

# Dog Bite Site Stream Restoration Plan

Mitchell County, North Carolina

State Contract No. D06056-A



Prepared for:  
North Carolina Ecosystem Enhancement Program



**July 2008**



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Stream Restoration Plan  
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KCI Project No. 12065439

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## EXECUTIVE SUMMARY

The Dog Bite Site (DBS) is a full-delivery stream mitigation project located in central Mitchell County, North Carolina. The project site is situated within the French Broad Basin in the 06010108 8-digit hydrologic unit code and the North Carolina Division of Water Quality Subbasin 04-03-06. The project watershed is located in a rural setting within the Southern Crystalline Ridges and Mountains ecoregion of the Blue Ridge physiographic province.

The DBS is made up of 3,718 existing linear feet of stream. The primary hydrologic feature on the site is White Oak Creek (WOC), of which there is 3,068 existing linear feet. The site also includes two tributaries to WOC. Tributary 1 (T1) is 431 existing linear feet and enters WOC on the eastern side of the site. Tributary 2 (T2) is 219 existing linear feet and enters WOC near the center of the site from the south. WOC drains to Cane Creek, which then flows into the North Toe River. The project watershed is 0.54 square mile (342 acres).

Historic aerial photographs are available for the site from the years 1956, 1982, 1993, and 1998. Prior to 1956 the site had been partially cleared along the project streams. From 1956 to 1982, the DBS was further cleared for pasture. Between 1982 and 1993, two ponds were created to support the dairy operation, but there was no further forest clearing.

The site was a dairy farm in the past and is now used for both Christmas tree farming and livestock grazing. The construction of two ponds on the site resulted in WOC being channelized around the ponds. All of the project streams have been impacted by livestock, land clearing, and channelization. These impacts have resulted in portions of the project streams having bank erosion, areas of incision, poor bed variability, and low sinuosity. Certain project reaches have at least a partially vegetated riparian zone, while other reaches do not have a riparian zone at all. Overall, the DBS streams are in varying degrees of instability.

The DBS offers the opportunity to restore a significant headwater system. By developing a healthy, interconnected riparian corridor, the site will also help to reduce nutrient and excess sediment inputs. This is especially significant, because the site is classified as a Trout Water stream and is a tributary to Cane Creek. The proposed project reaches were designed as restoration or enhancement based on the level of departure from a stable stream system. The streams at the DBS will be restored to B channels, although C channels will exist in isolated areas where there is an existing floodplain. Riparian vegetation at the DBS site will be restored using Montane Oak-Hickory Forest species.

The project goals are to:

- Improve water quality with reduced nutrient and sediment levels.
- Create high-quality aquatic and terrestrial habitat.

In order to meet these goals, the following objectives must be accomplished:

- Plant a functional Montane Alluvial Forest community along with a Montane Oak-Hickory Forest to create an effective riparian buffer.
- Arrest bed elevation lowering and stream widening.
- Create in-stream habitat by restoring a profile with defined pools and adding dead woody debris habitat structures.
- Stop bank erosion by developing the appropriate channel dimension and by stabilizing with vegetation.
- Remove the livestock waste pond adjacent to the stream.
- Exclude livestock from the riparian areas with fencing.

Project success will be assessed by utilizing measurements of stream dimension, pattern, and profile; site photographs, and vegetation sampling. The monitoring report format will be similar to that set out in the most recent EEP monitoring protocol. Monitoring shall be conducted annually for a total period of five years or until the project meets its success criteria.

### Mitigation Summary

Reach	Existing Stationing	Proposed Stationing	Mitigation Type	Priority Approach	Existing Linear Footage	Designed Linear Footage
WOC-1	10+00-12+54	10+00-12+54	Enhancement I	-	254	254
WOC-2	12+71-19+19	12+71-19+25	Restoration	P3	633	639
WOC-3	19+19-22+68	19+25-22+74	Enhancement I	-	349	349
WOC-4	22+82-36+71	22+88-36+31	Restoration	P3	1,374	1,325
WOC-5	36+71-41+29	36+31-40+89	Enhancement I	-	458	458
T1-1	50+00-50+95	50+00-50+95	Enhancement I	-	95	95
T1-2	50+95-54+48	50+95-54+69	Restoration	P3	336	359
T2	60+00-62+19	60+00-62+57	Restoration	P3	219	257
Total					3,718	3,736
Total Proposed Stream Enhancement I						<b>1,156</b>
Total Proposed Stream Restoration						<b>2,580</b>

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## 1.0 INTRODUCTION

The Dog Bite Site (DBS) is a full-delivery stream mitigation project being developed for the North Carolina Ecosystem Enhancement Program (EEP). This restoration plan presents detailed information about the existing site and watershed conditions, the morphological design criteria, and the project design parameters based upon natural channel restoration methodologies.

## 2.0 PROJECT SITE IDENTIFICATION AND LOCATION

### 2.1 Directions to Project Site

The DBS is located southeast of Bakersville in central Mitchell County and its location is shown in Figure 1. The center of the site is situated at approximately 35.9956 degrees north and –82.1302 degrees west (WGS1984). The project area is located at the center of the United States Geological Survey (USGS) Quadrangles Bakersville, Carvers Gap, Spruce Pine, and Micaville.

To reach the site from Raleigh, begin by proceeding west on I-40 for approximately 200 miles. Then take Exit 86 for NC-226 toward Shelby/Marion. Take a right onto NC-226, traveling north. Follow NC-226 through Marion and Spruce Pine. Just before reaching Bakersville, make a right onto White Oak Road. Follow White Oak Road for approximately 1.5 miles and then make a left onto Wilson Dairy Road. The road will dead end at the Wilson property and the DBS is on the left.

### 2.2 USGS Hydrologic Unit Code and NCDWQ River Basin Designations

The project site is situated within the French Broad Basin in the 06010108 8-digit hydrologic unit code (HUC) and the 06010108040010 14-digit HUC. This 14-digit HUC is not a Targeted Local Watershed as identified by the EEP. The site is found within the North Carolina Division of Water Quality (DWQ) Subbasin 04-03-06.

## 3.0 WATERSHED CHARACTERIZATION

The project watershed is located in a rural setting within the Southern Crystalline Ridges and Mountains ecoregion of the Blue Ridge physiographic province (Figure 2). The topography within this ecoregion is characterized by rough dissected ridges and valleys (Griffith et al. 2002). Elevations within the project watershed range from 4,000 feet above mean sea level (AMSL) at the top of the drainage to 2,700 feet AMSL where WOC leaves the project site.

### 3.1 Project Drainage Area

The project streams all drain into White Oak Creek (WOC) (Figure 3), which then flows into Cane Creek and ultimately into the North Toe River. Tributaries 1 and 2 have 0.08 square mile (48 acres) and 0.07 square mile (46 acres) drainages, respectively. The DBS has a total drainage area of 0.54 square mile (342 acres) and shares a portion of its southern boundary with the 14-digit HUC.

### 3.2 Water Surface Classification/Water Quality

The NCDWQ assigns surface waters a classification in order to help protect, maintain, and preserve water quality. WOC from its source to Cane Creek has a classification of Class C with a supplemental classification of Trout Waters (NCDENR DWQ, 2008a).

- **Class C Waters** in North Carolina are protected for secondary recreation, fishing, wildlife, fish and aquatic life propagation and survival, agriculture, and other uses suitable for Class C. Secondary recreation includes wading, boating, and other uses involving human body contact with water where such activities take place in an infrequent, unorganized, or incidental manner. There are no restrictions on watershed development or types of discharges.
- **Trout Waters** is a supplemental classification intended to protect freshwaters for natural trout propagation and survival of stocked trout. This designation affects wastewater quality but not the type

of discharges and there are no watershed development restrictions except stream buffer zone requirements by the NC Division of Land Resources (NCDENR DWQ, 2008b).

None of the project streams or streams immediately downstream of the site are currently designated as impaired under Section 303(d) of the Clean Water Act (NCDENR, DWQ 2008c).

### **3.3 Geology and Soils**

The underlying rocks at the site include metamorphic rocks of the Ashe Metamorphic Suite and Tallulah Falls Formation. The member of the group present at the site is the Muscovite-biotite gneiss, which is described as locally sulfidic; interlayered and gradational with mica schist, minor amphibolite and hornblende gneiss (NCDENR, NCGS 1985).

The Soil Survey of Mitchell County shows that the primary soil series at the project site are Bandana, Dellwood-Reddies and Thunder-Saunook as shown in Figure 4 (USDA, NRCS 2004). Bandana sandy loam is described as a deep, somewhat poorly drained soil that occurs within valleys of mountains and intermountain hills on floodplains. Dellwood-Reddies complex is a very deep, moderately well drained soil that occurs within valleys of mountains and intermountain hills on floodplains dominantly at the upper end of mountain valleys. The third soil series present is the Thunder-Saunook complex that has 15 to 30 percent slopes and is very bouldery. The soil is very deep and well drained. The Thunder-Saunook occurs on intermountain hills and low intermediate mountains on coves, colluvial fans, drainageways and benches.

### **3.4 Historical Land Use and Development Trends**

#### **3.4.1 Historical Resources**

Historic aerial photographs were obtained from the Mitchell County Natural Resources Conservation Service (NRCS) office, the USGS Earth Explorer, and USGS digital orthoquadrangles in order to assess the existing and historic site conditions. A review of the site history helps to understand the chronology of land disturbance and aid in the development of an appropriate restoration strategy. The historic aerial photographs are located in Appendix A.

Historic aerial photographs are available for the site from the years 1956, 1982, 1993, and 1998. By 1956, most of the forest surrounding the stream had been cleared and there was a thin riparian buffer left along some parts of the stream. From 1956 to 1982, the DBS was further cleared for pasture, with most of the clearing taking place on the eastern side of the site. At this point all of the forest along the project reaches had been cleared. Between 1982 and 1993, two ponds were created to support the dairy operation, but there was no further forest clearing. The 1998 aerial shows the site looking similar to the previous aerial. Overall, the watershed has changed minimally from 1956 to 1998, remaining mostly forested.

#### **3.4.2 Land Use and Development Potential**

The DBS site is located solely on one property. In the past the property had been used as a dairy farm. Dairy operations ended in 1996 and since then most of the property has been put into Christmas tree cultivation. Using an Anderson Level I classification, the predominate land uses in the project watershed consist of 2% agriculture, 80% forest, 17% pasture, and less than 1% wetland, open water, and urban or built-up land (See Table 2 and Figure 5) (McKerrow 2003). The surrounding area is rural with low development pressure.

### **3.5 Endangered/Threatened Species**

A formal review by the North Carolina Natural Heritage Program (NHP) was requested in July 2006 to identify the presence of rare species, critical habitats, and priority natural areas on the project site and to determine the potential impact of the proposed project on these resources. In their letter dated August 1,

2006, the NHP indicated “no record of rare species, significant natural communities, or significant natural heritage areas at the site nor within a mile of the project area”. In addition, no threatened or endangered species were identified in the project area during the existing conditions site assessment.

### **3.6 Cultural Resources**

To evaluate the presence of significant cultural resources on the subject property and any potential to impact these properties, KCI requested in July 2006 a formal review by the North Carolina Department of Cultural Resources, State Historic Preservation Office (SHPO). The formal SHPO review letter dated August 30, 2006 determined that “the project as proposed will not affect any historic structures.” SHPO also recommended that KCI conduct a formal archeological survey of the site. The site survey conducted by a KCI archeologist concluded that “the site has a very low likelihood of impacting any intact archeological resources.” Following the archeological site survey, SHPO’s letter dated October 23, 2006 recommended that no further archeological investigation be conducted.

### **3.7 Potential Constraints**

The site was evaluated for any site constraints that have the potential to hinder a successful mitigation project. Below is a description of any potential issues that may affect the project’s success.

#### **3.7.1 Property Ownership and Boundary**

The proposed restoration project is located on one parcel (Mitchell County PIN 0873-00-61-3570) owned by June Wilson. KCI has facilitated the purchase of a conservation easement on the site, which has been transferred to the State of North Carolina (see Appendix B). The conservation easement will protect the project streams in perpetuity.

#### **3.7.2 Site Access**

The site is located on Wilson Dairy Road as shown in Figure 1. Once on Wilson Dairy Road, the site can be accessed at the end of the road where there is a house and horse stables.

#### **3.7.3 Utilities**

There are no utilities mapped on the project site.

#### **3.7.4 FEMA/Hydrologic Trespass**

No portion of the site is located in a significant flood hazard area as recognized by the Federal Emergency Management Agency (FEMA). A portion of WOC is found on FEMA Map 37121C0076 C (Mitchell County Flood Insurance Study, Effective September 2, 1988) and is shown as Zone X.

The proposed restoration is not anticipated to produce hydrologic trespass conditions on the existing property or on any neighboring properties.

## **4.0 PROJECT SITE STREAMS (EXISTING CONDITIONS)**

The DBS is made up of 3,718 existing linear feet of WOC and its two tributaries (T1 and T2). WOC has 3,068 existing linear feet on the project site and flows from east to west across the property. There are 431 existing linear feet in T1 and 219 existing linear feet in T2. T1 enters WOC toward the eastern end of the project and T2 enters WOC near the middle of the project. The existing site conditions and site assessment locations for cross-sections and longitudinal profiles are shown in Figure 6. The project site photographs (Appendix C) show the current conditions at the DBS and the existing conditions data (Appendix D) summarize the site assessment.

### **4.1 General Site Description**

The project streams have been impacted in a number of different ways. Cattle impacts from the closed dairy operation and channelization have created varying levels of unstable stream conditions throughout

the site. At the beginning of the project, just downstream of a stable ford crossing, Reach 1 of WOC (WOC-1) begins where WOC flows out of the forest. This reach is characterized by a long series of riffles and runs and lacks stable pool features. WOC-1 has been modified as indicated by the spoil piles running adjacent to both sides of the stream. The reach appears vertically stable with a gravel and cobble bed, but the banks along this reach exhibit varying levels of stability, with some banks being undercut and actively eroding. This reach ends at a stable ford crossing near Station 12+54. After the ford crossing, Reach 2 begins (WOC-2). WOC-2 has also been channelized and spoil piles run parallel to the channel along both banks. This portion of the stream feeds an irrigation pond that is located in the relict stream channel. There is a six-inch gravity fed PVC pipe that enters the pond from the stream at Station 13+55. When the pond was constructed the stream was channelized around the right side of the pond. This section of stream has become incised and has an artificially low width to depth ratio. WOC-2 also does not have a well vegetated riparian buffer and lacks a natural stream pattern. Similar to WOC-1, WOC-2 is dominated by riffle and run features and does not have any pools to provide aquatic habitat diversity. The pond flows out of a riser that is built immediately downstream of the pond. The flow from the riser spills out onto a concrete slab and then flows back into WOC-2 at Station 17+50. Downstream of the pond, WOC-2 is still characterized by a sparse riparian buffer and lacks a natural stream pattern; the stream has also become more incised than at the beginning of the reach.

Reach 3 (WOC-3) begins at Station 19+19 where WOC flows into a slightly more wooded area that is characterized by small groups of tag alder (*Alnus serrulata*) and some larger trees that provide shade to the channel. This reach is confined by the valley wall on the north side of the stream. WOC-3 is less incised than the previous reach and also has a larger width to depth ratio, indicating that it is slightly more stable than WOC-2. The unstable areas of WOC-3 are characterized by poorly defined banks in some areas and eroding banks in others. Like the previous reaches, this reach lacks any deep water habitat that would be provided by pools. There is a seep entering from the southern hillside that contributes a small amount of flow to the stream near Station 21+85. The downstream half of WOC-3 leaves the cover of the canopy and ends at a ford crossing.

Reach 4 (WOC-4) begins after the ford crossing at Station 22+82. After the ford, livestock have unrestricted livestock access to the stream. WOC-4 has experienced considerable bank and bed damage. There is no riparian vegetation and sediment and nutrient inputs to the stream are high. At the beginning of the reach, the stream steepens and is constrained between a pond berm on the left and the valley wall on the right. The pond on the left side of the stream is a waste lagoon from the former dairy operation. This portion of the reach has been channelized, is incised, lacks a riparian buffer, and has poor aquatic habitat diversity. Downstream of the pond there is another ford crossing and WOC-4 flows into a wider valley bottom. Here WOC-4 has two well defined, but unstable meanders. The first meander is characterized by a steep grade with cascading drops over the cobble bed. The second meander is confined by a twelve-foot tall shear embankment as the stream flows into the valley wall. After these two meanders, the stream alternates between sections where it is confined and incised to sections where the valley bottom is wider and the stream is adjacent to an abandoned terrace. The riparian buffer of WOC-4 becomes brushier and widely-spaced large trees become more frequent as the stream flows west.

The last reach of the project stream (WOC-5) begins at Station 36+71. The valley becomes wider at the downstream end of the project and there is a terrace that is present throughout most of this reach. The riparian buffer is also more developed in this reach as it is interspersed with trees that provide partial shade to the stream. WOC-5 exhibits some variability in the stream pattern, but lacks a diverse stream bed. The stream cross-section is not well defined in areas and its dimension is not consistent throughout the reach. In some instances, WOC-5 has become over-widened as evidenced by large mid-channel bars. WOC-5 is the last reach along WOC and the stream exits the project site at Station 41+25.

In addition to WOC, the DBS has two tributaries, both first order perennial hydrologic features. T1's first reach (T1-1) begins at Station 50+00 in a sparsely forested area. This reach is incised and lacks pool habitat. T1-1 quickly leaves the forest canopy and the second reach (T1-2) begins at Station 50+95. This reach was channelized through high ground to the current location of its confluence with WOC at Station 14+40. As the channel has begun to fill in over the years, T1-2 has developed diffuse flow and there is not a defined channel until approximately 90 feet before the confluence with WOC. Some of the flow coming down T1 diverges from the channelized path and seeps to the location of T1's original flowpath, which has its confluence with WOC near Station 16+00. Due to the lack of a defined channel on T1-2, there is no stream habitat connection between T1-1 and WOC. There is also no riparian buffer along T1-2; the reach is in an overgrown field without any canopy cover.

T2 begins at Station 60+00. This tributary enters the DBS from a pipe under Wilson Dairy Road. As the stream exits the pipe, it enters an active livestock grazing area where there is no riparian vegetation and the stream banks have been trampled and have eroded away. The reach quickly flows from an area with minimal stream banks to an incised channel with eroding banks and no riparian vegetation. T2 is a steep reach that loses significant elevation as it flows down the side of the valley and joins WOC at Station 27+44.

#### 4.2 Channel Stability Assessment

A qualitative stability assessment was performed to estimate the level of departure from a stable stream system and determine the likely causes of any channel disturbance. This assessment facilitates the decision-making process with respect to restoration alternatives and establishing goals for successful restoration.

At the start of WOC-1, the stream is not incising, due to the compact cobble bed, but it is experiencing areas of bank erosion as the stream widens. Erosion has primarily been caused by the lack of floodprone area, a result of berms along both sides of the channel. Riffles and runs are evident features along this reach, but there are no pools. The lack of pools along all of WOC does not allow for adequate energy dissipation from the normal flow, which ultimately causes more bank erosion and unstable flows. The bank height ratios along this reach are between 3.0 and 4.0.

WOC-2 exhibits more instability than WOC-1 because it has been straightened and channelized and there is less riparian vegetation. Where the stream was channelized around the irrigation pond, the stream has a bank height ratio of between 1.6 and 2.6, is narrow, deep and slowly widening, leading to eroding banks. Downstream of WOC-2, WOC-3 has the stabilizing benefit of dispersed riparian vegetation, but is still undergoing isolated areas of widening and incision and lacks a defined riffle-pool sequence. WOC-3 has a bank height ratio of 3.8.

Portions of WOC-4 have unrestricted livestock access, which has contributed to bank and bed degradation. The reach's instability is also due to the fact that the upper portion of WOC-4 is confined in a narrow portion of the valley and is channelized around a steep pond berm. The stream continues down the valley where there is riparian vegetation, but still a natural stream pattern. While these two factors would normally contribute to stability, the steep grade of the valley and lack of pools continues to cause instability, leading to bank erosion and poor habitat diversity. This reach has a range of bank height ratios between 1.8 and 3.7.

WOC-5 has a more established riparian buffer and a larger width to depth ratio than the previous reaches. As a result, WOC-5 has less bank erosion and a slightly more stable cross-section. However, due to the increased channel width, poorly defined banks, and a lower channel slope, there is a greater accumulation of fine materials, which has created mid-channel bars. The bank height ratio of this reach ranges from 1.4 to 3.1.

The two tributaries are both unstable, but they are in different evolutionary stages. T1 and T2 have bank height ratios of 3.6 and 4.2, respectively. T1-1, while in a more forested area, is experiencing incision and widening, as evidenced by the undercut trees on the stream banks. Once T1 leaves the tree line, the channelized stream has filled in and does not have a defined flow path. The instability on T2 has been caused by livestock and the lack of riparian vegetation. T2 has extensive bed and bank degradation due to these two disturbances.

#### 4.3 Bankfull Verification

The standard methodology used in natural channel design is based on the ability to select the appropriate bankfull discharge and generate the corresponding bankfull hydraulic geometry from a stable reference system. The determination of bankfull stage is the most critical component of the natural channel design process.

Bankfull can be defined as “the stage at which channel maintenance is most effective, that is, the discharge at which moving sediment, forming or removing bars, forming or changing bends and meanders, and generally doing work that results in the average morphologic characteristics of the channels” (Dunne and Leopold 1978). Several characteristics that commonly indicate the bankfull stage include breaks in slope, changes in vegetation, highest depositional features (i.e. point bars), and highest scour line. The identification of bankfull stage, especially in a degraded system, can be difficult. Therefore, the following verification measures were undertaken to facilitate the correct identification of the bankfull stage on the DBS.

Using pressure transducer stream gauges, stream stage data were collected at two locations on the DBS: Gauge 1 immediately upstream of WOC-1 at a stable riffle and Gauge 2 on WOC-2 at Station 20+90. Data were collected for 10 months (July 2007 through April 2008.) Water levels were correlated to an estimated discharge using a rating curve generated for each gauged section. Over the course of the monitoring period the stream gauges showed that the stream stage changed minimally. These data reveal the consistency of the baseflow. The minor variations in the stream discharge indicate that bankfull events occur less frequently at the DBS than in comparable watersheds. This can be attributed to the strong influence of groundwater in this system and the well forested watershed upstream that intercepts a large amount of the precipitation.

Regional geometry relationships are typically utilized in ungauged areas to approximate bankfull discharge, area, width, and depth as a function of drainage area based on interrelated variables from other similar streams in the same hydrophysiographic province. The regional relationships for the rural mountains of North Carolina were used to verify the bankfull discharges in the project reaches (Harman et al. 2000). Based on the project’s drainage areas, the following bankfull discharges were calculated for the project streams: 63 cfs for WOC, 14 cfs for T1, and 14 cfs for T2. However, these calculations should be used with caution because the smallest drainage area used in the regional geometry regression to relate drainage area and discharge was 2 square miles. Also, only one of the streams used in the regression had a slope greater than 2.5%.

A HEC-HMS (Hydrologic Modeling System) model was developed for the DBS watershed. This type of model is designed to simulate the precipitation-runoff processes of dendritic watershed systems. For the DBS, four subbasins were delineated for the model. Various rain events were simulated within the model to evaluate the discharge associated with each event. For design purposes, a two-year rain event was used to approximate an event that would create bankfull conditions. This event generated much lower discharges than the regional curve relationships, 23 cfs for WOC and 3 cfs for both T1 and T2. These discharges were used to evaluate the design discharge.

These bankfull verification methods produced a range of bankfull discharge estimates for the DBS. Each of these methods were examined and evaluated to ascertain which data were the most reliable and consistent with our knowledge of the site. The methods that were site specific - the on-site gauges, the HEC-HMS model, and the in-stream bankfull indicators - had the most influence when determining the design discharges. A combination of these methods produced a design discharge for WOC of approximately 40 cfs and for the two tributaries of 14 cfs.

#### 4.4 Vegetation

The immediate valley surrounding the project streams has been cleared of trees; woody vegetation remains along riparian corridors in varying age classes and densities. Because of previous impacts to the existing forest stands, no distinct vegetative communities exist on the site. Below is a description of the distribution of common plant species across the DBS.

Along WOC, the riparian corridor contains a mixed community of northern red oak (*Quercus rubra*), sycamore (*Platanus occidentalis*), black walnut (*Juglans nigra*), white oak (*Quercus alba*), tulip poplar (*Liriodendron tulipifera*), pussy willow (*Salix discolor*), black willow (*Salix nigra*), river birch (*Betula nigra*), black birch (*Betula lenta*), yellow birch (*Betula alleghaniensis*), eastern white pine (*Pinus strobus*), yellow buckeye (*Aesculus octandra*), red maple (*Acer rubrum*), wild hydrangea (*Hydrangea arborescens*), multiflora rose (*Rosa multiflora*), tag alder (*Alnus serrulata*), and green ash (*Fraxinus pennsylvanica*).

During construction, the number of mature trees removed from the existing riparian areas will be minimized as much as possible. Any valuable trees that may provide immediate shade to the restored channel will be left in place if feasible. In the enhancement areas, certain trees may be able to remain on one bank if the opposite bank can be reshaped to accommodate the appropriate dimension for the stream.

### 5.0 REFERENCE SITES

A reference reach is a channel with a stable dimension, pattern, and profile within a particular valley morphology. The reference reach is used to develop dimensionless morphological ratios (based on bankfull stage) that can be extrapolated to disturbed/unstable streams to restore a stream of the same type and disposition as the reference stream (Rosgen 1998). For this project, two reference reaches were used to design the proposed restoration reaches: an unnamed tributary to Fisher River in Surry County, North Carolina (see Appendix E for detailed reference reach data) and an onsite reference. The stable cross-sections immediately upstream of the project stream will serve as dimensional references. In addition to working within the existing site constraints, UT to Fisher River will serve as the basis for designing the planform of the restored stream.

#### 5.1 UT to Fisher River Reference Site

An unnamed tributary to Fisher River (UTFR), a first order rural stream in Surry County, was selected as a reference reach for the restoration of the project streams (Figure 7). The reference reach is located on Fisher Valley Road off of Exit 93 from Interstate 77. The valley slope is approximately 1.6%. The sediment distribution and transport are similar to the project streams. The local topography is characterized by rolling hills. Approximately 300 linear feet of UTFR was surveyed and was classified as a B4c channel.

UTFR flows northeast into Fisher River and drains approximately 0.38 square mile of predominantly forested land with a small section of rangeland (Figure 8). The reference reach watershed is within the Northern Inner Piedmont ecoregion in the Piedmont physiographic province. The site is in the 14-digit hydrologic unit 03040101090010 in the Yadkin Basin and is in the DWQ Subbasin 03-07-02. The reference reach watershed elevations range from 1,420 feet AMSL at the headwaters of the site to 1,210 at the bottom of the reference reach.

## 5.2 White Oak Creek Reference Site

A short reach of White Oak Creek, upstream of the project site, was surveyed by KCI in August 2007 (Appendix H). The valley slope is approximately 8.0%. The sediment distribution and transport are the same as the project streams. A stable riffle cross-section was surveyed and classified as a B4a channel to be used as a dimensional reference.

## 5.3 Reference Vegetative Communities

There are two communities described by Schafale and Weakley that are representative of reference systems appropriate for the DBS site (1990).

The natural community identified as representative of the streamside areas was the Montane Alluvial Forest. This community type is described as existing along river and stream floodplains at moderate to high elevations in more isolated patches when compared to broader floodplain forests. The canopy species that are typically found within a Montane Alluvial Forest include eastern hemlock (*Tsuga canadensis*), sycamore, yellow birch, white oak, red maple, tulip poplar, and river birch. Species that dominate the understory are ironwood (*Carpinus caroliniana*), witch hazel (*Hamamelis virginiana*), and black willow. Typical shrubs include rhododendron (*Rhododendron maximum*), tag alder, and doghobble (*Leucothoe fontanesiana*) (Schafale and Weakley 1990).

Montane Oak-Hickory Forest was identified as the community type appropriate for stream valleys and slopes leading away from small stream floodplains. Typical species found in the Montane Oak-Hickory Forest canopy include white oak, northern red oak, chestnut oak (*Quercus prinus*), mockernut hickory (*Carya alba*), pignut hickory (*Carya glabra*), tulip poplar, and red maple. The understory layer commonly has flowering dogwood (*Cornus florida*), sourwood (*Oxydendrum arboreum*), red maple, black gum (*Nyssa sylvatica*) and serviceberry (*Amelanchier arborea*). Typical shrubs include rhododendron (*Rhododendron maximum*), *Vaccinium spp.*, maple leaf viburnum (*Viburnum acerifolium*) and witch hazel (Schafale and Weakley 1990).

# 6.0 PROJECT SITE RESTORATION PLAN

## 6.1 Restoration Project Goals and Objectives

The DBS has experienced degradation along all of its reaches from livestock, the removal of upland and riparian vegetation, pond construction, and channelization. These impacts have left the streams with unstable banks, incised streambeds, inappropriate planform, and poor bed variability. There is considerable potential to improve and protect this headwater system and provide an interconnected assemblage of aquatic and terrestrial habitat upstream of important trout waters.

Based on these site-specific conditions, the restoration goals for the DBS are as follows:

- Improve water quality with reduced nutrient and sediment levels.
- Create high-quality aquatic and terrestrial habitat.

In order to meet these goals, the following objectives must be accomplished:

- Plant a functional Montane Alluvial Forest community along with a Montane Oak-Hickory Forest to create an effective riparian buffer.
- Arrest bed elevation lowering and stream widening.
- Create in-stream habitat by restoring a profile with defined pools and adding dead woody debris habitat structures.
- Stop bank erosion by developing the appropriate channel dimension and by stabilizing with vegetation.
- Remove the livestock waste pond adjacent to the stream.

- Exclude livestock from the riparian areas with fencing.

#### 6.1.1 Design Approach

When approaching the design for the DBS, the project objectives were balanced against the existing site constraints. Below is a description of the site-specific approach used for the design for the DBS.

One of the major site constraints is the valley topography at the DBS. The valley slope varies in steepness and in many places confines the existing and potential restored planform. The overall approach to the design of WOC is a combination of Priorities 2 and 3 restoration (Rosgen 1997). This will involve creating a new stream profile and dimension and a bankfull bench that will tie into the valley side. Where WOC currently is confined by the upstream pond, the new planform will move the stream away from the pond to allow for a greater flood prone area on both sides of the stream. To account for the steep slopes of the reaches on WOC (from 3.3% to 7.5%), the design will include frequent grade control structures that will mimic the natural step pool sequences found in streams of this type. These step pools will create the deep water habitat that the stream is currently lacking. While there will be planform adjustments in the restoration reaches, many of these adjustments will be minor due to confinement within the valley and the low sinuosity typical of this type of mountain stream. The restored planform will be of a similar beltwidth as the existing stream, but with more defined meanders. Similar to stable step pool dominated mountain streams, the planform of the restored stream will not solely dictate the riffle and pool sequence. Many of the step pools will be located in straight sections of the channel and will be associated with rock or wood drop structures.

Another component of the restoration of WOC will be the addition of habitat features. These habitat structures will primarily be composed of dead woody debris to narrow the flow path of the channel in areas where the stream has over-widened. Adding these structures will provide diverse habitat niches within the stream and buffer areas. The in-stream structures will primarily be in pools to enhance the deep water habitat that does not currently exist at the site. Some log grade control structures will be installed at grade changes in the middle of riffles. These sections of grade change will create bed diversity within the riffles, as some riffles will have some steeper sections and some less steep sections within the same riffle. The enhancement sections of WOC will have their profiles altered, with some existing high quality riffles being preserved and new pools being created with structures. The cross-sections will also be altered, creating a bankfull channel that will match the restoration reaches.

T1 will be restored in a similar fashion, but the tributary will be relocated from where it was historically channelized back to its approximate original location. The bankfull bench will tie into the existing terrace in the stream's former location. This restoration approach will be Priority 3. T2 will be restored by creating a stable cross-section, adjusting the current planform, and building a bankfull bench (Priority 3). Grade control structures will be incorporated into the design for T2 to stabilize the tributary's steep slope.

For this project, the two reference reaches described in Section 5.0 will be used to guide the design of the cross-sections, profile, and planform. However, an ideal reference reach was not found for the DBS. The UT to Fisher River Reference Site has a slope lower than 2%. In the mountain region of North Carolina, stable B3/4 streams with slopes ranging from 3-7% are scarce. KCI has conducted numerous reference reach searches throughout North Carolina and has not been able to find stable B3/4 channels within this slope range.

#### 6.1.2 Designed Channel Classification

The mainstem and tributaries are divided into eight separate reaches based on the restoration or enhancement approach applied to the portions of the channels (Table 1). The project reaches are identified in Figure 9. The morphological design criteria for each of the reaches are found in Tables 4a through 4c. The streams at the DBS will generally be restored to B channels, with the first four reaches of WOC

restored and enhanced to B4a streams, and the last reach enhanced to a B4 stream. The two tributaries will also be restored and enhanced to B4a stream types. Channels in isolated areas where the streams are not entrenched in a valley and have access to a floodplain will function as C channels. As WOC flows through the property, the stream slope decreases. This changing slope affects the restoration design, so that the proposed cross-sections were adjusted differently for each reach. The designed cross-sections for the DBS streams are typically designed to have a width to depth ratio of just over 12 and entrenchment ratios between 2 and 2.2. These cross-sections will be stable and self maintaining, but it is expected that due to site constraints and relatively small cross-section, these ratios on the constructed channel may vary slightly and fall into another channel classification. Even if this is the case, the designed channel classification will most likely still be maintained as B4a and B4 channels due to the continuum of physical variables within stream reaches (Rosgen 1996).

WOC-1 runs from Station 10+00 to 12+54 and ends at a 15-foot wide easement exception where there is a rock ford crossing. WOC-1 will be improved as Enhancement I, which involves adjusting the stream to have the appropriate profile and dimension (USACE et. al 2003). Work on WOC-1 will also involve keeping as many of the trees in the existing riparian buffer as possible. The second reach on WOC will be restored. WOC-2 begins at the easement exception at Station 12+71 and will be slightly meandered away from the berm that surrounds the irrigation pond on the left side of the channel, where T1-2 will join WOC. Then WOC-2 will cross a 15-foot rock ford crossing easement exception and flow back to its existing location in the valley before WOC-3 begins at Station 19+25. The restoration of WOC-2 will also maintain and stabilize the irrigation pond inlet and outlet. Like WOC-1, the mitigation type of WOC-3 will be Enhancement I. This reach begins at Station 19+25 where there is a more developed riparian buffer and ends at Station 22+73 where there is a 15-foot wide easement exception with another rock ford crossing. From the easement exception at Station 22+88, the restoration of WOC-4 will involve constructing a more appropriate planform and a stable cross-section and profile. The old cattle lagoon to the left of the stream will be removed. The designed length of WOC-4 is shorter than the existing length due to the elimination of two unstable meanders that currently run into steep valley walls. In this section the channel will be brought back towards the center of the valley with slightly shorter meanders, thereby reducing the length of this reach. WOC-4 will cross the last 15-foot rock ford crossing easement exception on WOC and end at Station 36+31, where WOC-5 begins. WOC-5 has a stable planform, but will be improved as Enhancement I and flows from the end of WOC-4 to the end of the project at Station 36+31.

Tributary 1 is separated into two reaches. The mitigation type for T1-1 is Enhancement I. This reach begins in a wooded area at Station 50+00 and ends at Station 50+95, where the stream enters a clearing. T1-2 will have a defined channel restored back to the old stream location. This reach begins at the end of T1-1, crosses a 15-foot rock ford crossing easement exception and will be restored until it ends at the confluence with WOC at Station 54+69. T2 will be restored for its entire length, beginning at Station 60+00 and ending at the confluence with WOC at Station 62+57.

#### 6.1.3 Targeted Buffer Communities

Once all of the work on the project streams has been completed, livestock exclusion fencing will be installed along the easement boundary on the lower half of the site where livestock will still be kept on the project parcel. In the areas where there will not be any cattle, the easement boundaries will be marked with metal posts.

The project will restore a Montane Alluvial Forest community within the floodprone area and low-lying parts of the valley with a Montane Oak-Hickory Forest community along the valley slopes throughout the rest of the site. These communities will fit into the natural topography and setting created by the newly restored channels (Schafale and Weakley 1990).

## 6.2 Sediment Analysis

The sediment competency of the DBS was studied in detail and the assessment data are available in Appendix D. Pebble counts and bulk samples were taken throughout the project reaches. Based on this analysis, the majority of the project reaches are dominated by gravel and cobble material.

As WOC-1 comes onto the project site, it has predominately a gravel bed with sand overwash covering most of the gravel. A pebble count at Station 10+75 (Existing) found the channel to be 41% sand and 34% gravel with a D84 of 79.0 mm. A bulk sample on WOC-1 provided a measured D84 of 29.1 mm and 78% gravel in the pavement. The subpavement was composed of slightly finer material with a D84 of 16.9 mm.

WOC-2 is more clearly dominated by gravel as demonstrated by the measured D84 from the two cross-section pebble counts of 60.0 mm and 150.0 mm. The bulk sample also found that the pavement and sub-pavements were primarily gravel with D84 values of 51.0 mm and 27.7 mm, respectively.

The gravel bed continues through WOC-3. This is reflected in the 67% gravel in the pebble count and the D84 of 64.0 mm. WOC-3 also reflects the trend of coarse pavement and slightly less course sub-pavement. The pavement D84 was 42.0 mm and the sub-pavement D84 was 29.0 mm. The data in Appendix D also indicate the same trends in the pebble counts and bulk samples for WOC-4 and WOC-5.

T1-1 has a similar gravel bed as the mainstem with a pebble count with a D84 of 160 mm, 46% gravel, and 35% cobble. When T1 loses its defined channel and T1-2 begins, the channel becomes a vegetated swale dominated by fine sediments. These fine sediments are a result of the relic channel being filled when the stream was relocated. Aggradation has also occurred as fine materials become trapped by the vegetation and there is no concentrated flow to wash out these materials. The pebble count from this reach reflected this, being composed entirely of sand and silt. T2 has been so impacted by cattle that the bed is primarily composed of silt from the eroding banks and adjacent grazing area. The pebble count of this compacted bed was made up of 90% silt.

The sediment sampling found that the streambed of the DBS streams are predominately compacted with gravels and sands cemented between larger cobbles. These streams are threshold channels, which are defined as streams where the bed material inflow is negligible and the channel boundary is immobile even at high flows (Shields et al. 2003). At the DBS, there is a lack of incoming bed material from the small surrounding forested watershed and cattle have hardened the bed with tightly packed gravel and cobble. While the bulk of the streambed is made up of compacted gravel, there is a large amount of cobble material that is scattered throughout the stream and acts to armor many of the steep riffles. This is especially typical of the enhancement reaches where there are more stable riffles than in the restoration reaches. As opposed to an active bed system, a threshold channel never achieves full sediment transport; the system only achieves partial sediment transport. Therefore, threshold mobility evaluation of these streams is not appropriate for the site.

To verify that the restored and enhanced streams would not aggrade and collect excessive fine materials, the shear stresses of the proposed riffle cross-sections were calculated. These shear stresses were validated for the design riffle cross-sections and channel gradient using the equation:

$$\tau = \gamma R s$$

Where:       $\tau$  = shear stress ( $\text{lbs}/\text{ft}^2$ )  
 $\gamma$  = specific gravity of water ( $62.4 \text{ lbs}/\text{ft}^3$ )  
 $R$  = hydraulic radius (ft)  
 $s$  = average water slope (ft/ft)

All of the shear stresses calculated were greater than is necessary to move the fine wash load that has been found in the stream. This should promote a stable channel bottom without excessive aggradation of fine materials.

### **6.3 Natural Plant Community Restoration**

Riparian plantings shall consist of native woody species. To achieve a mature survivability of 260 stems per acre, 680 stems per acre (8 feet by 8 feet spacing) will be planted. Plant placement and groupings will be randomized during installation in order to develop a more naturalized appearance. Woody vegetation planting will take place during dormancy. Species to be planted in the bankfull bench and low-lying areas as Montane Alluvial Forest may consist of the following:

Tag Alder	<i>Alnus serrulata</i>	Sycamore	<i>Platanus occidentalis</i>
River Birch	<i>Betula nigra</i>	Tulip Poplar	<i>Liriodendron tulipifera</i>
Yellow Birch	<i>Betula alleghaniensis</i>	White Oak	<i>Quercus alba</i>
Witch Hazel	<i>Hamamelis virginiana</i>	Winterberry	<i>Ilex verticillata</i>
Spicebush	<i>Lindera benzoin</i>		

The valley slopes will be planted as Montane Oak-Hickory Forest and may consist of the following species:

Sweetshrub	<i>Calycanthus floridana</i>	Mockernut Hickory	<i>Carya alba</i>
Chestnut Oak	<i>Quercus prinus</i>	Tulip Poplar	<i>Liriodendron tulipifera</i>
White Oak	<i>Quercus alba</i>	Serviceberry	<i>Amelanchier arborea</i>
Witch Hazel	<i>Hamamelis virginiana</i>	Black Gum	<i>Nyssa sylvatica</i>
Black Walnut	<i>Juglans nigra</i>	Spicebush	<i>Lindera benzoin</i>

On the restored stream banks, live stakes will be used to provide natural stabilization. Appropriate species identified for live staking include:

Silky Dogwood	<i>Cornus amomum</i>	Silky Willow	<i>Salix sericea</i>
Black Willow	<i>Salix nigra</i>	Elderberry	<i>Sambucus canadensis</i>

A herbaceous seed mix composed of appropriate native species will also be developed and used to further stabilize and restore the riparian and bank zones following construction.

