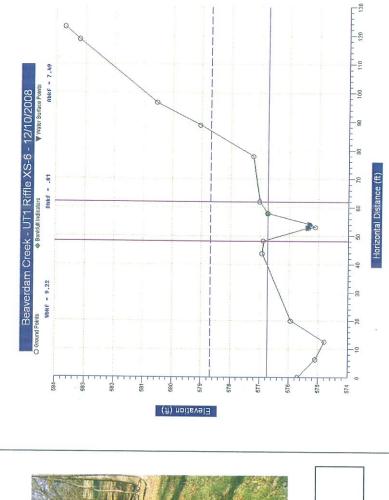








Summary Dafa		· ·				PROJECT	PROJECT Beaverdam Creek	
All dimensions in feet.							D06054-C	
							0-YEAR	
Bankfull Area	7.49 ft <sup>2</sup>				TASK	Cross-Section		
Bankfull Width	9.22 ft				REACH	15		
Mean Depth	0.81 ft			- Ai	DATE	12/10/08		
Maximum Depth	1.95 ft				1	90/01		
Width/Depth Ratio	11.38		×**	::				
Entrenchment Ratio	9.39	æ :			V	CROSS SECTION:	9	
Classification	E4/1					SECTION.		
					Enhancement	FEATURE:	Riffle	





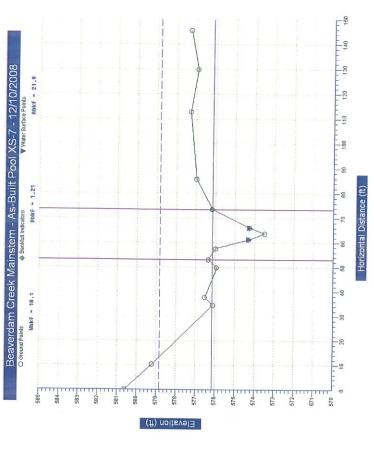




Summary Data				PROJECT	PROJECT Beaverdam Creek	
All dimensions in feet.					D06054-C	
					0-YEAR	
Bankfull Area	21.87 ft <sup>2</sup>		TASK	Cross-Section		
Bankfull Width	18.08 ft		REACH	Mainstem		
Mean Depth	1.21 ft		DATE	15/10/08		
Maximum Depth	2.67 ft	**	2	12/10/08		
Width/Depth Ratio	14.94	**				
Entrenchment Ratio	7.32			CROSS	7	
Classification	C4/1			SECTION:	_	
			Enhancemen	FEATURE:	Pool	





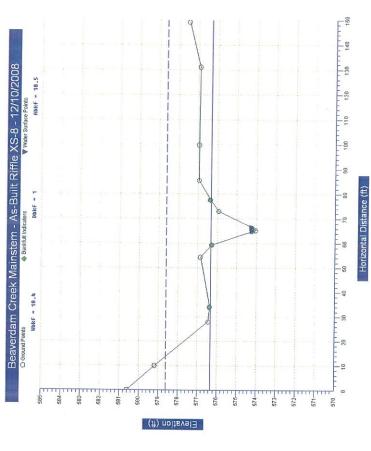




Summary Data				PROJECT	PROJECT Beaverdam Creek
All dimensions in feet.					D06054-C
					0-YEAR
Bankfull Area	18.48 ft <sup>2</sup>	20	TASK	Cross-Section	
Bankfull Width	18.43 ft		REACH	Mainstem	
Mean Depth	1 ft		TAC	19/10/00	
Maximum Depth	2.3 ft			00/00	
Width/Depth Ratio	18.43	;; ;;	,		
Entrenchment Ratio	7.36		V	CROSS	80
Classification	C4/1			SECTION.	
			Fillancement	FEATURE:	Riffle









054-C		1+2										- 3	7 710 0			1										D84=220.56mm
EEP Project No. D06054-C	X Sec	Sta No.			[								0C7 871 u)		uo										1000	
Project		S		Histogram								2	Particle Size (mm)		Particle Size Distribution										100	Particle Size (mm)
	UT2	11/20/2008		Hist								71 0	Particle		rticle Size										10	Particle
Beaverdam Creek Restoration	Ū	11/20											i -		Pa										_	D50= 33.1mm
dam Cre	Reach	ıte										500000	02.0												0.1	
Beaver	Rea	Date	يد ٠٠٠	 	20	16	4 5	<b>Ran</b>	mi %	0 4	7 7	1 6			90	06	80	ou 20	9 9 9	9viti 02 :	slum 3	Cr S	3 =	2 0		
	ve			:																						
	% Cumulative	12	13	13:	13	13	13	13	13	13	13	13	15	18	25	38	50	89	80	06	92	92	92	92	100	
	% in Range	12	2	0	0	0	0	0	0	0	0	0	2	3	7	13	12	18	12	10	2	0	0	0	8	100
Pebble Count - Pool	Count	7	_	0	0	0	0	0	0	0	0	0	1	2	4	8	7	11	7	9		0	0	0	5	09
Pebb	Particle Size (mm)	<0.062	0.062-0.125	0.125-0.25	0.25-0.5	0.5-1.0	1.0-2.0	2.0-4.0	4.0-5.7	5.7-8.0	8.0-11.3	11.3-16.0	16.0-22.6	22.6-32	32-45	45-64	64-90	90-128	128-180	180-256	256-362	362-512	512-1024	1024-2048	<2048	Totals
	Material	Silt/Clay	Very Fine Sand	Fine Sand	Medium Sand	Coarse Sand	Very Coarse Sand	Very Fine Gravel	Fine Gravel	Fine Gravel	Medium Gravel	Medium Gravel	Coarse Gravel	Coarse Gravel	Very Coarse Gravel	Very Coarse Gravel	Small Cobble	Small Cobble	arge Cobble	arge Cobble	Small Boulder	Small Boulder	Medium Boulder	arge Boulder	Bedrock	Tot

1+23.57

128 256 512 2048		1000 10000 D84=220.56mm
8 16 32 64 Particle Size (mm)	Particle Size Distribution	10 100 Particle Size (mm)
0.062 0.25 1 4	100 90 80 70 60 60 40 10 10 10 10 10 10 10 10 10 1	0.1 1 D50=33.1mm
9gneЯ ni % 4 5 5 ∞ 0 4 5 0 0	Cumulative % Fine	

	Pebble	Pebble Count - Riffle	e		Beaver
	Particle Size (mm)	Count	% in Range	% Cumulative	Rea
	<0.062	11	17	17	Dat
Very Fine Sand	0.062-0.125	8	12	29	
	0.125-0.25	·—	2	31.	
Medium Sand	0.25-0.5	0	0	31	18
	0.5-1.0	0	. 0	31	16 -
Very Coarse Sand	1.0-2.0	4	9	37	12 -
Very Fine Gravel	2.0-4.0	0	0	37	ogu O
	4.0-5.7	0	0	37	sЯ n ∞ ^
	5.7-8.0	0	0	37	i %
Medium Gravel	8.0-11.3	3	5	42	2 -
Medium Gravel	11.3-16.0	0	0	42	0
Coarse Gravel	16.0-22.6	3	5	46	0.00
Coarse Gravel	22.6-32	2	3	49	
	32-45	9	6	58	,
	45-64	9	6	89	100
Small Cobble	64-90	9	6	77	80
Small Cobble	90-128	1	2	78	) y
arge Cobble	128-180	2	3	82	піЯ <i>3</i>
arge Cobble	180-256	3	5	86	e evi
Small Boulder	256-362	0	0	86	islua 4
Small Boulder	362-512	0	0	98	
Medium Boulder	512-1024	1	2	88	20
arge Boulder	1024-2048	1	2	89	10
	<2048	7	11	100	
To	Totals	65	100		

Date 11/20/2008	Sta No.	No. 1+46.40
	The second secon	
26 14 14 14 15 16 16 16 16 16 16 16 16 16 16 16 16 16	Histogram	
12 - 32 - 32 - 32 - 32 - 32 - 32 - 32 -		
⊗ ∞ ∞		
ni % 0 4 4 0 0		
0.062 0.25 1 4 8	16 32 64 128 Particle Size (mm)	28 256 512 2048
	Particle Size Distribution	
000		
% ovinellum 02 00 00 00 00 00 00 00 00 00 00 00 00 0		
· (1 -	,	
0.1 1 1 1 D50= 90mm P8	10 100 Particle Size (mm)	1000 10000 D84=210.4mm

	Pebble	Pebble Count - Riffle	9			Beaverdam (
Material	Particle Size (mm)	Count	% in Range	% Cumulative		Reach
Silt/Clay	<0.062	5	7	7		Date
Very Fine Sand	0.062-0.125	0	0	7		- 3
Fine Sand	0.125-0.25	0	0	7 :		
Medium Sand	0.25-0.5	0	, 0	7	::	20
Coarse Sand	0.5-1.0	0	0	7		16
Very Coarse Sand	1.0-2.0	0	0	7		41
Very Fine Gravel	2.0-4.0	0	0	7		10 E
Fine Gravel	4.0-5.7	0	0	7		n Ra
Fine Gravel	5.7-8.0	1	П	6		9 4
Medium Gravel	8.0-11.3	1	1	10		2 -
Medium Gravel	11.3-16.0	1	1	12		0
Coarse Gravel	16.0-22.6	2	3	14		0.062 0.2
Coarse Gravel	22.6-32	9	6	23	_	
Very Coarse Gravel	32-45	6	13	36		
Very Coarse Gravel	45-64	11	16	52		00 06
Small Cobble	64-90	5	7	59		80
Small Cobble	90-128	9	6	89		70
Large Cobble	128-180	12	17	86		1i4 %
Large Cobble	180-256	7	10	96		S svii
Small Boulder	256-362	3	4	100		islum 04
Small Boulder	362-512	0	0	100		Cm 30
Medium Boulder	512-1024	0	0	100		50
Large Boulder	1024-2048	0	0	100		0 0
Bedrock	<2048	0	0	100		0 0
TC	Totals	69	100			Ď

	128 256 512 2048 m)	1000 10000 D84=175.5mm
Histogram	8 16 32 64 128	Particle Size Distribution
	0.062 0.25 1 4	0.1 1 D50= 61.4mm
27	9gnsM m; % 2 4 5 5 5 5 6 5 6 7 6 7 6 7 6 7 6 7 6 7 6 7	Cumulative % Fine 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9

4+90.86

X Sec Sta No.