In addition to planting the proposed community types, vegetative restoration will also include eliminating invasive species that have taken over portions of the site. The most prevalent invasive species at the DBS is multiflora rose (*Rosa multiflora*).

## **7.0 PERFORMANCE CRITERIA**

Monitoring shall consist of the collection and analysis of stream stability and riparian/stream bank vegetation survivability data to support the evaluation of the project in meeting established restoration objectives. Specifically, project success will be assessed utilizing measurements of stream dimension, pattern, and profile; site photographs, and vegetation sampling.

### **7.1 Stream Stability**

The purpose of monitoring is to evaluate the stability of the restored stream. Following the procedures established in the USDA Forest Service Manual, *Stream Channel Reference Sites* (Harrelson et al. 1994) and the methodologies utilized in the Rosgen stream assessment and classification system (1994 and

1996), data collected will consist of detailed dimension and pattern measurements, longitudinal profiles, and bed materials sampling.

**Dimension** – Permanent cross-sections will be established at 5 riffle and 4 pool locations along the restored project reaches. The following cross-sections will be used to evaluate stream dimension:

- 2 riffles and 2 pools on WOC-2
- 3 riffles and 2 pools on WOC-4

Permanent monuments will be established by conventional survey. The cross-section surveys shall provide a detailed measurement of the stream and banks and will include points on the adjacent floodplain or valley, at the top of bank, bankfull, at all breaks in slope, the edge of water, and thalweg. Width/depth and entrenchment ratios will be calculated for each cross-section based on the survey data.

Cross-section measurements should show little or no change from the as-built cross-sections. If changes do occur, they will be evaluated to determine whether they are minor adjustments associated with settling and increased stability or whether they indicate movement toward an unstable condition.

**Profile** – A detailed longitudinal profile will be conducted along the entire length of WOC. Measurements will include slopes (average, pool, and riffle) as well as calculations of pool-to-pool spacing. Annual measurements should indicate that bedform features are stable with little change from the as-built survey. The pools should maintain their depth with lower water surface slopes, while the riffles should remain shallower and steeper than the average values for the stream.

**Pattern** - Measurements associated with the channel pattern shall be taken on the restored sections of the stream included in the longitudinal profiles after the as-built survey. These data will include belt width, meander length, and radius of curvature. Subsequently, sinuosity, meander width ratios, radius of curvature, and meander length/bankfull width ratios will be calculated. Pattern data will only be calculated again if visual monitoring indicates that significant changes have occurred to the stream planform.

**Bed Materials** – Pebble counts will be conducted at each monitored cross-section for the purpose of repeated classification and to evaluate sediment transport.

**Verification of Bankfull Events** – During the monitoring period, a minimum of two bankfull events must be recorded within the five-year monitoring period. These two bankfull events must occur in separate monitoring years. Bankfull events will be verified using on-site gauges.

**Photograph Reference Points** – Twenty photograph reference points will be established to assist in characterizing the site and to allow qualitative evaluation of the site conditions. The location and bearing/orientation of each photo point will be documented to allow for repeated use.

**Cross-section Photograph Reference Points** – Each cross-section will be photographed to show the form of the channel with the tape measure stretched over the channel for reference in each photograph. An effort will be made to consistently show the same area in each photograph.

**Visual Assessment** – An annual site walk will be conducted at the end of each monitoring period to document any stream problem areas. Particular attention will be paid to the enhancement reaches and the two tributaries. Specific problem areas that could arise include excessive bank erosion, bed deposition or aggradation, or problems with the installed structures. The findings of the visual assessment as well as any recommended corrective actions for problem areas will be summarized in the monitoring reports by way of a Current Conditions Plan View figure.

## **7.2 Vegetation**

The success of the riparian buffer plantings will be evaluated using seven ten-by-ten meter vegetative sampling plots and will use the CVS-EEP stream vegetation monitoring protocol (Lee et al. 2006). The corners of each monitoring plot will be permanently marked in the field. The coordinates of the plot corners will be recorded using conventional survey. The monitoring will consist of the following data inventory: composition and number of surviving species, total number of stems per acre, diameter at decimeter height, diameter at breast height for trees greater than 5 feet in height, and vigor. Additionally, a photograph will be taken of each plot that will be replicated each monitoring year. Riparian vegetation must meet a minimum survival success rate of 320 stems/acre after three years, 288 stems/acre after four years, and 260 stems/acre after five years. If monitoring indicates that the specified survival rate is not being met, appropriate corrective actions will take place, which may include invasive species control, the removal of dead/dying plants and replanting.

## **7.3 Schedule/Reporting**

The first scheduled monitoring will be conducted during the first full growing season following project completion. Monitoring shall subsequently be conducted annually for a total period of five years or until the project meets its success criteria.

Annual monitoring reports will be prepared and submitted after all monitoring tasks for each year are completed. The report will document the monitored components of the restoration plan and include all collected data, analyses, and photographs. Each report will provide the new monitoring data and compare the most recent results against previous findings. The monitoring report format will be similar to that set out in the most recent EEP monitoring protocol.

Variations from the designed project reaches can be anticipated due to unknown site conditions, inputs from outside the restoration site, regional climatic variations, or acts of God, etc. Regular management activities will be implemented as necessary to ensure that the goals and objectives of the project are met. These activities will be conducted throughout the year and may include invasive species control or other management activities. If the monitoring identifies failures in the project site, a remedial action plan will be developed to investigate the causes of the failure and propose actions to rectify the problem.

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## Tables



**Table 1. Project Restoration Components**

Reach	Existing Stationing	Proposed Stationing	Mitigation Type	Priority Approach	Existing Linear Footage	Designed Linear Footage	Comments
WOC-1	10+00-12+54	10+00-12+54	Enhancement I	-	254	254	Excludes 15-ft crossing
WOC-2	12+71-19+19	12+71-19+25	Restoration	P3	633	639	Excludes 15-ft crossing
WOC-3	19+19-22+68	19+25-22+73	Enhancement I	-	349	349	Excludes 15-ft crossing
WOC-4	22+82-36+71	22+88-36+31	Restoration	P3	1,374	1,325	Excludes 15-ft crossing
WOC-5	36+71-41+29	36+31-40+89	Enhancement I	-	458	458	
T1-1	50+00-50+95	50+00-50+95	Enhancement I	-	95	95	
T1-2	50+95-54+48	50+95-54+69	Restoration	P3	336	359	Excludes 15-ft crossing
T2	60+00-62+19	60+00-62+57	Restoration	P3	219	257	
				Total	3,718	3,736	
Total Proposed Stream Enhancement I							<b>1,156</b>
Total Proposed Stream Restoration							<b>2,580</b>

**Table 2. Project Watershed Land Use**

Land Use	Acreage	Percentage of Watershed
Agriculture	6.8	2%
Forest land	273.6	80%
Rangeland	58.1	17%
Wetland	0.7	< 1%
Water	1.3	< 1%
Urban or built-up	1.5	< 1%

**Table 3. Project Drainage Areas**

Reach	Drainage Area (Acres)	Drainage Areas (Square Miles)
WOC	342.4	0.535
T1	48.4	0.076
T2	45.8	0.072

**Table 4A. Morphological Criteria for WOC-1, WOC-2, and WOC-3**

Variables	Existing	Existing	Existing	Ref. Reach	Ref. Reach	Proposed	Proposed	Proposed
	WOC-1*	WOC-2**	WOC-3 <sup>+</sup>			WOC-1 <sup>++</sup>	WOC-2	WOC-3
Rosgen Stream Type	F5b	E/B4a	B4a	B4c	B4a	B4a	B4a	B4a
Mitigation Type	Enh. I	Restoration	Enh. I	N/A	N/A	Enh. I	Restoration	Enh. I
Drainage Area ( $\text{mi}^2$ )	0.23	0.36	0.38	0.38	0.23	0.23	0.36	0.38
Bankfull Width ( $W_{\text{bfk}}$ ) (ft)	8.8-9.7	5.0-8.3	14.2	9.0-10.0	8.8	8.6	8.6	9.0
Bankfull Mean Depth ( $d_{\text{bfk}}$ ) (ft)	0.5-0.6	0.6-0.9	0.5	1.1-1.2	0.6	0.7	0.7	0.7
Bankfull Cross-Sectional area ( $A_{\text{bfk}}$ ) ( $\text{ft}^2$ )	4.9-5.0	4.6-6.7	7.1	10.4-10.7	5.1	6.3	6.3	6.6
Width/depth Ratio ( $W_{\text{bfk}}/d_{\text{bfk}}$ )	15.8-18.8	5.4-13.8	28.4	8.0-10.0	15.2	12.3	12.3	12.3
Maximum Depth ( $d_{\text{mbkf}}$ ) (ft)	0.7	0.8-1.4	0.8	1.3-1.5	0.9	0.9	0.9	0.9
Width of flood prone area ( $W_{\text{fpa}}$ ) (ft)	10-11	9-11	25	13-21	12	19	19	19
Entrenchment Ratio (ER)	1.1-1.2	1.2-2.1	1.8	1.3-2.3	1.4	2.2	2.2	2.1
Sinuosity (stream length/valley length) (K)	1.0	1.0	1.0	1.2	-	1.0	1.0	1.0
Dimension	Pool Depth (ft)	-	-	0.7	1.2-1.4	-	1.0	1.0
	Riffle Depth (ft)	0.5-0.6	0.6-0.9	0.5	1.1-1.2	0.6	0.7	0.7
	Max Pool Depth (ft)	-	-	1.3	2.1-2.4	-	1.6	1.6
	Pool Width (ft)	-	-	19.8	8.4-11.6	-	10.2	10.2
	Riffle Width (ft)	8.8-9.7	5.0-8.3	14.2	9.0-9.9	8.8	8.6	8.6
	Pool XS Area (sf)	-	-	14.2	11.6-13.4	-	10.1	10.1
	Riffle XS Area (sf)	4.9-5.0	4.6-6.7	7.1	10.4-10.7	5.1	6.3	6.6
	Pool depth/mean riffle depth	-	-	1.4	1.0-1.3	-	1.4	1.4
	Pool width/riffle width	-	-	1.4	0.8-1.3	-	1.2	1.2
	Pool area/riffle area	-	-	2.0	1.1-1.3	-	1.6	1.6
	Max pool depth/ $d_{\text{bfk}}$	-	-	2.6	1.9-2.0	-	2.3	2.3
	Bank Height Ratio (BHR)	3.3-4.2	1.6-2.6	3.8	1.0	1.1	1.0	1.0
	Mean Bankfull Velocity (V) (fps)	6.3-6.7	6.2-7.9	4.6-5.4	4.1-4.5	6.7	7.1	6.4
	Bankfull Discharge (Q) (cfs)	31-33	31-53	33	42-46	34	40	40
Pattern	Meander length ( $L_m$ ) (ft)	-	32-45	39	93-136	-	-	80-140
	Radius of curvature ( $R_c$ ) (ft)	-	8-15	8	13-42	-	-	15-30
	Belt width ( $W_{\text{blt}}$ ) (ft)	20	21	18	45	-	20	15-30
	Meander width ratio ( $W_{\text{blt}}/W_{\text{bfk}}$ )	2.1-2.3	2.5-4.2	1.3	4.5-5.0	-	2.1-2.3	1.7-3.5
	Radius of curvature/bankfull width	-	1.0-3.0	0.6	1.3-4.4	-	-	1.7-3.5
	Meander length/bankfull width	-	3.9-9.0	2.7	9.0-15.0	-	-	9.3-16.3
Profile	Valley slope	0.0780	0.0585	0.0440	0.0160	-	0.0780	0.0585
	Average water surface slope	0.0754	0.0617	0.0406	0.0130	-	0.0754	0.0593
	Riffle slope	0.0440-0.0989	0.0301-0.0898	0.0407-0.0571	0.013-0.028	-	0.0549-0.1071	0.0430-0.0741
	Pool slope	-	-	-	0-0.0010	-	0-0.0030	0-0.0030
	Pool to pool spacing	-	-	117	30-59	-	45-52	25-78
	Pool length	-	-	-	3-25	-	6-8	5-8
	Riffle slope/avg water surface slope	0.58-1.31	0.49-1.46	1.00-1.41	1.00-2.20	-	0.73-1.42	0.73-1.25
	Pool slope/avg water surface slope	-	-	-	0	-	0-0.04	0-0.05
	Pool length/bankfull width	-	-	-	0.3-2.5	-	0.7-0.9	0.6-0.9
	Pool to pool spacing/bankfull width	-	-	8.2	3.3-6.0	-	5.2-6.0	2.9-9.1

\*WOC-1 is not a meandering channel and is only composed of riffles and runs, therefore no pattern data or pool data were collected.

\*\*WOC-2 is only composed of riffles and runs, therefore no pool data were collected.

<sup>+</sup> A pool cross-section was surveyed for WOC-3 but there were no pools in the representative profile, therefore no pool profile data were collected.

<sup>++</sup> Since WOC-1 will be enhanced there will not be any pattern adjustments so the proposed pattern data is the same as the existing pattern data.

**Table 4B. Morphological Criteria for WOC-4 and WOC-5**

Variables	Existing	Existing	Ref. Reach UTFR	Ref. Reach	Proposed	Proposed	
	WOC-4*	WOC-5*		WOC	WOC-4	WOC-5	
Rosgen Stream Type	G/F4b	C/B4	B4c	B4a	B4a	B4	
Mitigation Type	Restoration	Enh. I	N/A	N/A	Restoration	Enh. I	
Drainage Area ( $\text{mi}^2$ )	0.5	0.5	0.4	0.2	0.5	0.5	
Bankfull Width ( $W_{\text{bkf}}$ ) (ft)	9.2-10.6	13.7-27.2	9.0-10.0	8.8	9.8	10.6	
Bankfull Mean Depth ( $d_{\text{bkf}}$ ) (ft)	0.6-0.9	0.4-0.6	1.1-1.2	0.6	0.8	0.8	
Bankfull Cross-Sectional area ( $A_{\text{bkf}}$ ) ( $\text{ft}^2$ )	6.4-7.9	8.1-11.7	10.4-10.7	5.1	7.7	8.9	
Width/depth Ratio ( $W_{\text{bkf}}/d_{\text{bkf}}$ )	10.7-17.2	23.2-63.2	8.0-10.0	15.2	12.5	12.6	
Maximum Depth ( $d_{\text{mbkf}}$ ) (ft)	0.9-1.3	1.0-1.5	1.3-1.5	0.9	1.0	1.1	
Width of flood prone area ( $W_{\text{fpa}}$ ) (ft)	12-21	18-97	13-21	12	20	22	
Entrenchment Ratio (ER)	1.1-2.0	1.3-3.6	1.3-2.3	1.4	2.0	2.1	
Sinuosity (stream length/valley length) (K)	1.1	1.0	1.2	-	1.1	1.0	
<i>Dimension</i>	Pool Depth (ft)	-	-	1.2-1.4	-	1.2	1.3
	Riffle Depth (ft)	0.6-0.9	0.4-0.6	1.1-1.2	0.6	0.8	0.8
	Max Pool Depth (ft)	-	-	2.1-2.4	-	1.8	2.0
	Pool Width (ft)	-	-	8.4-11.6	-	11.0	11.8
	Riffle Width (ft)	9.2-10.6	13.7-27.2	9.0-9.9	8.8	9.8	10.6
	Pool XS Area (sf)	-	-	11.6-13.4	-	13.5	15.8
	Riffle XS Area (sf)	6.4-7.9	8.1-11.7	10.4-10.7	5.1	7.7	8.9
	Pool depth/mean riffle depth	-	-	1.0-1.3	-	1.5	1.6
	Pool width/riffle width	-	-	0.8-1.3	-	1.1	1.1
	Pool area/riffle area	-	-	1.1-1.3	-	1.8	1.8
	Max pool depth/ $d_{\text{bkf}}$	-	-	1.9-2.0	-	2.3	2.5
	Bank Height Ratio (BHR)	1.8-3.7	1.4-3.1	1.0	1.1	1.0	1.0
	Mean Bankfull Velocity (V) (fps)	5.1-6.9	3.8-4.7	4.1-4.5	6.7	5.5	5.0
	Bankfull Discharge (Q) (cfs)	33-51	38-45	42-46	34	40	40
<i>Pattern</i>	Meander length ( $L_m$ ) (ft)	81-244	84-106	93-136	-	95-160	84-106
	Radius of curvature ( $R_c$ ) (ft)	14-52	20-24	13-42	-	20-40	20-24
	Belt width ( $W_{\text{blt}}$ ) (ft)	31-80	34	45	-	15-40	34
	Meander width ratio ( $W_{\text{blt}}/W_{\text{bkf}}$ )	2.9-8.7	1.3-2.5	4.5-5.0	-	1.5-4.1	3.2
	Radius of curvature/bankfull width	1.3-5.7	0.7-1.8	1.3-4.4	-	2.0-4.1	1.9-2.3
	Meander length/bankfull width	7.6-26.5	3.1-7.7	9.0-15.0	-	9.7-16.3	7.9-10.0
<i>Profile</i>	Valley slope	0.0434	0.0331	0.0160	-	0.0434	0.0331
	Average water surface slope	0.0399	0.0335	0.0130	-	0.0405	0.0323
	Riffle slope	0.0410-0.0767	0.0357-0.0653	0.013-0.028	-	0.0321-0.0638	0.0152-0.0667
	Pool slope	0	0-0.0022	0-0.0010	-	0-0.0030	0-0.0030
	Pool to pool spacing	231	27-35	30-59	-	30-83	32-83
	Pool length	7-14	5-9	3-25	-	5-16	7-9
	Riffle slope/avg water surface slope	1.03-1.92	1.07-1.95	1.00-2.20	-	0.79-1.58	0.47-2.10
	Pool slope/avg water surface slope	0	0-0.07	0	-	0-0.07	0-0.09
	Pool length/bankfull width	0.7-1.5	0.2-0.7	0.3-2.5	-	0.5-1.6	0.7-0.8
	Pool to pool spacing/bankfull width	21.8-25.1	1.0-2.6	3.3-6.0	-	3.1-8.5	3.0-7.8

\* No pool cross-sections were surveyed, but pools were identified on the longitudinal survey.

**Table 4C. Morphological Criteria for T1 and T2**

Variables	Existing	Existing	Existing	Ref. Reach UTFR	Ref. Reach WOC	Proposed	Proposed	Proposed
	T1-1*	T1-2**	T2 <sup>+</sup>			T1-1 <sup>++</sup>	T1-2	T2
Rosgen Stream Type	B/G4	B5a	B/G5	B4c	B4a	B4a	B4a	B4a
Mitigation Type	Enh. I	Restoration	Restoration	N/A	N/A	Enh. I	Restoration	Restoration
Drainage Area (mi <sup>2</sup> )	0.08	0.08	0.07	0.38	0.23	0.08	0.08	0.07
Bankfull Width (W <sub>bkf</sub> ) (ft)	5.7	19.5	6.6	9.0-10.0	8.8	6.6	6.6	6.2
Bankfull Mean Depth (d <sub>bkf</sub> ) (ft)	0.4	0.3	0.4	1.1-1.2	0.6	0.5	0.5	0.5
Bankfull Cross-Sectional area (A <sub>bkf</sub> ) (ft <sup>2</sup> )	2.3	6.5	2.5	10.4-10.7	5.1	3.2	3.2	3.0
Width/depth Ratio (W <sub>bkf</sub> /d <sub>bkf</sub> )	14.1	58.5	17.4	8.0-10.0	15.2	13.6	13.6	12.4
Maximum Depth (d <sub>mbkf</sub> ) (ft)	0.6	0.8	0.6	1.3-1.5	0.9	0.6	0.6	0.6
Width of flood prone area (W <sub>fpa</sub> ) (ft)	8	38	10	13-21	12	14	14	13
Entrenchment Ratio (ER)	1.4	1.9	1.5	1.3-2.3	1.4	2.1	2.1	2.1
Sinuosity (stream length/valley length) (K)	1.1	1.0	1.1	1.2	-	1.1	1.1	1.1
Dimension	Pool Depth (ft)	-	-	-	1.2-1.4	-	0.8	0.8
	Riffle Depth (ft)	0.4	0.3	0.4	1.1-1.2	0.6	0.5	0.5
	Max Pool Depth (ft)	-	-	-	2.1-2.4	-	1.2	1.2
	Pool Width (ft)	-	-	-	8.4-11.6	-	7.4	7.4
	Riffle Width (ft)	5.7	19.5	6.6	9.0-9.9	8.8	6.6	6.2
	Pool XS Area (sf)	-	-	-	11.6-13.4	-	5.8	5.8
	Riffle XS Area (sf)	2.3	6.5	2.5	10.4-10.7	5.1	3.2	3.0
	Pool depth/mean riffle depth	-	-	-	1.0-1.3	-	1.6	1.6
	Pool width/riffle width	-	-	-	0.8-1.3	-	1.1	1.1
	Pool area/riffle area	-	-	-	1.1-1.3	-	1.8	1.8
	Max pool depth/d <sub>bkf</sub>	-	-	-	1.9-2.0	-	2.4	2.4
	Bank Height Ratio (BHR)	3.6	-	4.2	1.0	1.1	1.0	1.0
	Mean Bankfull Velocity (V) (fps)	5.9	-	6.5	4.1-4.5	6.7	5.2	4.9
	Bankfull Discharge (Q) (cfs)	14	-	16.4	42-46	34	14	14
Pattern	Meander length (L <sub>m</sub> ) (ft)	-	-	-	93-136	-	-	70-105
	Radius of curvature (R <sub>c</sub> ) (ft)	-	-	-	13-42	-	-	10-25
	Belt width (W <sub>blt</sub> ) (ft)	-	-	-	45	-	-	15-30
	Meander width ratio (W <sub>blt</sub> /W <sub>bkf</sub> )	-	-	-	4.5-5.0	-	-	2.3-4.5
	Radius of curvature/bankfull width	-	-	-	1.3-4.4	-	-	1.5-3.8
	Meander length/bankfull width	-	-	-	9.0-15.0	-	-	10.6-15.9
Profile	Valley slope	0.0737	0.0583	0.1153	0.016	-	0.0750	0.0590
	Average water surface slope	0.0681	0.0601	0.1129	0.013	-	0.0750	0.0590
	Riffle slope	0.0721-0.0874	-	-	0.013-0.028	-	0.0764-0.0876	0.0497-0.0579
	Pool slope	-	-	-	0-0.0010	-	0-0.0030	0-0.0030
	Pool to pool spacing	-	-	-	30-59	-	76	35-45
	Pool length	-	-	-	3-25	-	9	5-17
	Riffle slope/avg water surface slope	1.06-1.28	-	-	1.00-2.20	-	1.02-1.17	0.84-0.98
	Pool slope/avg water surface slope	-	-	-	0	-	0-0.04	0-0.05
	Pool length/bankfull width	-	-	-	0.3-2.5	-	1.4	0.8-2.6
	Pool to pool spacing/bankfull width	-	-	-	3.3-6.0	-	11.5	5.3-6.8

\*T1-1 is not a meandering channel and is only composed of riffles and runs, therefore no pattern data or pool data were collected.

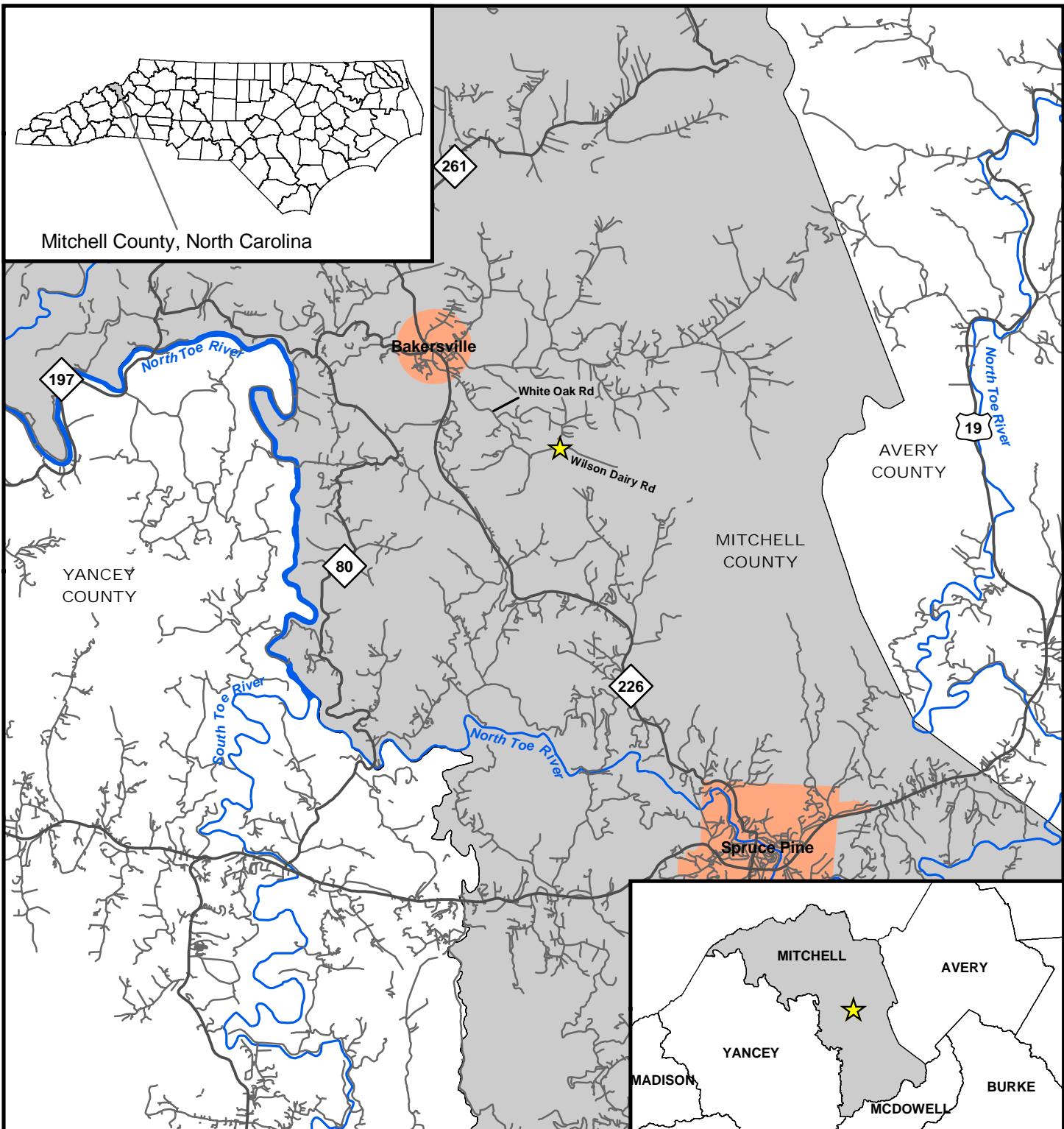
\*\*T1-2 is not a meandering channel and does not have a well defined channel with distinct bed features, therefore no pattern data were collected and only limited dimension and profile data were collected.

+T2 is not a meandering channel and does not have distinct bed features, therefore no pattern data were collected and only limited dimension and profile data were collected.

++ Since T1-1 will be enhanced there will not be any pattern adjustments so the proposed pattern data is the same as the existing pattern data.

## Figures





**Figure 1. Vicinity Map**

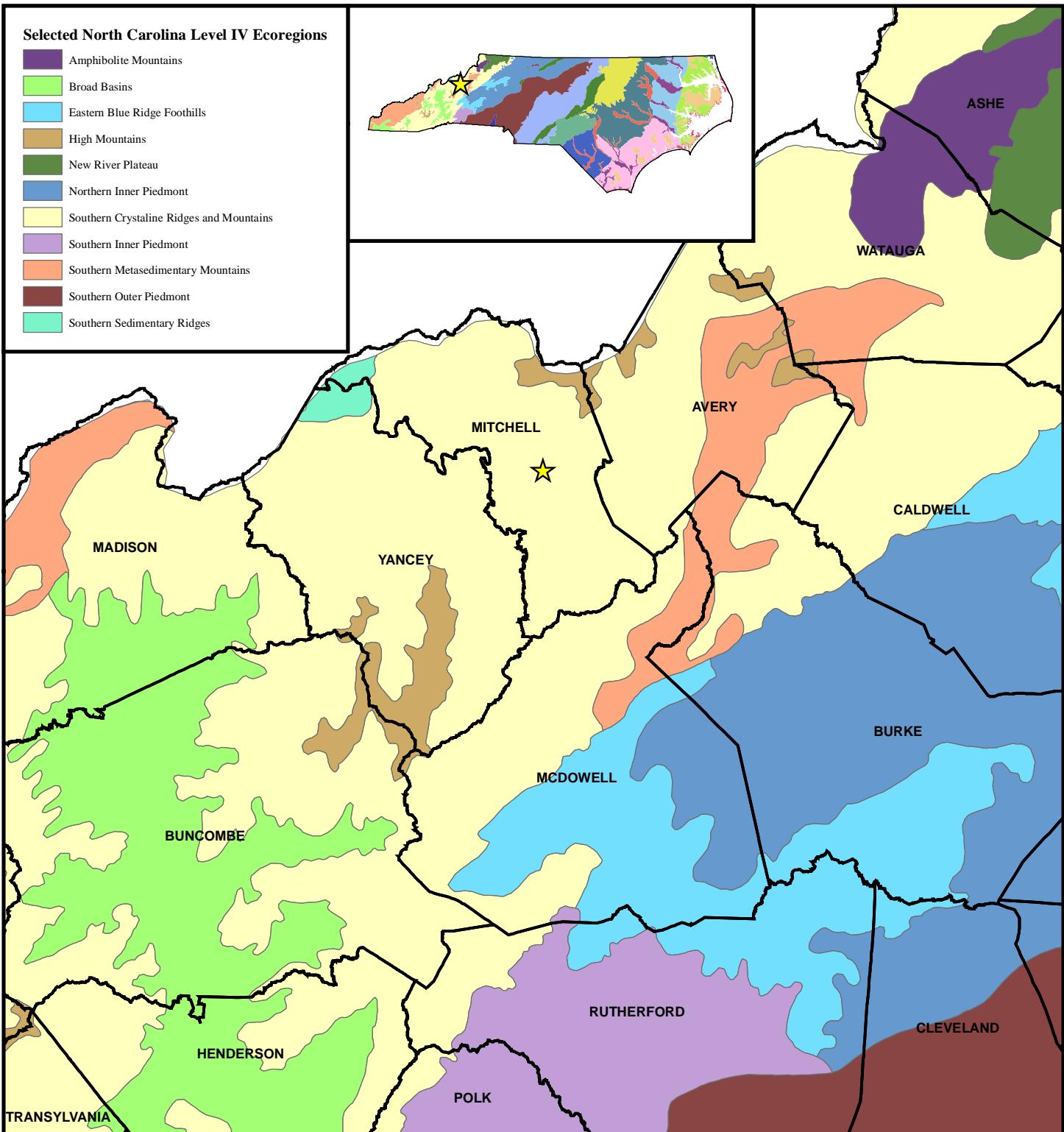
- ★ Project Site Location
- Major Roads
- Other Roads
- ~~~~~ Major Rivers
- Cities and Towns



1:126,720

1 inch equals 2 miles

2 1 0 2 Miles



**Figure 2. North Carolina Ecoregions**



Project Site Location



County Boundaries



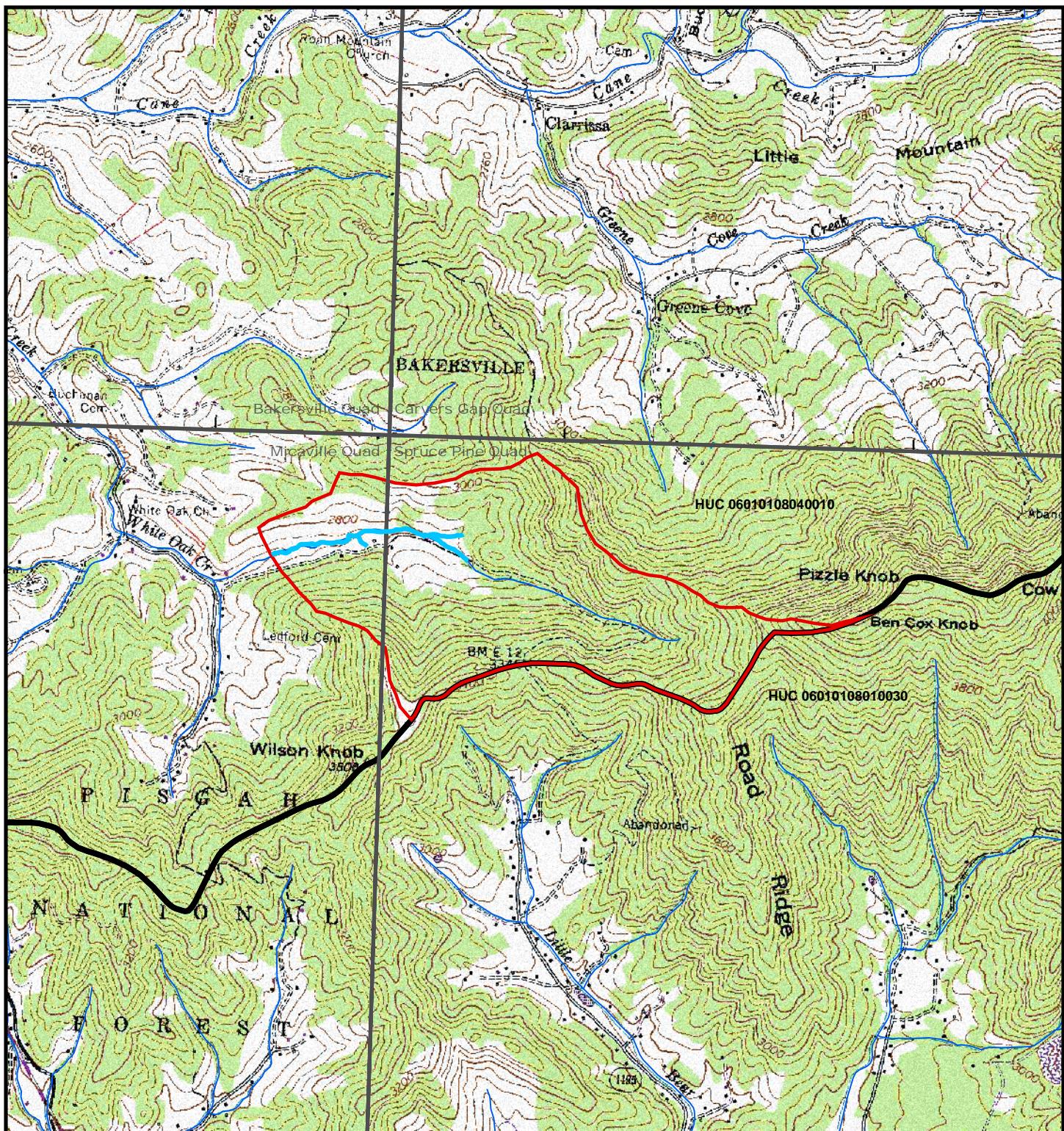
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1 inch equals 10 miles

10      5      0      10  
Miles

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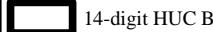




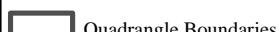
**Figure 3. Project Watershed**

 Project Watershed (0.53 sq. mile)

 14-digit HUC Boundaries

 Project Streams

 Other Streams

 Quadrangle Boundaries

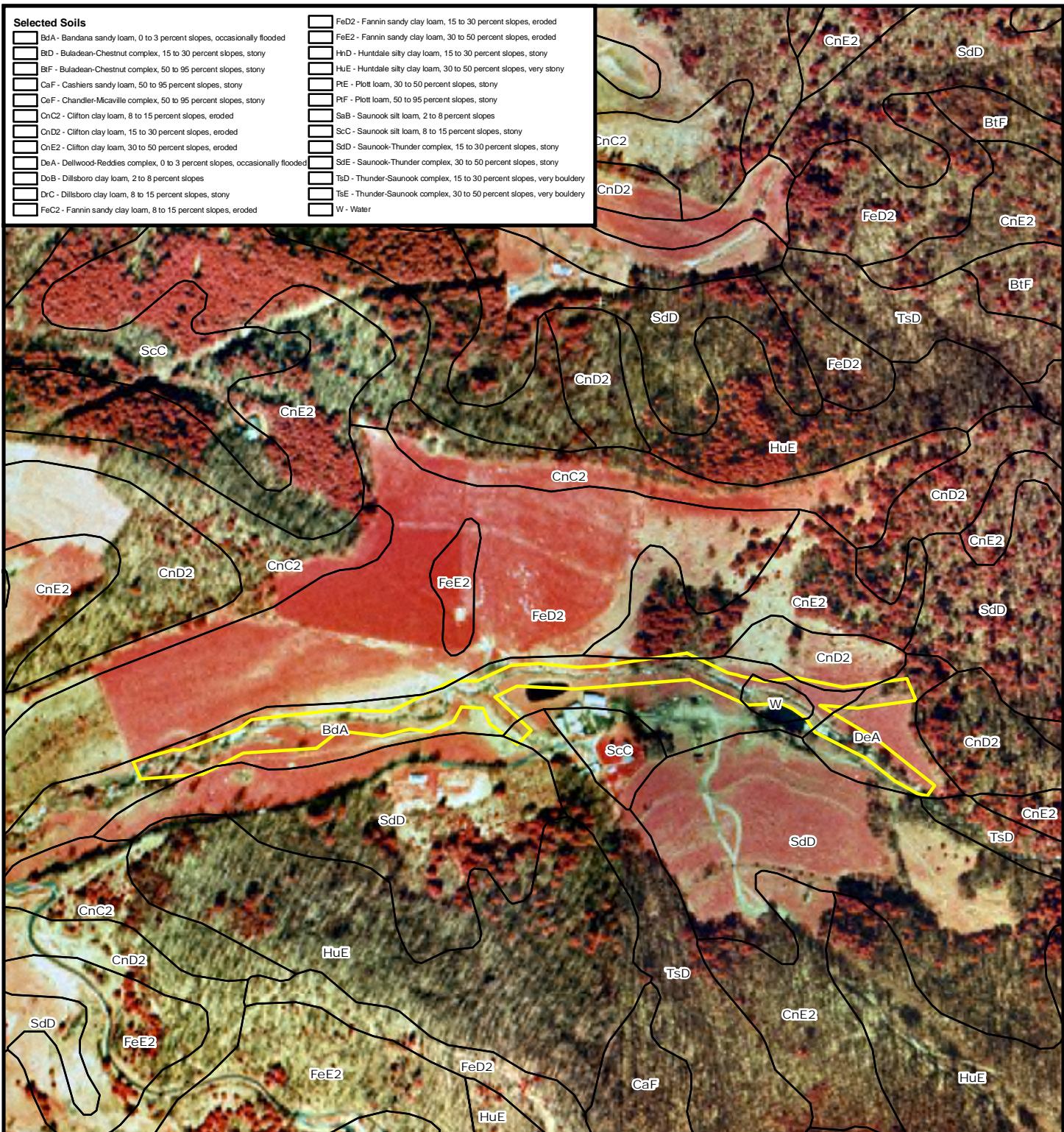
Source: USGS Topographic Quadrangles  
Bakersville (1978), Carvers Gap (1960),  
Micaville (1978), and Spruce Pine (1978)



1:24,000

1 inch equals 2,000 feet

2,000 1,000 0 2,000  
Feet



**Figure 4. Project Site NRCS Soil Survey**



**K C I**  
TECHNOLOGIES

Project Easement Boundary

Source: SSURGO Dataset for Mitchell County based on  
Soil Survey of Mitchell County, NC, USDA NRCS, 2004;  
imagery from USGS DOQs 1998.

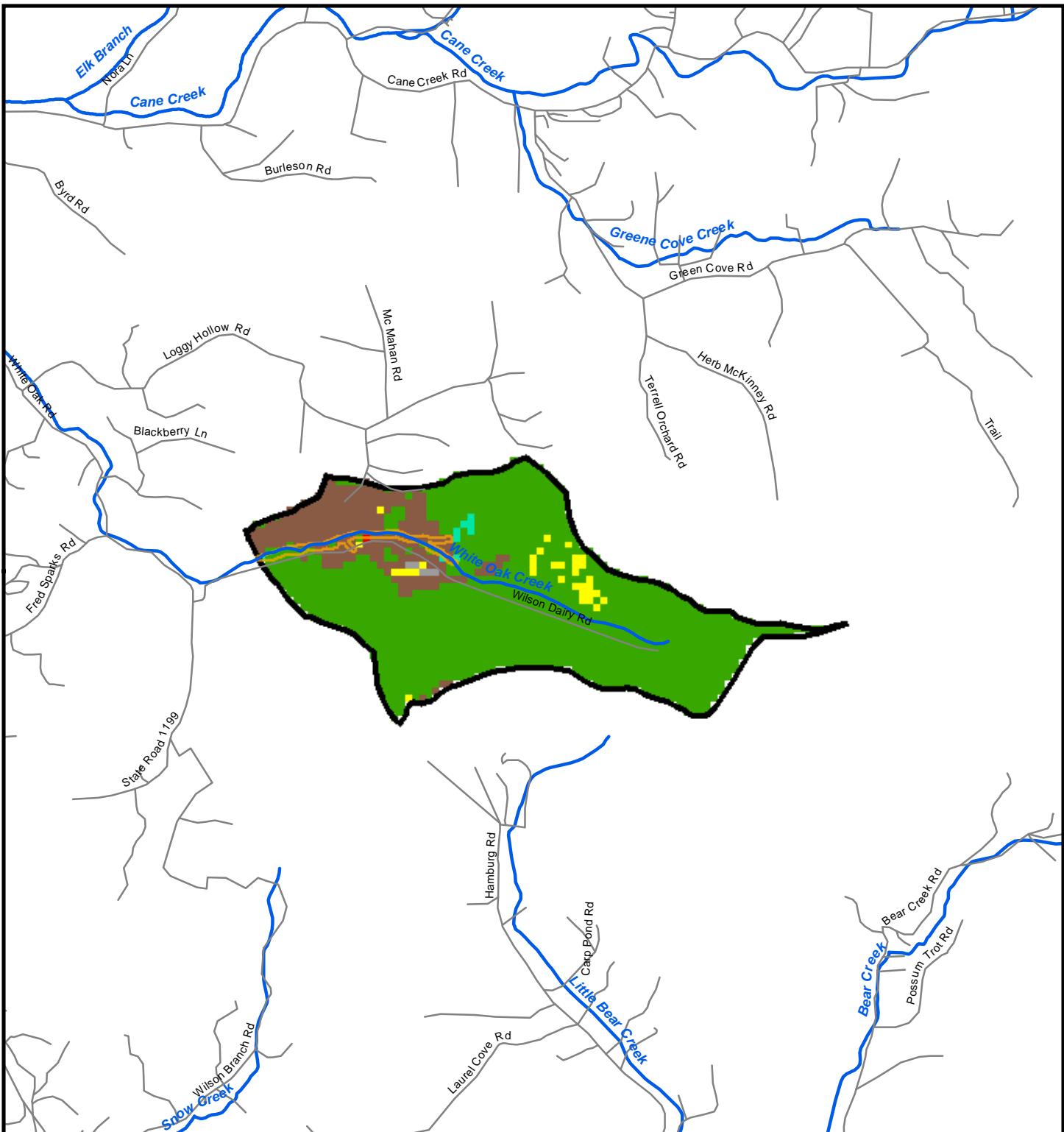


1:6,000

1 inch equals 500 feet

500 250 0 500





**Figure 5. Project Watershed Land Use**

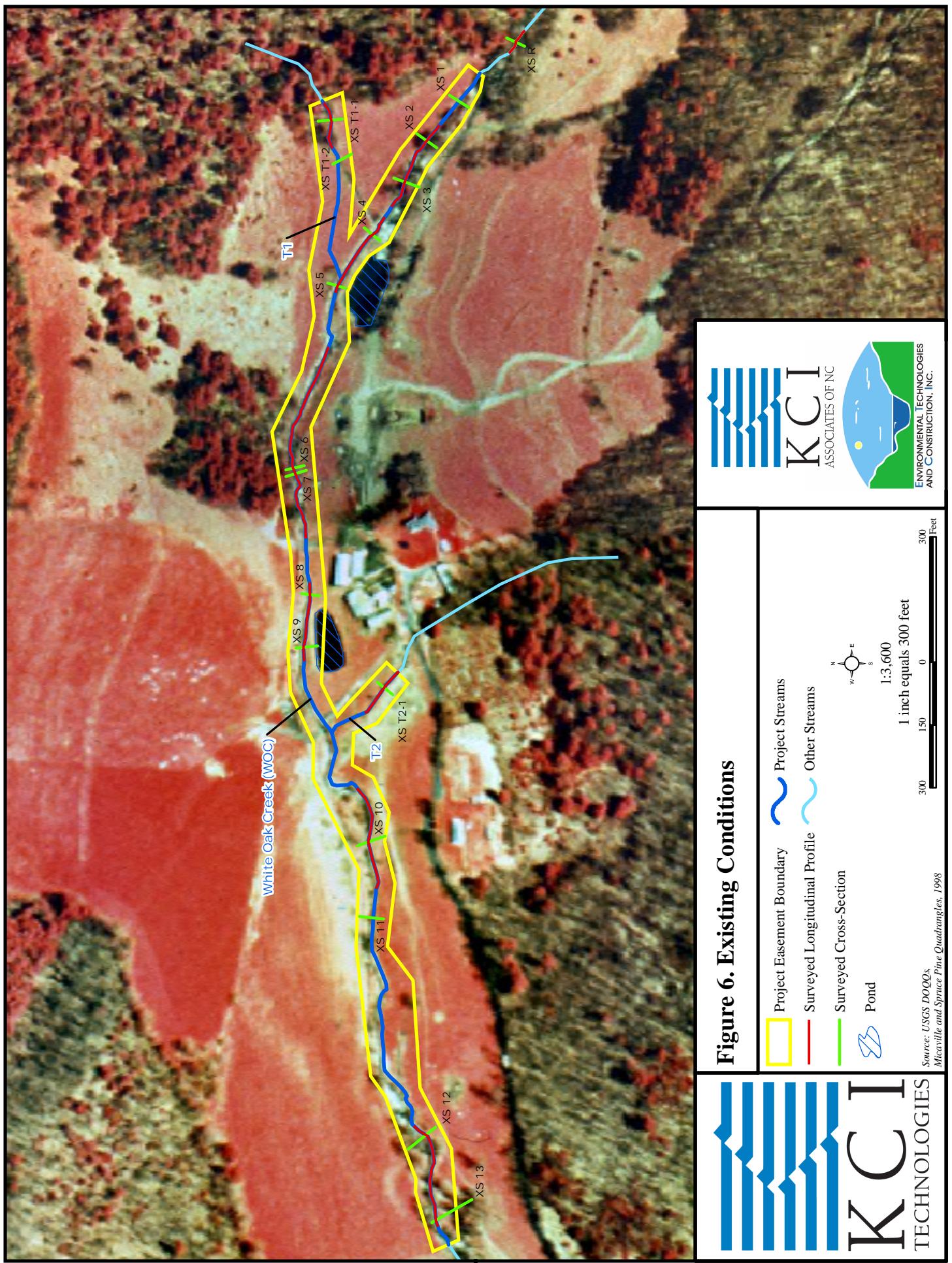


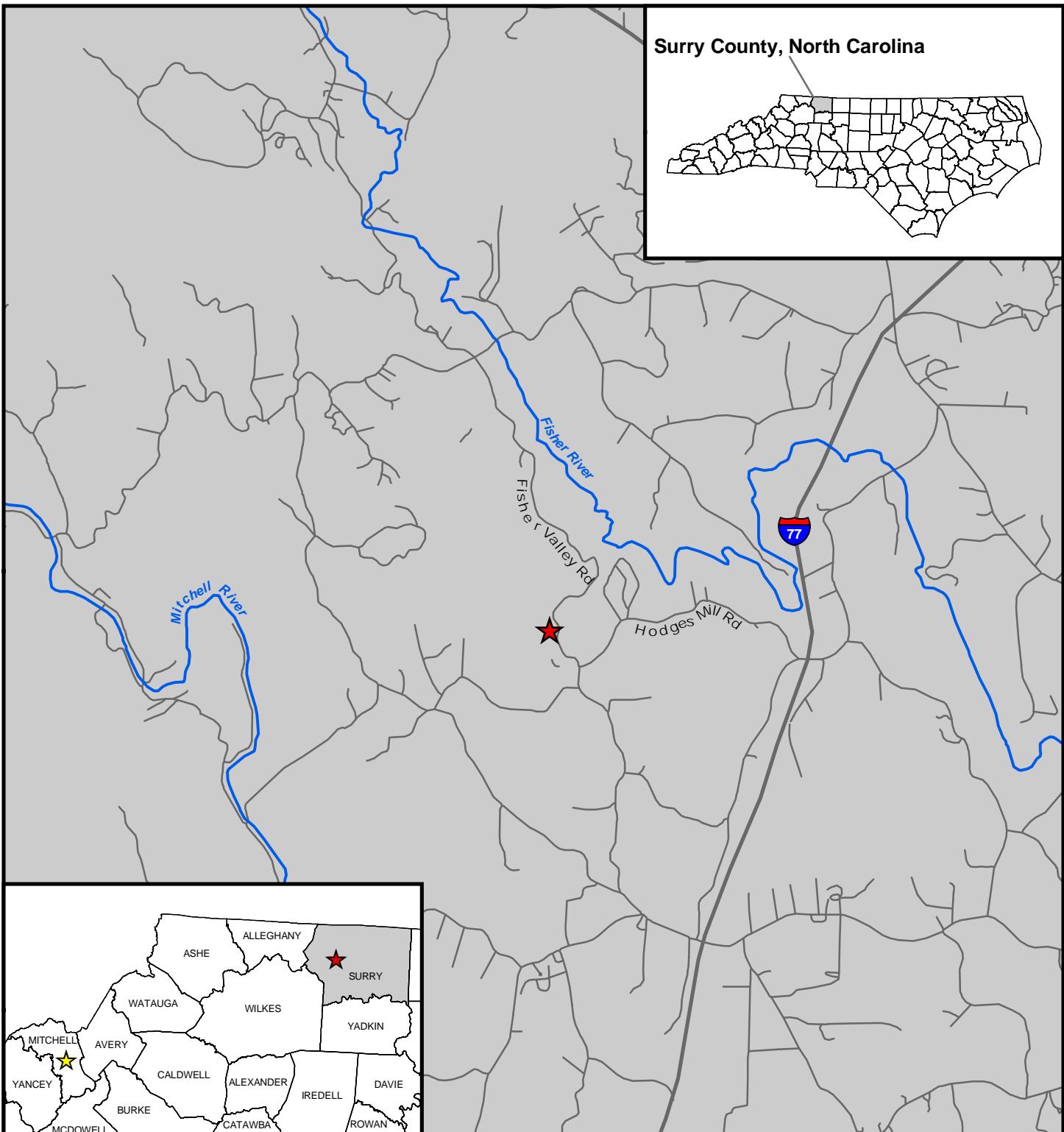
Source: NC GAP Land Cover Dataset  
Using Anderson I Classification Scheme

Urban or Built-Up Land	Project Watershed
Agriculture	Project Easement Boundary
Rangeland	Roads
Forest Land	Streams
Wetland	
Barren Land	

N  
W S E  
1:24,000  
1 inch equals 2,000 feet  
2,000 1,000 0 2,000  
Feet







**Figure 7. Reference Site Vicinity Map (UT to Fisher River)**

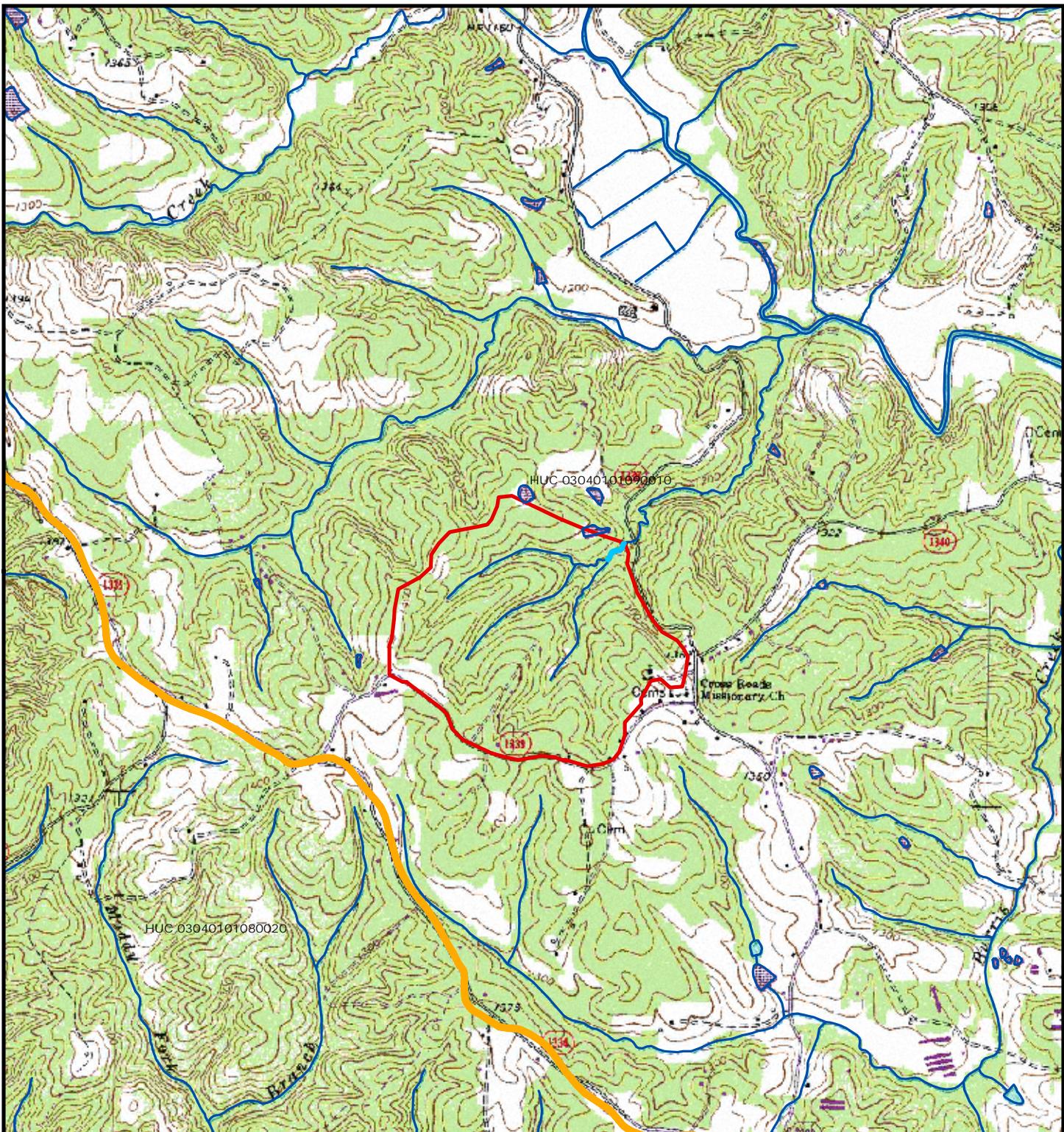
- Project Site
- Reference Site (UT to Fisher River)
- Major Streams
- Major Roads
- Other Roads
- County Boundaries



1:63,360

1 inch equals 1 miles

1 0.5 0 1  
Miles



**Figure 8. Reference Site Watershed (UT to Fisher River)**

Reference Reach Watershed (0.38 sq. mile)

14-digit HUC boundaries

Reference Reach (UT to Fisher River)

Other Streams



1:24,000

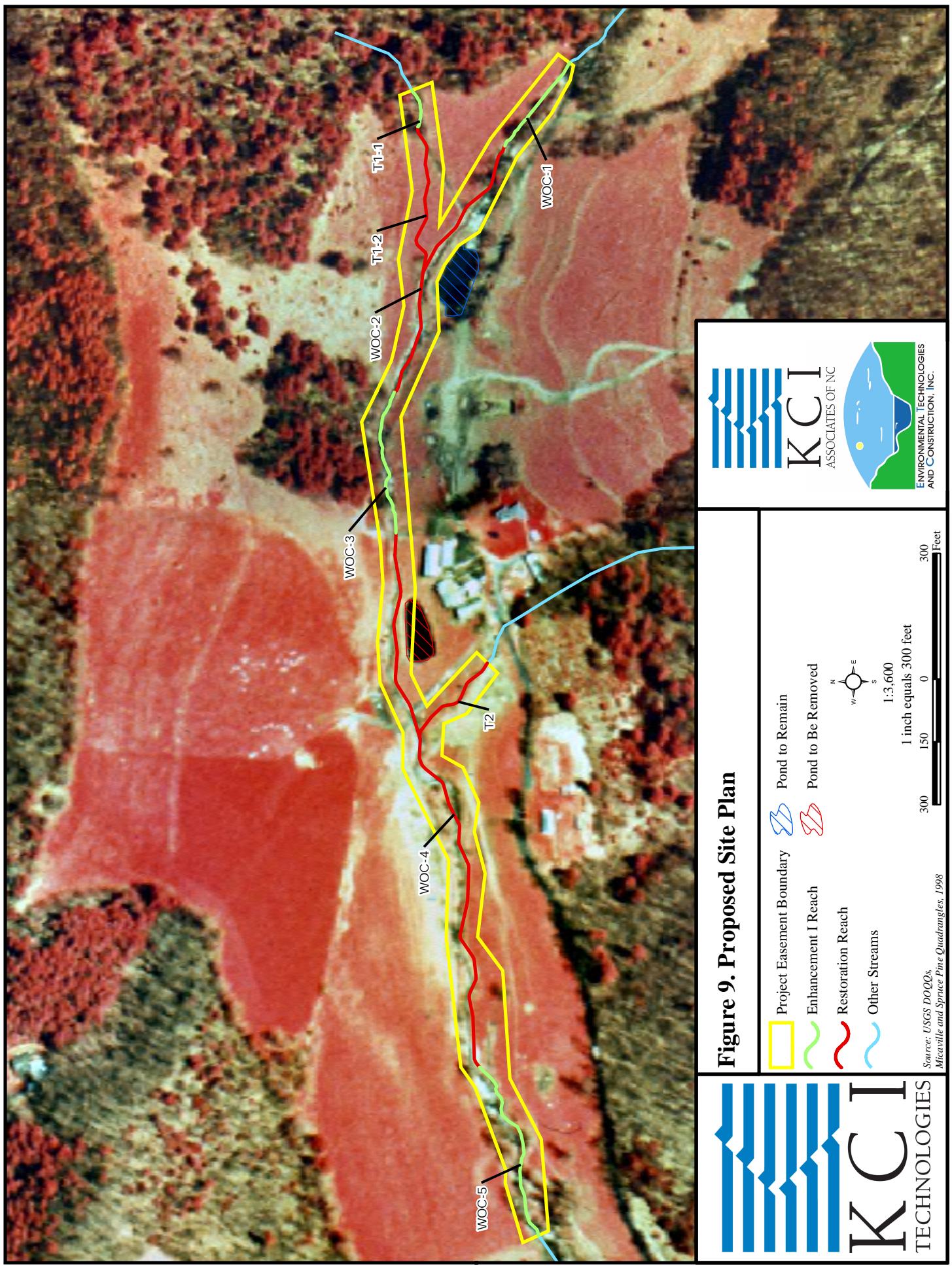
1 inch equals 2,000 feet

2,000 1,000 0 2,000  
Feet

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Source: USGS Topographic Quadrangle Bottom (1971)

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AND CONSTRUCTION, INC.





## Stream Plan Sheets



# CONTRACT #: D06056-A

KCI JOB# : 12065439



**VICINITY MAP**  
NOT TO SCALE

**DIRECTIONS TO SITE**

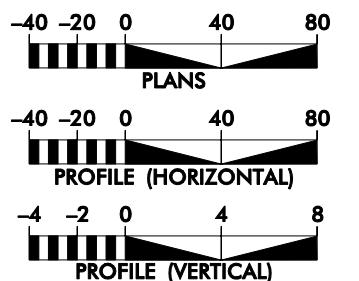
TO REACH THE SITE FROM RALEIGH, BEGIN BY PROCEEDING WEST ON I-40 FOR APPROXIMATELY 200 MILES. THEN TAKE EXIT 86 FOR NC-226 TOWARD SHELBY/MARION. TAKE A RIGHT ONTO NC-226, TRAVELING NORTH. FOLLOW NC-226 THROUGH MARION AND SPRUCE PINE. JUST BEFORE REACHING BAKERSVILLE, MAKE A RIGHT ONTO WHITE OAK ROAD. FOLLOW WHITE OAK ROAD FOR APPROXIMATELY 1.5 MILE AND THEN MAKE A LEFT ONTO WILSON DAIRY ROAD. THE ROAD WILL DEAD END AT THE WILSON PROPERTY AND THE DOG BITE SITE IS ON THE LEFT.

**INDEX OF SHEETS**

- \* 1 TITLE SHEET
- \* 1A PROJECT LEGEND
- \* 2 THRU 2A DETAILS: STABILIZATION
- \* 3 THRU 3A DETAILS: TYPICAL CROSS-SECTIONS
- \* 4 THRU 8 PLAN AND PROFILE
- 9 THRU 11 PLANTING PLAN
- \* 12 THRU 16 SEDIMENTATION & EROSION CONTROL PLAN

\* INCLUDED IN RESTORATION PLAN

**GRAPHIC SCALES**



**PROJECT DATA**

STREAM RESTORATION LENGTH = 2,580 FEET  
STREAM ENHANCEMENT LENGTH = 1,156 FEET

Prepared in the Office of:  
**KCI**  
TECHNOLOGIES  
ENGINEERS • PLANNERS • ECOLOGISTS  
SUITE 220, LANDMARK CENTER II  
460 SIX FORKS RD., RALEIGH, NC

GARY M. MRYNCZA, PE  
PROJECT ENGINEER  
  
ADAM SPILLER  
NATURAL CHANNEL DESIGN  
  
SIGNATURE: \_\_\_\_\_  
P.E.

**PROJECT ENGINEER**

Prepared for:

**Ecosystem Enhancement**  
PROGRAM  
GUY PEARCE  
CONTRACT ADMINISTRATOR

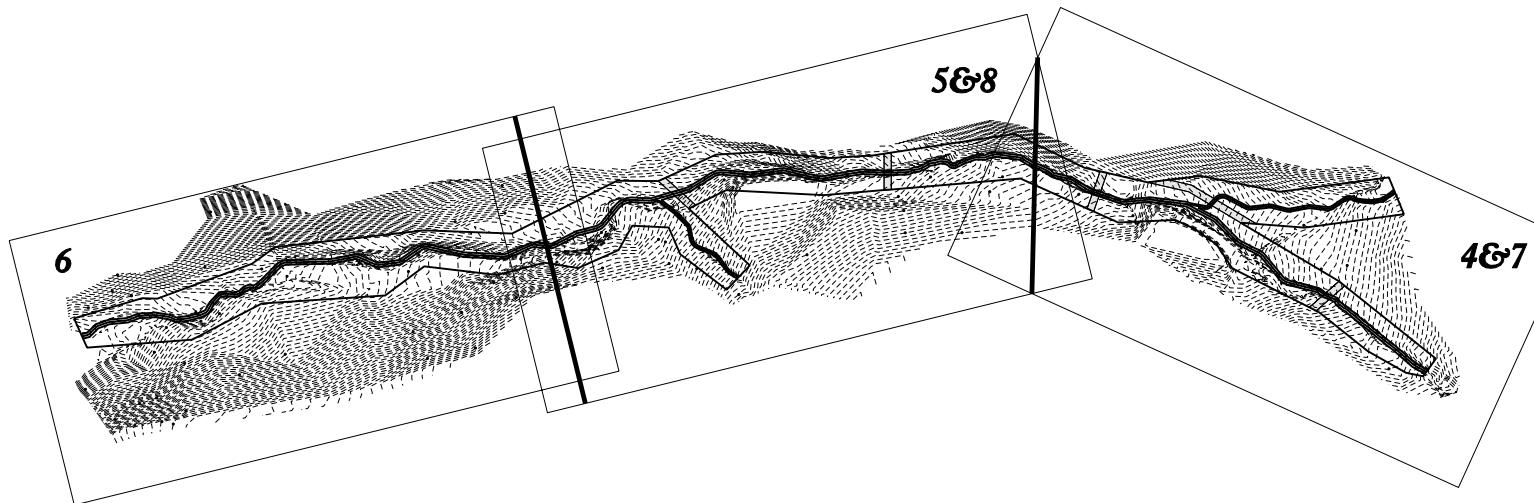
# STATE OF NORTH CAROLINA ECOSYSTEM ENHANCEMENT PROGRAM

STATE	CONTRACT NUMBER	SHEET NO.	TOTAL SHEETS
N.C.	D06056-A	1	19

A	SUBMITTED WITH RESTORATION PLAN	JULY 2008
SYN.	DESCRIPTION	DATE APPROVED
	REVISIONS	

# Mitchell County

**LOCATION: DOG BITE SITE  
WHITE OAK CREEK  
BAKERSVILLE, NORTH CAROLINA**  
**TYPE OF WORK: STREAM RESTORATION AND ENHANCEMENT**

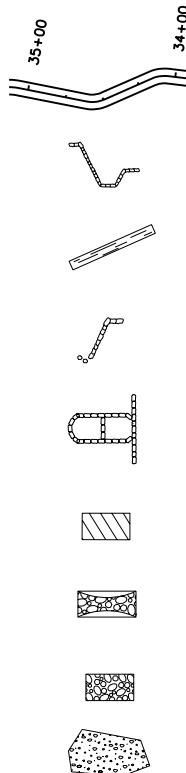


NC GRID  
NAD 83

# PROJECT LEGEND

## STREAM RESTORATION

- Proposed Stationed Thalweg w/Aproximate Bankfull Limits .....
- Proposed Offset Rock Cross Vane .....
- Log Sill Grade Control .....
- J-Hook /Log Vane /Root Wad .....
- Proposed Log Step or Step Pool .....
- Proposed Channel Block .....
- Proposed Riffle Grade Control .....
- Proposed Rock Ford Crossing .....
- Proposed Stone Stabilization .....



## TOPOGRAPHY

- Minor Contour Line .....
- Major Contour Line .....

## SEDIMENT & EROSION CONTROL

- Stabilized Construction Entrance .....
- Silt Fence .....
- Limits of Disturbance .....
- Temporary Stream Crossing .....
- Silt Fence Rock Outlet .....
- Rock Silt Screen (Std. Drawing 1636.01) .....