UT1 11/20/2008

Creek Restoration EEP Project No. D06054-C

Beaver	lative	Dat			# .c.	10		<b>器</b> ut		P % T	2 -	0	00.0			100	- 08			eni's % evi	Fine % Fine	Cumulative % Fine	Cumulative % Fine	Cumulative % Fine	Cumulative % Fine
	% Cumulative	16	32	47	63	63	63	64	65	19	89	71	74	9/	79	83	68	96	96	96 97 97 97 97 97	96 97 97 100 100	96 97 100 100 100 100 1	996 97 100 100 100 100	96 96 97 100 100 100 100	99 97 100 100 100 100 100
	% in Range	16	16	16	16	0	0	-1	1	2	1	2	3	2	κ	. 4	9	9	6 6	6 6 3	6 6 9 3 1 0 0	6 3 3 0	6 0 0 0	9 1 6 6 0 0 0 0 0 0 0	6 3 0 0 0 0
Pebble Count - Pool	Count	15	15	15	15	0	0	1	1	2	1	2		2	3	4	9	9	6 6	6 6 3	6 6 9	6 6 0 0 0 0	6 0 0 0 0	6 0 0 0 0 0 0	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
Pebbl	Particle Size (mm)	<0.062	0.062-0.125	0.125-0.25	0.25-0.5	0.5-1.0	1.0-2.0	2.0-4.0	4.0-5.7	5.7-8.0	8.0-11.3	11.3-16.0	16.0-22.6	. 22.6-32	32-45	45-64	64-90	64-90 90-128	64-90 90-128 128-180	64-90 90-128 128-180 180-256	64-90 90-128 128-180 180-256 256-362	64-90 90-128 128-180 180-256 256-362 362-512	64-90 90-128 128-180 180-256 256-362 362-512 512-1024	64-90 90-128 128-180 180-256 256-362 362-512 512-1024	90-128 128-180 180-256 256-362 362-512 512-1024 1024-2048
	Material	Silt/Clay	Very Fine Sand	Fine Sand	Medium Sand	Coarse Sand	Very Coarse Sand	Very Fine Gravel	Fine Gravel	Fine Gravel	Medium Gravel	Medium Gravel	Coarse Gravel	Coarse Gravel	Very Coarse Gravel	Very Coarse Gravel	Small Cobble	Small Cobble Small Cobble	Small Cobble Small Cobble Large Cobble	Small Cobble Small Cobble Large Cobble Large Cobble	Small Cobble Small Cobble Large Cobble Large Cobble Small Boulder	Small Cobble Small Cobble Large Cobble Large Cobble Small Boulder Small Boulder	Small Cobble  Small Cobble  Large Cobble  Large Cobble  Small Boulder  Small Boulder	Small Cobble  Small Cobble  Large Cobble  Small Boulder  Small Boulder  Medium Boulder	Small Cobble  Small Cobble  Large Cobble  Small Boulder  Small Boulder  Large Boulder  Large Boulder

054-C	4	5+31.80		6 512 2048	0 10000
EEP Project No. D06054-C	X Sec	Sta No.	ram	Particle Size (mm) 256	stribution  100 100 100 2ce (mm) D84=67.5mm
Creek Restoration EEP	UTI	11/20/2008	Histogram	1 4 8 Partice	Particle Size Distribution
Beaverdam Cre	Reach	Date	18	0 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	Cumulative % Fine  0 0 8 5 6 8 5 8 9 0  10 20 30 4 5 5 0 0  10 0 0 0 0 0

erdam Creek Restoration EEP Project No. D06054-C	teach UT1 X Sec 5	Date 11/20/2008 Sta No. 17+31.58	Histogram	0.062 0.25 1 4 8 Pleticle Size (mm)  Particle Size Distribution  Particle Size Distribution	0.1 1 10 100 1000 10000 D50= 21.0mm Particle Size (mm) D84=114.8mm
Beaverdam	Reach	Date	 ×× بدير	Sumative % Fine 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	

054-C		17+(							RESPON				6 512 2													1000 D84=143.6mm
EEP Project No. D06054-C	X Sec	Sta No.		am									Particle Size (mm) 256		ribution										100	
Beaverdam Creek Restoration EEP P	LT7	11/20/2008		Histogram								•	Particle		Particle Size Distribution								\	1		D50= 76.1mm Particle Size (mm)
Beaverdam Cı	Reach	Date	٠٠ , ١	2. v v	25	20	9	38uc	sÆni	% 50		0	0.062 0.23			06	08	) Jo	8 8	os svii	nulad 40	Cm 30	20	01 0	100	
	% Cumulative	5	5	5 :	5	5	5	9	8	6	12	15	18	25	29	40	62	83	98	76	86	100	100	100	100	
	% in Range		0	0	0	0	0	2	2	2	3	3	3	9	5	111	22	22	3	11	2	2	0	0	0	100
Count - Riffle	Count	3	0	0	0	0	0	1	1	1	2	2	2	4	3	7	14	14	2	7	1	1	0	0	0	65
Pebble	Particle Size (mm)	<0.062	0.062-0.125	0.125-0.25	0.25-0.5	0.5-1.0	1.0-2.0	2.0-4.0	4.0-5.7	5.7-8.0	8.0-11.3	11.3-16.0	16.0-22.6	22.6-32	32-45	45-64	64-90	90-128	128-180	180-256	256-362	362-512	512-1024	1024-2048	<2048	Totals
	Material	Silt/Clay	Very Fine Sand	Fine Sand	Medium Sand	Coarse Sand	Very Coarse Sand	Very Fine Gravel	Fine Gravel	Fine Gravel	Medium Gravel	Medium Gravel	Coarse Gravel	Coarse Gravel	Very Coarse Gravel	Very Coarse Gravel	Small Cobble	Small Cobble	Large Cobble	Large Cobble	Small Boulder	Small Boulder	Medium Boulder	Large Boulder	Bedrock	Tc

9	17+62.09		512 2048 512 10000
X Sec	Sta No.	ram	Size Distribution  Size Distribution  Size Distribution  O 100  urticle Size (mm) D84=143.6mm
UTI	11/20/2008	Histogram	25 1 4 8 particle Size (mm)  Particle Size Distribution  Particle Size Distribution  1 10 100  D50=76.1mm Particle Size (mm)
Reach	Date		Cumulative % Fine  Our 2000.0  Our 2000 o 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

7-4-C		1+3											512 2												‡ <sup>-</sup>	, mm
Beaverdam Creek Restoration EEP Project No. D06054-C	X Sec	Sta No.								1000007			m) 28 250		п										10001	1000 D84=64.4mm
Project	X	Ste		gram									Particle Size (mm)		istributio										001	Particle Size (mm)
tion EEP	m Creek	2008		Histogram								-	<sup>o</sup> Particl		Particle Size Distribution										<u> </u>	Particle S
K Restora	Beaverdam Creek	11/20/2008											4		Parl										-	.15mm
am Creel	lh Th	ره										3000	0.002 0.23												<u> </u>	D50= 0.15mm
Beaverd	Reach	Date	يد ٠٠		30	25	20 -	eglji Mge	ध्य पीं	2% 4	0	0	0.00		9	90 - 06	- 08	91 0/	riT % 8	e svii	slum 6		- 20	10	1 -0	i.
	4)		-	:	;									_												_
	% Cumulative	21	45	73 :	73	73	73	73	73	73	73	73	73	79	84	84	94	97	100	100	100	100	100	100	100	
	% in Range	21	24	27	0 ,	0	0	0	0	0	0	0	0	9	5	0	10	3	3	0	0	0	0	0	0	100
Pebble Count - Pool	Count	13	15	17	0	0	0	0	0	0	0	0	0	4	3	0	9	2	2	0	0	0	0	0	0	62
Pebb	Particle Size (mm)	<0.062	0.062-0.125	0.125-0.25	0.25-0.5	0.5-1.0	1.0-2.0	2.0-4.0	4.0-5.7	5.7-8.0	8.0-11.3	11.3-16.0	16.0-22.6	22.6-32	32-45	45-64	64-90	90-128	128-180	180-256	256-362	362-512	512-1024	1024-2048	<2048	Totals
	Material	Silt/Clay	Very Fine Sand	Fine Sand	Medium Sand	Coarse Sand	Very Coarse Sand	Very Fine Gravel	Fine Gravel	Fine Gravel	Medium Gravel	Medium Gravel	Coarse Gravel	Coarse Gravel	Very Coarse Gravel	Very Coarse Gravel	Small Cobble	Small Cobble	Large Cobble	Large Cobble	Small Boulder	Small Boulder	Medium Boulder	Large Boulder	Bedrock	To