## MISCELLANEOUS

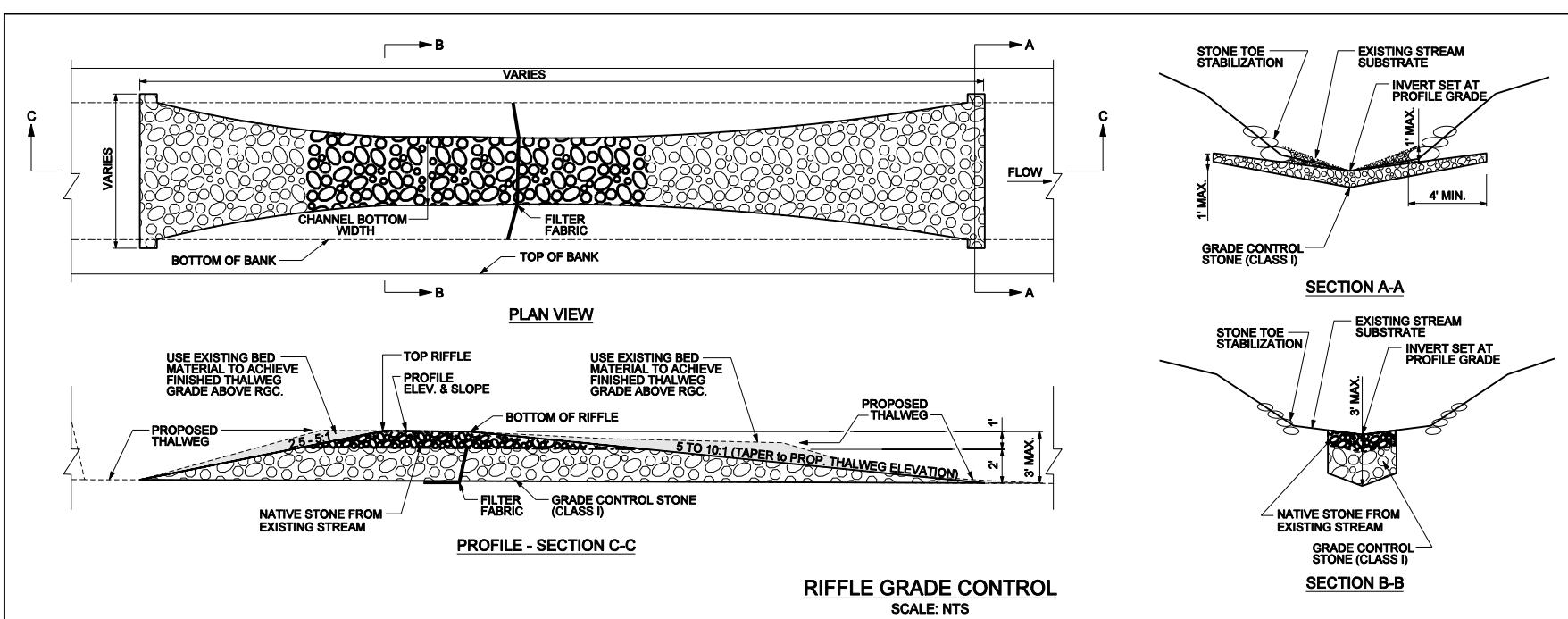
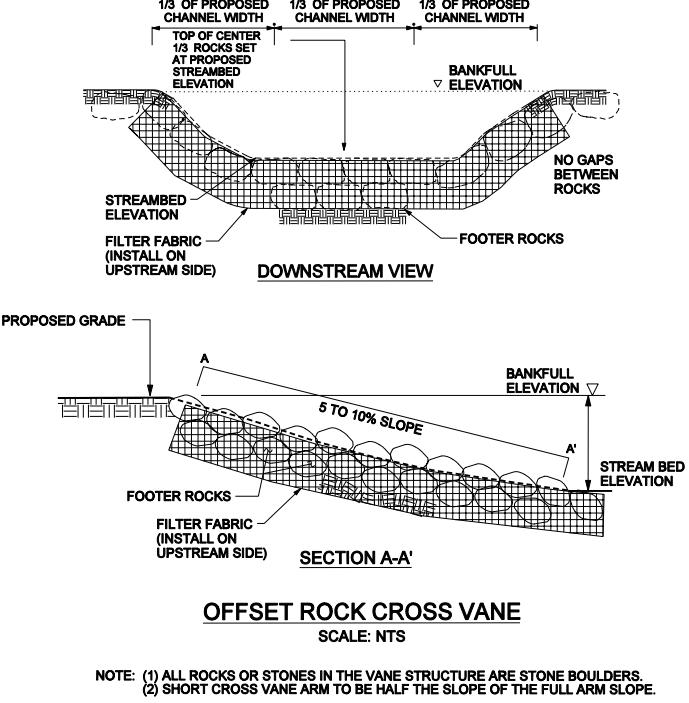
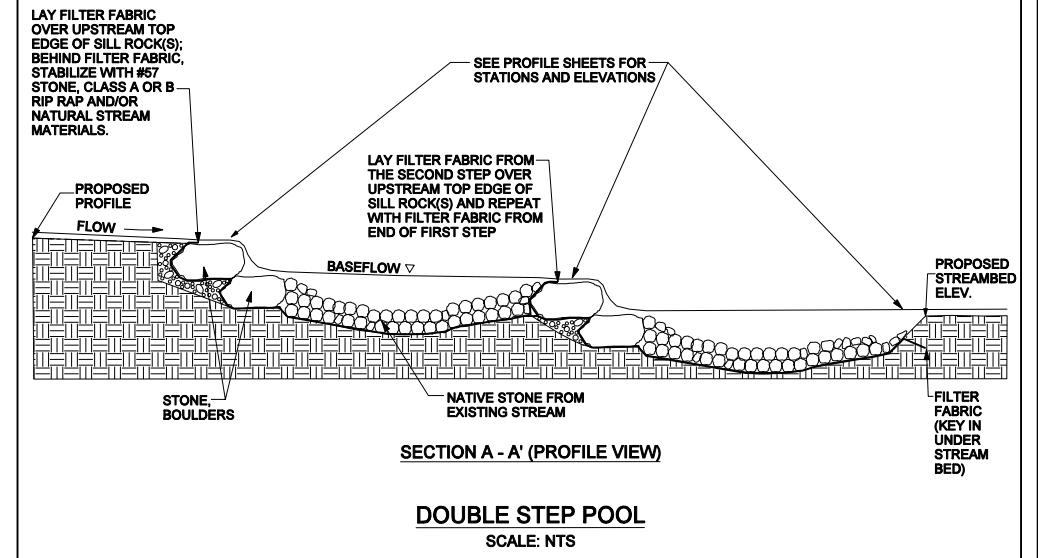
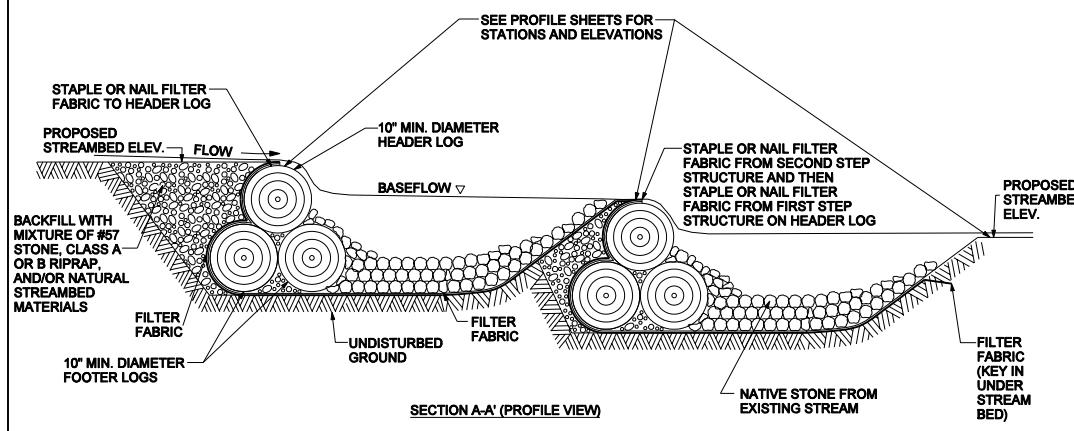
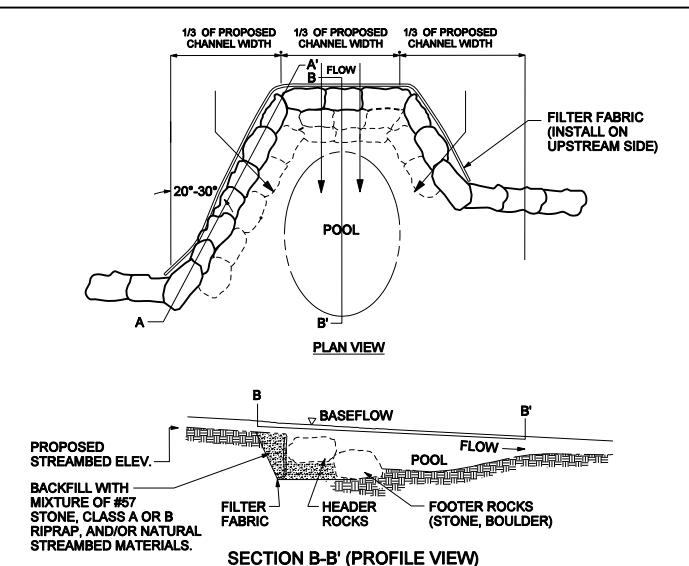
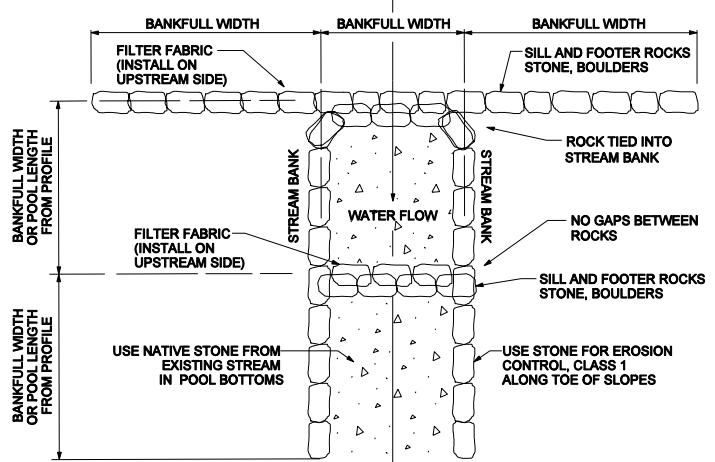
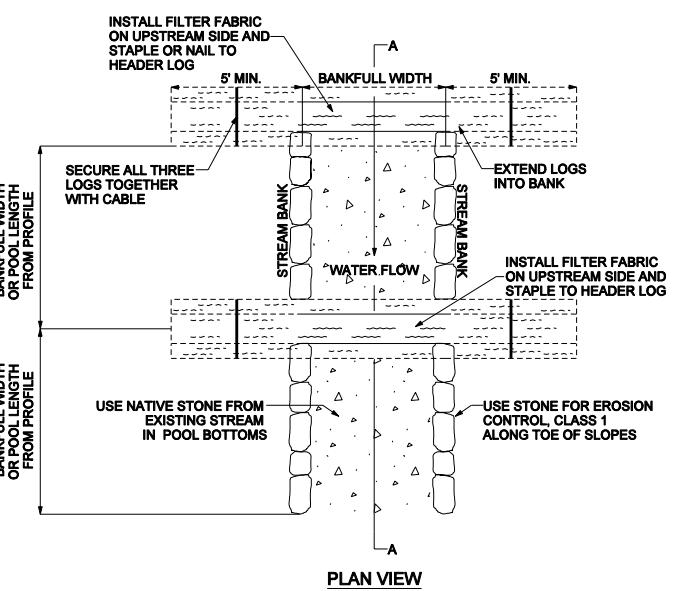
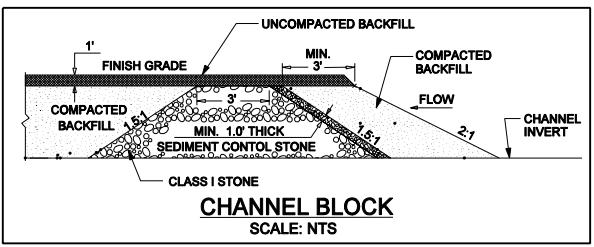
- Barbed Wire Fence .....



DATE: JULY 2008	
SCALE: N.T.S.	
PROJECT LEGEND	
SHEET 1A OF 16	
SYN	DESCRIPTION
APPROVED	DATE
REVISIONS	

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**Ecosystem Enhancement**  
PHILIP J. MUNAWAR

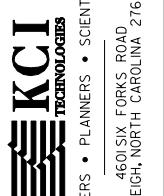


**DOG BITE  
STREAM RESTORATION PROJECT**  
BAKERSVILLE, MITCHELL COUNTY, NORTH CAROLINA

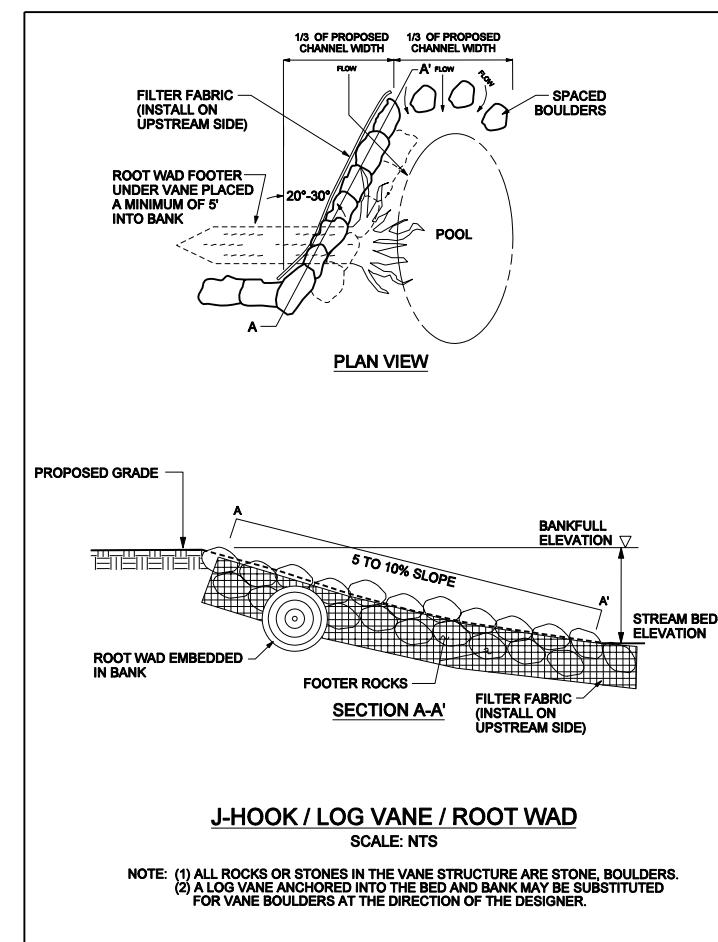
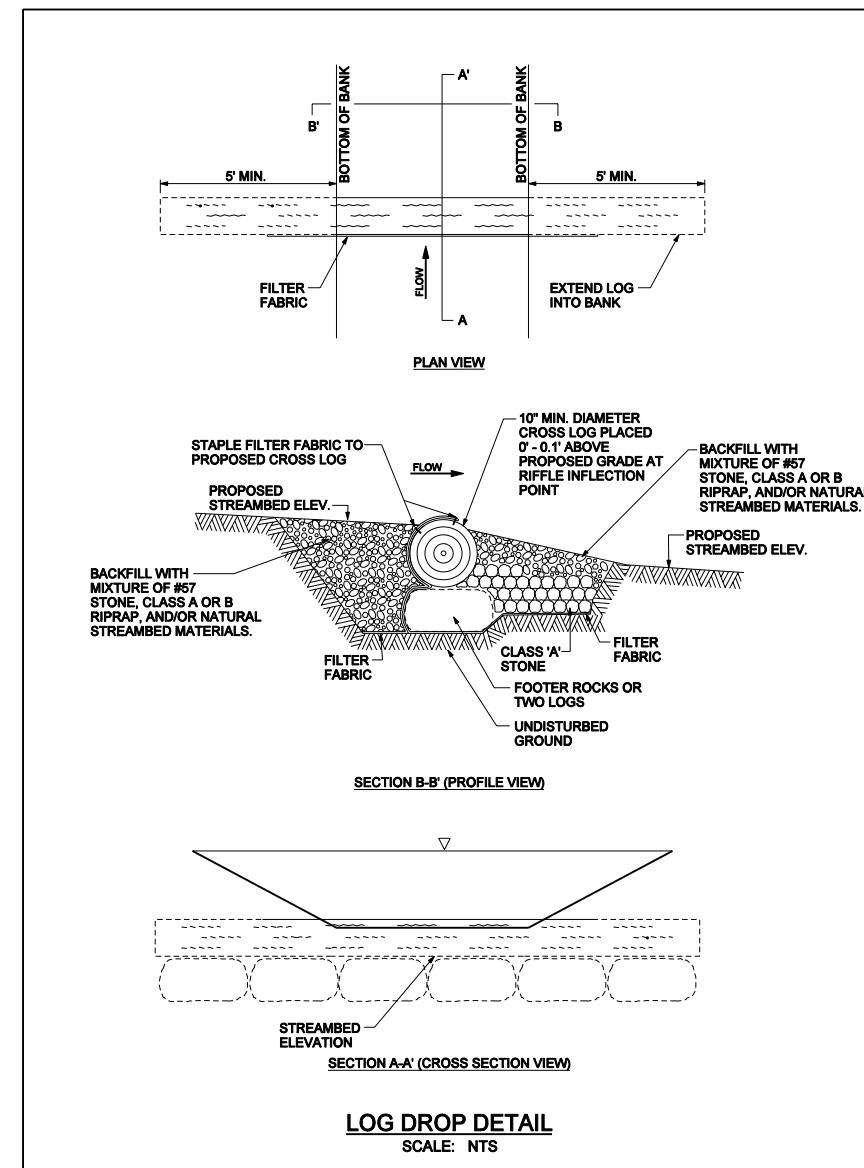
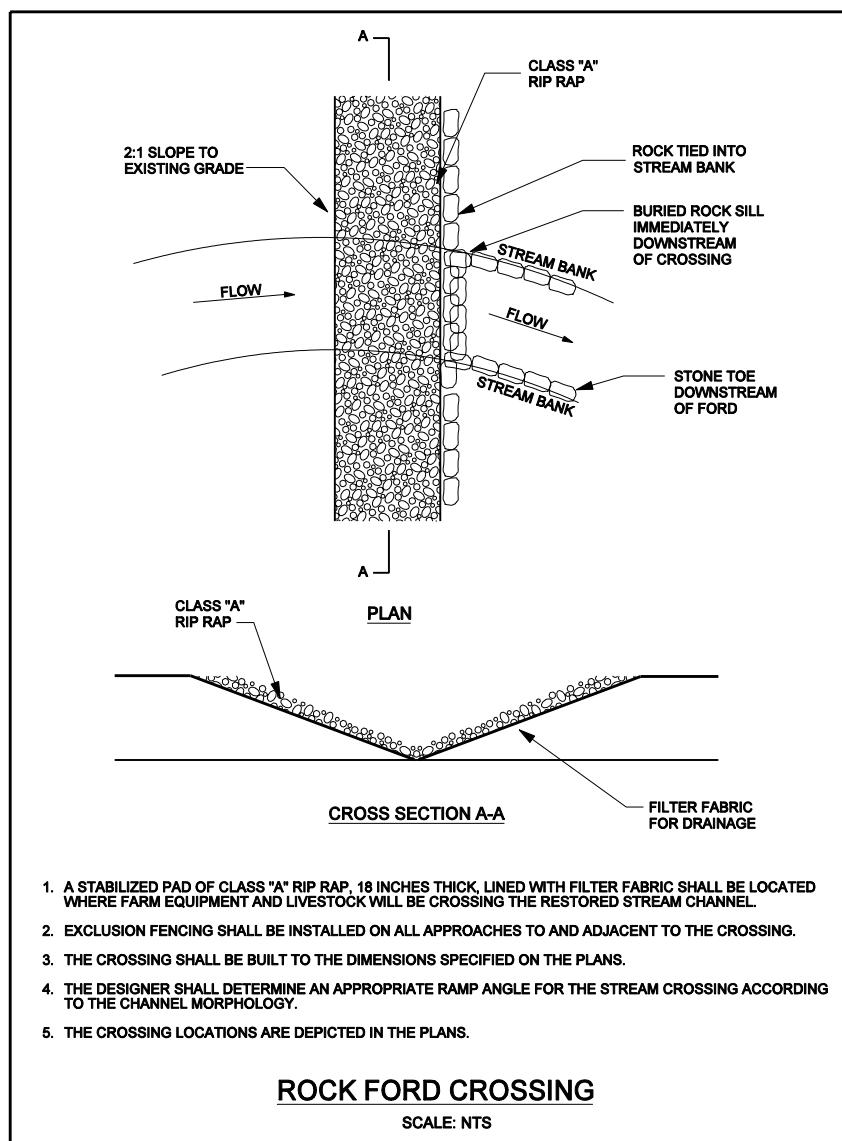
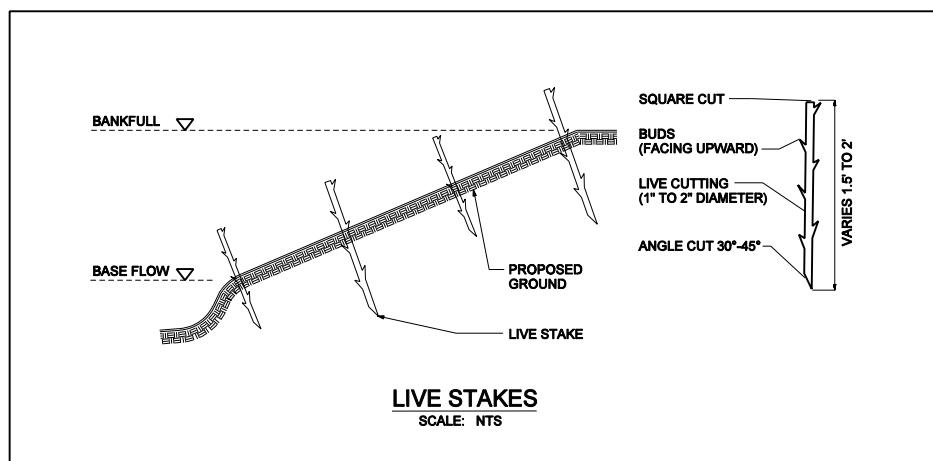
DATE: JULY 2008  
SCALE: N.T.S.

DETAILS:  
STABILIZATION

SHEET 2 OF 16

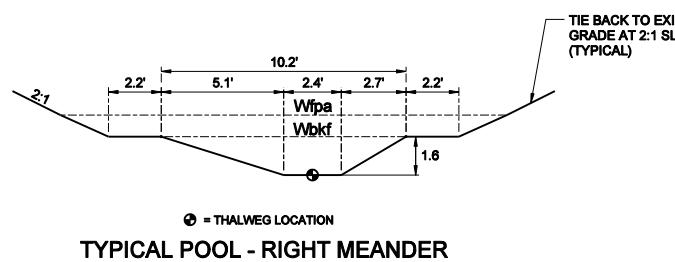
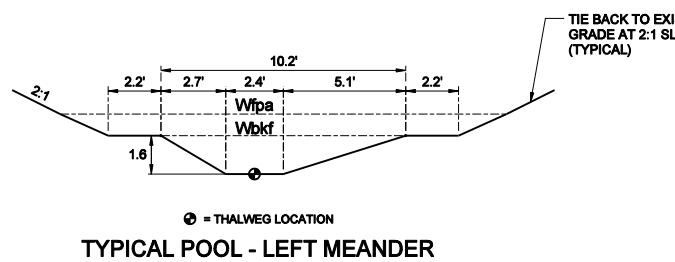
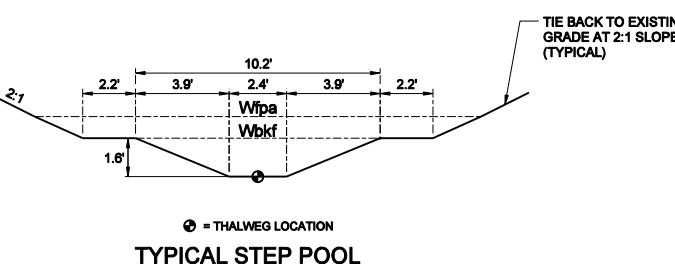
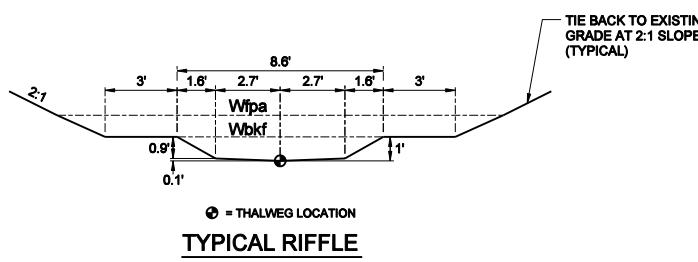


REVISIONS	REVISIONS	REVISIONS
JULY 2008	JULY 2008	JULY 2008
APPROVED	APPROVED	APPROVED
DATE	DATE	DATE
SYM.	SYM.	SYM.
DESCRIPTION	DESCRIPTION	DESCRIPTION
A	A	A
SUBMITTED WITH RESTORATION PLAN	SUBMITTED WITH RESTORATION PLAN	SUBMITTED WITH RESTORATION PLAN

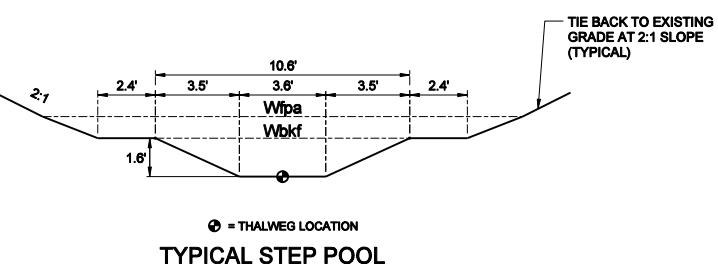
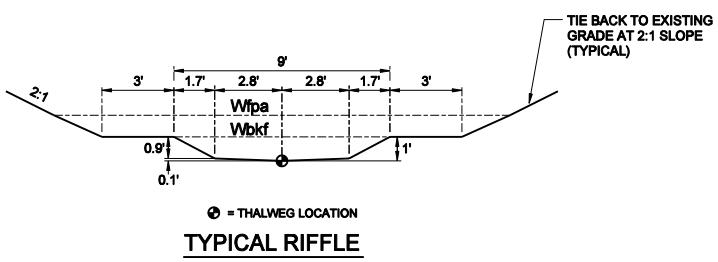


SUBMITTED WITH RESTORATION PLAN		APPROVED	
JULY 2008			
SHEET 2A OF 16			
DETAILS: STABILIZATION			
DATE: JULY 2008	SCALE: N.T.S.		
<b>KCI TECHNOLOGIES</b> ENGINEERS • PLANNERS • SCIENTISTS 460 SIX FORKS ROAD RALEIGH, NORTH CAROLINA 27609		Ecosystem Enhancement	REVISIONS

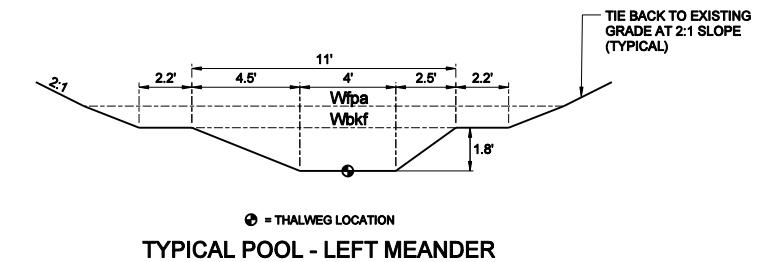
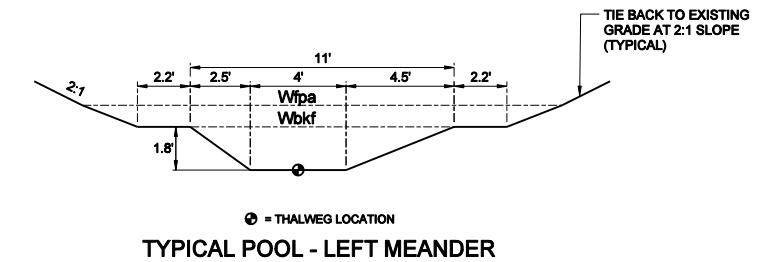
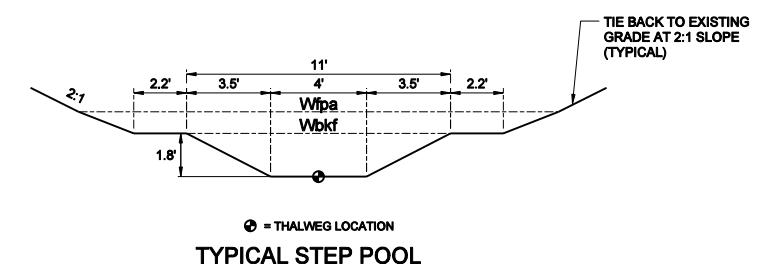
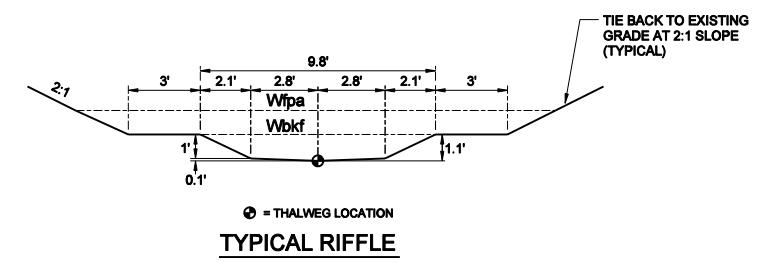
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**STATION 10+00 TO STATION 19+25**  
**"B4a" STREAM TYPE**  
**ENHANCEMENT 1 AND RESTORATION**



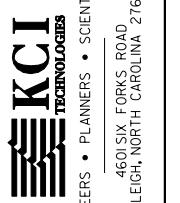
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**STATION 19+25 TO STATION 22+74**  
**"B4a" STREAM TYPE**  
**ENHANCEMENT I**



**WOC-4**  
**STATION 22+88 TO STATION 36+31**  
**"B4a" STREAM TYPE**  
**RESTORATION**



SUBMITTED WITH RESTORATION PLAN		REVISIONS
SHEET	DATE	
JULY 2008		



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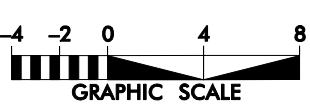
RALEIGH, NORTH CAROLINA 27609

**DOG BITE**  
**STREAM RESTORATION PROJECT**  
BAKERSVILLE, MITCHELL COUNTY, NORTH CAROLINA

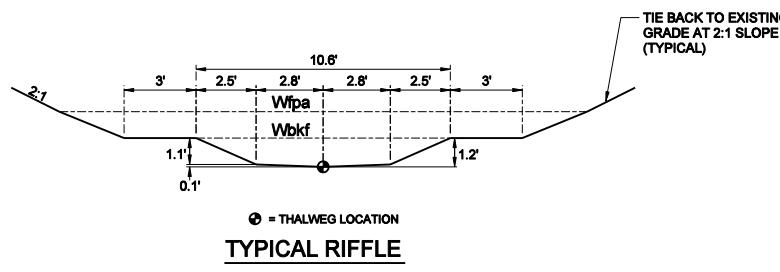
DATE: JULY 2008  
SCALE: N.T.S.

DETAILS:  
TYPICAL XS

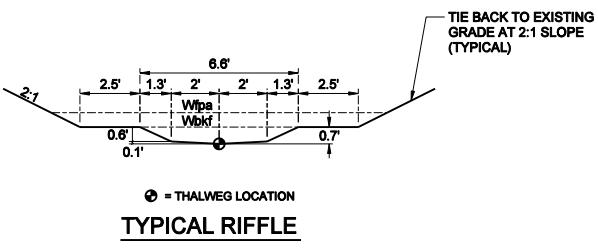
SHEET 3 OF 16



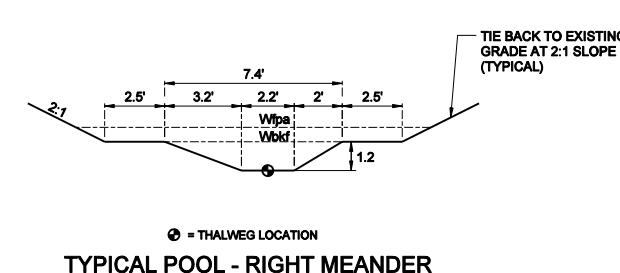
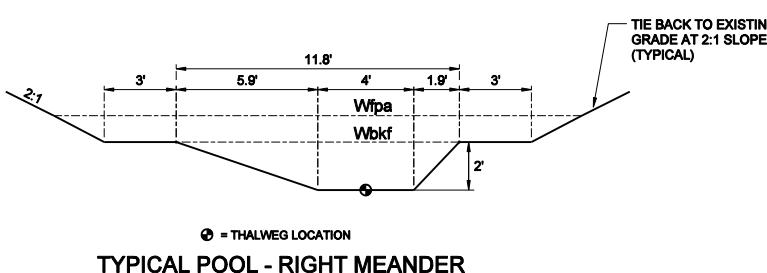
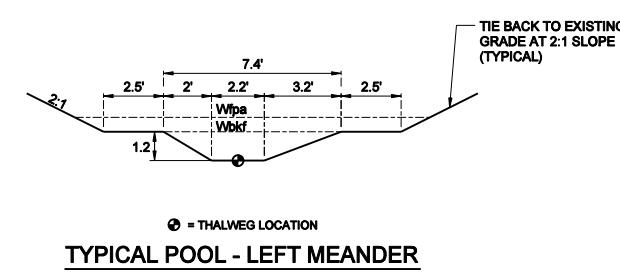
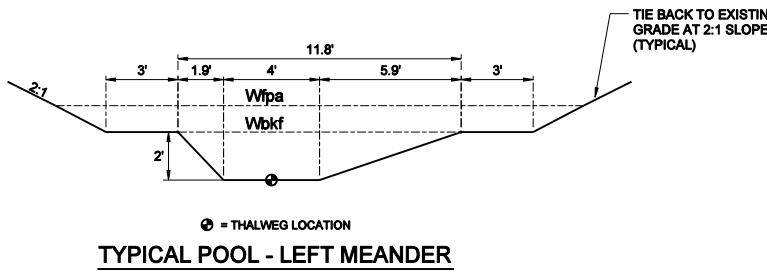
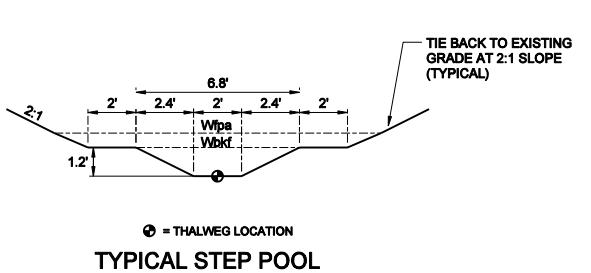
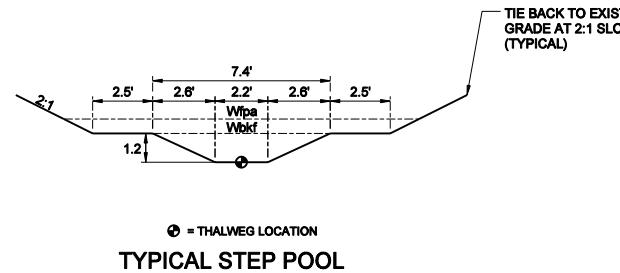
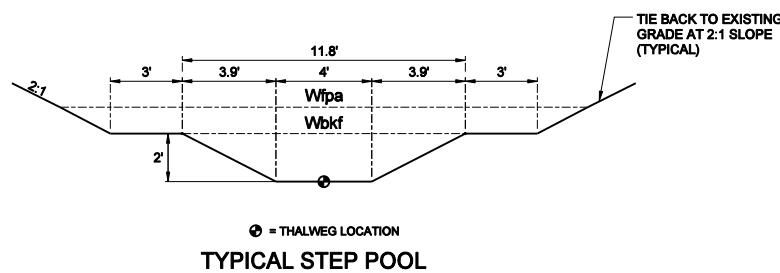
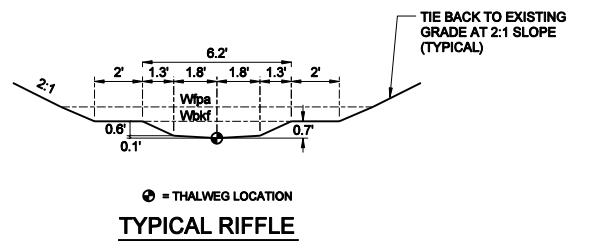
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**STATION 36+31 TO STATION 40+89**  
**"B4" STREAM TYPE**  
**ENHANCEMENT I**



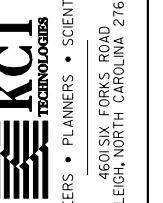
**T1-1 AND T1-2**  
**STATION 50+00 TO STATION 54+69**  
**"B4a" STREAM TYPE**  
**ENHANCEMENT II AND RESTORATION**



**T2**  
**STATION 60+00 TO STATION 62+57**  
**"B4a" STREAM TYPE**  
**RESTORATION**



SUBMITTED WITH RESTORATION PLAN		REVISIONS
SYM.	DESCRIPTION	
JULY 2008		



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**DOG BITE**  
**STREAM RESTORATION PROJECT**  
BAKERSVILLE, MITCHELL COUNTY, NORTH CAROLINA

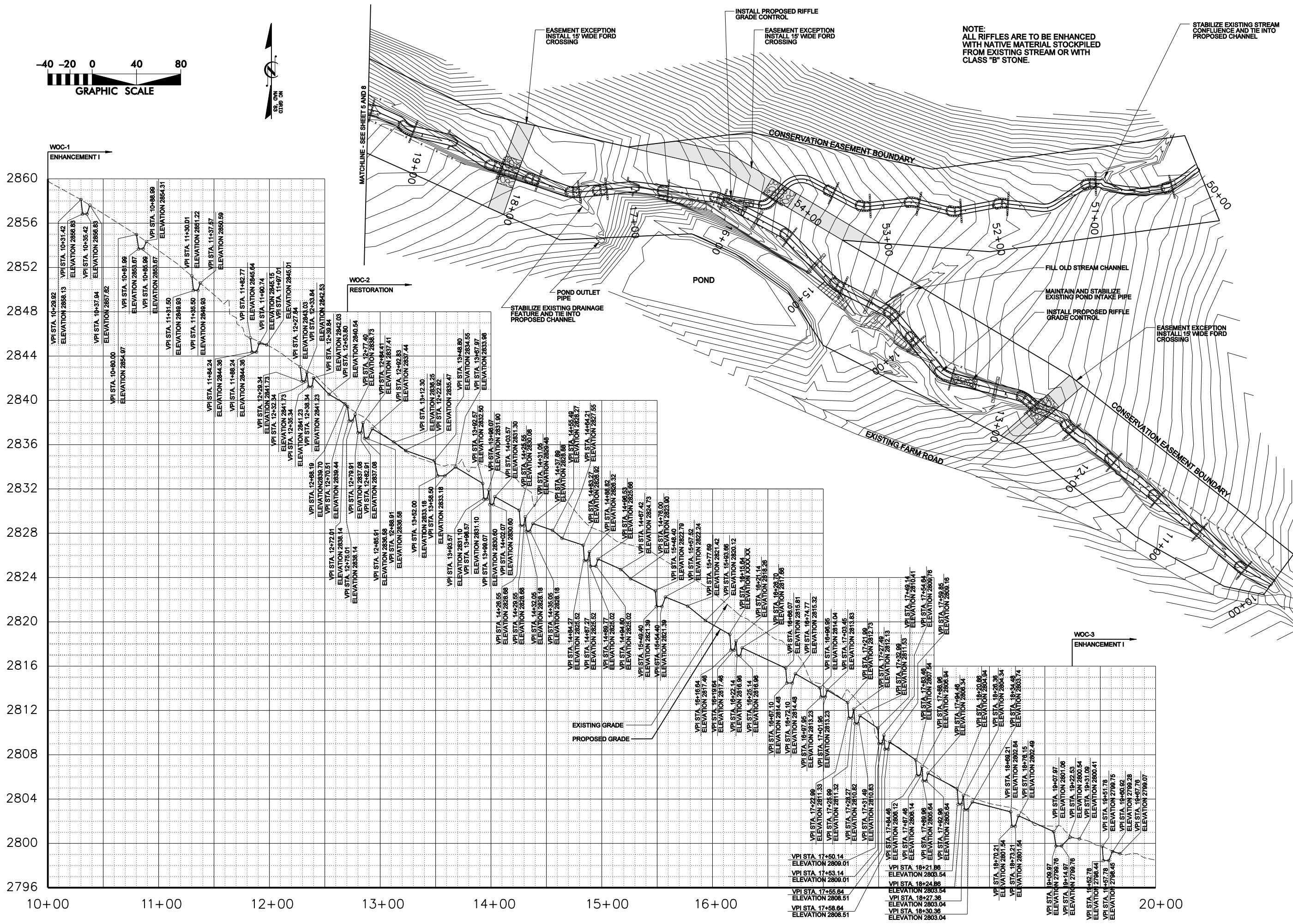
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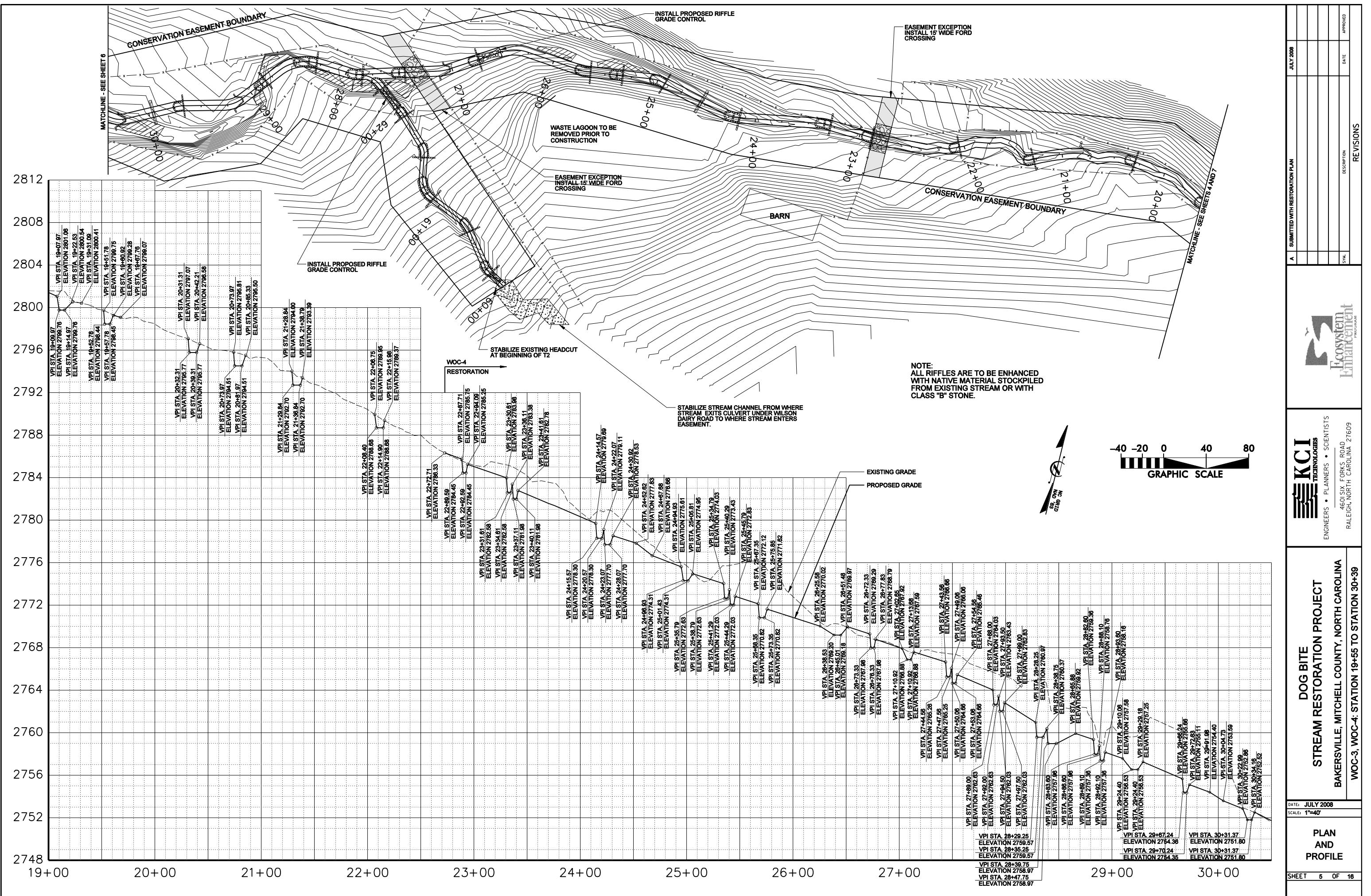


DETAILS:  
TYPICAL XS

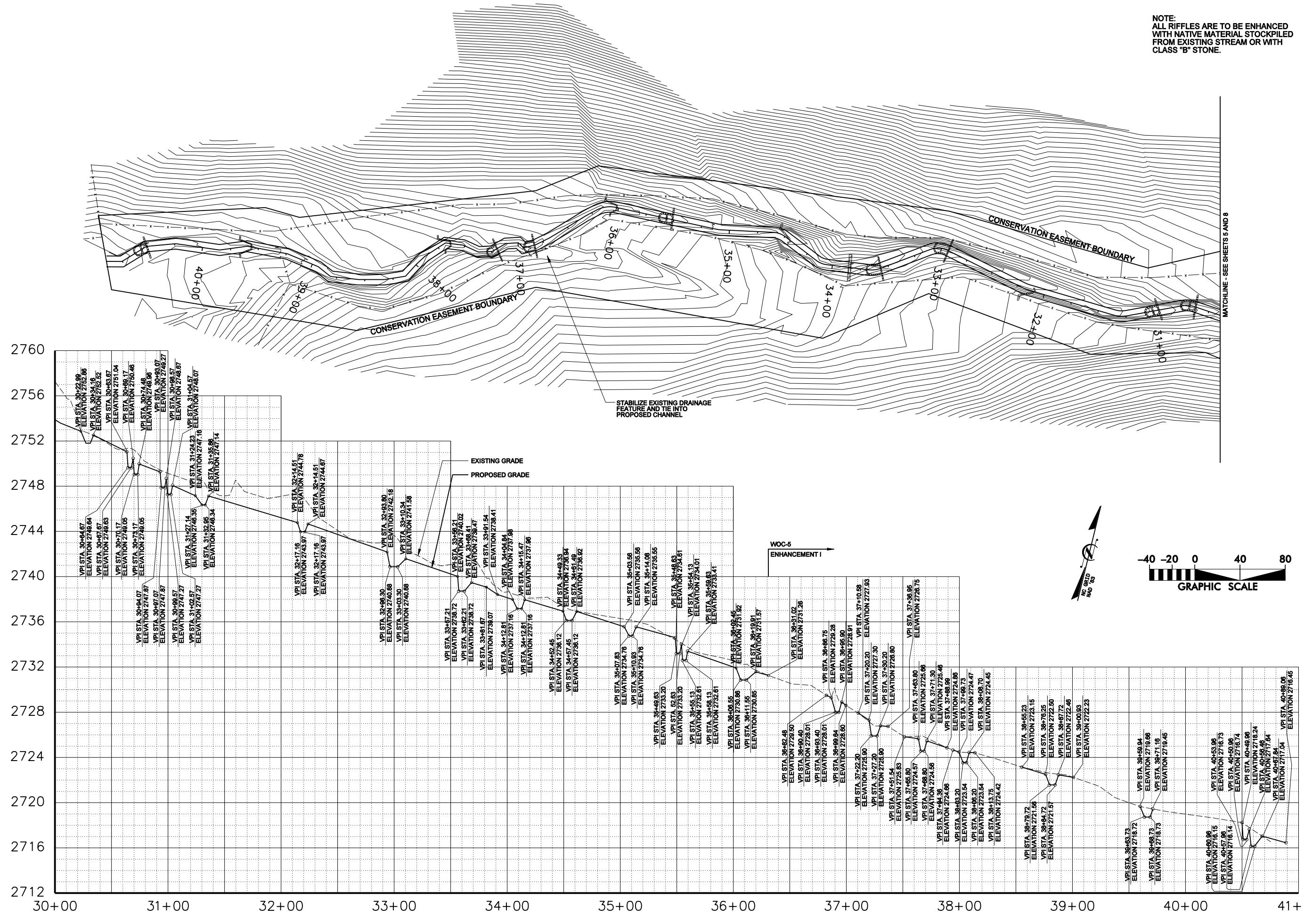
SHEET 3A OF 16

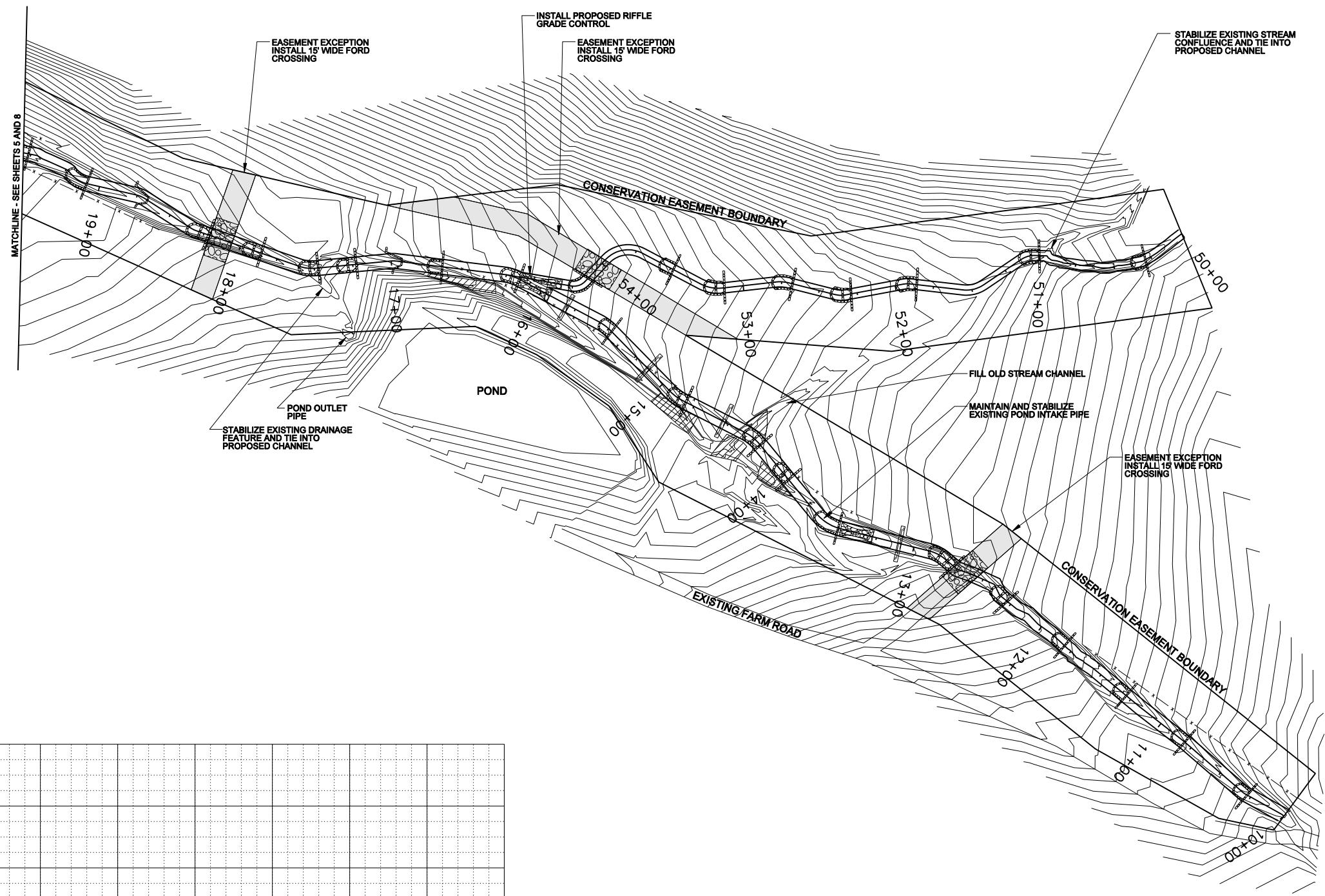
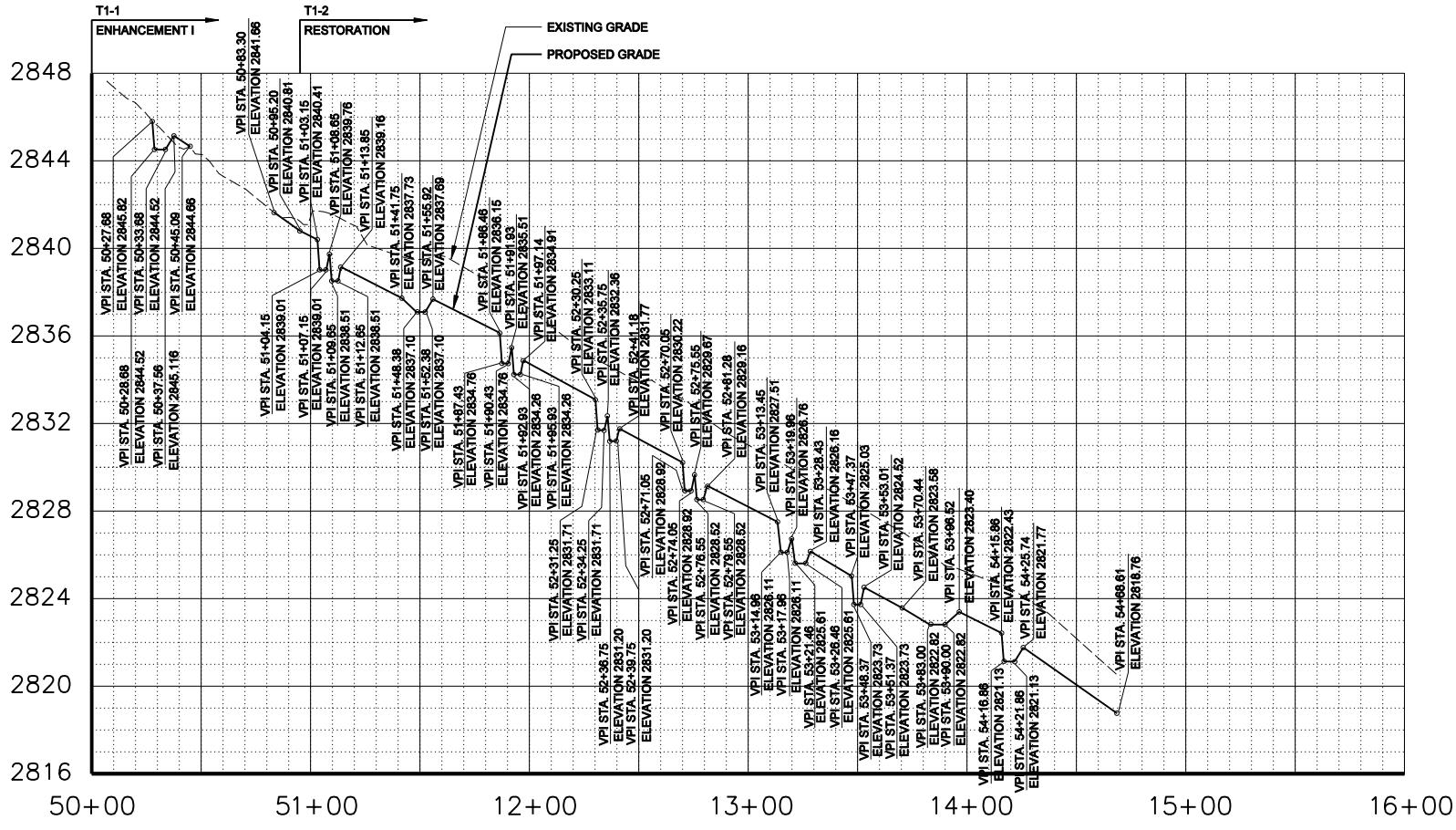
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GRAPHIC SCALE



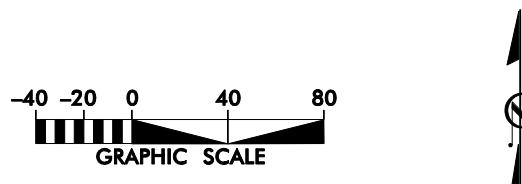


NOTE:  
ALL RIFFLES ARE TO BE ENHANCED  
WITH NATIVE MATERIAL STOCKPILED  
FROM EXISTING STREAM OR WITH  
CLASS "B" STONE.





**NOTE:**  
ALL RIFFLES ARE TO BE ENHANCED  
WITH NATIVE MATERIAL STOCKPILED  
FROM EXISTING STREAM OR WITH  
CLASS "B" STONE.



**DOG BITE  
STREAM RESTORATION PROJECT**

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BAKERSVILLE, MITCHELL COUNTY, NORTH CAROLINA

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T1: STATION 50+00 TO STATION 54+69

PAGE 7 OF 16

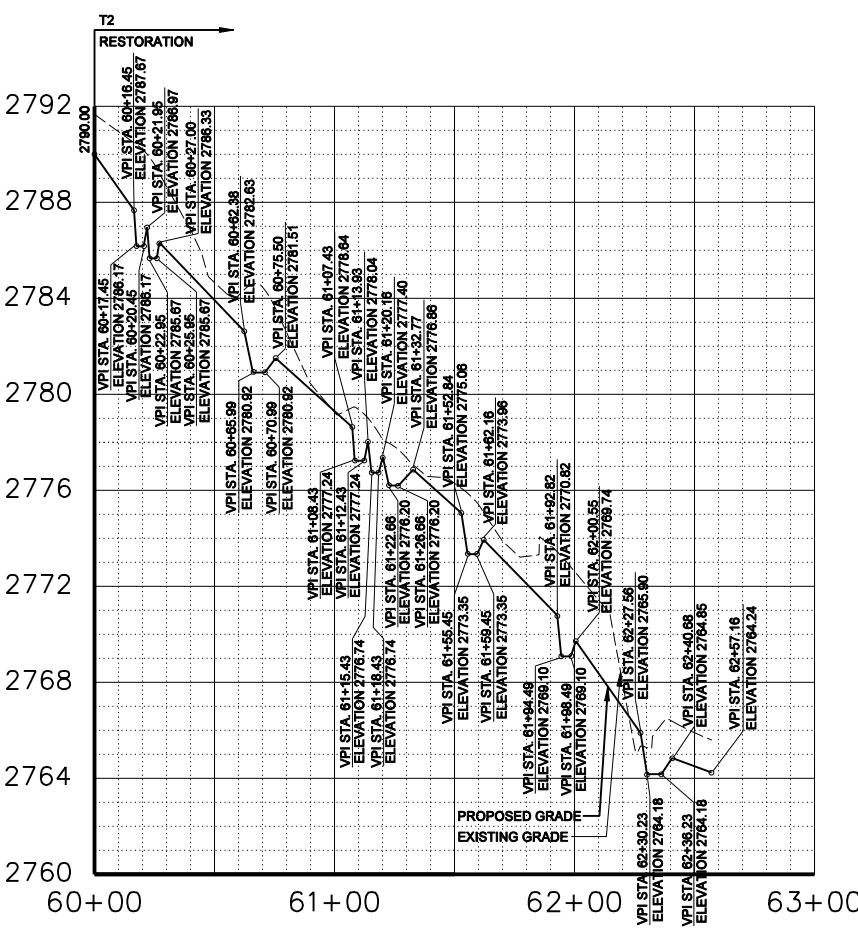
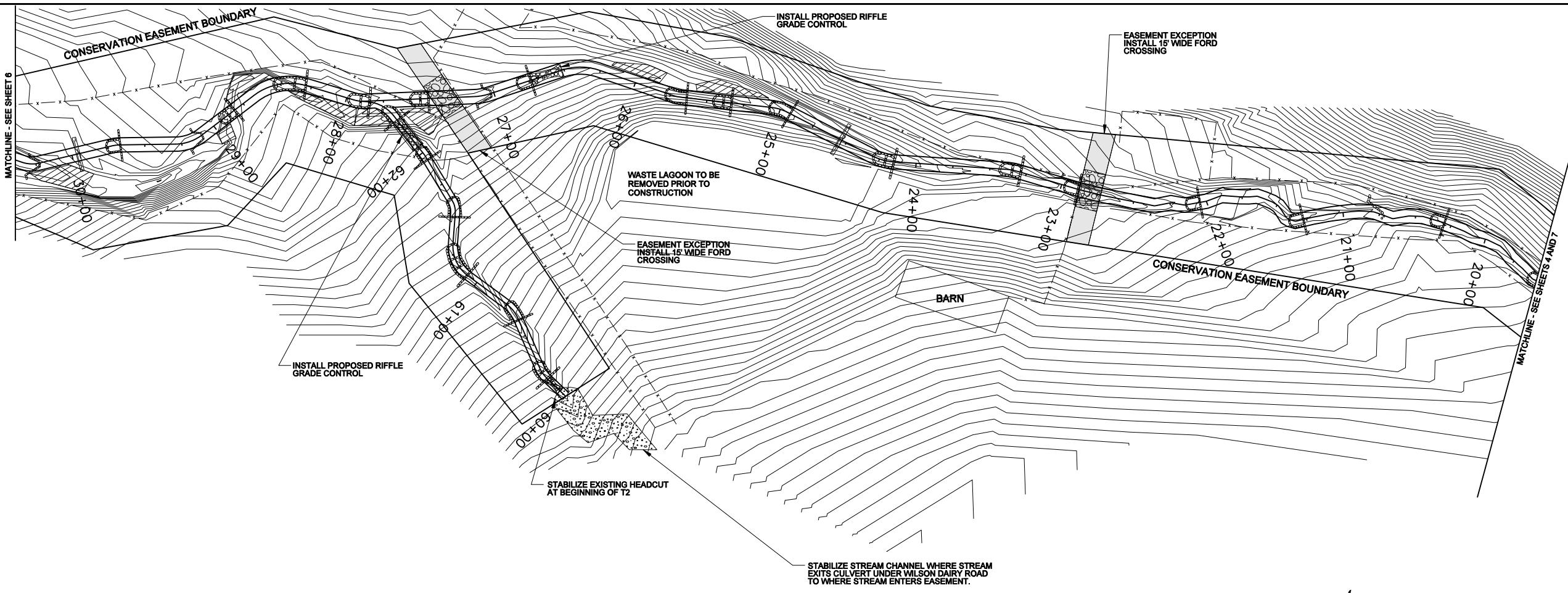
A SUBMITTED WITH RESTORATION PLAN		JULY 2008	
S.M.	DESCRIPTION	DATE	APPROVED

REVISIONS

**Ecosystem  
Enhancement**  
PROJECT

**KCI**  
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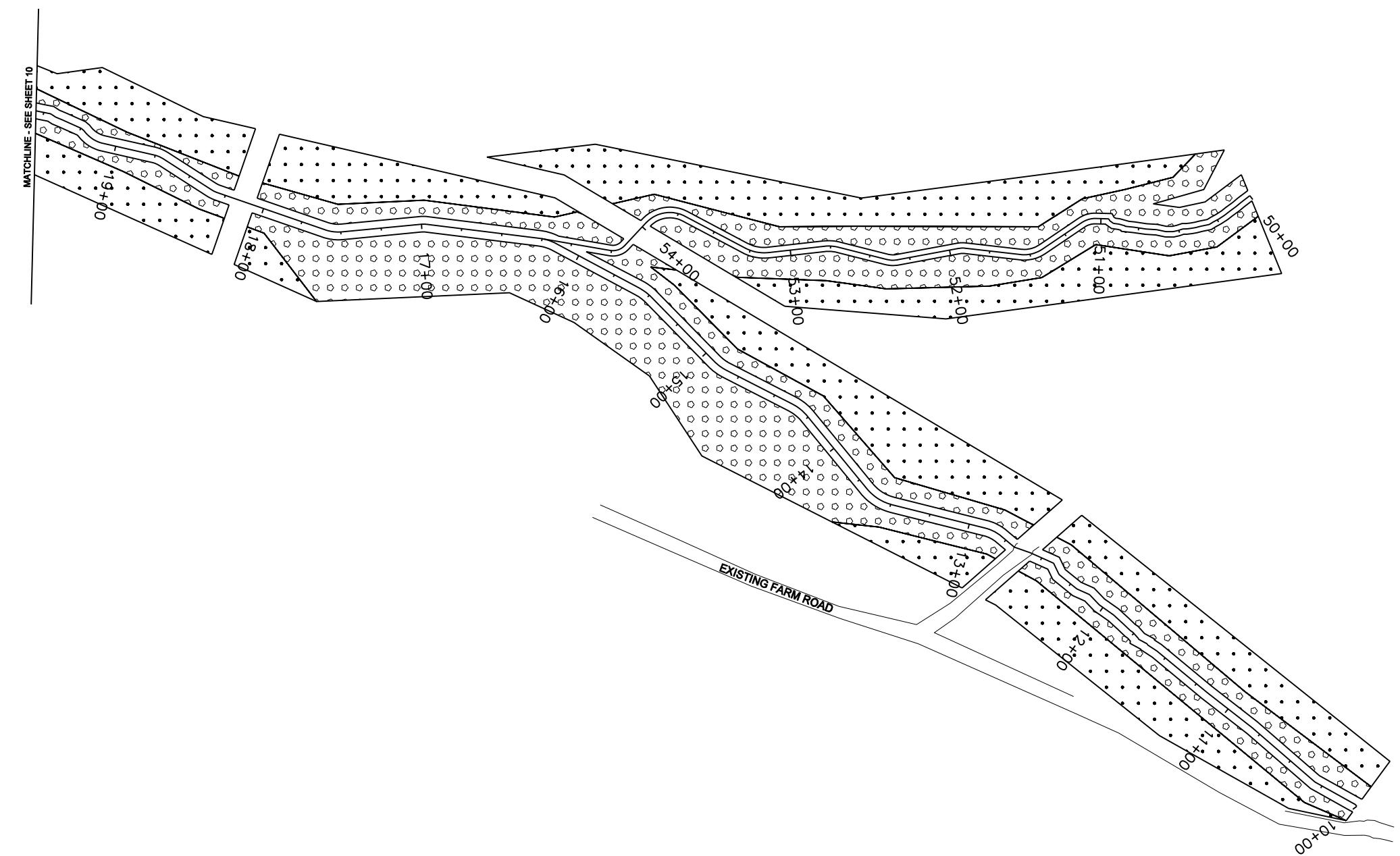
E: JULY 2008  
E: 1"=40'



DOG BITE  
STREAM RESTORATION PROJECT  
BAKERSVILLE, MITCHELL COUNTY, NORTH CAROLINA  
T2: STATION 60+00 TO STATION 62+57

PLAN  
AND  
PROFILE  
SHEET 8 OF 16

DATE: JULY 2008	SCALE: 1"=40'	APPROVED
A SUBMITTED WITH RESTORATION PLAN		
SYM. DESCRIPTION		
JULY 2008		
KCI TECHNOLOGIES ENGINEERS • PLANNERS • SCIENTISTS 460 SIX FORKS ROAD RALEIGH, NORTH CAROLINA 27609	 Ecosystem Enhancement	

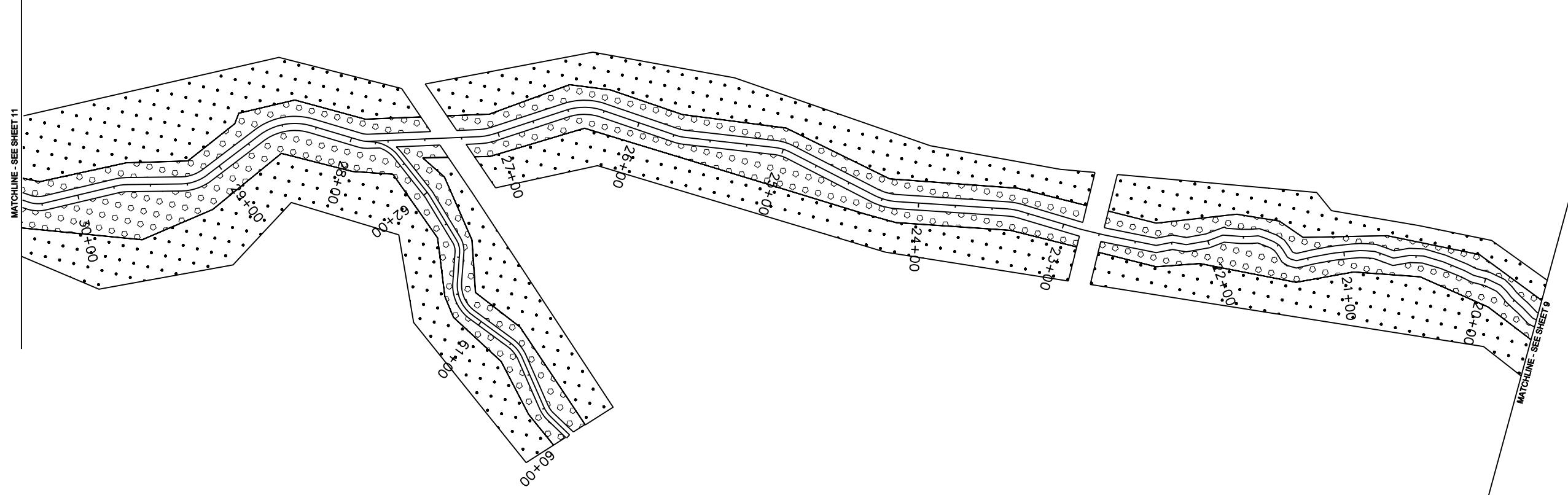


**DOG BITE STREAM RESTORATION PROJECT**  
BAKERSVILLE, MITCHELL COUNTY, NORTH CAROLINA  
WOC-1, WOC-2, WOC-3: STATION 10+00 TO STATION 19+55

### PLANTING PLAN

SHEET 9 OF 16

A SUBMITTED WITH RESTORATION PLAN		JULY 2008	
Ecosystem Enhancement		APPROVED	
DATE:	JULY 2008	DATE:	
SCALE:	1"=40'	SCALE:	
KCI TECHNOLOGIES		ENGINEERS • PLANNERS • SCIENTISTS	
460 SIX FORKS ROAD		RALEIGH, NORTH CAROLINA 27609	



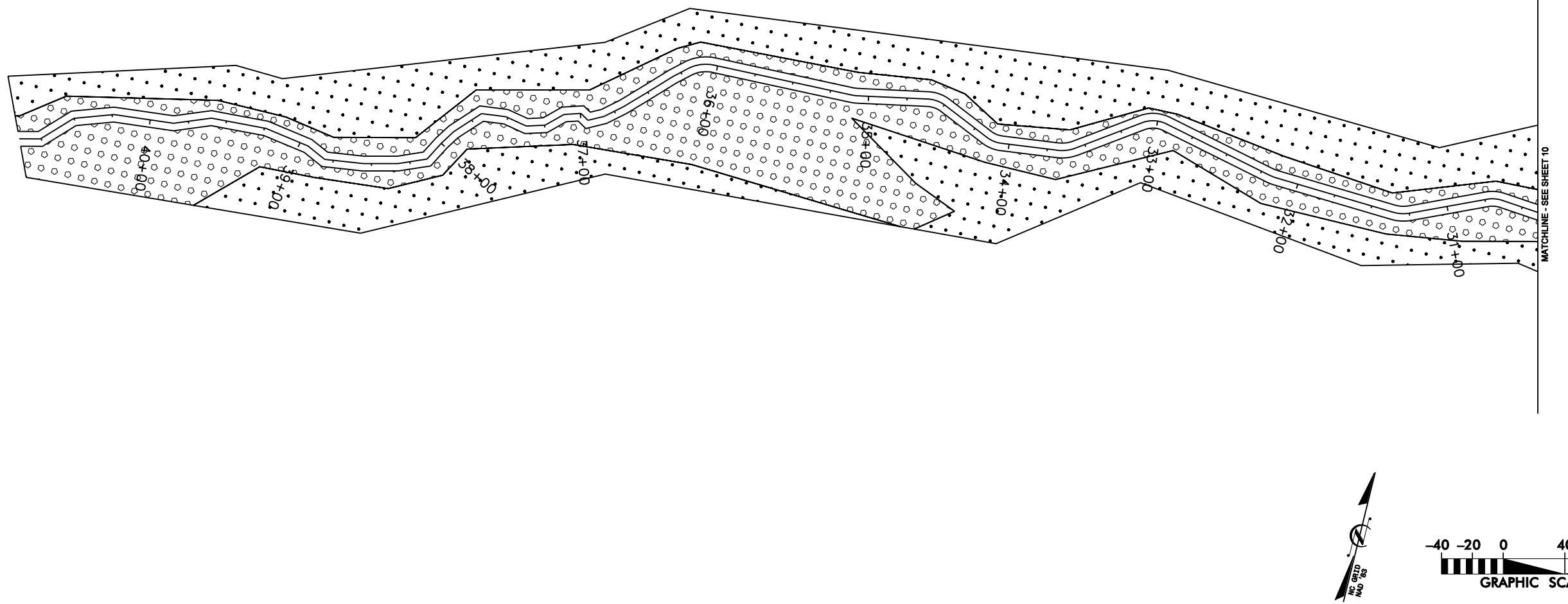
**DOG BITE  
STREAM RESTORATION PROJECT**  
BAKERSVILLE, MITCHELL COUNTY, NORTH CAROLINA  
WOC-3, WOC-4: STATION 19+55 TO STATION 30+39

DATE: JULY 2008  
SCALE: 1"=40'  
  
PLANTING  
PLAN  
  
SHEET 10 OF 16

**KCI**  
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460 SIX FORKS ROAD  
RALEIGH, NORTH CAROLINA 27609



A	SUBMITTED WITH RESTORATION PLAN	JULY 2008
SYM.	DESCRIPTION	DATE APPROVED
	REVISIONS	



**DOG BITE  
STREAM RESTORATION PROJECT  
WAKERSVILLE, MITCHELL COUNTY, NORTH CAROLINA  
WOC-4, WOC-5: STATION 30+39 TO STATION 4**

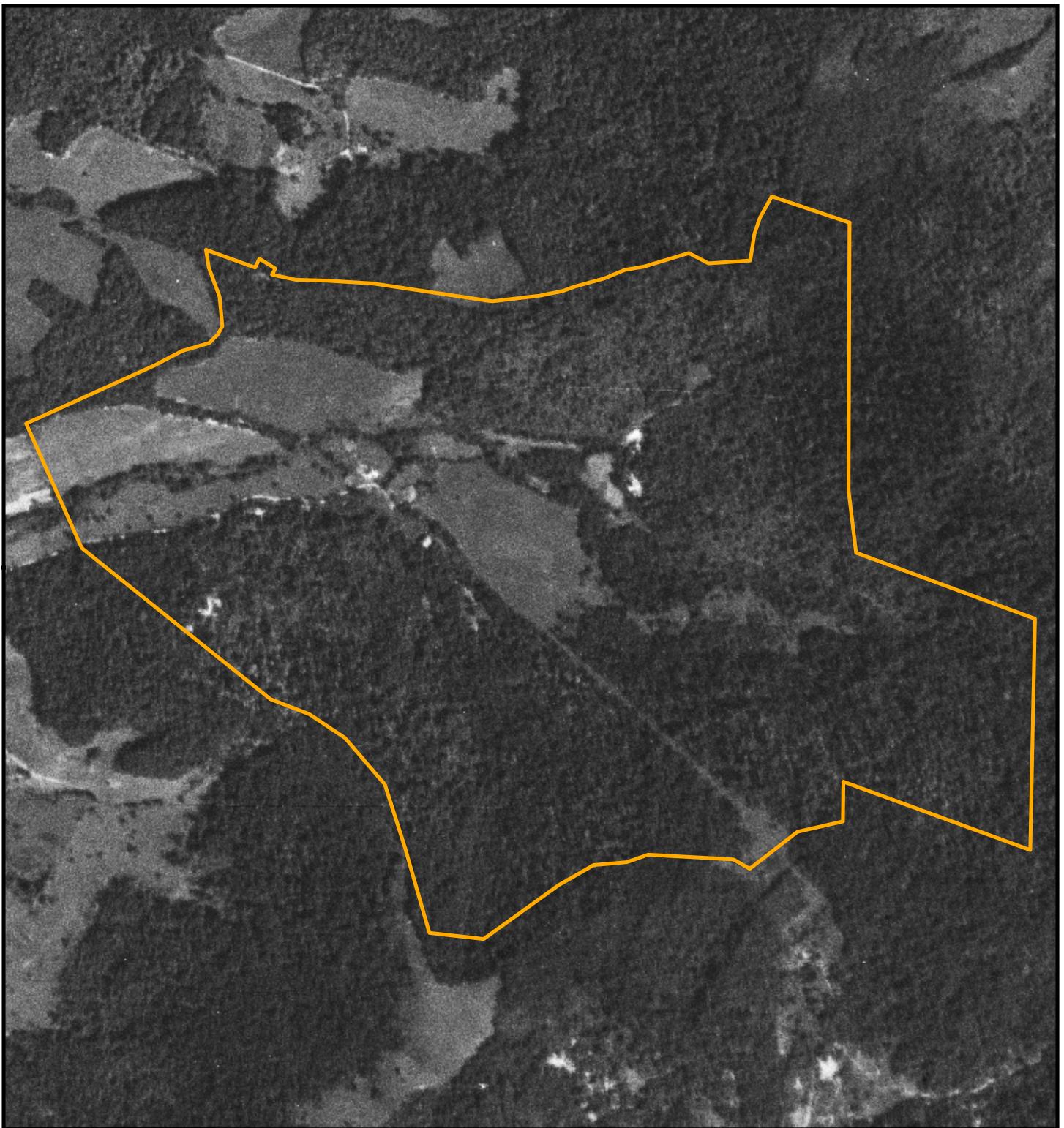
**KCI** TECHNOLOGIES  
ENGINEERS • PLANNERS • SCIENTISTS  
460 SIX FORKS ROAD  
RALEIGH, NORTH CAROLINA 27609



Ecosystem  
Enhancement  
PROGRAM

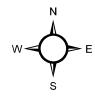
## Appendix A Historic Aerial Photographs





## Historic Aerial Photograph - 1956

Limits of Project Parcel



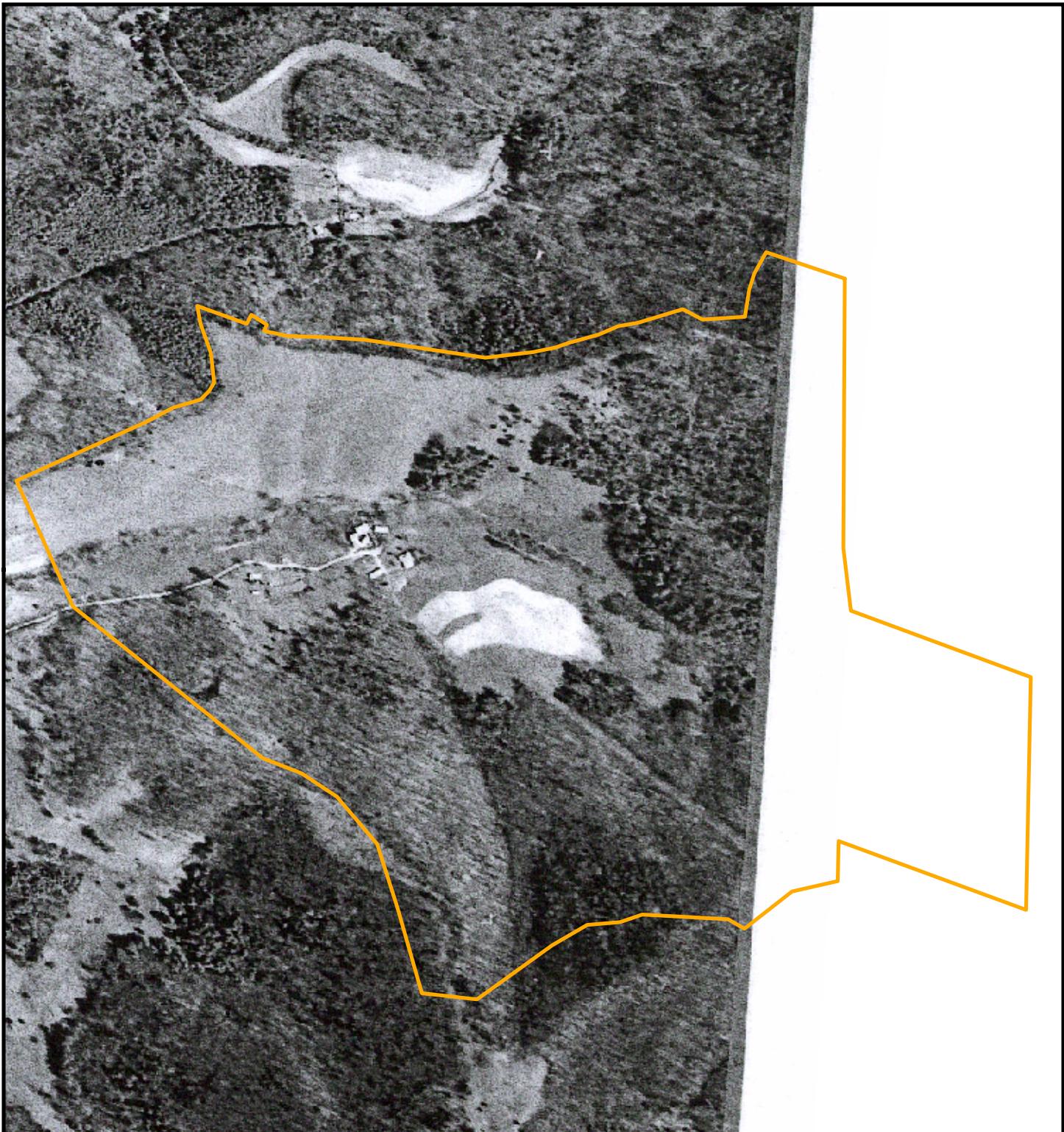
1:8,400

1 inch equals 700 feet

700      350      0      700 Feet

Source: USGS Aerial Photography, August 1956





## Historic Aerial Photograph - 1982

Limits of Project Parcel

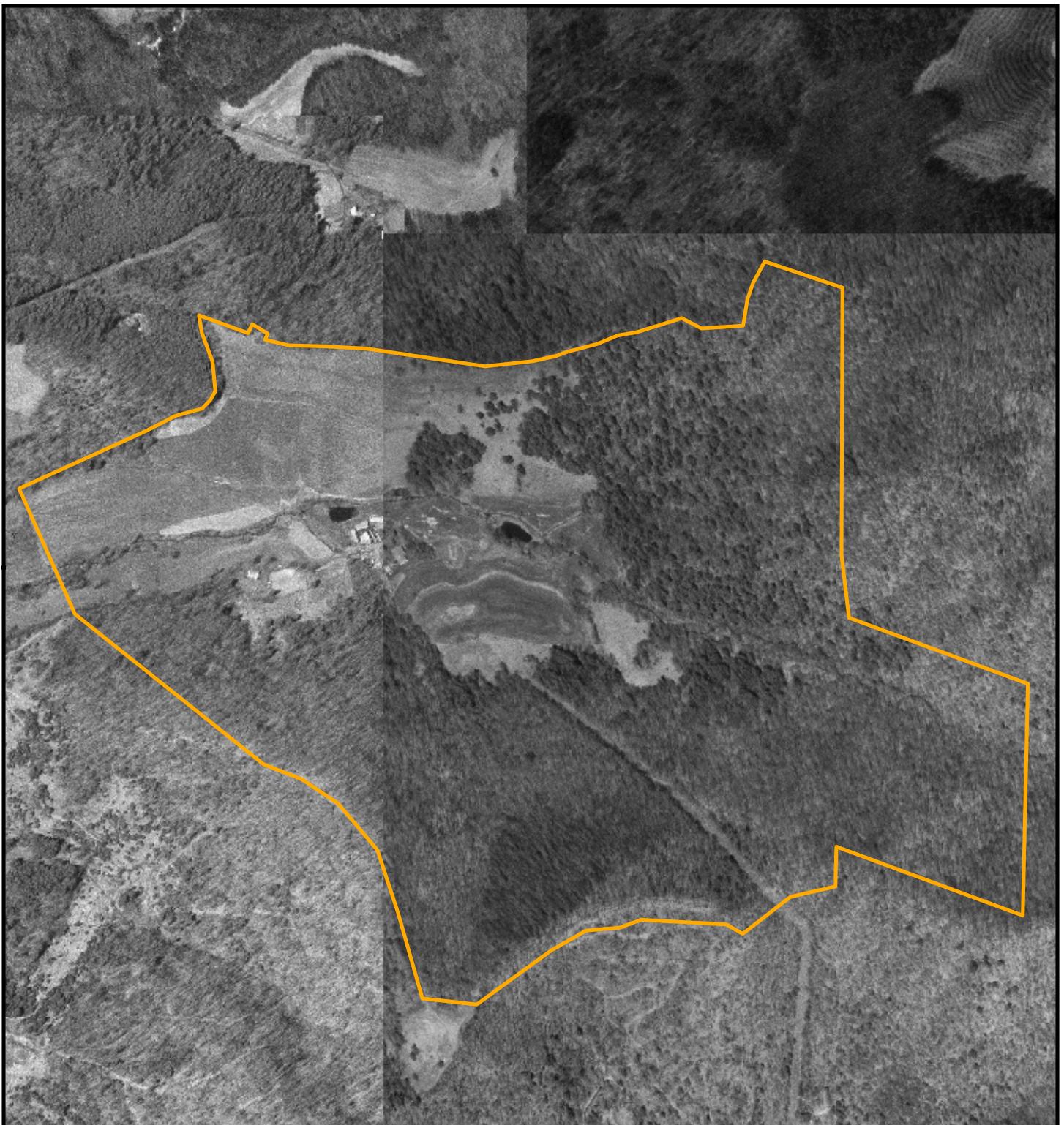


1:8,400  
1 inch equals 700 feet

700 350 0 700 Feet

Source: USDA, NRCS Mitchell County, 1982

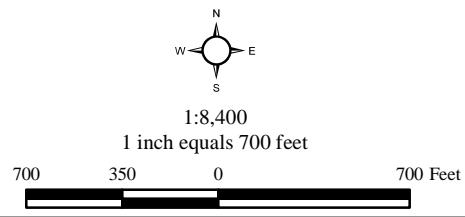




## Historic Aerial Photograph - 1993

□ Limits of Project Parcel

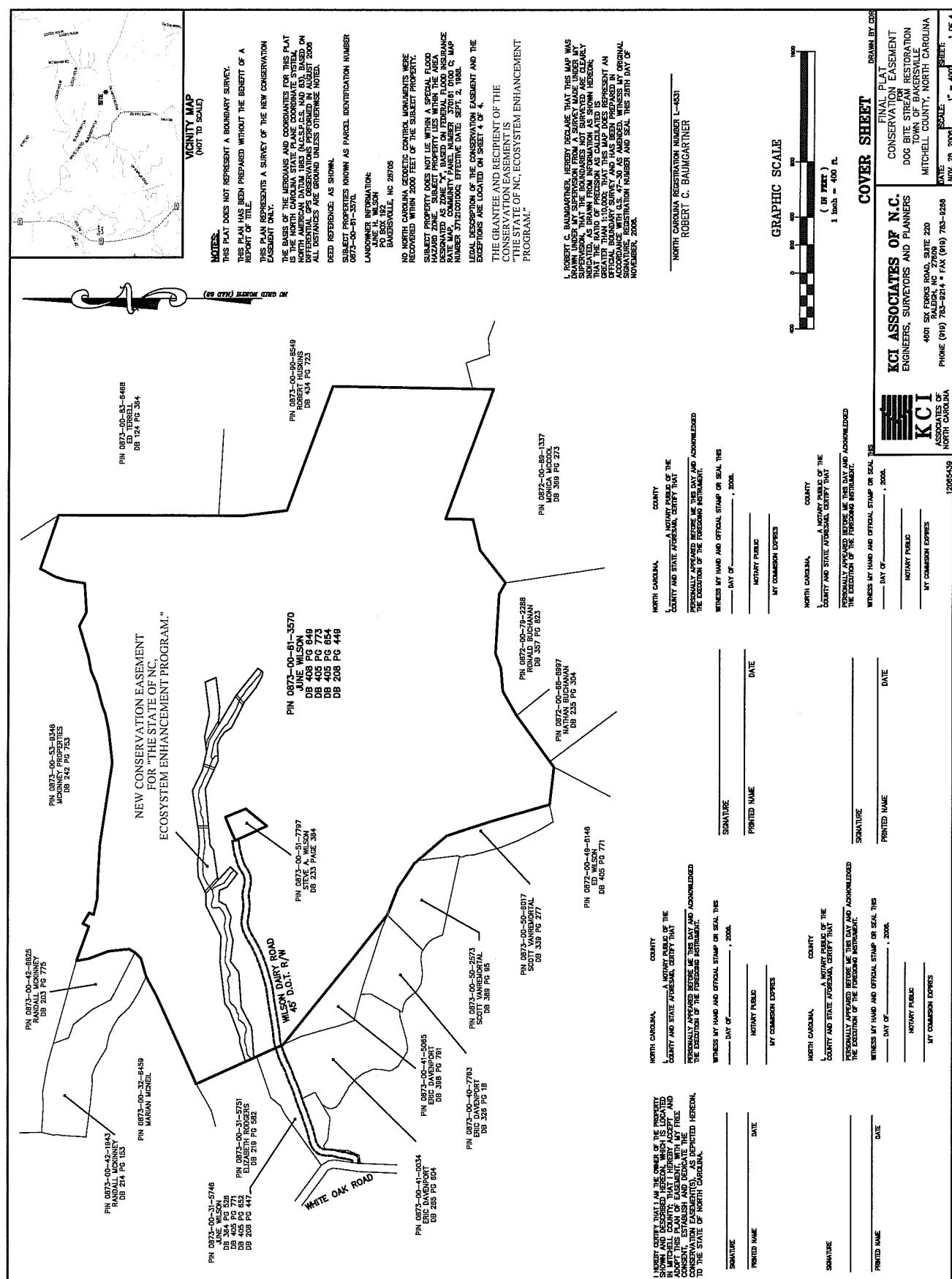
Source: USGS DOQs, 1993





## Appendix B Conservation Easement





NOTES:  
FOR GENERAL NOTES SEE THE NOTE SECTION ON THE COVER

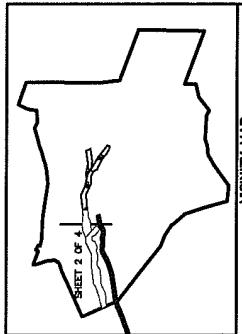
I, ROBERT C. BAUMGARTNER, hereby declare that this map was drawn under my supervision from a survey made under my direction. As shown from information as shown herein, the ratio of precision as indicated is 1:4000. I further declare that no feature shown has been omitted, except as may be indicated by the legend or otherwise. I have examined the original notes and field work and have verified the same. An original copy of the notes and field work is being retained in accordance with G.S. § 97-30 as required.

NORTH CAROLINA REGISTRATION NUMBER L-431  
ROBERT C. BAUMGARTNER

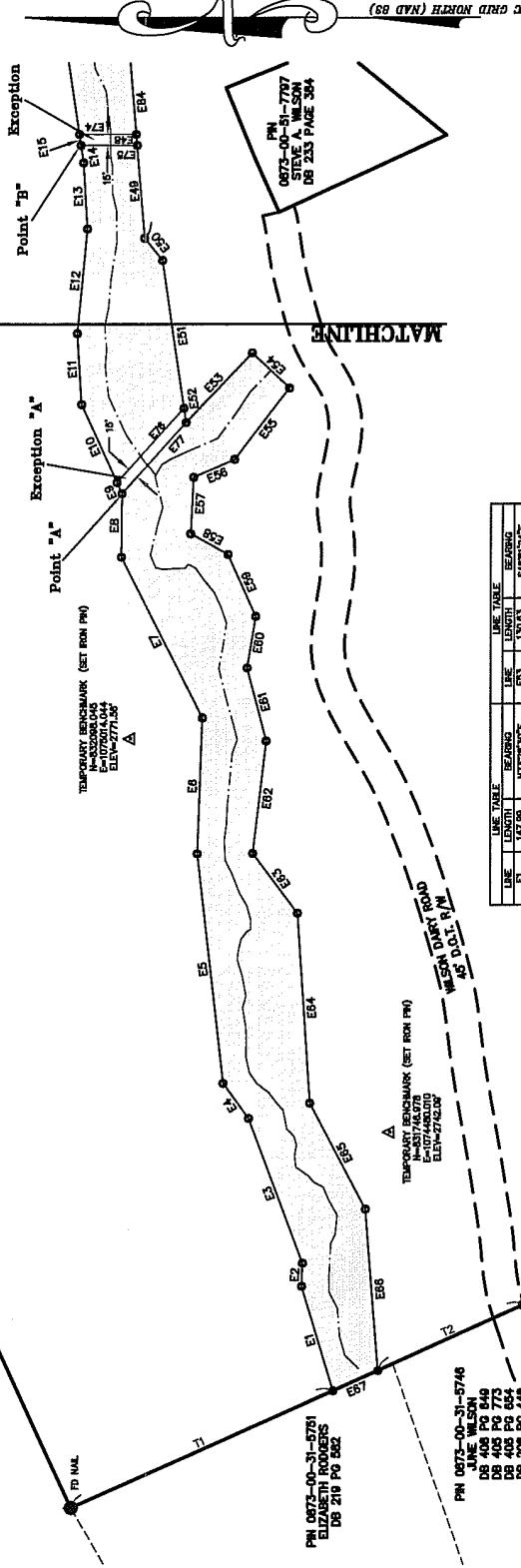
PN 0873-00-42-1843  
RANDALL McNEIL  
DB 214 PG 103

PN 0873-00-32-0459  
MARIAN McNEIL

VICINITY MAP  
(NOT TO SCALE)



SHEET 1  
SHEET 2  
SHEET 3  
SHEET 4  
SHEET 5



LINE	LINE TYPE	BEARING	LINE TYPE		
			LINE	LINE	BEARING
E1	15' 45"	N242°09.45'	E15	15' 45"	S34°47.33'
E2	21' 37"	N073°50.22'	E24	70' 0.00	S33°20.33'
E3	21' 45"	N073°50.25'	E25	12' 1.59	N30°34.35'
E4	59' 35"	N45°29.29'	E26	80' 0.35	N24°24.57'
E5	37' 35"	N45°29.27'	E27	76' 0.13	N072°27.25'
E6	16' 00"	S82°53.07'	E28	20' 0.32	S20°43.85'
E7	24' 29"	S82°53.07'	E29	27' 4.52	N40°03.98'
E8	85' 01"	S09°34.95'	E30	71.07	N02°06.50'
E9	18' 54"	N082°29.25'	E31	101.84	S37°18.03'
E10	116' 75"	N082°29.25'	E32	182.82	N33°32.77'
E11	97' 75"	N082°29.25'	E33	101.32	S53°11.57'
E12	14' 53"	S062°50.01'	E34	20' 0.36	S20°19.77'
E13	12' 00"	S062°50.01'	E35	20' 0.36	S20°19.77'
E14	23' 01"	S062°50.01'	E36	20' 0.36	S20°19.77'
E15	15' 17"	N81°50.95'	E37	58.58	N52.05/54.74'
E16	18' 00"	S83°02.45'	E38	70.86	N00°00.00'
E17	126' 72"	S83°02.45'	E39	73.94	N00°00.00'
E18	30' 45"	S082°15.75'	E40	54.75	N17°59.45'
E19	20' 00"	S082°15.75'	E41	54.75	S17°59.45'
E20	19' 44"	S082°15.75'	E42	15.86	S01°00.52'
E21	19' 44"	S082°15.75'	E43	50.83	S01°00.52'
E22	72		E44	210.21	N24°31.48'

LEGEND

- EXISTING IRON PIPE
- TEMPORARY BENCHMARK (SET IRON PM)
- ▲ DOG BITE MARK
- ◆ EXISTING NAIL



1 inch = 100 ft.

GRAPHIC SCALE



KCI

KCI ASSOCIATES OF N.C.  
ENGINEERS, SURVEYORS AND PLANNERS



KCI

ASSOCIATES OF N.C.



KCI

CONSOLIDATED PLAT  
CONSERVATION EASEMENT  
DOG BITE STREAM RESTORATION

MITCHELL COUNTY, NORTH CAROLINA

JULY 2008

PAGE NO. 220

FILE NO. 783-2224

PHONE (910) 783-5214 • FAX (910) 783-2226

DATE: JULY 22, 2008

SCALE: 1" = 100'

SHEET: 2 OF 4

DRAWN BY: CDS

REVISER:

APPROVED:

OWNER:

PERMIT:

PERMIT NO.:

EXPIRATION DATE:

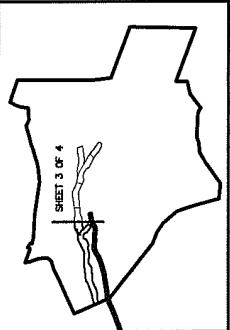
ISSUED BY:

**NOTES:**  
1. FOR GENERAL NOTES SEE THE NOTE SECTION ON THE COVER

I, ROBERT C. BAUMGARTNER, HEREBY DECLARE THAT THIS MAP WAS DRAWN SO THAT THE BOUNDARIES AND LINES ARE CLEARLY INDICATED, AS DRAWN FROM THE INFORMATION AS SHOWN, THAT THE LAND OWNED AND USED IS PRESENTLY AN OFFICIAL BOUNDARY SURVEY AND HAS BEEN PREPARED IN ACCORDANCE WITH S.S. 47-70 AS AMENDED, ATTESTED BY MY SIGNATURE, AND DATED THIS 25TH DAY OF NOVEMBER, 2004.