	-	n) 256 512 2048	1000 10000 D84=64.4mm
Histogram		Particle Size Distribution	10 100 Particle Size (mm)
30 25 30	<b>政形 時% 心</b> ○	O.002 0.25 1 Page & Fine 20 0.062 0.25 1 Page 20 0.	0.1 1 D50= 0.15mm

1+35.96

06054-C	-	1+4											256 512 2													1000 D84=162.8mm
EEP Project No. D06054-C	X Sec	Sta No.		am									Particle Size $(4 \text{ mm})^{16}$		ibution										+	
Beaverdam Creek Restoration EEP P	Beaverdam Creek	11/20/2008	18.5	Histogram									1 4 8 Particle 3		Particle Size Distribution							\				D50= 40.5mm Particle Size (mm)
Beaverdam C	Reach	Date	27.3	 _i_ **	14	12	10	Fau	Ag mi	7	2 -	0	0.062 0.25			00 06	08	16 70	% Fin 60	Positive O			20	00 (	0 -	
	% Cumulative	∞	6	10 .	13	14	14	16	18	18	23	28	29	42	54	61	70	77	87	94	66	100	100	100	100	
	% in Range	 80	_	П	3	1	0	3	1	0	5	5	1	13	13	9	6	8	10	9	5	1	0	0	0	100
Count - Riffle	Count	9	1	1	2	1	0	2	1	0	4	4	1	10	10	5	7	9	~	5	4	1	0	0	0	79
Pebble	Particle Size (mm)	<0.062	0.062-0.125	0.125-0.25	0.25-0.5	0.5-1.0	1.0-2.0	2.0-4.0	4.0-5.7	5.7-8.0	8.0-11.3	11.3-16.0	16.0-22.6	22.6-32	32-45	45-64	64-90	90-128	128-180	180-256	256-362	362-512	512-1024	1024-2048	<2048	Totals
	Material	Silt/Clay	Very Fine Sand	Fine Sand	Medium Sand	Coarse Sand	Very Coarse Sand	Very Fine Gravel	Fine Gravel	Fine Gravel	Medium Gravel	Medium Gravel	Coarse Gravel	Coarse Gravel	Very Coarse Gravel	Very Coarse Gravel	Small Cobble	Small Cobble	Large Cobble	Large Cobble	Small Boulder	Small Boulder	Medium Boulder	Large Boulder	Bedrock	To

		128 256 512 2048			1000 10000 D84=162.8mm
Histogram		8 Particle Size (mm)	Particle Size Distribution		10 100 Particle Size (mm)
14	Sagne Finity of O	0.062 0.25 1 4	ive % Fine 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Cumulation of the control of the con	0.1 1 D50= 40.5mm

1+44.70

### ECOSYSTEM ENHANCEMENT PROGRAM

Mitigation Plan – Beaverdam Creek and Unnamed Tributaries EEP Contract # D06054-C

Appendix D

**Supporting Documentation** 

Worksheet 5-3. Field form for Level II stream classification (Rosgen, 1996; Rosgen and Silvey, 2005).

Stream:	Beaverdam Creek Mainstem Reach		
Basin:	Lower Yadkin - Pee Dee Drainage Area: 162.24 acres	0.2535	mi <sup>2</sup>
_ocation:	South of Wingate, Union Co., NC (Parker Site)		
Twp.&Rge:	; Sec.&Qtr.: ;		
Cross-Sect	ion Monuments (Lat./Long.): 34.92778 Lat / 80.43639 Long	Date	: 12/10/2008
Observers:	MFH, WEK, JMH	Valley Type	: VIII
	Bankfull WIDTH (W <sub>bkf</sub> )		
	WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	18.43	ft
	Bankfull DEPTH (d <sub>bkf</sub> )		
	Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a	1.00	
	riffle section ( $d_{bkf} = A / W_{bkf}$ ).	1.00	ft
	Bankfull X-Section AREA (A <sub>bkf</sub> )		3
	AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle	18.48	
	section.	10.40	ft <sup>2</sup>
	Width/Depth Ratio (W <sub>bkf</sub> / d <sub>bkf</sub> )		
	Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	18.43	ft/ft
	-		]1011
	Maximum DEPTH (d <sub>mbkf</sub> )  Maximum depth of the bankfull channel cross-section, or distance between the	2.20	
	bankfull stage and Thalweg elevations, in a riffle section.	2.30	ft
	WIDTH of Flood-Prone Area (W <sub>fpa</sub> )		1
	Twice maximum DEPTH, or $(2 \times d_{mbkf})$ = the stage/elevation at which flood-prone area	135.63	
	WIDTH is determined in a riffle section.	100.00	ft
	Entrenchment Ratio (ER)		- 1
	The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa}/W_{bkf}$ )	7.36	
	(riffle section).		ft/ft
	Channel Materials (Particle Size Index ) D <sub>50</sub>		1
	The D <sub>50</sub> particle size index represents the mean diameter of channel materials, as	24.28	
	sampled from the channel surface, between the bankfull stage and Thalweg elevations.	24.20	
			]mm
	Water Surface SLOPE (S)		
	Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient	0.0106	
	at bankfull stage.		ft/ft
	Channel SINUOSITY (k)		1
	Sinuosity is an index of channel pattern, determined from a ratio of stream length		
	divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	1.21	
l			
	Stream C 4/1 (See Figure 2)		]
	Type (See Figure 2-	14)	

Worksheet 5-4. Morphological relations, including dimensionless ratios of river reach sites (Rosgen and Silvey, 2005).

S	tream: Beaverdam	Creek M	ainstem	Reach			ocatio	n: Sout	h of W	ingate, Unio	on Co., NC	(Parke	er Site	<del></del>
C	bservers: MFH, JMH,	WEK			Dat	e: 12/10/2008			у Туре:			n Type:		
					Rive	r Reach Sumr	nary D	ata						W. S.
	Mean Riffle Depth (d <sub>b</sub>	<sub>kf</sub> )	1.00	ft	Riffle Width (W <sub>bkf</sub> )			18.43	ft	Riffle Area (A	۹ <sub>bkf</sub> )	18.48		ft <sup>2</sup>
on	Mean Pool Depth (d <sub>bk</sub>	<sub>tfp</sub> )	1.21	ft	Pool	Width (W <sub>bkfp</sub> )		18.08	ft	Pool Area (A	<sub>bkfp</sub> )	21	.87	ft <sup>2</sup>
Channel Dimension	Mean Pool Depth/Mea	an Riffle	1.21	d <sub>bkfp</sub> / d <sub>bkf</sub>	Pool Width/Riffle V		th	0.98	W <sub>bkfp</sub> / W <sub>bkf</sub>	Pool Area / F	Riffle Area	1.	18	A <sub>bki</sub>
el D	Max Riffle Depth (d <sub>mb</sub>	<sub>kf</sub> )	1.50	ft	Max	Pool Depth (d <sub>mb</sub>	cfp)	2.77	ft	Max Riffle Depth/Mean Riffle De			pth	1.0
ann	Max Pool Depth/Mear	n Riffle Dep	oth	2.77						Point Bar Sk	ope			0
င်	Streamflow: Estimate	d Mean Ve	locity at B	ankfull Sta	ge (u <sub>b</sub>	kf)		1.89	ft/s	Estimation M	lethod		v = Q	
	Streamflow: Estimated	d Discharge	e at Bankf	ull Stage (	Q <sub>bkf</sub> )			34.5	cfs	Drainage Are	ea	0.2	535	mi <sup>2</sup>
	Geometry		Mean	Min	Max		Dir	noncion	loce Cr	eometry Ratio	ta ve geara			
	Meander Length (Lm)		17.00	17.00	28.0		er Leng	gth Rati o	(Lm/W	bkf)	15	Mean 0.92	Min 0.92	Ma
ern	Radius of Curvature (I	Rc)	72.68	59.01	93.8	.85 ft Radius of Curvature/Riffle Width (Rc/W <sub>bkf</sub> )						3.94	3.20	5.0
Pattern	Belt Width (W <sub>blt</sub> )		50.00	50.00	50.0	00 ft Meander Width Ratio (W <sub>blt</sub> /W <sub>bkf</sub> )						2.71	2.71	
Channel	Individual Pool Length	1	28.68	16.87	39.6	39.62 ft Pool Length/Riffle Width						1.56	0.92	
Cha	Pool to Pool Spacing		47.57	29.82	58.3	58.36 ft Pool to Pool Spacing/Riffle Width						2.58	1.62	+
	Riffle Length		17.62	14.71	22.9	1 ft Riffle L	ength/F	Riffle Wid	dth			0.96	0.80	+
	Volley Slene (VS)		450	lam						Constitution	T			
	Valley Slope (VS)		158	ft/ft		age Water Surfa	e Slop	e (S)		106  ft/ft	Sinuosity (	VS/S)		1.4
	Stream Length (SL)		5.49	ft	Valle	y Length (VL)				).35  ft	Sinuosity (	SL/VL)		1.4
	Low Bank Height (LBH)	end	0.88 1.88	ft ft	Max Riffle start 0.88 ft Bank-Height Ratio Depth end 1.88 ft (LBH/Max Riffle D								stan end	
Ф	Facet Slopes Riffle Slope (S <sub>rif</sub> )	Mean 0.0458	Min 0.0319	Max 0.0720	ft/ft	Riffle Slope/A				e Ratios		Mean	Min	Ma
Profile	Run Slope (S <sub>run</sub> )			lessoner.	ft/ft	Run Slope/Ave						4.31	3.00	6.7
le P	Pool Slope (S <sub>p</sub> )	0.0027	0.0005	0.0089										
Channel	Glide Slope (S <sub>g</sub> )	0.0021	0.0003			Pool Slope/Av					Name of the last	0.26	0.05	0.8
ਹ	Feature Midpoint <sup>a</sup>	Mean I	Min	Max	ft/ft	Glide Slope/Av	gardias,			Service Co	NEST SERVICE			
	Riffle Depth (d <sub>rif</sub> )	1.50	0.88	1.88	ft	Riffle Depth/M				h Ratios		Mean 1.50	Min	Ma
	Run Depth (d <sub>run</sub> )		Tajasi.		ft	Run Depth/Me							0.00	1.0
	Pool Depth (d <sub>p</sub> )	2.77	2.16	3.15	ft	Pool Depth/Me						2.77	2.16	2.1
	Glide Depth (d <sub>g</sub> )				ft	Glide Depth/M							0	U.1
	MINE CARACTERS	Rea	ch <sup>b</sup>	Riffi	e	Pow	4, 25 <b>ž</b>		, b	MENINE	1027 12941	0.142	Managa	
	% Silt/Clay	13		7.6		Bar	D <sub>16</sub>	Rea 0.		Riffle <sup>c</sup> 3.6	Bar	Protru		leigh mm
rials	% Sand	26	.2	6.3			D <sub>35</sub>	0.		27.0		C		mm
Channel Materials	% Gravel	31			В		D <sub>50</sub>	24		40.5		0		mm
Jel N	% Cobble	25		32.9			D <sub>84</sub>	118		162.8		0		
han	% Boulder	3.		6.3			D <sub>95</sub>	224		283.9		0		mm
	L	the same of the same of the same of	Little I ame and the	P. William and Co.			- 25	An An	i	200.0	ı i	U		mm