ROBERT C. BAUMGARTNER

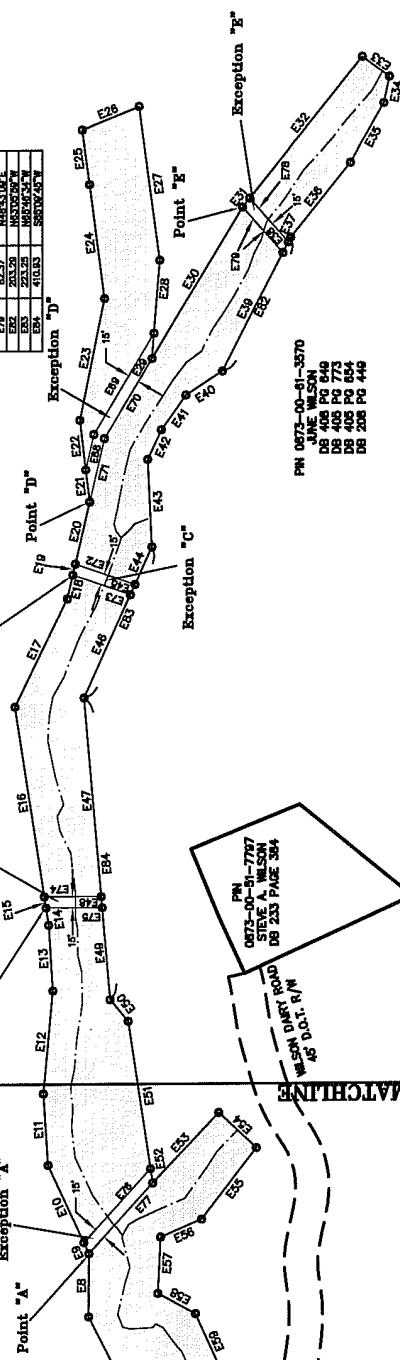
PIN 007-00-45-0348  
WACHNEY PROPERTIES  
DB 242 PG 753



VICINITY MAP  
(NOT TO SCALE)

SHEET 3 OF 4

LINE	LINE, LENGTH	BEARING	LINE, LENGTH	LINE, LENGTH
E1	SBK 324.24 E	SBK 324.24 E	E20	TAW 100.00 N
E2	SBK 324.24 E	SBK 324.24 E	E21	TAW 100.00 N
E3	SBK 324.24 E	SBK 324.24 E	E22	45.77 N
E11	97.73 S	SBK 251.25 E	E12	45.77 N
E12	140.31 S	SBK 251.25 E	E13	119.15 S
E13	86.52 S	SBK 250.01 E	E14	94.82 S
E14	2.87 S	SBK 250.01 E	E15	15.06 S
E15	51.17 S	SBK 250.01 E	E16	11.53 S
E17	76.10 S	SBK 250.01 E	E18	70.75 S
E18	53.13 S	SBK 250.01 E	E19	125.72 S
E19	16.00 S	SBK 250.01 E	E20	39.35 S
E20	86.88 S	SBK 250.01 E	E21	202.05 S
E21	76.85 S	SBK 250.01 E	E22	52.27 S
E23	67.63 S	SBK 250.01 E	E24	105.64 S
E24	184.26 S	SBK 250.01 E	E25	70.50 S
E25	73.88 S	SBK 250.01 E	E26	121.99 S
E26	81.00 S	SBK 250.01 E	E27	70.15 S
E27	206.00 S	SBK 250.01 E	E28	67.02 S
E28	31.15 S	SBK 250.01 E	E29	125.45 S
E29	238.45 S	SBK 250.01 E	E30	125.77 S
E31	16.24 S	SBK 252.25 E	E71	87.92 S
E32	243.32 S	SBK 252.25 E	E72	85.12 S
E33	46.46 S	SBK 105.79 W	E73	82.17 S
E34	56.56 S	SBK 105.79 W	E74	111.02 S
E35	59.45 S	SBK 105.79 W	E75	70.99 S
E36	120.22 S	SBK 105.79 W	E76	120.22 S
E37	71.14 S	SBK 105.79 W	E77	134.75 S
E38	161.16 S	SBK 105.79 W	E78	70.04 S



PIN 007-00-707  
STEVE A. W. EDN  
DB 243 PAGE 304

MATCHLINE  
W.E. 51' D.O.T. N  
45'

PIN 007-00-51-3570  
JUNE WILSON  
DB 408 PG 949  
DB 410 PG 973  
DB 405 PG 825  
DB 293 PG 449



GRAPHIC SCALE  
(IN FEET)  
1 inch = 100 ft.

<b>KCI ASSOCIATES OF N.C.</b> <b>ENGINEERS, SURVEYORS AND PLANNERS</b> <b>KCI</b> 4801 BEEF CREEK ROAD, SUITE 220 ASHEVILLE, NC 28803 PHONE: (828) 252-9214 • FAX: (828) 252-9246	DRAWN BY C.R.B. CONSERVATION ELEMENT DOG BITE STREAM RESTORATION MITCHELL COUNTY, NORTH CAROLINA DATE: NOV. 26, 2004 SCALE: 1" = 100 ft. SHEET: 3 OF 4
--	--



## Appendix C Project Site Photographs





Looking downstream at a long riffle/run sequence that characterizes WOC-1.



Poor riparian buffer and an eroding bank near the beginning of WOC-2.



Immediately upstream of the outlet into the irrigation pond on WOC-2.



The end of WOC-2. WOC-3 begins under the trees in the background.



A long riffle/run sequence and eroding bank near the beginning of WOC-3.



Looking upstream at the beginning of WOC-4 with the livestock barn in the background.



The waste lagoon, which will be removed, with WOC-4 at the base of the berm on the right side of the lagoon.



Upstream view of WOC-4 after it passes the waste lagoon; there have been extensive livestock impacts in this location. The lagoon berm is on the right side in this photo.



WOC-4 immediately before it becomes further entrenched in the valley.



Bank erosion along WOC-4 after the confluence with T2.



Looking down at WOC-4, which is entrenched within the valley in this section.



Bank erosion along WOC-4.



WOC-5 near the end of the project site.



The beginning of T1-1 where a headcut has developed and the stream has become incised.



Looking downstream along T1-1 where the stream is incised.



Looking downstream at the beginning of T1-2 where the channel has filled in; the tributary flows diffusely until its confluence with WOC.



Looking upstream along T2 towards Wilson Dairy Road, where there are heavy cattle impacts.



Looking upstream along T2 immediately before the confluence with WOC.

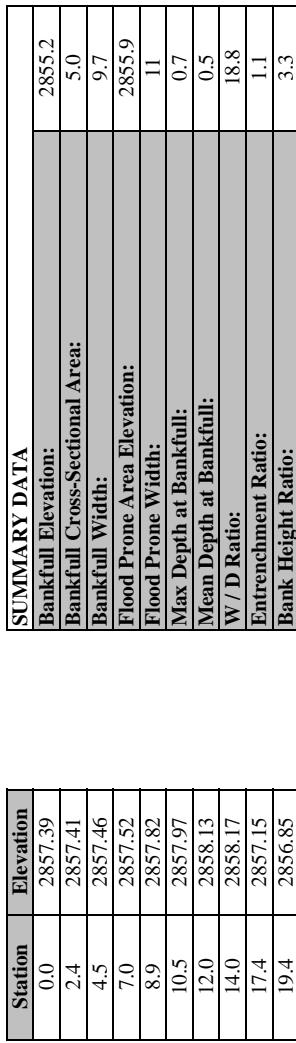


## Appendix D Existing Conditions Data

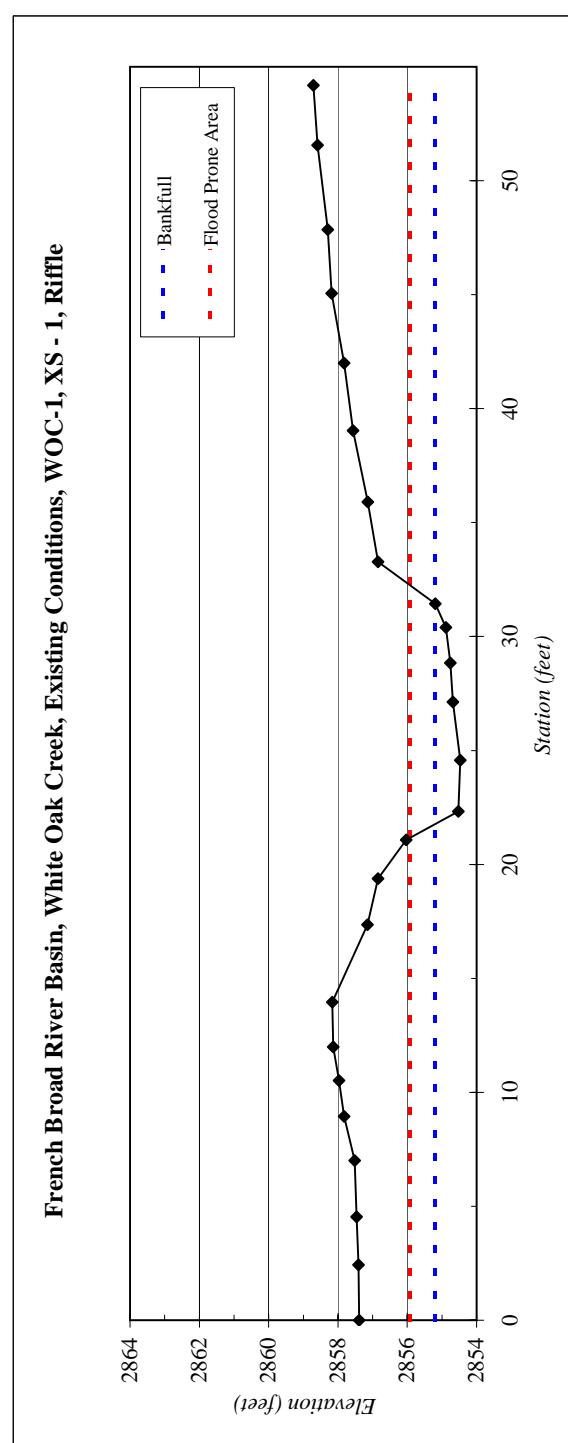


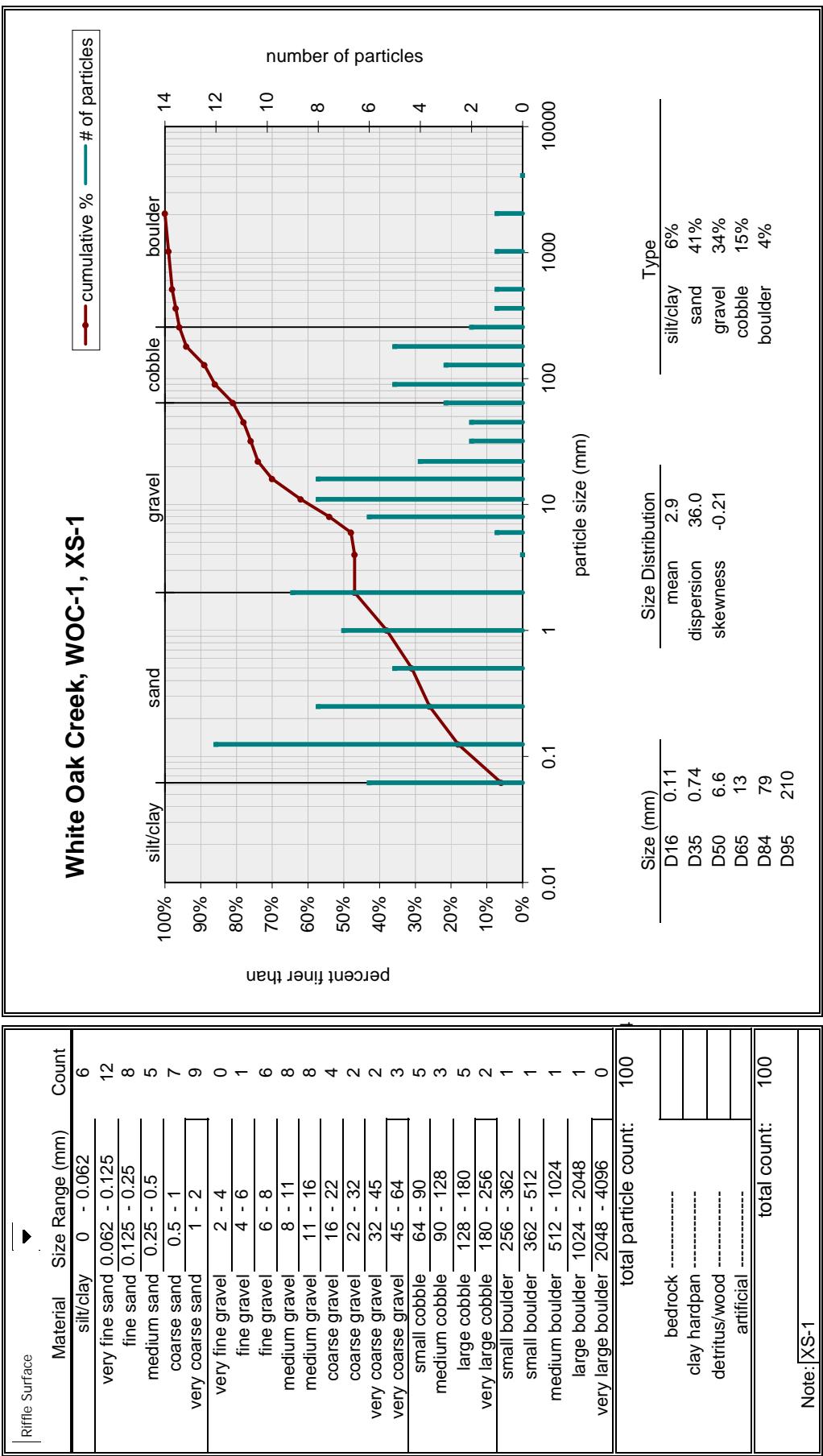


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-1
XS ID	XS - 1, Riffle
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B. Hemel, Z. Mlyneca



**French Broad River Basin, White Oak Creek, Existing Conditions, WOC-1, XS - 1, Riffle**



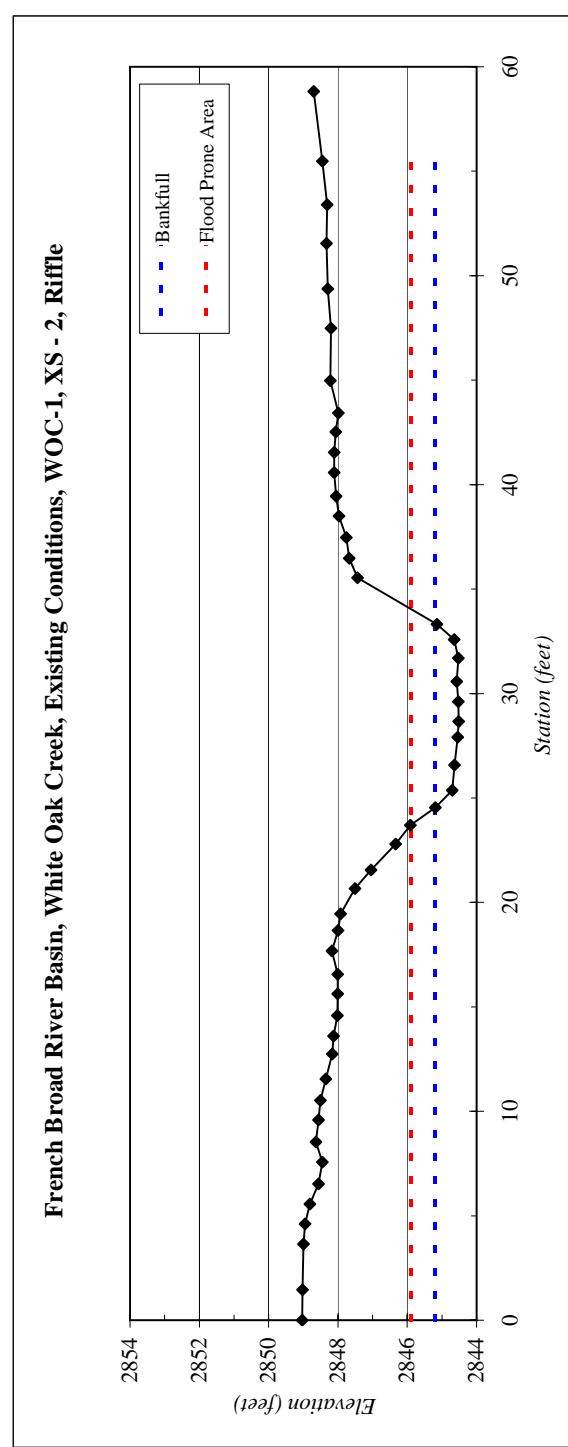


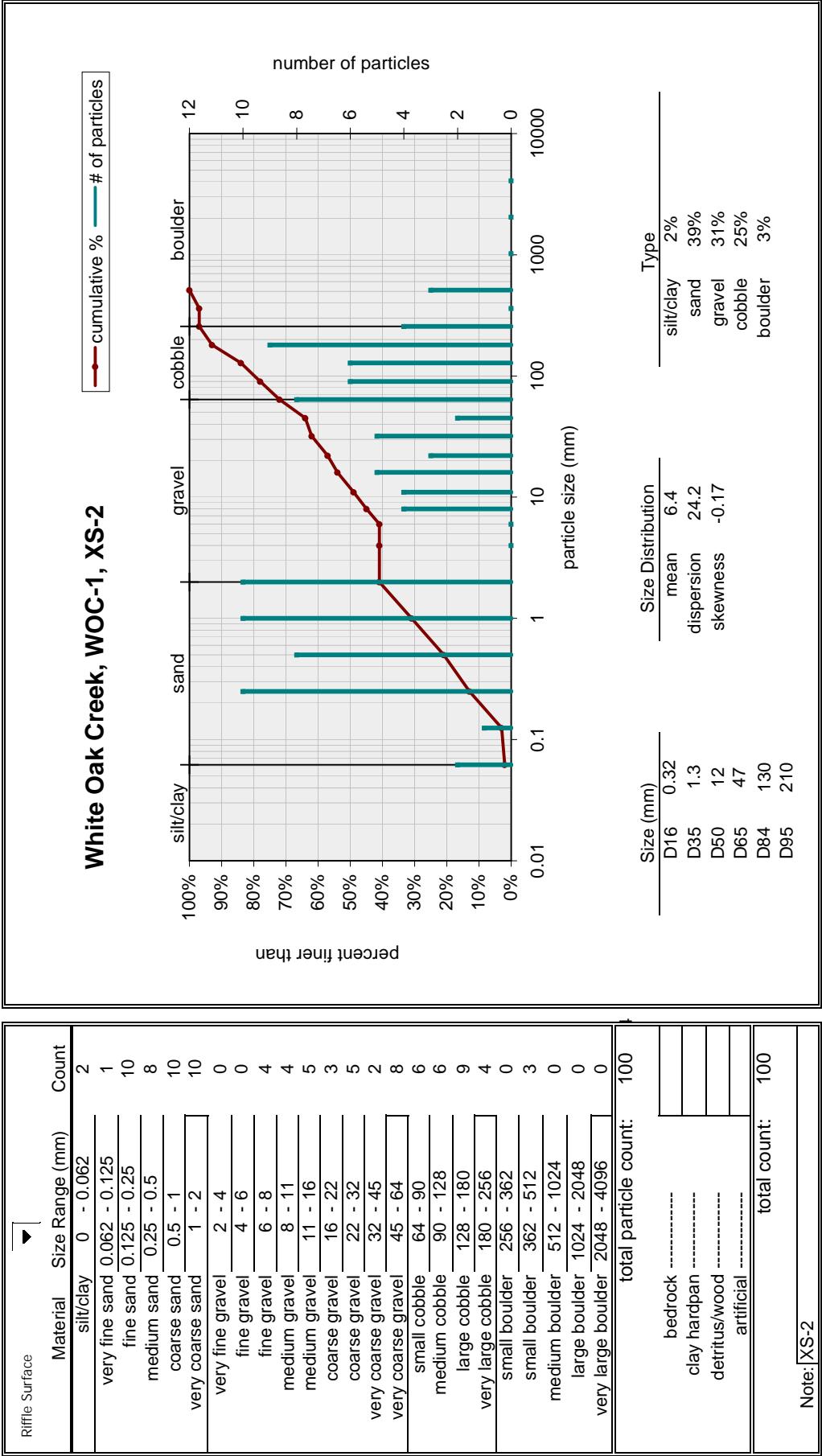


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-1
XS ID	XS - 2, Riffle
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B. Hemel, Z. Mlyneca

SUMMARY DATA	
Bankfull Elevation:	2845.2
Bankfull Cross-Sectional Area:	4.9
Bankfull Width:	8.8
Flood Prone Area Elevation:	2845.9
Flood Prone Width:	10
Max Depth at Bankfull:	0.7
Mean Depth at Bankfull:	0.6
W / D Ratio:	15.8
Entrenchment Ratio:	1.2
Bank Height Ratio:	4.2

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-1, XS - 2, Riffle



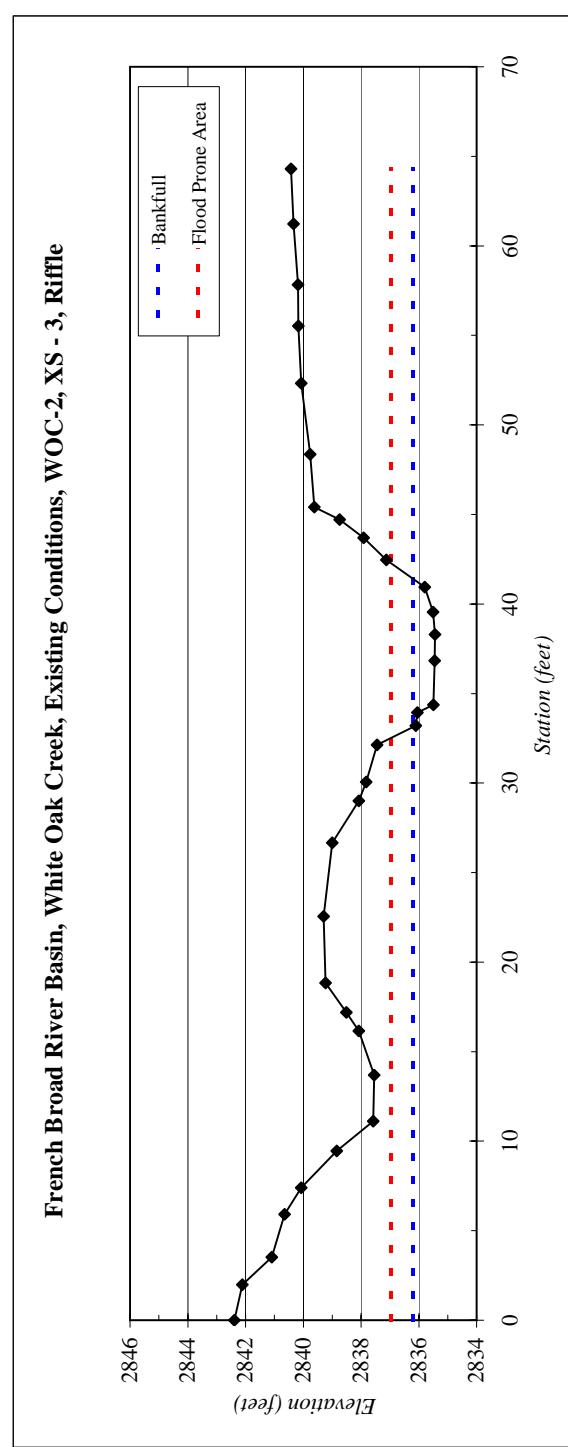


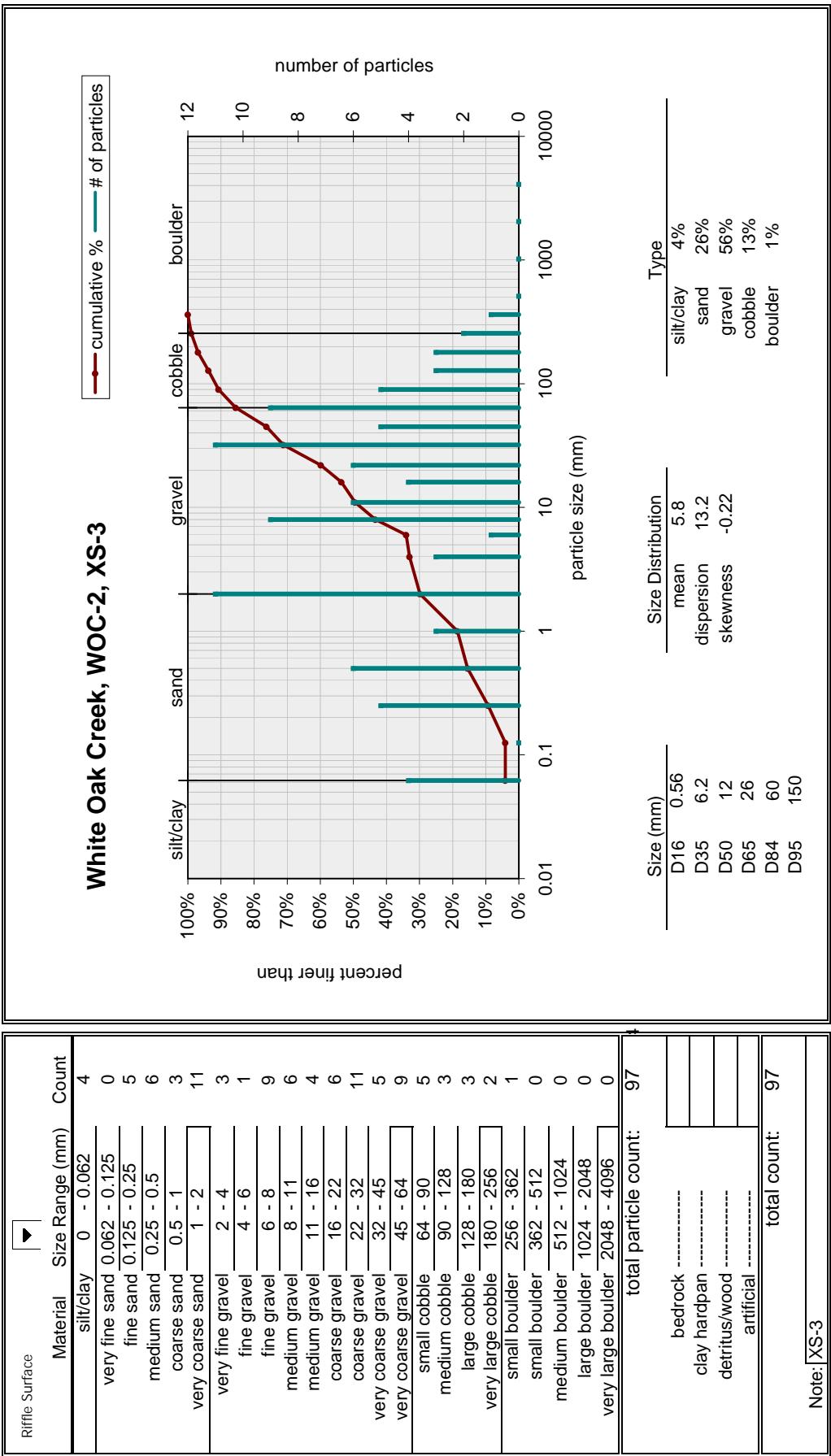


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-2
XS ID	XS - 3, Riffle
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B. Hemel, Z. Mlyneca

Station	Elevation	SUMMARY DATA
0.0	2842.38	Bankfull Elevation:
2.0	2842.11	Bankfull Cross-Sectional Area:
3.5	2841.09	Bankfull Width:
5.9	2840.65	Flood Prone Area Elevation:
7.4	2840.07	Flood Prone Width:
9.4	2838.85	Max Depth at Bankfull:
11.1	2837.58	Mean Depth at Bankfull:
13.7	2837.54	W / D Ratio:
16.2	2838.08	Entrenchment Ratio:
17.2	2838.51	Bank Height Ratio:
18.8	2839.23	
22.6	2839.29	
26.7	2839.00	
29.0	2838.07	
30.1	2837.82	
32.1	2837.45	
33.2	2836.10	
33.9	2836.05	
34.4	2835.49	
36.8	2835.45	
38.3	2835.44	
39.5	2835.50	
40.9	2835.80	
42.5	2837.12	
43.7	2837.91	
44.7	2838.75	
45.4	2839.62	
48.4	2839.76	
52.3	2840.08	
55.5	2840.17	
57.8	2840.18	
61.2	2840.34	
64.3	2840.43	

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-2, XS - 3, Riffle



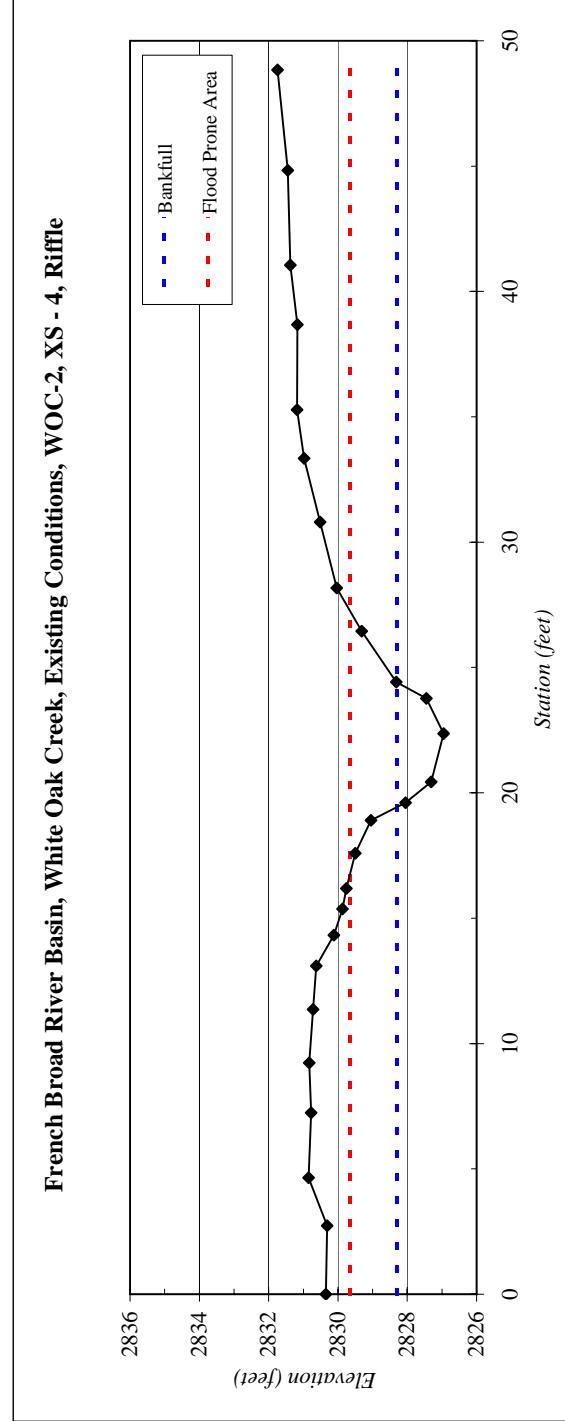


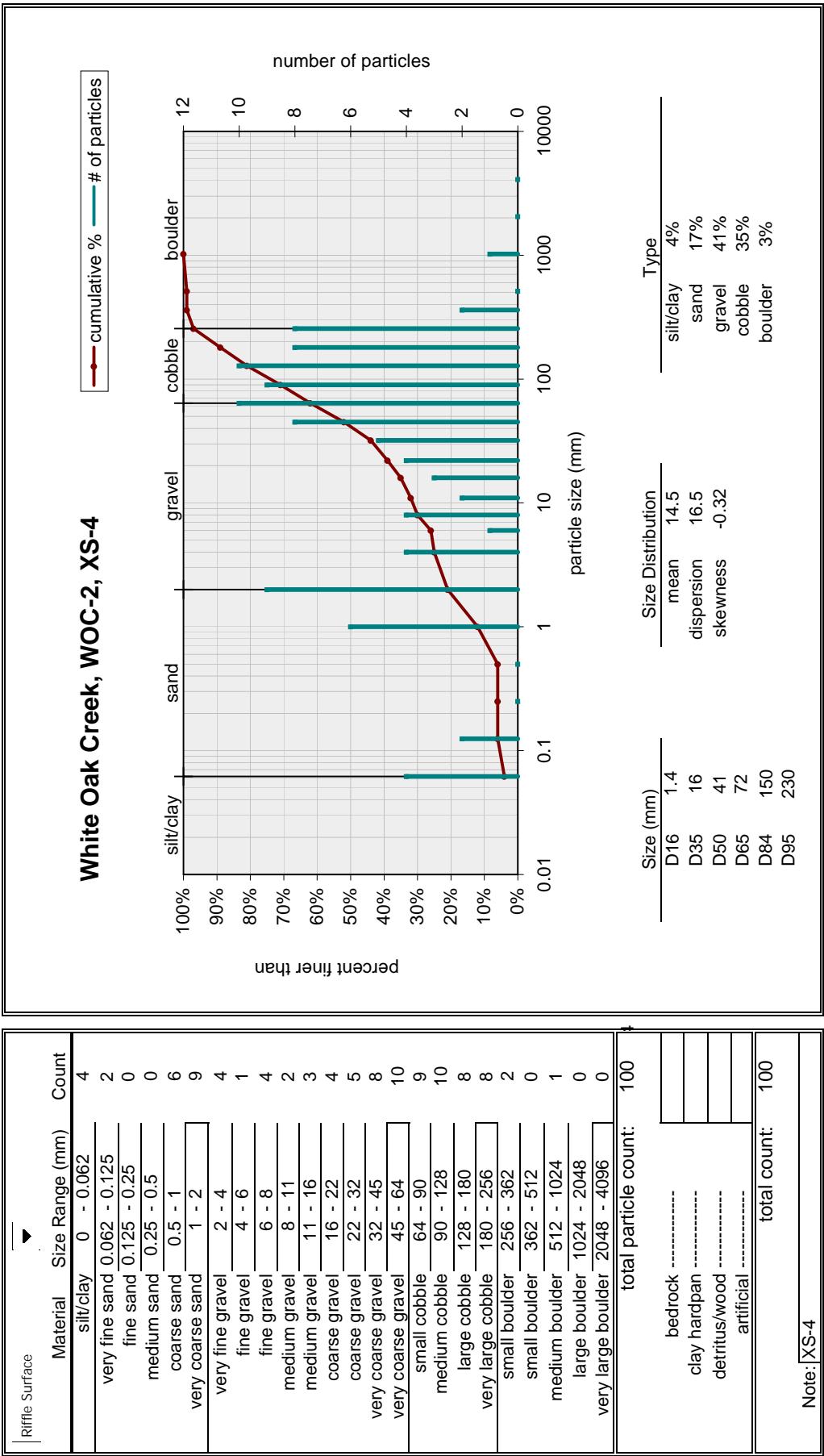


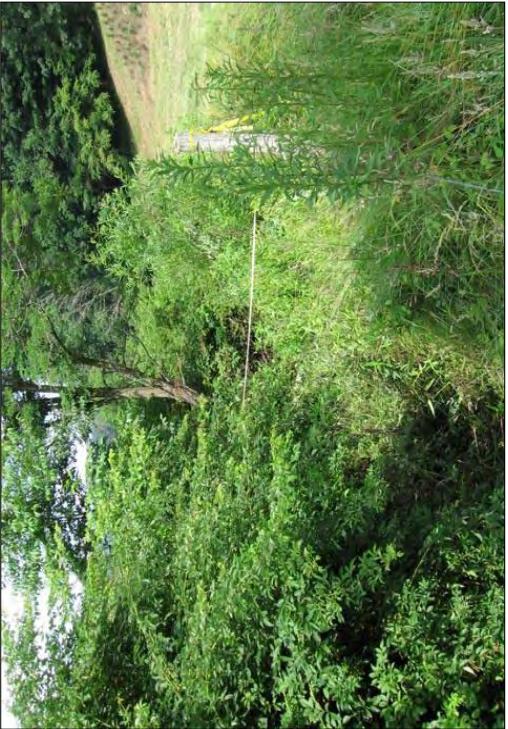
River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-2
XS ID:	XS - 4, Riffle
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B. Hemel, Z. Mlyneca

SUMMARY DATA	
Bankfull Elevation:	2828.3
Bankfull Cross-Sectional Area:	4.6
Bankfull Width:	5.0
Flood Prone Area Elevation:	2829.7
Flood Prone Width:	11
Max Depth at Bankfull:	1.4
Mean Depth at Bankfull:	0.9
W / D Ratio:	5.4
Entrenchment Ratio:	2.1
Bank Height Ratio:	1.6

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-2, XS - 4, Riffle



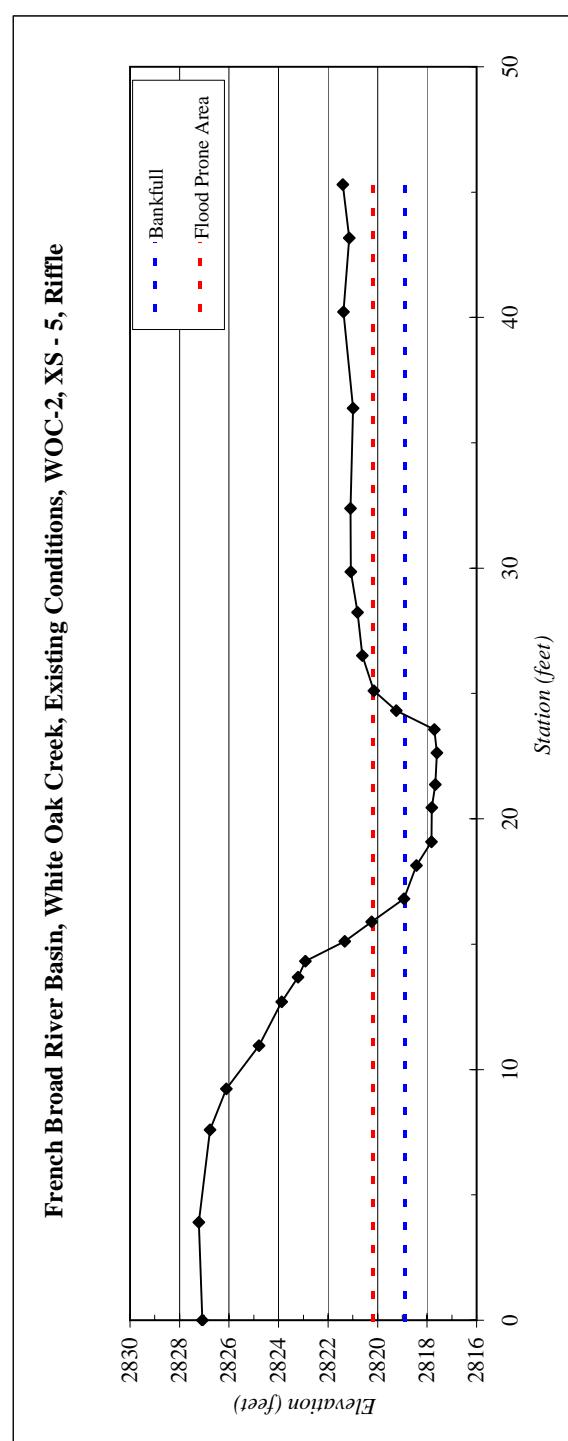




River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-2
XS ID	XS - 5, Riffle
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B. Hemel, Z. Mlyneca

SUMMARY DATA	
Bankfull Elevation:	2818.9
Bankfull Cross-Sectional Area:	6.7
Bankfull Width:	7.3
Flood Prone Area Elevation:	2830.2
Flood Prone Width:	9
Max Depth at Bankfull:	1.3
Mean Depth at Bankfull:	0.9
W / D Ratio:	8.0
Entrenchment Ratio:	1.3
Bank Height Ratio:	2.0

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-2, XS - 5, Riffle

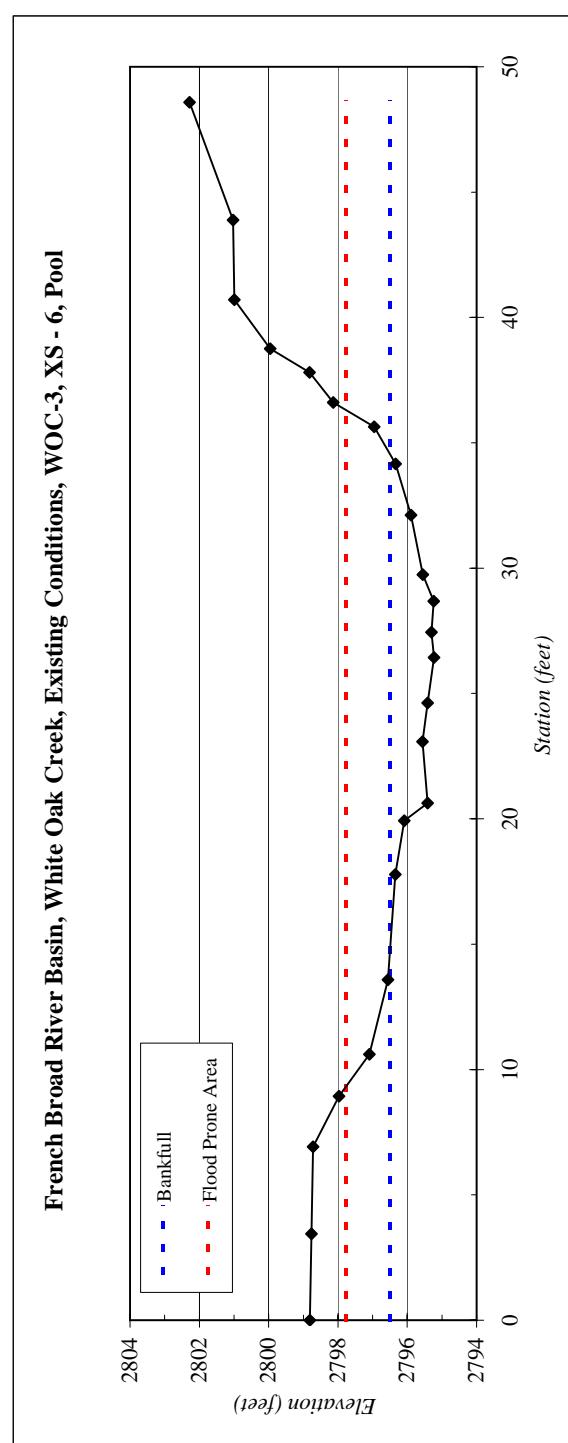




River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-3
XS ID:	XS - 6, Pool
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B. Hemel, Z. Mlyneca

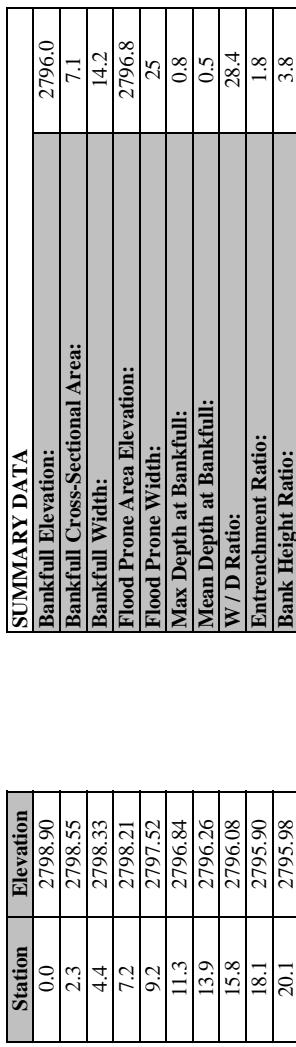
SUMMARY DATA	
Bankfull Elevation:	2796.5
Bankfull Cross-Sectional Area:	14.2
Bankfull Width:	19.8
Flood Prone Area Elevation:	2797.8
Flood Prone Width:	26
Max Depth at Bankfull:	1.3
Mean Depth at Bankfull:	0.7
W / D Ratio:	27.6
Entrenchment Ratio:	1.3
Bank Height Ratio:	2.7

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-3, XS - 6, Pool

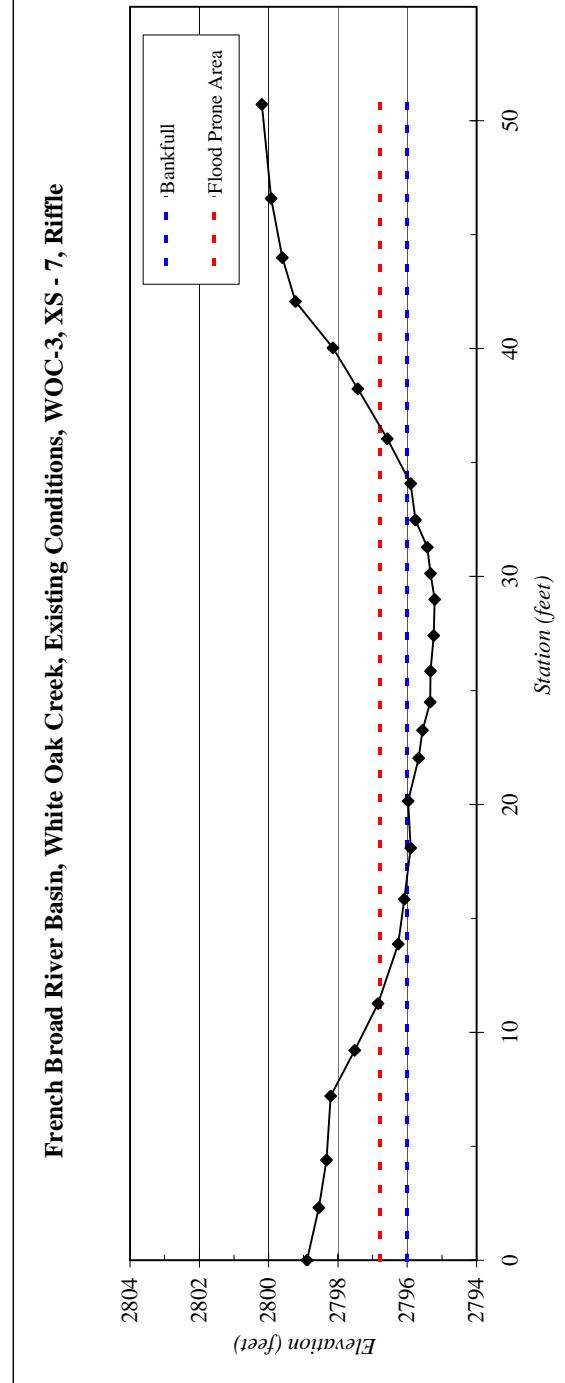


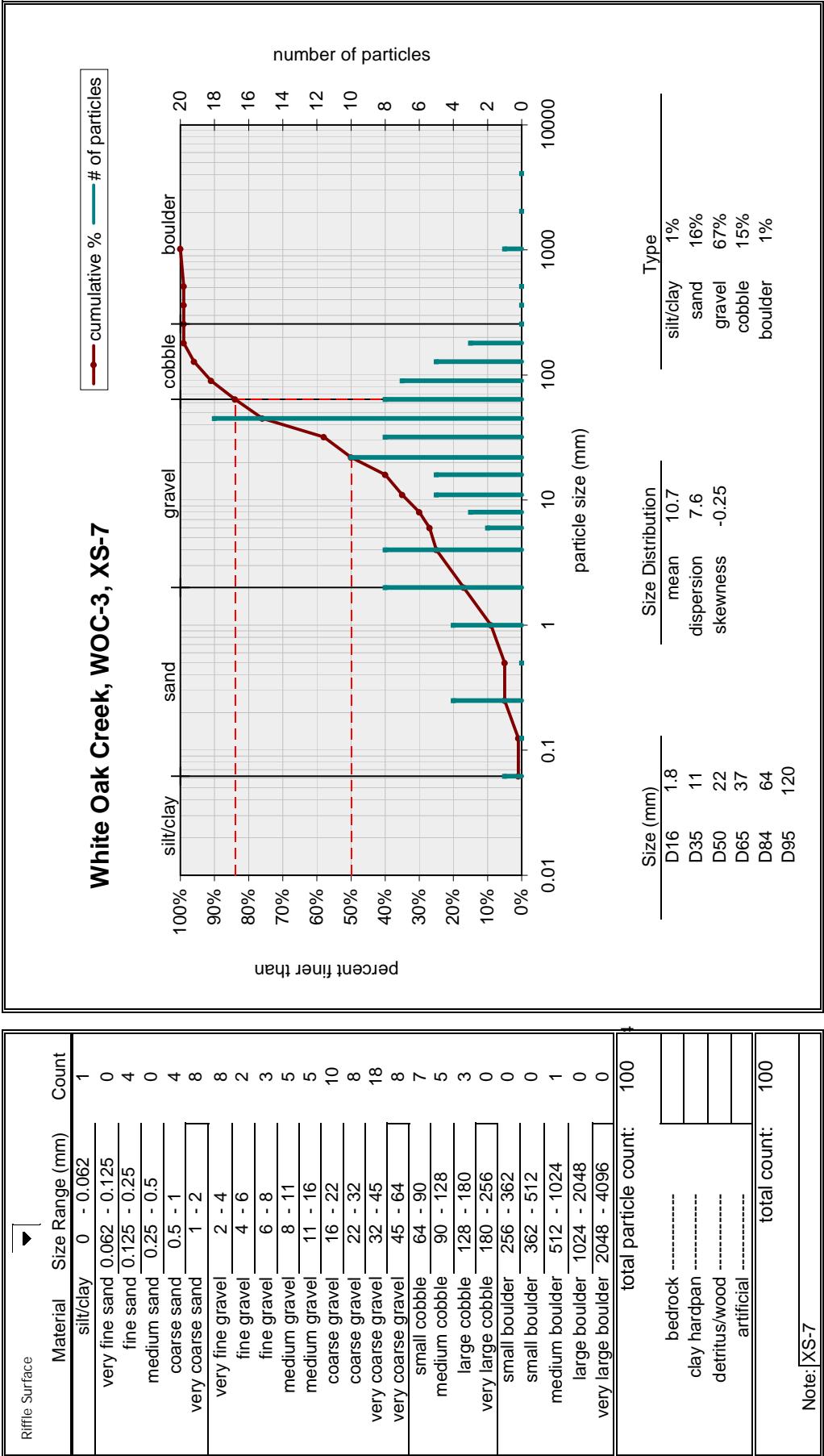


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-3
XS ID:	XS - 7, Riffle
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B. Hemel, Z. Mlyneca



### French Broad River Basin, White Oak Creek, Existing Conditions, WOC-3, XS - 7, Riffle



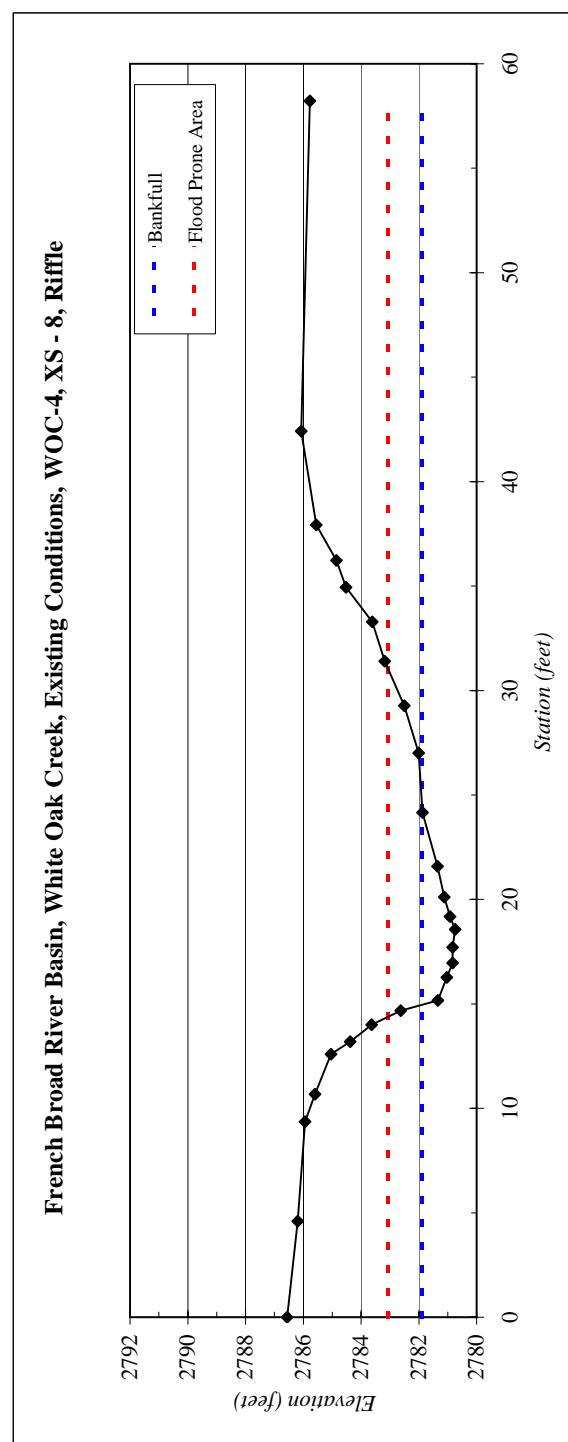




River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-4
XS ID:	XS - 8, Riffle
Drainage Area (sq mi):	0.5
Date:	2/18/2008
Field Crew:	B. Hemel, Z. Mlyneca, B. Roberts, A. Spiller

Station	Elevation	SUMMARY DATA
0.0	2786.56	Bankfull Elevation:
4.6	2786.19	Bankfull Cross-Sectional Area:
9.4	2785.94	Bankfull Width:
10.7	2785.60	Flood Prone Area Elevation:
12.6	2785.04	Flood Prone Width:
13.2	2784.37	Max Depth at Bankfull:
14.0	2783.63	Mean Depth at Bankfull:
14.7	2782.63	W / D Ratio:
15.2	2781.34	Entrenchment Ratio:
16.3	2781.03	Bank Height Ratio:
17.0	2780.83	
17.7	2780.83	
18.6	2780.75	
19.2	2780.92	
20.1	2781.12	
21.6	2781.35	
24.2	2781.87	
27.0	2782.01	Bankfull
29.3	2782.50	
31.4	2783.18	Flood Prone Area
33.3	2783.61	
34.9	2784.52	
36.2	2784.85	
37.9	2785.55	
42.4	2786.07	
58.2	2785.78	

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-4, XS - 8, Riffle

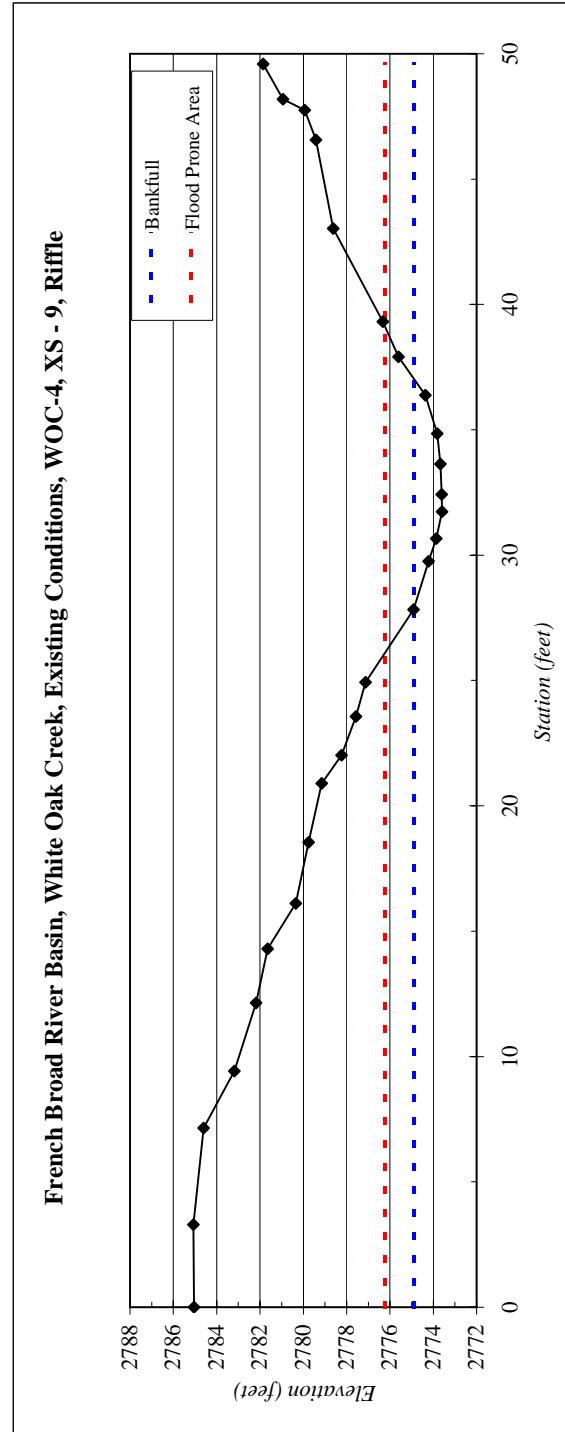


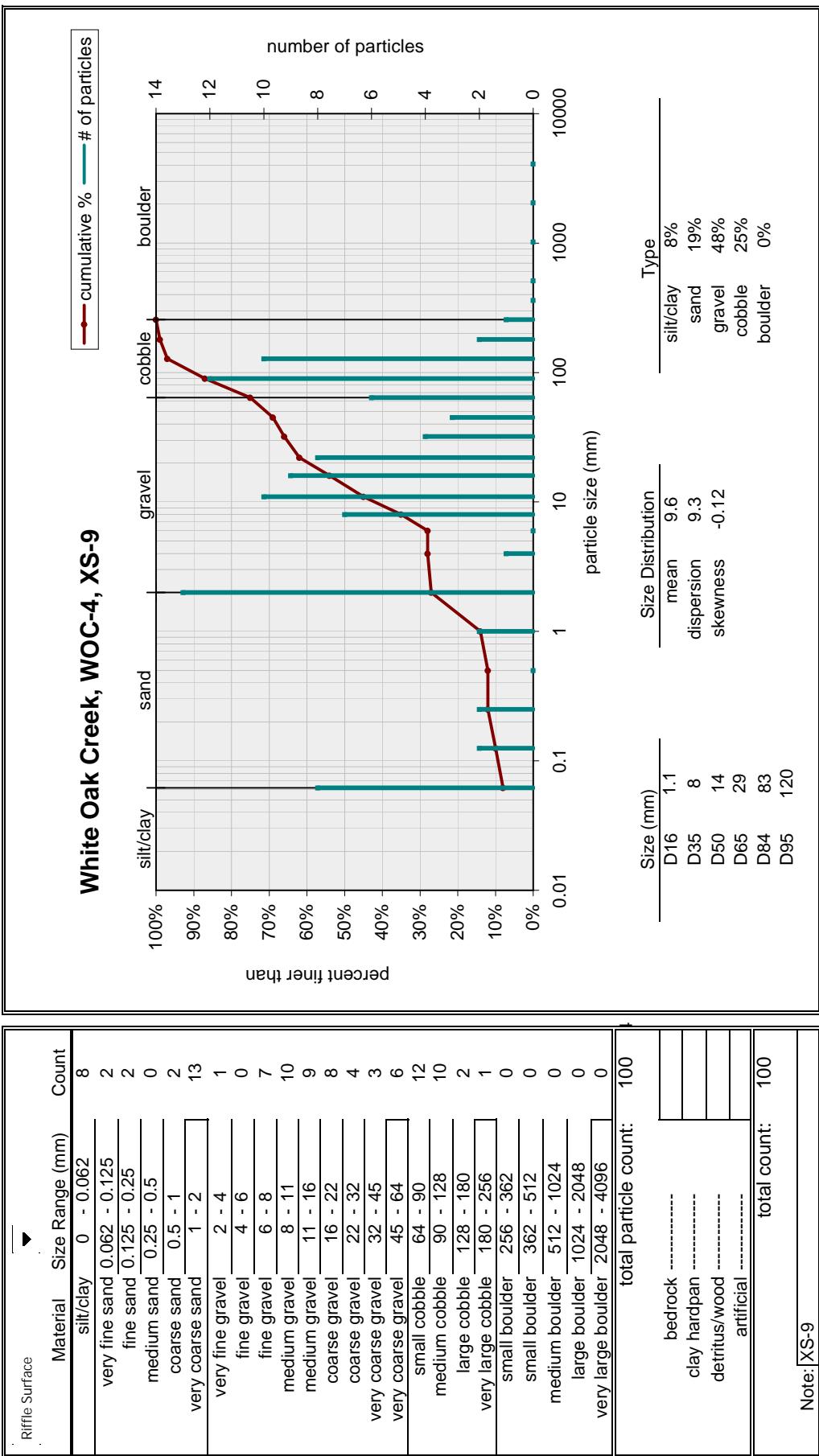


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-4
XS ID:	XS - 9, Riffle
Drainage Area (sq mi):	0.5
Date:	2/18/2008
Field Crew:	B. Hemel, Z. Mlyneca, B. Roberts, A. Spiller

Station	Elevation	SUMMARY DATA
0.0	2785.05	Bankfull Elevation:
3.3	2785.07	Bankfull Cross-Sectional Area:
7.1	2784.60	Bankfull Width:
9.4	2783.18	Flood Prone Area Elevation:
12.1	2782.18	Flood Prone Width:
14.3	2781.65	Max Depth at Bankfull:
16.1	2780.35	Mean Depth at Bankfull:
18.5	2779.75	W / D Ratio:
20.9	2779.14	Entrenchment Ratio:
22.0	2778.24	Bank Height Ratio:
23.6	2777.58	
24.9	2777.13	
27.8	2774.91	
29.8	2774.22	
30.7	2773.86	
31.7	2773.59	
32.4	2773.61	
33.6	2773.67	Bankfull
34.8	2773.81	
36.4	2774.37	Flood Prone Area
37.9	2775.60	
39.3	2776.33	
43.0	2778.61	
46.6	2779.41	
47.7	2779.94	
48.2	2780.94	
49.6	2781.86	

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-4, XS - 9, Riffle



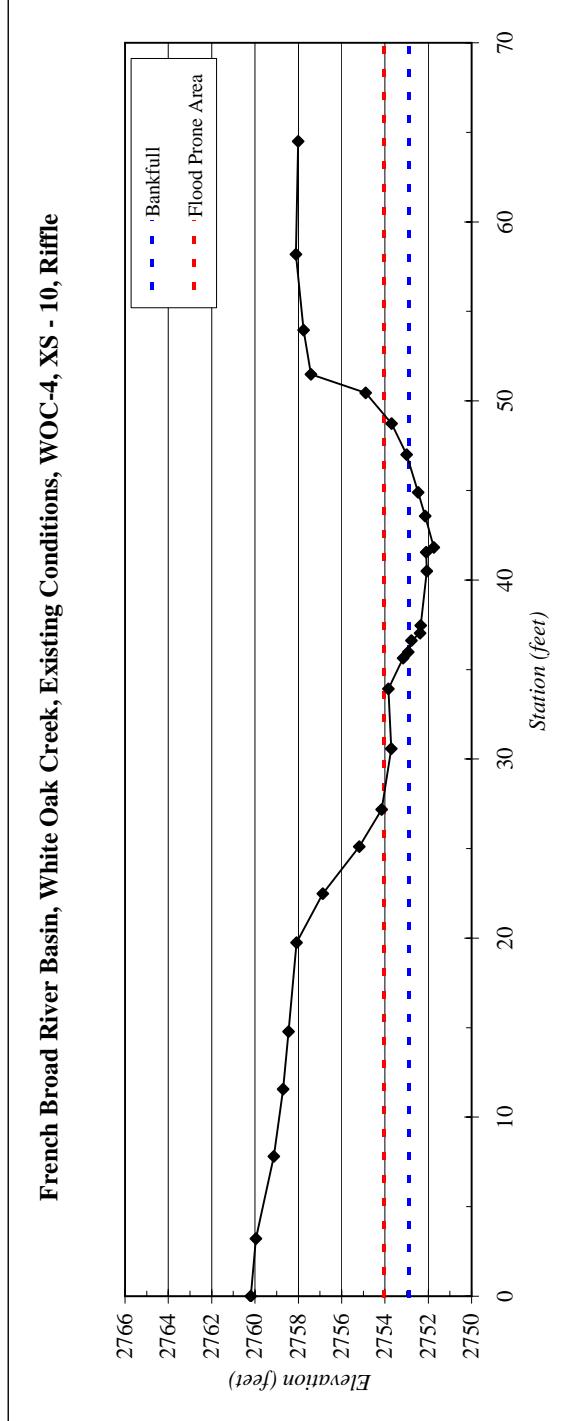


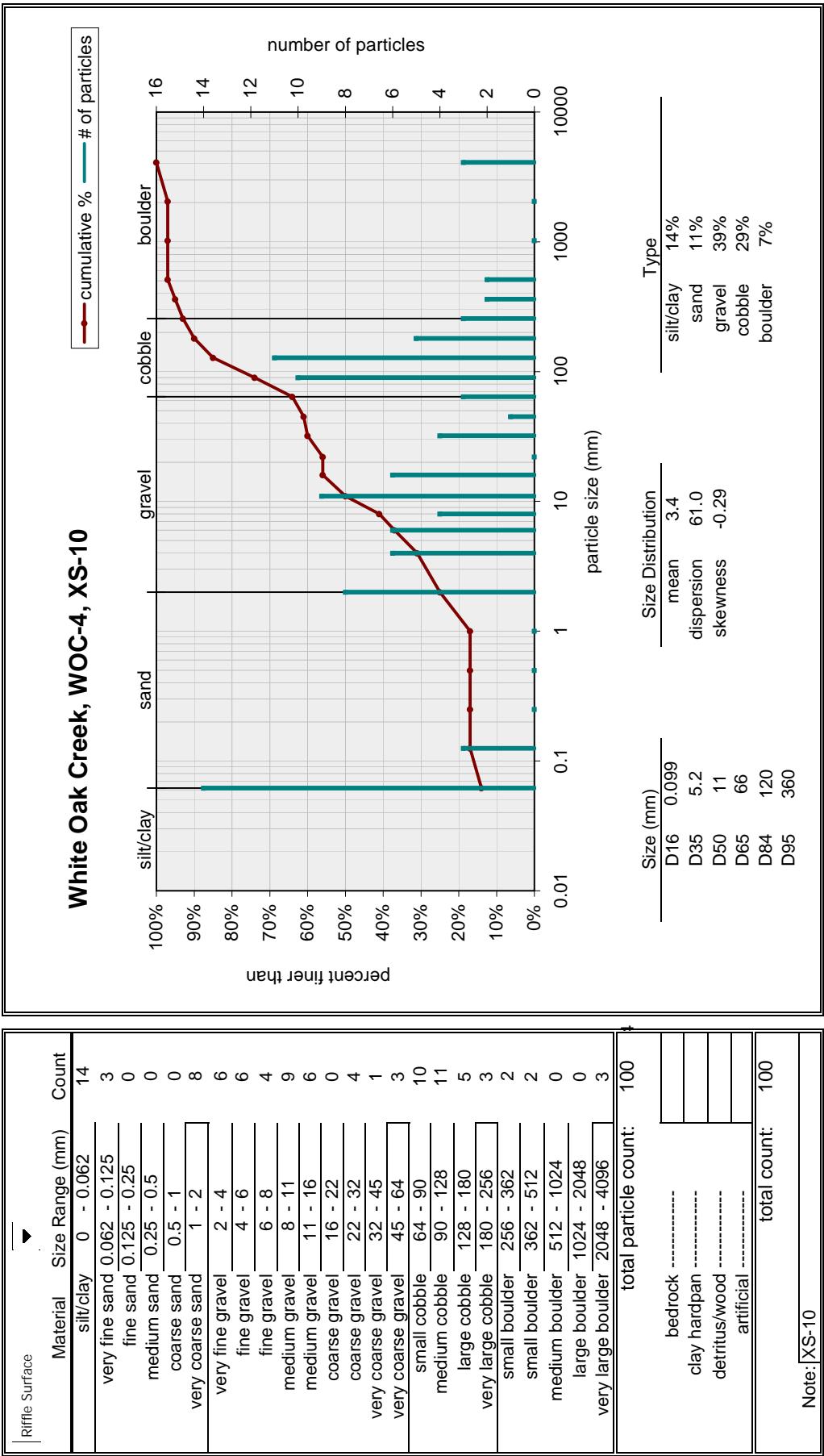


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-4
XS ID:	XS - 10, Riffle
Drainage Area (sq mi):	0.5
Date:	2/18/2008
Field Crew:	B. Hemel, Z. Mlyneca, B. Roberts, A. Spiller

Station	Elevation	SUMMARY DATA
0.0	2760.20	Bankfull Elevation:
3.2	2759.96	Bankfull Cross-Sectional Area:
7.8	2759.13	Bankfull Width:
11.6	2758.70	Flood Prone Area Elevation:
14.8	2758.45	Flood Prone Area Width:
19.7	2758.07	Max Depth at Bankfull:
22.5	2756.87	Mean Depth at Bankfull:
25.1	2755.19	W / D Ratio:
27.2	2754.15	Entrenchment Ratio:
30.6	2753.71	Bank Height Ratio:
33.9	2753.84	
35.6	2753.15	
36.0	2752.92	
36.6	2752.78	
37.0	2752.38	
37.5	2752.35	
40.5	2752.07	
41.6	2752.09	