a Min, max, mean depths are the average mid-point values except pools, which are taken at deepest part of pool.

b Composite sample of riffles and pools within the designated reach.

c Active bed of a riffle.

d Height of roughness feature above bed.

## BDC MS Bank Erosion Rate Estimate.txt RIVERMORPH BEHI SUMMARY REPORT

· · · · · · · · · · · · · · · · · · ·
River Name: Beaverdam Creek Reach Name: Beaverdam Mainstem
Table 1. Bank Identification Summary
Bank Name 1 XS-7 Pool BEHI 2 XS-8 Riffle BEHI

Table 2. Predicted Annual Bank Erosion Rates

Bank	BEHI Numeric Rating	BEHI Adjective Rating	NBS Adjective Rating	Length ft cu	Loss yds/yr	Loss tons/yr
1 2	16.4 15.1	Low Low	Very Low Low	332.84 142.65	0.66 0.4	0.86 0.52
Totals	5			475.49	1.06	1.38

Total Reach Ln: 475.49 Total Loss (tons/yr) per ft of Reach: 0.0029

### XS-7 Pool Vert Vel N-B Stress Method.txt RIVERMORPH BANK EROSION HARZARD INDEX (BEHI)

River Name: Beaverdam Creek Reach Name: Beaverdam Mainstem

BEHI Name: XS-7 Pool BEHI Survey Date: 01/16/2009

Bankfull Height: 2.67 ft Bank Height: 2.67 ft Root Depth: 0.75 ft

Root Density: 95 % Bank Angle: 15.12 Degrees Surface Protection: 95 %

Bank Material Adjustment: Silt/Clay 0

Bank Stratification Adjustment: None O

Erosion Loss Curve: Yellowstone

NBS Method #7: Vertical Velocity Near-Bank Shear Stress Method

1b/sq/ft

NB Shear Stress: 0.51 lb/sq/ft Shear Ratio: 0.67

Velocity at Surface: 3.24 fps
Depth: 2.67 ft
Bankfull Slope: 0.01064

Velocity at Bed: 1.87 fps
Hydraulic Radius: 1.15 ft
Shear Stress: 0.76

BEHI Numerical Rating: 16.4 BEHI Adjective Rating: Low NBS Numerical Rating: 0.67 NBS Adjective Rating: Very Low

Total Bank Length: 332.84 ft Estimated Sediment Loss: 0.66 Cu Yds per Year Estimated Sediment Loss: 0.86 Tons per Year

### XS-8 Riffle Vert Vel N-B Stress Method.txt RIVERMORPH BANK EROSION HARZARD INDEX (BEHI)

River Name: Beaverdam Creek Reach Name: Beaverdam Mainstem BEHI Name: XS-8 Riffle BEHI

Survey Date: 01/17/2009

Bankfull Height: 2.3 ft Bank Height: 2.3 ft Root Depth: 0.75 ft

Root Density: 95 % Bank Angle: 10.74 Degrees Surface Protection: 95 %

Bank Material Adjustment: Silt/Clay 0

Bank Stratification Adjustment: None O

Erosion Loss Curve: Yellowstone

NBS Method #7: Vertical Velocity Near-Bank Shear Stress Method

Bankfull Slope: 0.01064

1b/sq/ft

NB Shear Stress: 0.69 lb/sq/ft Shear Ratio: 1.07

Velocity at Surface: 3.24 fps
Depth: 2.3 ft

Velocity at Bed: 1.87 fps
Hydraulic Radius: 0.97 ft

Shear Stress: 0.64

BEHI Numerical Rating: 15.1 BEHI Adjective Rating: Low NBS Numerical Rating: 1.07 NBS Adjective Rating: Low

Total Bank Length: 142.65 ft Estimated Sediment Loss: 0.4 Cu Yds per Year Estimated Sediment Loss: 0.52 Tons per Year

Worksheet 5-3. Field form for Level II stream classification (Rosgen, 1996; Rosgen and Silvey, 2005).

Stream:	Beaverdam Creek, Reach - UT1 (Riffle XS-6)		
Basin:	Yadkin - Pee Dee Drainage Area: 151.74 acres	0.2371	mi <sup>2</sup>
_ocation:	South of Wingate, Union Co., NC (Parker Site)	7	
Twp.&Rge:	Sec.&Qtr.:;		
Cross-Sect	ion Monuments (Lat./Long.): 34.92778 Lat / 80.43639 Long	Date	: 12/10/200
Observers:	MFH, WEK, JMH	Valley Type	: VIII
	Bankfull WIDTH (W <sub>bkf</sub> )		5
	WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	9.22	ft
	Bankfull DEPTH $(d_{bkf})$ Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a riffle section $(d_{bkf} = A / W_{bkf})$ .	0.81	ft
	Bankfull X-Section AREA (A <sub>bkf</sub> )		
	AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle section.	7.49	ft <sup>2</sup>
	Width/Depth Ratio (W <sub>bkf</sub> / d <sub>bkf</sub> )  Bankfull WIDTH divided by bankfull mean DEPTH, in a riffle section.	11.38	ft/ft
	Maximum DEPTH (d <sub>mbkf</sub> )  Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	1.95	ft
	WIDTH of Flood-Prone Area ( $W_{fpa}$ ) Twice maximum DEPTH, or (2 x d <sub>mbkf</sub> ) = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	86.55	ft
	Entrenchment Ratio (ER)		1
2 ×	The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{\rm fpa}$ / $W_{\rm bkf}$ ) (riffle section).	9.39	ft/ft
	Channel Materials (Particle Size Index ) $D_{50}$ The $D_{50}$ particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg elevations.	36.1	mm
	Water Surface SLOPE (S)  Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel widths in length, with the "riffle-to-riffle" water surface slope representing the gradient at bankfull stage.	0.0042	ft/ft
	Channel SINUOSITY (k) Sinuosity is an index of channel pattern, determined from a ratio of stream length divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).	1.49	
	Stream Type  E 4/1  (See Figure 2-	14)	

Worksheet 5-4. Morphological relations, including dimensionless ratios of river reach sites (Rosgen and Silvey, 2005).

5	Stream: <b>Beaverdan</b>	n Creek, I	Reach -	UT1 (Riff						ingate, Union Co.,			e)
C	Observers: MFH, WEK	, JMH			Dat	e: 12/10/2008			у Туре		tream Type		
					Rive	er Reach Sum	mary E	ata		Arran Carlo		100	
	Mean Riffle Depth (d	okf)	0.81	ft	Riffle	e Width (W <sub>bkf</sub> )		9.22	ft	Riffle Area (A <sub>bkf</sub> )		7.49	ft <sup>2</sup>
on	Mean Pool Depth (d <sub>bl</sub>	<sub>cfp</sub> )	1.03	ft	Pool	Width (W <sub>bkfp</sub> )		9.64	ft	Pool Area (A <sub>bkfp</sub> )		9.86	ft <sup>2</sup>
Channel Dimension	Mean Pool Depth/Me Depth	an Riffle	1.27	d <sub>bkfp</sub> / d <sub>bkf</sub>	Pool	Width/Riffle Wid	dth	1.05	W <sub>bkfp</sub> /	Pool Area / Riffle Are	ea	1.32	A <sub>bkfp</sub>
el Di	Max Riffle Depth (d <sub>mb</sub>	Max Riffle Depth (d <sub>mbkf</sub> ) 1.46			Max	Pool Depth (d <sub>mb</sub>	okfp)	2.51	ft	Max Riffle Depth/Me	an Riffle D	epth	1.8
ann	Max Pool Depth/Mear	n Riffle De	pth	3.10						Point Bar Slope		l mai	N/A
ပ်	Streamflow: Estimated Mean Velocity at Bankfull Sta				age (u	bkf)		4.3	ft/s	Estimation Method		V = Q	
	Streamflow: Estimate	d Discharg	ge at Banl	rfull Stage	(Q <sub>bkf</sub> )			32.2	cfs	Drainage Area	0.	2371	mi <sup>2</sup>
	Geometry		Mean	Min	Max		Din	nension	loce Go	ometry Ratios			
	Meander Length (Lm)		75.00	63.29	93.8	UP I		th Ratio			Mear 8.13	and the same of the same	Ma 10.1
ern	Radius of Curvature (	Rc)	20.00	17.00	25.0	0 ft Radius	s of Cur	vature/R	iffle Wid	dth (Rc/W <sub>bkf</sub> )	2.17	1.84	2.7
Channel Pattern	Belt Width (W <sub>blt</sub> )		50.00	50.00	50.0	0.00 ft Meander Width Ratio (W <sub>blf</sub> /W <sub>bkf</sub> )					5.42	5.42	5.4
nnel	Individual Pool Length	1	36.89	22.96	57.8	57.82 ft Pool Length/Riffle Width				4.00		6.2	
Chal	Pool to Pool Spacing		50.30	18.07	79.7	79.78 ft Pool to Pool Spacing/Riffle Width				5.46		8.6	
	Riffle Length		15.54	7.60	30.1	30.18 ft Riffle Length/Riffle Width				1.69	+	3.2	
	Valley Slope (VS)		061	ft/ft	LAvor	age Water Surfa	oo Clou	- (0)		040			
	Stream Length (SL)		ft			ce Siop	e (S)			sity (VS/S)		1.4	
	Low Bank Height (LBH)	start	1.02	fft fft	T valle					Bank-Height Ration (LBH/Max Riffle		star	1.4
	Facet Slopes	Mean	Min	Max			1000000			e Ratios	Mear		1 1.0 Ma
file	Riffle Slope (S <sub>rif</sub> )	0.0247	0.0088	0.0702	ft/ft	Riffle Slope/A					5.84		16.5
Profile	Run Slope (S <sub>run</sub> )				ft/ft	Run Slope/Ave	erage V	ater Sur	face SI	ope (S <sub>run</sub> / S)			
Channel	Pool Slope (S <sub>p</sub> )	0.0009	0.0000	0.0023	ft/ft	Pool Slope/Av	erage V	/ater Su	rface SI	ope (S <sub>p</sub> /S)	0.22	0.00	0.5
Chai	Glide Slope (S <sub>g</sub> )				ft/ft	Glide Slope/A	verage \	Vater Su	ırface S	Slope (S <sub>g</sub> / S)			
_	Feature Midpoint <sup>a</sup>	Mean	Min	Max			Dime	nsionles	s Dept	h Ratios	Mean	Min	Ma
	Riffle Depth (d <sub>rif</sub> )	1.46	1.02	1.84	ft	Riffle Depth/M	ean Riff	le Depth	(d <sub>rif</sub> / d <sub>l</sub>	okf)	1.80	1.26	2.2
	Run Depth (d <sub>run</sub> )				ft	Run Depth/Me	an Riffle	e Depth (	(d <sub>run</sub> / d <sub>t</sub>	okf)			
	Pool Depth (d <sub>p</sub> )	2.51	2.02	3.28	ft	Pool Depth/Me	ean Riffl	e Depth	(d <sub>p</sub> / d <sub>bk</sub>	f)	3.10	2.49	4.0
	Glide Depth (d <sub>g</sub> )				ft	Glide Depth/M	ean Riff	le Depth	(d <sub>g</sub> / d <sub>b</sub>	kf)			
		Rea	ch <sup>b</sup>	Riffl	e <sup>c</sup>	Bar		Rea	ch <sup>b</sup>	Riffle <sup>c</sup> Bar	Protr	usion H	leigh
(0)	% Silt/Clay	13.	01	4.6	2		D <sub>16</sub>	0.	-	17.33		0	mm
Materials	% Sand	15.	41	0			D <sub>35</sub>	10.	14	55.18		0	mm
Mate	% Gravel	34.	59	35.3	8		D <sub>50</sub>	36	1	76.07		0	mm
nel	% Cobble	35.	28	56.9	2 -		D <sub>84</sub>	125	.95	143.58		0	mm
Channel	% Boulder	1.7	71	3.0	В		D <sub>95</sub>	217	.59	242.45		0	mm
٦	% Bedrock	0		0			D <sub>100</sub>	511.	96	511.99		)	mm

a Min, max, mean depths are the average mid-point values except pools, which are taken at deepest part of pool.

b Composite sample of riffles and pools within the designated reach.

c Active bed of a riffle.

d Height of roughness feature above bed.

### UT1 A-B Erosion Rate Estimate.txt RIVERMORPH BEHI SUMMARY REPORT

River Name: Beaverdam Creek Reach Name: UT1

Table 1. Bank Identification Summary

Bank	Name
1	XS3 Riffle BEHI
2	XS4 Pool BEHI
3	XS5 Pool BEHI
4	XS6 Riffle BEHI

Table 2. Predicted Annual Bank Erosion Rates

Bank	BEHI Numeric Rating	BEHI Adjective Rating	NBS Adjed Ratir		Length ft	Loss cu yds/yr	Loss tons/yr
1 2 3 4	13.1 13.8 15.7 12.9	Low Low Low	Very Very Very	Low Low Low	351.77 820.79 820.79 351.77	0.43 1.05 1.34 0.43	1.37
Totals	5				2345.12	3.25	4.23

\_\_\_\_\_\_

Total Reach Ln: 2345.11 Total Loss (tons/yr) per ft of Reach: 0.0018

# XS3 Riffle BEHI.txt RIVERMORPH BANK EROSION HARZARD INDEX (BEHI)

River Name: Beaverdam Creek Reach Name: UT1 BEHI Name: XS3 Riffle BEHI Survey Date: 01/17/2009 Bankfull Height: 1.64 ft Bank Height: 1.64 ft Root Depth: 0.75 ft Root Density: 95 % Bank Angle: 15.12 Degrees Surface Protection: 95 % Bank Material Adjustment: Silt/Clay 0 Bank Stratification Adjustment: None 0 Erosion Loss Curve: Yellowstone NBS Method #1: Channel Pattern and/or Depositional Features for Adjustments in Near-Bank Stress Rating: Very Low BEHI Numerical Rating: 13.1 BEHI Adjective Rating: Low NBS Numerical Rating: NBS Adjective Rating: Very Low Total Bank Length: 351.77 ft Estimated Sediment Loss: 0.43 Cu Yds per Year Estimated Sediment Loss: 0.56 Tons per Year

### XS4 POOl BEHI.txt RIVERMORPH BANK EROSION HARZARD INDEX (BEHI)

River Name: Beaverdam Creek Reach Name: UT1 BEHI Name: XS4 Pool BEHI Survey Date: 01/17/2009 Bankfull Height: 1.72 ft Bank Height: 1.72 ft
Root Depth: 0.75 ft
Root Density: 95 %
Bank Angle: 22.86 Degrees Surface Protection: 95 % Bank Material Adjustment: Silt/Clay 0 Bank Stratification Adjustment: None 0 Erosion Loss Curve: Yellowstone NBS Method #1: Channel Pattern and/or Depositional Features for Adjustments in Near-Bank Stress Rating: Very Low BEHI Numerical Rating: 13.8 BEHI Adjective Rating: Low NBS Numerical Rating: NBS Adjective Rating: Very Low Total Bank Length: 820.79 ft Estimated Sediment Loss: 1.05 Cu Yds per Year Estimated Sediment Loss: 1.37 Tons per Year

### XS5 Pool BEHI.txt RIVERMORPH BANK EROSION HARZARD INDEX (BEHI)

\_\_\_\_\_\_ River Name: Beaverdam Creek Reach Name: UT1 BEHI Name: XS5 Pool BEHI Survey Date: 01/17/2009 Bankfull Height: 2.21 ft Bank Height: 2.21 ft Root Depth: 0.75 ft Root Density: 95 % Bank Angle: 26.51 Degrees Surface Protection: 95 % Bank Material Adjustment: Silt/Clay 0 Bank Stratification Adjustment: None O Erosion Loss Curve: Yellowstone NBS Method #1: Channel Pattern and/or Depositional Features for Adjustments in Near-Bank Stress Rating: Very Low BEHI Numerical Rating: 15.7 BEHI Adjective Rating: Low NBS Numerical Rating: NBS Adjective Rating: Very Low Total Bank Length: 820.79 ft Estimated Sediment Loss: 1.34 Cu Yds per Year Estimated Sediment Loss: 1.74 Tons per Year

# XS6 Riffle BEHI.txt RIVERMORPH BANK EROSION HARZARD INDEX (BEHI)

River Name: Beaverdam Creek Reach Name: UT1 BEHI Name: XS6 Riffle BEHI Survey Date: 01/17/2009 Bankfull Height: 1.95 ft Bank Height: 1.65 ft Root Depth: 0.75 ft Root Density: 95 % Bank Angle: 22.11 Degrees Surface Protection: 95 % Bank Material Adjustment: Silt/Clay 0 Bank Stratification Adjustment: None O Erosion Loss Curve: Yellowstone NBS Method #1: Channel Pattern and/or Depositional Features for Adjustments in Near-Bank Stress Rating: Very Low BEHI Numerical Rating: 12.9 BEHI Adjective Rating: Low NBS Numerical Rating: NBS Adjective Rating: Very Low Total Bank Length: 351.77 ft Estimated Sediment Loss: 0.43 Cu Yds per Year Estimated Sediment Loss: 0.56 Tons per Year

Worksheet 5-3. Field form for Level II stream classification (Rosgen, 1996; Rosgen and Silvey, 2005).

Stream:	Beaverdam Creek, Reach - UT2		.2
Basin:	Yadkin - Pee Dee Drainage Area: 48.96 acres	0.0765	mi <sup>2</sup>
_ocation:	Beaverdam Creek (Parker Site)		
Fwp.&Rge:			
Cross-Sect	tion Monuments (Lat./Long.): 34.92778 Lat / 80.43639 Long	Date	: 12/10/08
Observers:	: MFH, WEK, JMH	Valley Type	: VIII
	Bankfull WIDTH (W <sub>bkf</sub> )		
	WIDTH of the stream channel at bankfull stage elevation, in a riffle section.	11.55	ft
	Bankfull DEPTH (d <sub>bkf</sub> )		_ 
	Mean DEPTH of the stream channel cross-section, at bankfull stage elevation, in a		+
	riffle section (d <sub>bkf</sub> = A / W <sub>bkf</sub> ).	0.55	ft
	Bankfull X-Section AREA (A <sub>bkf</sub> )		38
	AREA of the stream channel cross-section, at bankfull stage elevation, in a riffle		
	section.	6.35	ft <sup>2</sup>
	Windshift on the Desir Call of the		
	Width/Depth Ratio (W <sub>bkf</sub> / d <sub>bkf</sub> )  Bankfull_WIDTH divided by bankfull mean DEPTH, in a riffle section.	04	6.75
	- A*	21	_ft/ft
	Maximum DEPTH (d <sub>mbkf</sub> )		
	Maximum depth of the bankfull channel cross-section, or distance between the bankfull stage and Thalweg elevations, in a riffle section.	4.04	
	g to taste, in a time escaeti.	1.31	_lft
	WIDTH of Flood-Prone Area (W <sub>fpa</sub> )		
	Twice maximum DEPTH, or $(2 \times d_{mbkf})$ = the stage/elevation at which flood-prone area WIDTH is determined in a riffle section.	444.70	
	THE THE ESCHAMOS HE SHIP SECONDIN	114.79	_ft
	Entrenchment Ratio (ER)		
	The ratio of flood-prone area WIDTH divided by bankfull channel WIDTH ( $W_{fpa}/W_{bkf}$ ) (riffle section).	0.04	
	(viiiio cocusii).	9.94	_ft/ft
	Channel Materials (Particle Size Index ) D <sub>50</sub>		
	The D <sub>50</sub> particle size index represents the mean diameter of channel materials, as sampled from the channel surface, between the bankfull stage and Thalweg		
	elevations.	57.89	mm
	Western Street Cl. ODE (O)		J
	Water Surface SLOPE (S) Channel slope = "rise over run" for a reach approximately 20–30 bankfull channel		
	widths in length, with the "riffle-to-riffle" water surface slope representing the gradient		0
	at bankfull stage.	0.00623	ft/ft
	Channel SINUOSITY (k)		_ 7
	Sinuosity is an index of channel pattern, determined from a ratio of stream length		
	divided by valley length (SL / VL); or estimated from a ratio of valley slope divided by channel slope (VS / S).		
	Silanii Silapo (VO / O).	1.45	
	Stream C 4/1		7
	Type C 4/1 (See Figure 2-7	14)	

Worksheet 5-4. Morphological relations, including dimensionless ratios of river reach sites (Rosgen and Silvey, 2005).

	Stream: Beaverdam		Reach - l	JT2		Loc	cation:	Sout	h of W	ingate, Unic	n Co., NC	(Parke	r Site	•)
C	bservers: MFH, JMH,	WEK			Date	: 12/10/2008		Valle	у Туре	VIII	Stream	n Type:	C 4/	1
					Rive	r Reach Summa	ry Da	ıta						
	Mean Riffle Depth (d		0.55	ft	Riffle	Width (W <sub>bkf</sub> )	11	.55	ft	Riffle Area (A	A <sub>bkf</sub> )	6.	35	ft <sup>2</sup>
on	Mean Pool Depth (d <sub>bk</sub>	<sub>cfp</sub> )	1.17	ft	Pool \	Width (W <sub>bkfp</sub> )	13	.77	ft	Pool Area (A	<sub>bkfp</sub> )	16	.15	ft <sup>2</sup>
Channel Dimension	Mean Pool Depth/Mea Depth	an Riffle	2.13	d <sub>bkfp</sub> / d <sub>bk</sub>	Pool \	Width/Riffle Width		1.19	W <sub>bkfp</sub> /	Pool Area / F	Riffle Area	a 2.54		A <sub>bkf</sub>
	Max Riffle Depth (d <sub>mbkf</sub> ) 1.56 ft			ft	Max F	Pool Depth (d <sub>mbkfp</sub> )		2.53	ft	Max Riffle D	epth/Mean F	Riffle De	pth	2.8
ann	Max Pool Depth/Mean Riffle Depth 4.6			4.60			AVA NO			Point Bar Slo	ре			0
ပ	Streamflow: Estimated	d Mean Ve	locity at B	ankfull St	age (u <sub>b</sub>	kf)	2.	54	ft/s	Estimation M	lethod		/ = Q/	
	Streamflow: Estimated	d Discharg	e at Bank	full Stage	(Q <sub>bkf</sub> )		10	).4	cfs	Drainage Are			765	lmi <sup>2</sup>
	Geometry		Moon	OF SYNTA							(1-10-41) 7 (1-4)			CONT. US
	Meander Length (Lm)		Mean 58.92	Min 58.08	Max 59.76	ft Meander	Length	nsion Ratio	less Ge (Lm/W	ometry Ratio	S	Mean 5.10	Min 5.03	Ma
L	Radius of Curvature (	Rc)	14.50	12.50	16.00					dth (Rc/W <sub>bkf</sub> )				
Pattern	Belt Width (W <sub>blt</sub> )	-/	50.00		50.00							1.26	1.08	+
nel P	Individual Pool Length	1	30.09		40.97	-				okf)		4.33	4.33	
Channel	Pool to Pool Spacing		49.34			40.97 ft Pool Length/Riffle Width  70.04 ft Pool to Pool Spacing/Riffle Width						2.61	2.05	
O	Riffle Length		15.74	1	1	23.86 ft Riffle Length/Riffle Width					4.27	3.08	+	
	J. Tamio Longar		13.74	12.41	23.00	ili kille ter	guvku	me vvid	um			1.36	1.07	2.0
	Valley Slope (VS)	0.0	093	ft/ft	Avera	ge Water Surface	Slope	(S)	0.0	062 ft/ft	Sinuosity (	VS/S)		1.4
	Stream Length (SL) 284.31 ft				Valley	Length (VL)			190	). <b>71</b> ft	Sinuosity (	SL/VL)		1.4
	Low Bank Height (LBH)	`start , end	!	ft		Max Riffle Depth		1.24			ght Ratio (Bl x Riffle Dep	HR)		1.0
	Facet Slopes	Mean	Min	Max			Dimen	sionle	ss Slop	e Ratios		Mean	Min	Ma
file	Riffle Slope (S <sub>rif</sub> )	0.0213	0.0115	0.0451	ft/ft	Riffle Slope/Aver	age W	ater Si	urface S	Slope (S <sub>rif</sub> / S)		3.42	1.84	7.2
Channel Profile	Run Slope (S <sub>run</sub> )				ft/ft	Run Slope/Avera	ge Wa	iter Su	face SI	ope (S <sub>run</sub> / S)				
nel	Pool Slope (S <sub>p</sub> )	0.0020	0.0007	0.0038	ft/ft	Pool Slope/Avera	ige Wa	ater Su	rface S	lope (S <sub>p</sub> / S)		0.32	0.12	0.6
Shar	Glide Slope (S <sub>g</sub> )				ft/ft	Glide Slope/Aver	age W	ater Si	urface S	Slope (S <sub>a</sub> / S)		- 144		
٥	Feature Midpoint <sup>a</sup>	Mean	Min	Max		A SULED AND STREET	10.5	1011		th Ratios		Mean	Min	Ma
	Riffle Depth (d <sub>rif</sub> )	1.56	1.24	1.87	ft	Riffle Depth/Mea						2.84		-
	Run Depth (d <sub>run</sub> )				ft	Run Depth/Mean	Riffle	Depth	(d <sub>run</sub> / d <sub>l</sub>	okf)				
	Pool Depth (d <sub>p</sub> )	2.53	2.50	2.56	ft	Pool Depth/Mean	Riffle	Depth	(d <sub>p</sub> / d <sub>bl</sub>	·f)		4.60	4.55	4.6
	Glide Depth (d <sub>g</sub> )				ft	Glide Depth/Mea	n Riffle	Depth	d <sub>g</sub> / d <sub>t</sub>	<sub>skf</sub> )		etterge an Atomica of		
		Rea	ch <sup>b</sup>	Riffi	e <sup>c</sup>	Bar		Rea	ch <sup>b</sup>	Riffle	Bar	Protru	cion l	loiel
	% Silt/Clay	14		11.			D <sub>16</sub>	0.		25.4	_u,	C		mm
riais	% Sand	11	.2	1.7	7		D <sub>35</sub>	33	.0	59.3		C		mm
Materials	% Gravel	28	.0	25.	0		D <sub>50</sub>	57	.9	90.0		O		mm
nel	% Cobble	34	.4	51.	7 -		D <sub>84</sub>	213		210.4		O		mm
Channel	% Boulder	2.	4	1.7	7		D <sub>95</sub>	20		2048		0		mm
٥	% Bedrock	9.	6	8.3	}		D <sub>100</sub>	20		2048		0		mm

a Min, max, mean depths are the average mid-point values except pools, which are taken at deepest part of pool.

b Composite sample of riffles and pools within the designated reach.

c Active bed of a riffle.

d Height of roughness feature above bed.

#### UT2 A-B Bank Erosion Rate Estimate.txt RIVERMORPH BEHI SUMMARY REPORT

River Name: Beaverdam Creek Reach Name: UT2 Table 1. Bank Identification Summary

Bank

Name

XS1 Pool BEHI 1 XS2 Riffle BEHI

Table 2. Predicted Annual Bank Erosion Rates

Bank			NBS Adjective Rating	Length ft cu	Loss yds/yr	Loss tons/yr
1 2	16.1 9.6	Low Very Low	Very Low Very Low	199.02 85.29	0.36	0.47
Totals	5			284.31	0.36	0.47

Total Reach Ln: 284.31 Total Loss (tons/yr) per ft of Reach: 0.0017

# XS2 Riffle BEHI.txt RIVERMORPH BANK EROSION HARZARD INDEX (BEHI)

River Name: Beaverdam Creek Reach Name: UT2 BEHI Name: XS2 Riffle BEHI Survey Date: 01/17/2009 Bankfull Height: 1.31 ft Bank Height: 1.06 ft Root Depth: 0.75 ft Root Density: 95 % Bank Angle: 18.38 Degrees Surface Protection: 95 % Bank Material Adjustment: Silt/Clay 0 Bank Stratification Adjustment: None 0 Erosion Loss, Curve: Yellowstone NBS Method #1: Channel Pattern and/or Depositional Features for Adjustments in Near-Bank Stress Rating: Very Low BEHI Numerical Rating: 9.6 BEHI Adjective Rating: Very Low NBS Numerical Rating: NBS Adjective Rating: Very Low Total Bank Length: 85.29 ft Estimated Sediment Loss: O Cu Yds per Year Estimated Sediment Loss: O Tons per Year

### XS1 POOl BEHI.txt RIVERMORPH BANK EROSION HARZARD INDEX (BEHI)

River Name: Beaverdam Creek Reach Name: UT2 BEHI Name: XS1 Pool BEHI Survey Date: 01/17/2009 Bankfull Height: 2.41 ft Bank Height: 2.41 ft Root Depth: 0.75 ft Root Density: 95 % Bank Angle: 25 Degrees Surface Protection: 95 % Bank Material Adjustment: Silt/Clay 0 Bank Stratification Adjustment: None 0 Erosion Loss: Curve: Yellowstone NBS Method #1: Channel Pattern and/or Depositional Features for Adjustments in Near-Bank Stress Rating: Very Low BEHI Numerical Rating: 16.1 BEHI Adjective Rating: Low NBS Numerical Rating: NBS Adjective Rating: Very Low Total Bank Length: 199.02 ft Estimated Sediment Loss: 0.36 Cu Yds per Year Estimated Sediment Loss: 0.47 Tons per Year

# Beaverdam Creek & Tributaries RiverMorph® Version 4.3.0

As-Built Monumented Cross-Section Summary Reports

**December 10, 2008** 

# XS1 Pool Yr0.txt RIVERMORPH CROSS SECTION SUMMARY

River Name: Beaverere UT2 Cross Section Name: XS1 POC Survey Date: 12/10/2	OL YRO		
Cross Section Data Entry			
BM Elevation: Backsight Rod Reading:	0 ft 0 ft		
TAPE FS	ELEV		NOTE
0 0 15.02 0 35.67 0 42.1 0 45.05 0 47.15 0 50.16 0 56.7 0 81.69 0 114.43 0	589.29 588.4 587.51 585.13 583.14 582.16 583.11 584.57 585.04 585.19 586.13		MON.2 GND LB  LEW TW 0.95 P REW BKF RB GND GND MON.1
Cross Sectional Geometry			
Floodprone Elevation (ft) Bankfull Elevation (ft) Floodprone Width (ft) Bankfull Width (ft) Entrenchment Ratio Mean Depth (ft) Maximum Depth (ft) Width/Depth Ratio Bankfull Area (sq ft) Wetted Perimeter (ft) Hydraulic Radius (ft) Begin BKF Station	Channel 586.98 584.57 89.76 13.77 6.52 1.17 2.41 11.77 16.15 14.73 1.1 42.93 56.7	Left 586.98 584.57 6.89 1.58 2.41 4.36 10.86 9.24 1.17 42.93 49.82	Right 586.98 584.57 6.88 0.77 1.57 8.94 5.29 8.62 0.61 49.82 56.7

XS	1 Pool Yr0.	txt	
Entrainment Calculations			
Entrainment Formula: Rosge	en Modified	Shields Cur	ve
Slope Shear Stress (lb/sq ft) Movable Particle (mm)	Channel 0.00665 0.46 85.4	Left Side O	Right Side O

### XS2 Riffle YRO.txt RIVERMORPH CROSS SECTION SUMMARY

River Name: Beaver Reach Name: UT2 Cross Section Name: XS2 RI Survey Date: 12/10/				
Cross Section Data Entry				
BM Elevation: Backsight Rod Reading:	0 ft 0 ft			
TAPE FS	ELEV		NOTE	
0 0 29.49 0 50.87 0 62.12 0 67.58 0 69.8 0 70.77 0 71.56 0 74.9 0 82.01 0 101.99 0 131.14 0	586.16 585.45 584.38 584.05 583.1 582.99 583.13 584.23 585.01 585.01 585.12 586.13		MON.4 GND BKF MON. 3 LB LEW TW 0.10 R REW BKF MON.2 GND GND MON.1	
Cross Sectional Geometry				
Floodprone Elevation (ft) Bankfull Elevation (ft) Floodprone Width (ft) Bankfull Width (ft) Entrenchment Ratio Mean Depth (ft) Maximum Depth (ft) Width/Depth Ratio Bankfull Area (sq ft) Wetted Perimeter (ft) Hydraulic Radius (ft) Begin BKF Station	Channel 585.61 584.3 114.79 11.55 9.94 0.55 1.31 21 6.35 11.95 0.53 63.99 Page 1	Left 585.61 584.3 5.95 0.37 1.22 16.08 2.23 7.37 0.3 63.99	Right 585.61 584.3 5.6 0.74 1.31 7.57 4.12 7.01 0.59 69.94	

End BKF Station

XS2 Riffle YR0.txt
75.54

----69.94

75.54

----Entrainment Calculations
----Entrainment Formula: Rosgen Modified Shields Curve

Channel Left Side Right Side
0.00665
0 0.00665
0 0.22
Movable Particle (mm)

AND ADDRESS ADDRE

## XS3 Riffle.txt RIVERMORPH CROSS SECTION SUMMARY

River Name: Beaver Reach Name: UT1 Cross Section Name: XS3 RI Survey Date: 12/10/	F YRO		
Cross Section Data Entry			
BM Elevation: Backsight Rod Reading:	0 ft 0 ft		
TAPE FS	ELEV		NOTE
0 0 11.57 0 32.39 0 45.06 0 59.52 0 64.72 0 70.2 0 70.67 0 71.28 0 76.74 0 83.54 0 102.35 0 121.52 0 137.08 0	585.6 585.38 583.39 582.68 582.49 582.14 580.78 580.62 580.79 582.26 582.48 582.36 582.34		MON.1 GND GND MON.2 LB LEW TW 0.15 R REW BKF MON.3 GND FP MON.4
Cross Sectional Geometry			
Floodprone Elevation (ft) Bankfull Elevation (ft) Floodprone Width (ft) Bankfull Width (ft) Entrenchment Ratio Mean Depth (ft) Maximum Depth (ft) Width/Depth Ratio Bankfull Area (sq ft) Wetted Perimeter (ft) Hydraulic Radius (ft)	Channel 583.9 582.26 110.03 13.8 7.97 0.74 1.64 18.65 10.19 14.22 0.72 Page 1	Left 583.9 582.26  6.9  0.58 1.39 11.9 3.97 8.45 0.47	Right 583.9 582.26 6.9 0.9 1.64 7.67 6.21 8.55 0.73

Begin BKF Station End BKF Station	(S3 Riftle.t 62.94 76.74	62.94 69.84	69.84 76.74		
Entrainment Calculations					
Entrainment Formula: Rosgen Modified Shields Curve					
Slope Shear Stress (lb/sq ft) Movable Particle (mm)	Channel 0.00423 0.19 44.8	Left Side O	Right Side O		

### XS4 Pool.txt RIVERMORPH CROSS SECTION SUMMARY

River Name: Beaver Reach Name: UT1 Cross Section Name: XS4 PC Survey Date: 12/10/	OOL YRO		
Cross Section Data Entry			
BM Elevation:	0 ft		
Backsight Rod Reading:	0 ft		
TAPE FS	ELEV		NOTE
0 0 11.53 0 39.72 0 62.84 0 75.56 0 84.9 0 89.26 0 92.72 0 95.37 0 96.8 0 113.67 0	585.6 585.36 582.76 582.14 581.89 582.01 580.71 579.79 580.74 581.51 582.09 583.09		MON.1 GND GND FP LB LEW TW 0.85 P REW BKF GND MON.2
Cnocs Costional Communication			
Cross Sectional Geometry			
Floodprone Elevation (ft) Bankfull Elevation (ft) Floodprone Width (ft) Bankfull Width (ft) Entrenchment Ratio Mean Depth (ft) Maximum Depth (ft) Width/Depth Ratio Bankfull Area (sq ft) Wetted Perimeter (ft) Hydraulic Radius (ft) Begin BKF Station End BKF Station	Channel 583.23 581.51 102.77 10.22 10.05 0.91 1.72 11.23 9.28 10.82 0.86 86.58 96.8 Page 1	Left 583.23 581.51 10 0.93 1.72 10.75 9.27 10.69 0.87 86.58 96.58	Right 583.23 581.51 0.22 0.06 0.12 3.67 0.01 0.37 0.04 96.58 96.8

# XS4 Pool.txt

		of alless deeps deeps decid group group Galley deeps decid deeps deeps decid		
Entrainment Calculations				
Entrainment Formula: Rosgen Modified Shields Curve				
Slope Shear Stress (lb/sq ft) Movable Particle (mm)	Channel 0.00423 0.23	Left Side O	Right Side O	

## XS5 Pool.txt RIVERMORPH CROSS SECTION SUMMARY

River Name: Beaver Reach Name: UT1 Cross Section Name: XS5 PC Survey Date: 12/10/	OOL YRO			
Cross Section Data Entry				
BM Elevation: Backsight Rod Reading:	0 ft 0 ft			
TAPE FS	ELEV		NOTE	
0 0 4.37 0 20.96 0 33.56 0 43.84 0 46.61 0 48.27 0 49.78 0 53.11 0 77.94 0 95.22 0 113.05 0	575.92 575.77 574.96 576.4 576.77 575.15 574.56 575.32 576.87 577.58 580.89 582.77 583.69		MON.2 GND GND GND BKF LEW TW0.75 P REW RB GND GND GND GND GND MON.1	
Cross Sectional Geometry				
Floodprone Elevation (ft) Bankfull Elevation (ft) Floodprone Width (ft) Bankfull Width (ft) Entrenchment Ratio Mean Depth (ft) Maximum Depth (ft) Width/Depth Ratio Bankfull Area (sq ft) Wetted Perimeter (ft) Hydraulic Radius (ft) Begin BKF Station	Channel 578.98 576.77 85.25 9.06 9.41 1.15 2.21 7.88 10.44 10.1 1.03 43.84 Page 1	Left 578.98 576.77  4.53  1.25 2.21 3.62 5.64 7.24 0.78 43.84	Right 578.98 576.77 4.53 1.06 2.16 4.27 4.8 7.17 0.67 48.37	

End BKF Station

XS5 Pool.txt
52.9

Entrainment Calculations

Entrainment Formula: Rosgen Modified Shields Curve

Channel Left Side Right Side
0.00423
Shear Stress (lb/sq ft)
Movable Particle (mm)

XS5 Pool.txt
52.9

48.37

52.9

Channel Left Side Right Side
0.00423
0
0
58.3

# XS6 Riffle.txt RIVERMORPH CROSS SECTION SUMMARY

River Name: Beaver Reach Name: UT1 Cross Section Name: XS6 RI Survey Date: 01/02/	CF YRO		
Cross Section Data Entry			
BM Elevation: Backsight Rod Reading:	0 ft 0 ft		
TAPE FS	ELEV		NOTE
0       0         6.38       0         12.67       0         20.01       0         43.76       0         48.26       0         52.88       0         53.1       0         54.07       0         57.9       0         62.02       0         77.93       0         88.69       0         96.59       0         118.54       0         122.97       0	575.68 575.09 574.78 575.93 576.91 576.87 575.34 575.11 575.29 576.73 577 577.23 579.04 580.53 583.19 583.69		MON.4 GND GND MON.3 LB LEW TWO.25 R REW BKF RB MON.2 GND GND GND GND GND GND MON.1
Cross Sectional Geometry			
Floodprone Elevation (ft) Bankfull Elevation (ft) Floodprone Width (ft) Bankfull Width (ft) Entrenchment Ratio Mean Depth (ft) Maximum Depth (ft) Width/Depth Ratio Bankfull Area (sq ft)	Channel 578.68 576.73 86.55 9.22 9.39 0.81 1.95 11.38 7.49 Page 1	Left 578.68 576.73 3.35 0.55 1.11 6.09 1.86	Right 578.68 576.73 5.87 0.96 1.62 6.11 5.63

Wetted Perimeter (ft) Hydraulic Radius (ft) Begin BKF Station End BKF Station	XS6 Riffle.t 9.82 0.76 48.68 57.9	4.63 0.4 48.68 52.03	7.4 0.76 52.03 57.9		
Entrainment Calculations					
Entrainment Formula: Rosgen Modified Shields Curve					
Slope Shear Stress (lb/sq ft) Movable Particle (mm)	Channel 0.00423 0.20 46.6	Left Side O	Right Side O		

### XS7 Pool Yr O.txt RIVERMORPH CROSS SECTION SUMMARY

River Name: Beaver Reach Name: Beaver Cross Section Name: XS7 PO Survey Date: 12/10/	dam Mainste OL YRO	em	
Cross Section Data Entry			
BM Elevation: Backsight Rod Reading:	0 ft 0 ft		
TAPE FS	ELEV		NOTE
0 0 10.35 0 34.54 0 37.78 0 49.82 0 53.14 0 57.65 0 61.27 0 63.66 0 65.98 0 73.54 0 85.79 0 112.85 0 129.91 0	580.59 579.19 576.09 576.5 575.91 576.34 575.97 574.28 574.24 576.15 576.96 577.28 576.92 577.29		MON.1 GRD GRD FP GRD LB LEW TWO.8 P REW BKF RB GND GND GND MON. 2
Cross Sectional Coometry			
Cross Sectional Geometry			
Floodprone Elevation (ft) Bankfull Elevation (ft) Floodprone Width (ft) Bankfull Width (ft) Entrenchment Ratio Mean Depth (ft) Maximum Depth (ft) Width/Depth Ratio Bankfull Area (sq ft) Wetted Perimeter (ft)	Channel 578.82 576.15 132.38 18.08 7.32 1.21 2.67 14.94 21.87 18.96 Page 1	Left 578.82 576.15  9.72  1.34 2.67 7.25 13.01 12.49	Right 578.82 576.15 8.36 1.06 2.17 7.89 8.85 10.81

Hydraulic Radius (ft) Begin BKF Station End BKF Station	7 Pool Yr 0 1.15 55.46 73.54	.txt 1.04 55.46 65.18	0.82 65.18 73.54	
Entrainment Calculations				
Entrainment Formula: Rosgen Modified Shields Curve				
Slope Shear Stress (lb/sq ft) Movable Particle (mm)	Channel 0.0106 0.76 124.3	Left Side 0	Right Side O	

# XS8 Riffle Yr O.txt RIVERMORPH CROSS SECTION SUMMARY

River Name: Beaver Reach Name: Beaver Cross Section Name: XS8 RI Survey Date: 12/10/	rdam Mainste [F YRO	em	
Cross Section Data Entry			
BM Elevation: Backsight Rod Reading:	0 ft 0 ft		
TAPE FS	ELEV		NOTE
0 0 10 0 27.99 0 34.04 0 54.36 0 59.35 0 64.91 0 65.38 0 66.42 0 73.02 0 77.66 0 85.45 0 99.8 0 131.16 0	580.59 579.16 576.43 576.35 576.83 576.27 574.2 574.02 574.22 575.92 576.35 576.93 576.94 576.91 577.49		MON.1 GND BKF MON. 2 BKF LEW TWO.2 R REW RB BKF GND GND GND MON.4
Cross Sectional Geometry			
Floodprone Elevation (ft) Bankfull Elevation (ft) Floodprone Width (ft) Bankfull Width (ft) Entrenchment Ratio Mean Depth (ft) Maximum Depth (ft) Width/Depth Ratio Bankfull Area (sq ft) Wetted Perimeter (ft)	Channel 578.62 576.32 135.63 18.43 7.36 1 2.3 18.43 18.48 19.09 Page 1	Left 578.62 576.32  23.52  1 2.3 23.52 18.48 19.09	Right

Hydraulic Radius (ft) Begin BKF Station End BKF Station	8 Riffle Yr 0.97 58.9 77.34	0.txt 0.97 58.9 77.34	
Entrainment Calculations			
Entrainment Formula: Rosgen Modified Shields Curve			
Slope Shear Stress (lb/sq ft) Movable Particle (mm)	Channel 0.0106 0.64 109.7	Left Side O	Right Side O