41.8	2751.75	
43.6	2752.14	
44.9	2752.47	
47.0	2753.00	
48.7	2753.69	
50.5	2754.88	
51.5	2757.42	
53.9	2757.75	
58.2	2758.11	
64.5	2758.00	
69.7	2758.71	

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-4, XS - 10, Riffle



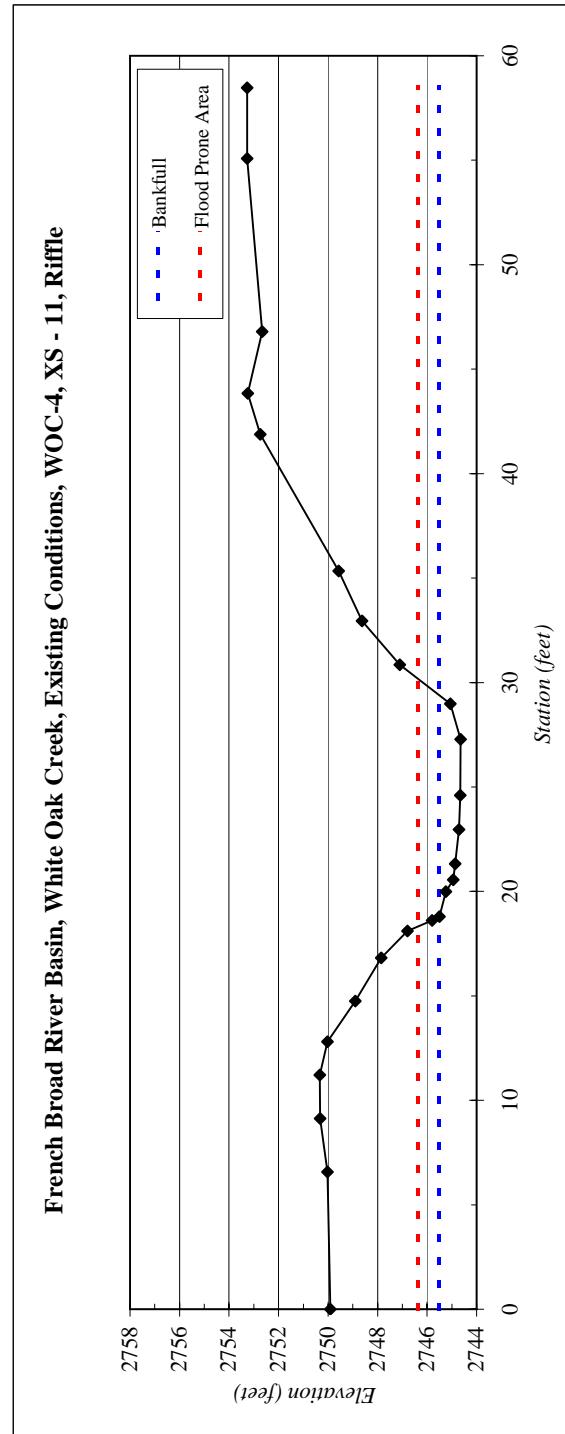




River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-4
XS ID:	XS - 11, Riffle
Drainage Area (sq mi):	0.5
Date:	2/18/2008
Field Crew:	B. Hemel, Z. Mlyneca, B. Roberts, A. Spiller

Station	Elevation	SUMMARY DATA
0.0	2749.91	Bankfull Elevation: 2745.5
6.6	2750.03	Bankfull Cross-Sectional Area: 6.8
9.1	2750.32	Bankfull Width: 10.6
11.2	2750.33	Flood Prone Area Elevation: 2746.4
12.8	2750.03	Flood Prone Width: 12
14.8	2748.89	Max Depth at Bankfull: 0.9
16.8	2747.85	Mean Depth at Bankfull: 0.6
18.1	2746.79	W / D Ratio: 16.5
18.6	2745.80	Entrenchment Ratio: 1.1
18.8	2745.50	Bank Height Ratio: 2.9
20.0	2745.25	
20.6	2744.94	
21.3	2744.87	
23.0	2744.71	
24.6	2744.66	
27.3	2744.65	
29.0	2745.06	
30.8	2747.10	
32.9	2748.63	
35.3	2749.58	
41.9	2752.74	
43.8	2753.24	
46.8	2752.66	
55.1	2753.26	
58.5	2753.27	

#### French Broad River Basin, White Oak Creek, Existing Conditions, WOC-4, XS - 11, Riffle

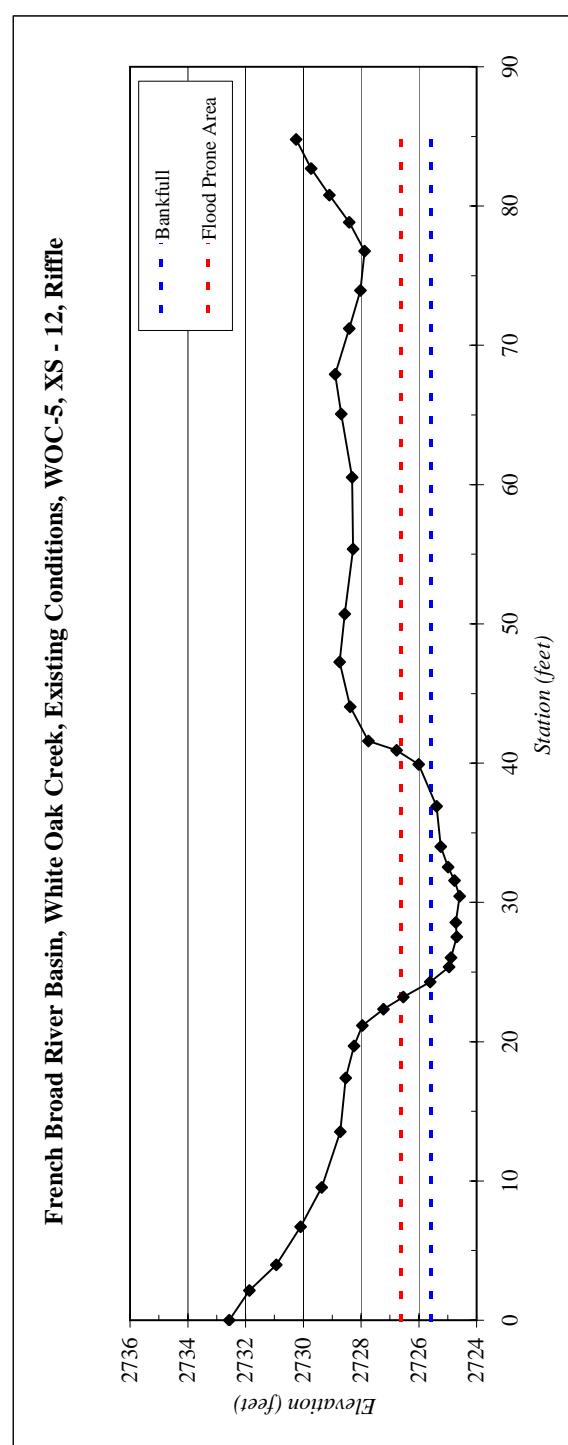


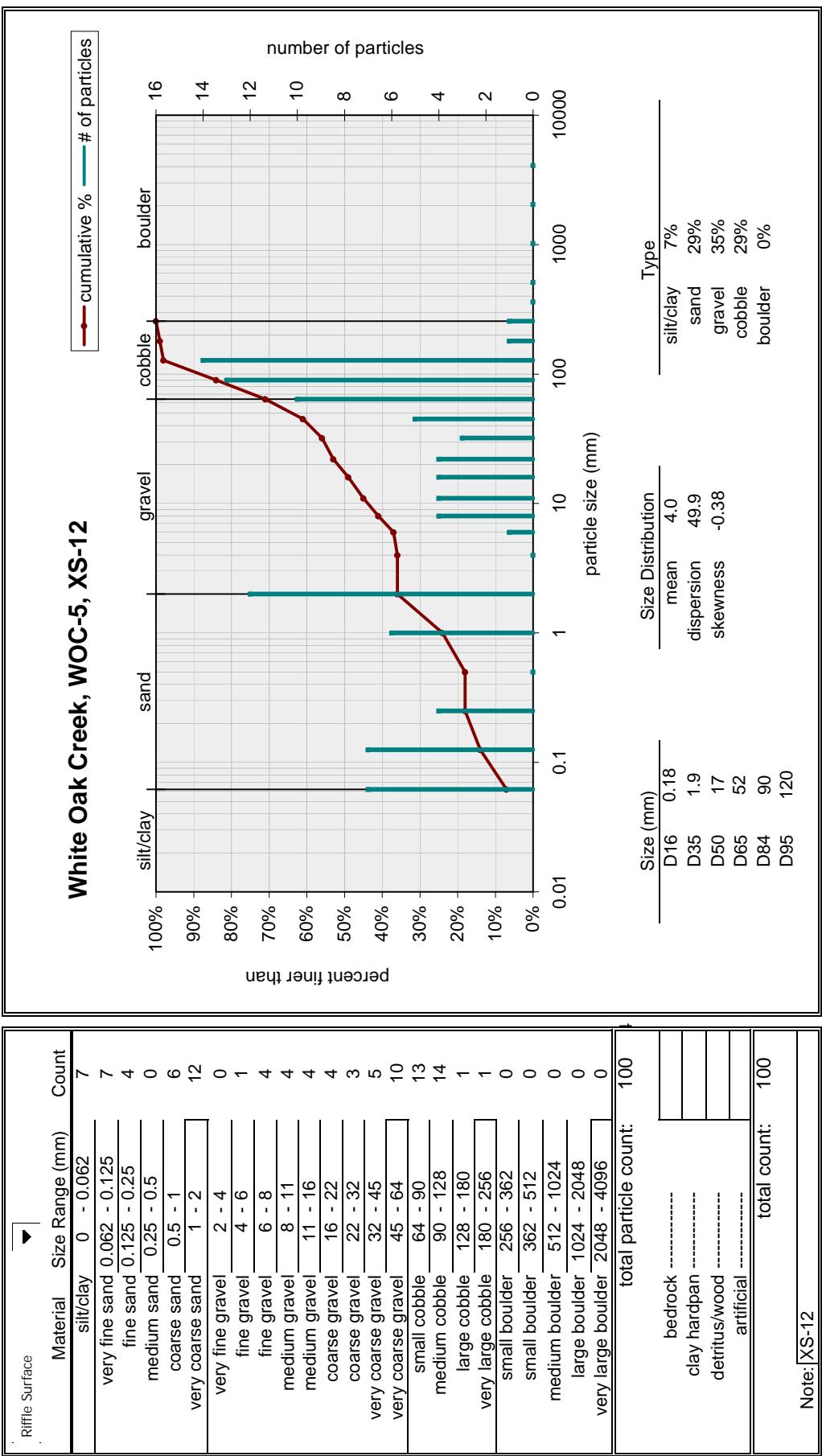


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-5
XS ID	XS - 12, Riffle
Drainage Area (sq mi):	0.5
Date:	2/18/2008
Field Crew:	B. Hemel, Z. Mlyneca, B. Roberts, A. Spiller

Station	Elevation	SUMMARY DATA
0.0	2732.57	Bankfull Elevation:
2.1	2731.86	Bankfull Cross-Sectional Area:
4.0	2730.93	Bankfull Width:
6.7	2730.09	Flood Prone Area Elevation:
9.5	2729.36	Flood Prone Width:
13.5	2728.72	Max Depth at Bankfull:
17.4	2728.53	Mean Depth at Bankfull:
19.7	2728.25	W / D Ratio:
21.2	2727.95	Entrenchment Ratio:
22.3	2727.23	Bank Height Ratio:
23.2	2726.54	
24.3	2725.60	
25.4	2724.96	
26.0	2724.89	
27.5	2724.69	
28.6	2724.72	
30.4	2724.59	
31.6	2724.77	
32.5	2724.99	
34.0	2725.24	
36.9	2725.38	
39.9	2726.00	
40.9	2726.77	
41.6	2727.75	
44.1	2728.37	
47.3	2728.74	
50.7	2728.57	
55.4	2728.28	
76.8	2727.88	
78.8	2728.41	
80.8	2729.10	
82.7	2729.72	
84.8	2730.24	

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-5, XS - 12, Riffle



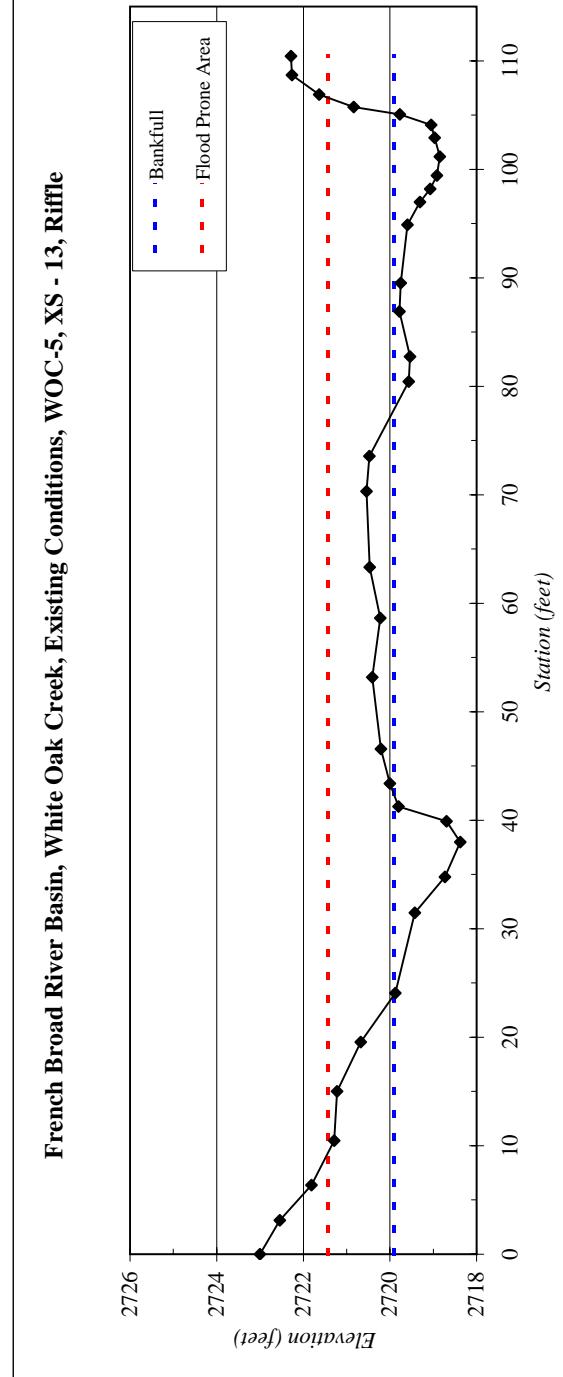


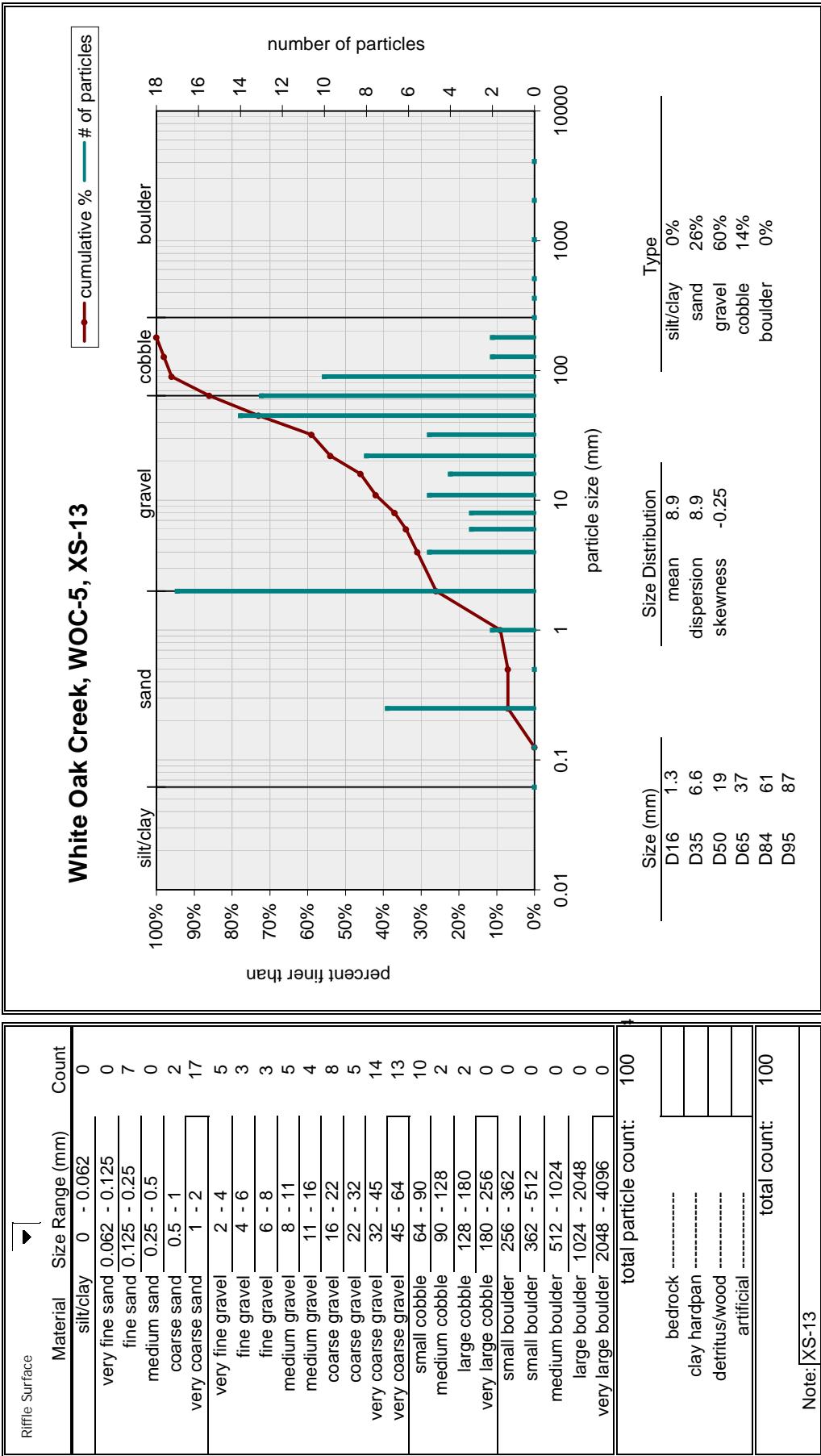


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions, WOC-5
XS ID:	XS - 13, Riffle
Drainage Area (sq mi):	0.5
Date:	2/18/2008
Field Crew:	B. Hemel, Z. Mlyneca, B. Roberts, A. Spiller

Station	Elevation	SUMMARY DATA
0.0	2723.00	Bankfull Elevation:
3.1	2722.54	Bankfull Cross-Sectional Area:
6.4	2721.81	Bankfull Width:
10.5	2721.29	Flood Prone Area Elevation:
15.0	2721.22	Flood Prone Area Width:
19.6	2720.67	Max Depth at Bankfull:
24.1	2719.88	Mean Depth at Bankfull:
31.5	2719.43	W / D Ratio:
34.8	2718.73	Entrenchment Ratio:
38.0	2718.38	Bank Height Ratio:
39.9	2718.70	
41.3	2719.80	
43.4	2720.00	
46.6	2720.21	
53.2	2720.41	
58.6	2720.22	
63.3	2720.47	
70.3	2720.54	
73.6	2720.48	
80.4	2719.56	
82.7	2719.54	
86.9	2719.78	
89.5	2719.75	
94.9	2719.59	
97.0	2719.31	
98.2	2719.07	
99.4	2718.92	
101.2	2718.85	
106.9	2721.64	
108.7	2722.26	
110.4	2722.29	

French Broad River Basin, White Oak Creek, Existing Conditions, WOC-5, XS - 13, Riffle



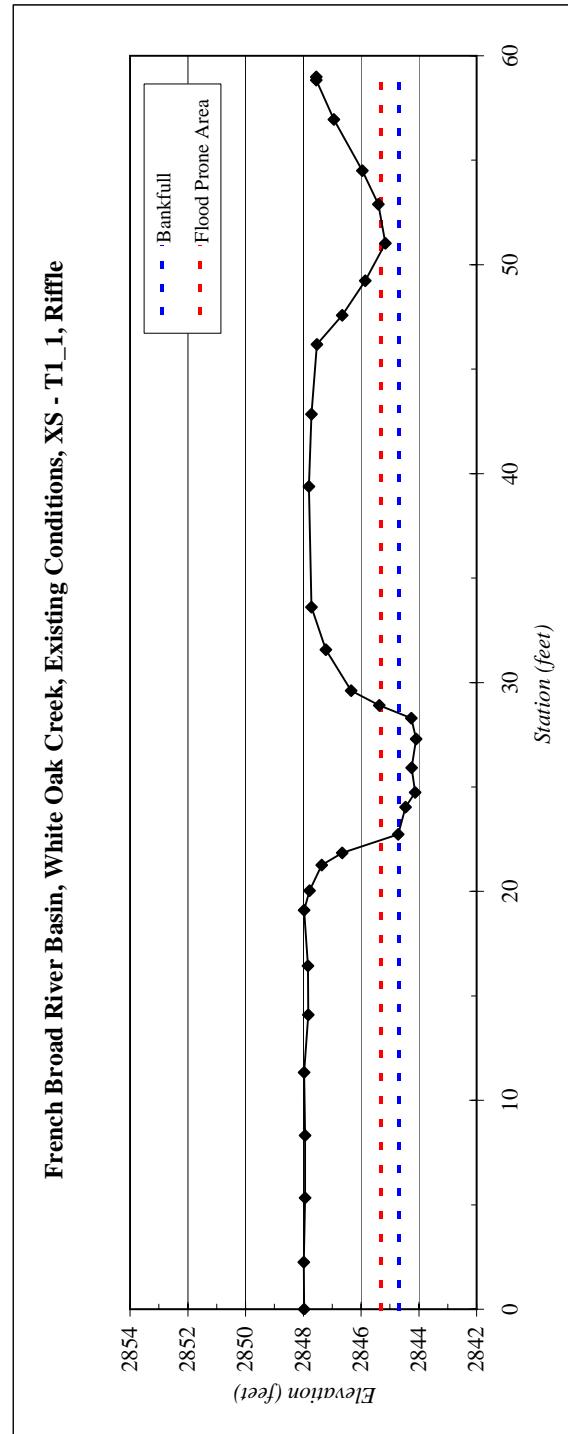


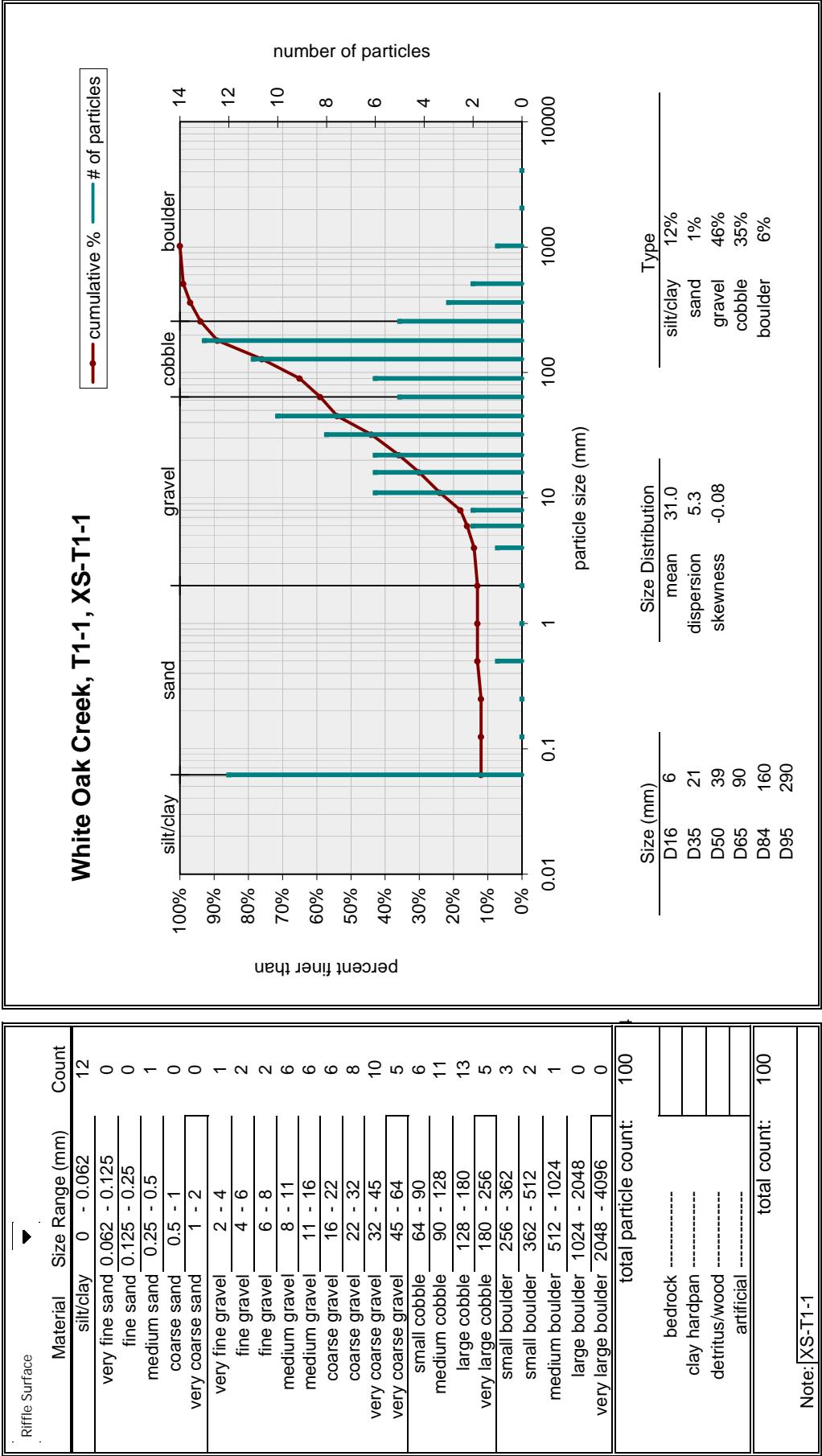


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions
XS ID:	XS - T1_1, Riffle
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B.Hemel, Z. Mlyneca

Station	Elevation	SUMMARY DATA
0.0	2847.98	Bankfull Elevation:
2.3	2847.98	Bankfull Cross-Sectional Area:
5.3	2847.93	Bankfull Width:
8.3	2847.94	Flood Prone Area Elevation:
11.3	2847.97	Flood Prone Width:
14.1	2847.83	Max Depth at Bankfull:
16.4	2847.84	Mean Depth at Bankfull:
19.1	2847.97	W / D Ratio:
20.0	2847.78	Entrenchment Ratio:
21.3	2847.36	Bank Height Ratio:
21.8	2846.65	
22.7	2844.71	
24.0	2844.46	
24.7	2844.13	
25.9	2844.25	
27.3	2844.09	
28.3	2844.26	
28.9	2845.37	
29.6	2846.34	
31.6	2847.22	
33.6	2847.71	
39.4	2847.80	
42.8	2847.71	
46.2	2847.52	
47.6	2846.65	
49.2	2845.86	
51.0	2845.16	
52.9	2845.40	
54.5	2845.95	
57.0	2846.94	
58.8	2847.56	
59.0	2847.56	

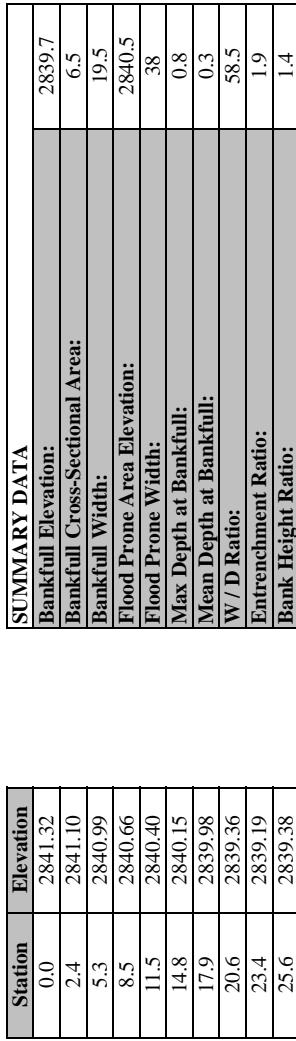
French Broad River Basin, White Oak Creek, Existing Conditions, XS - T1\_1, Riffle



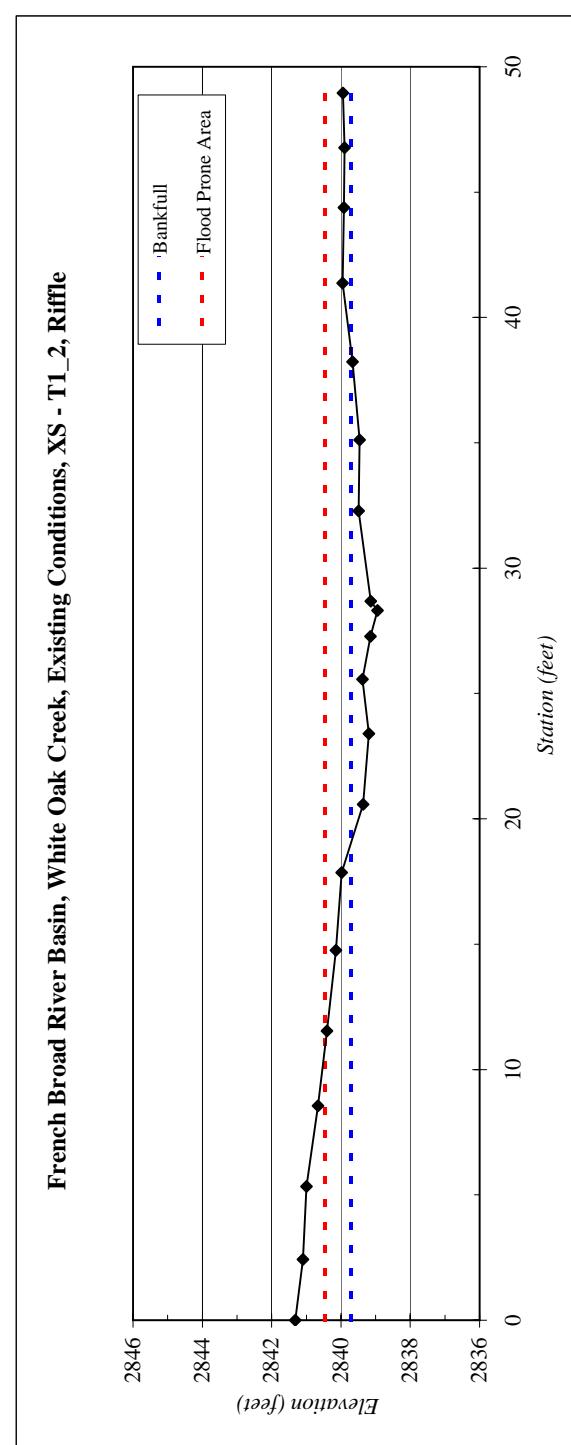


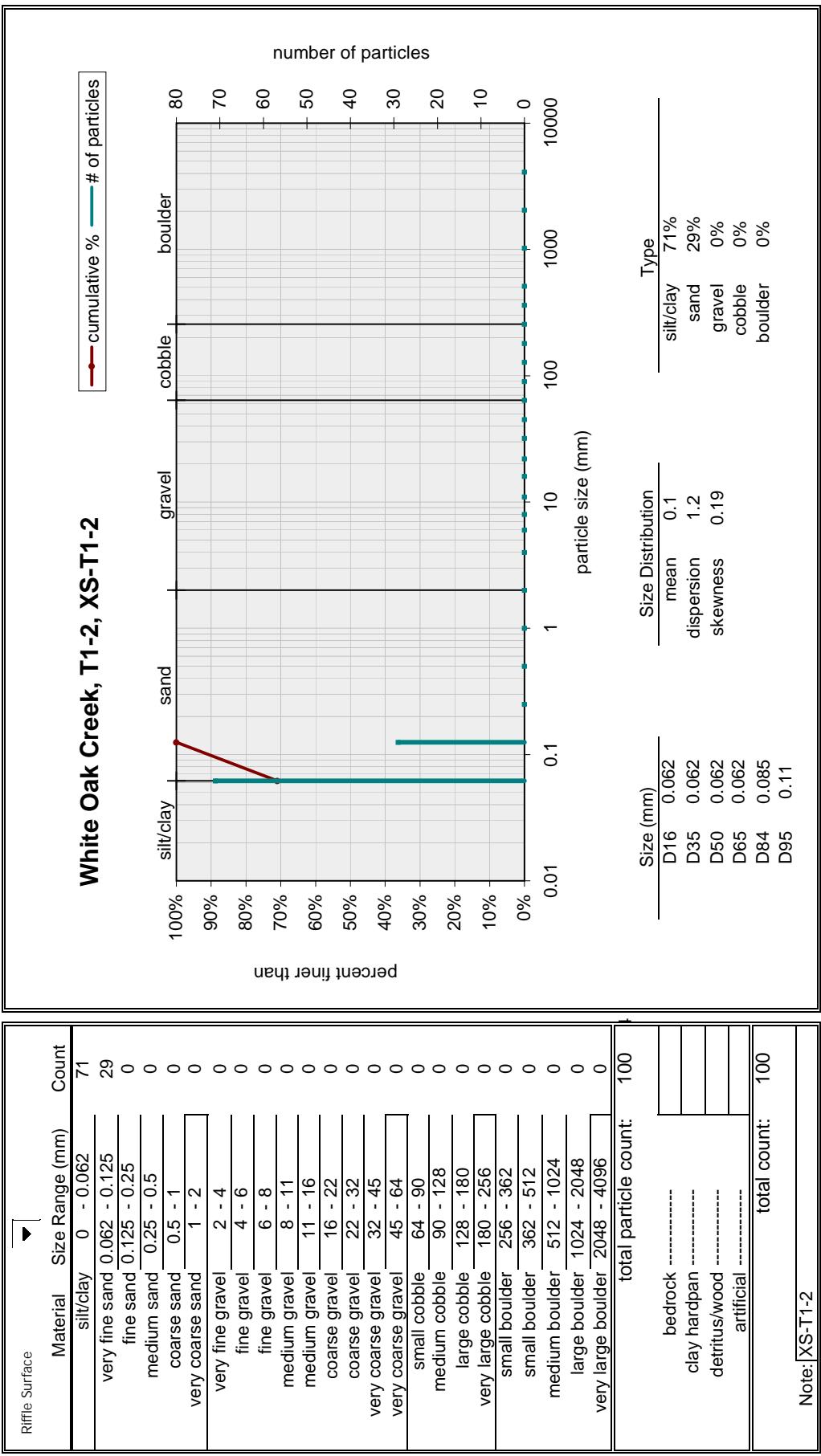


River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions
XS ID:	XS - T1_2, Riffle
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B. Hemel, Z. Mlyneca



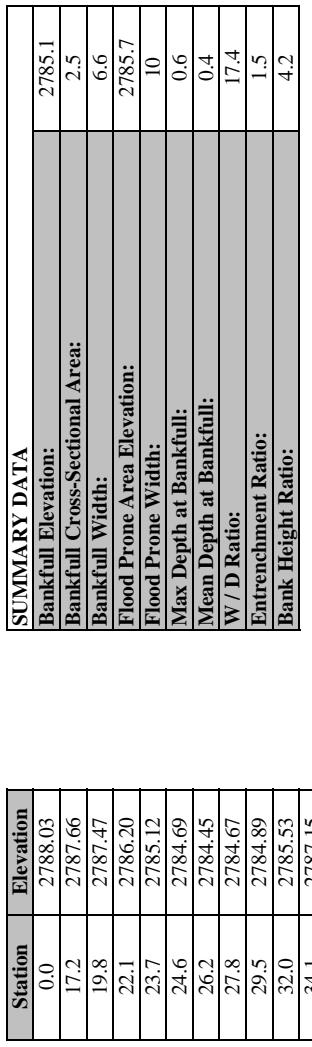
### French Broad River Basin, White Oak Creek, Existing Conditions, XS - T1\_2, Riffle



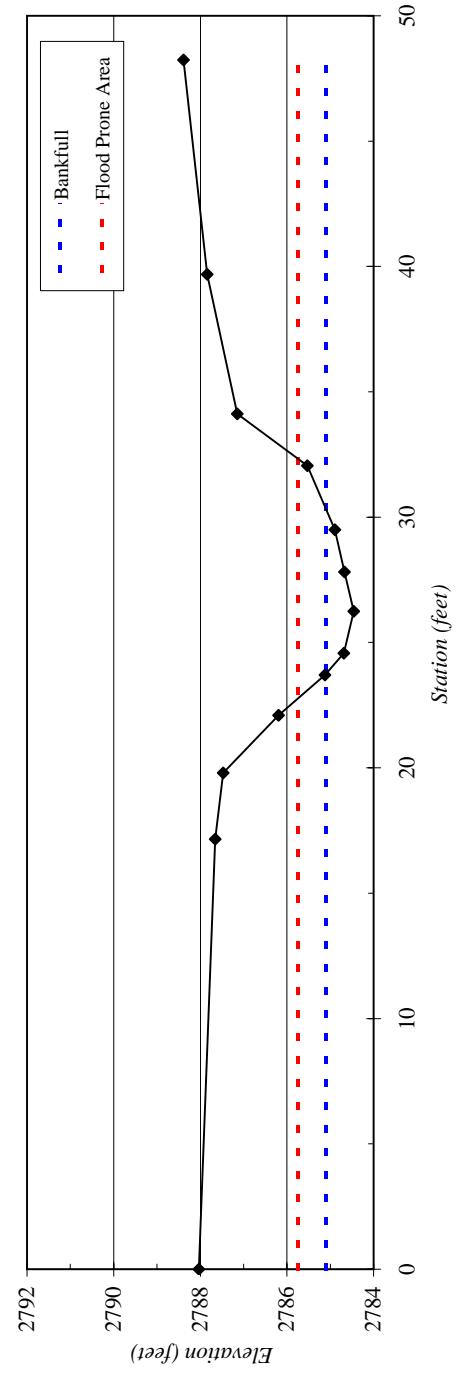


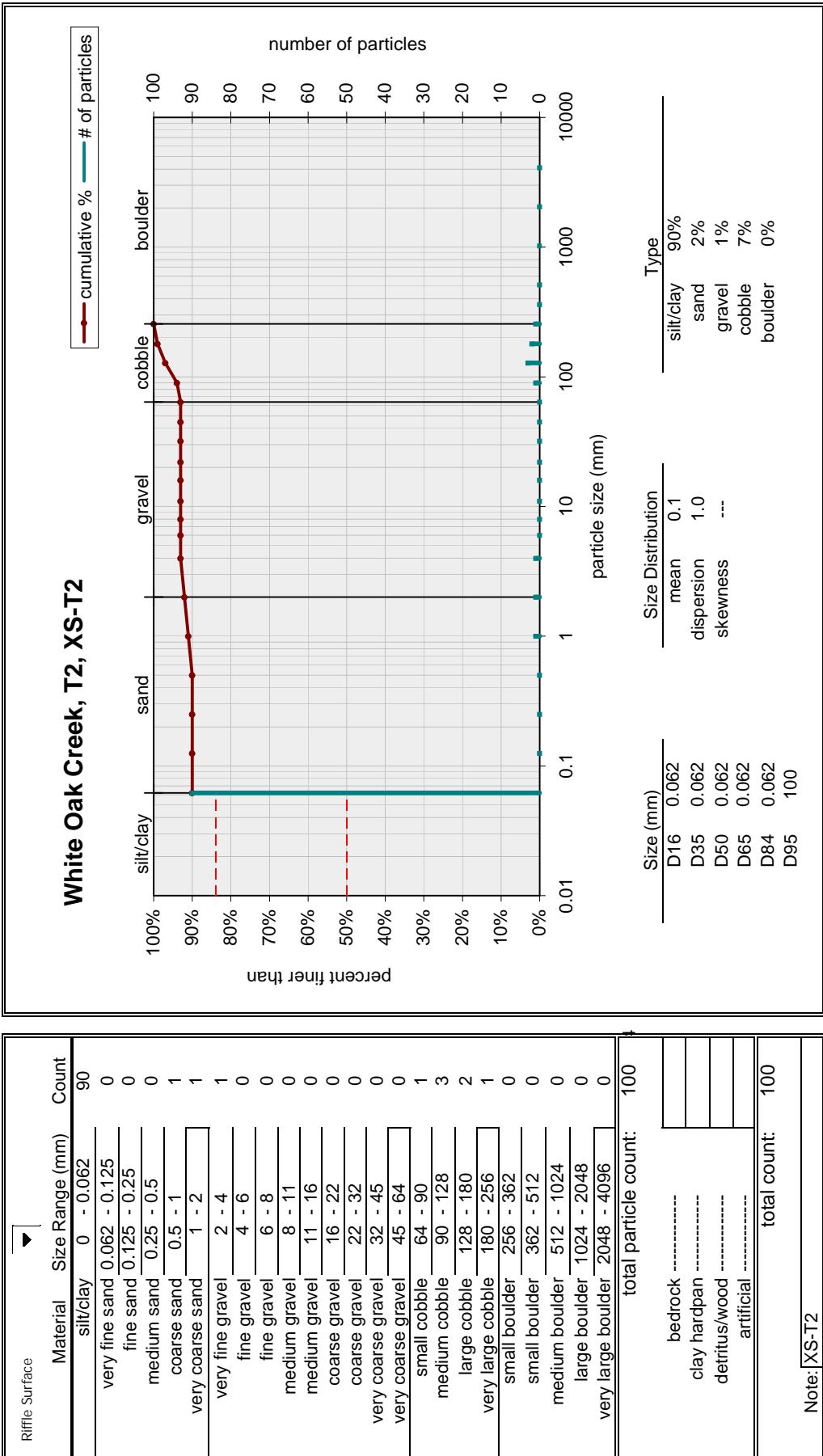


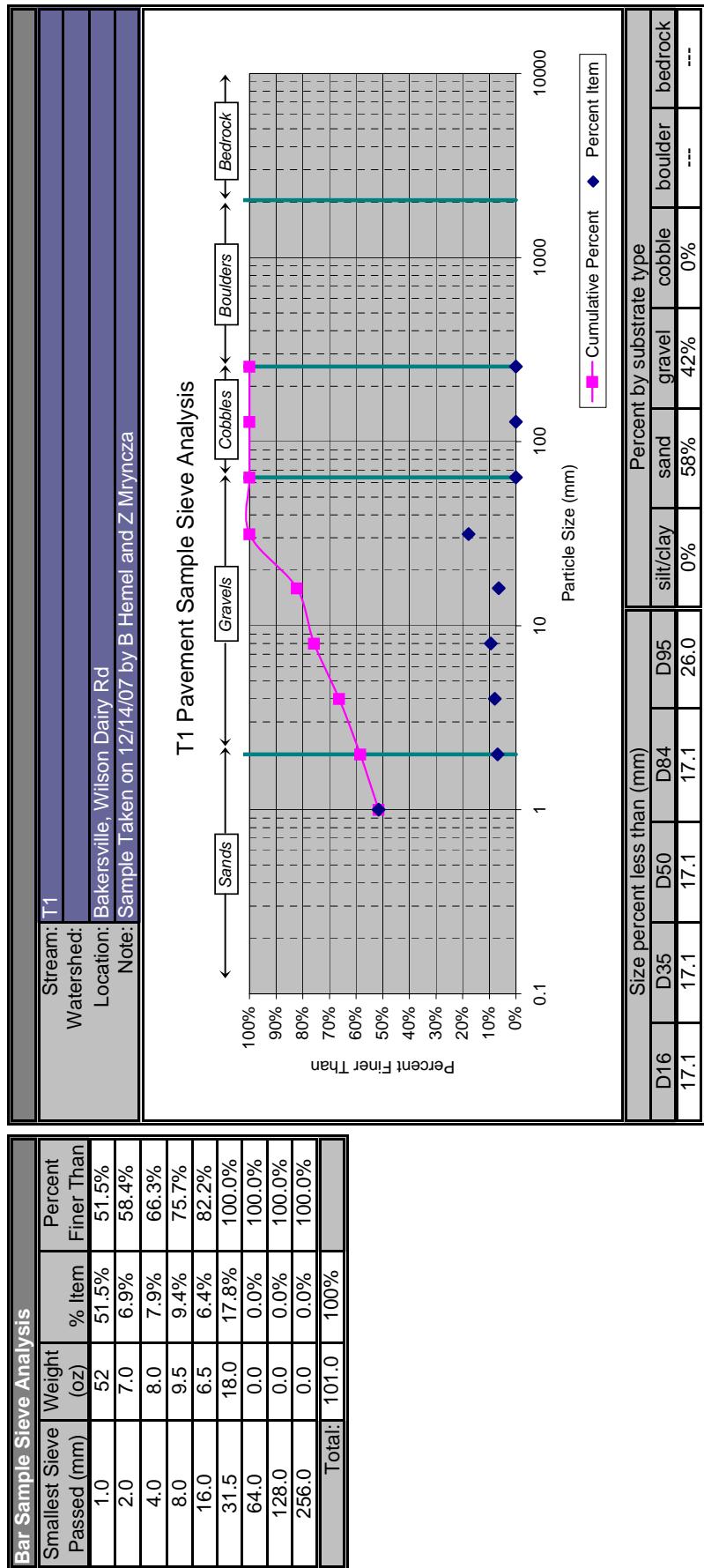
River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions
XS ID	XS - T2, Riffle
Drainage Area (sq mi):	0.5
Date:	2/18/2008
Field Crew:	B. Hemel, Z. Mlyneca, B. Roberts, A. Spiller

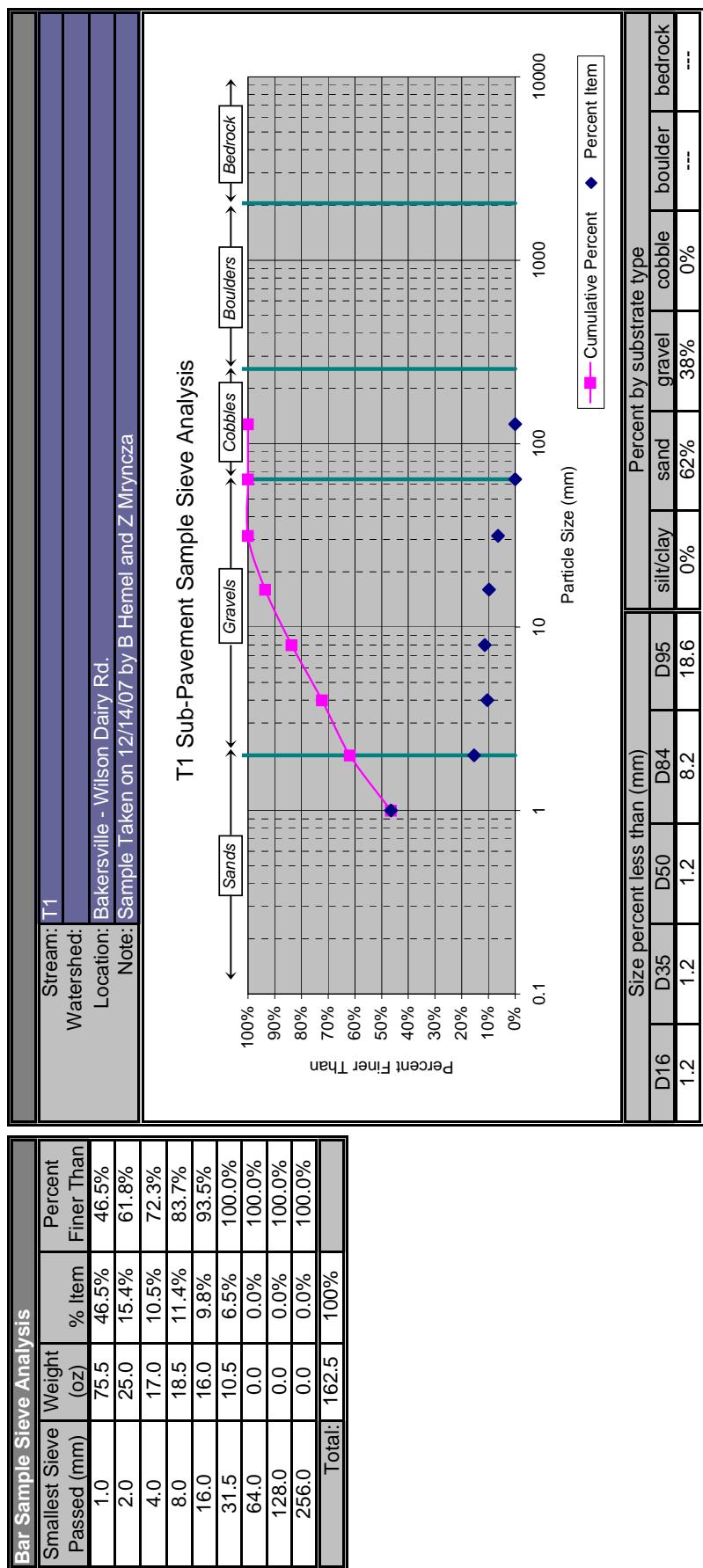


French Broad River Basin, White Oak Creek, Existing Conditions, XS - T2, Riffle

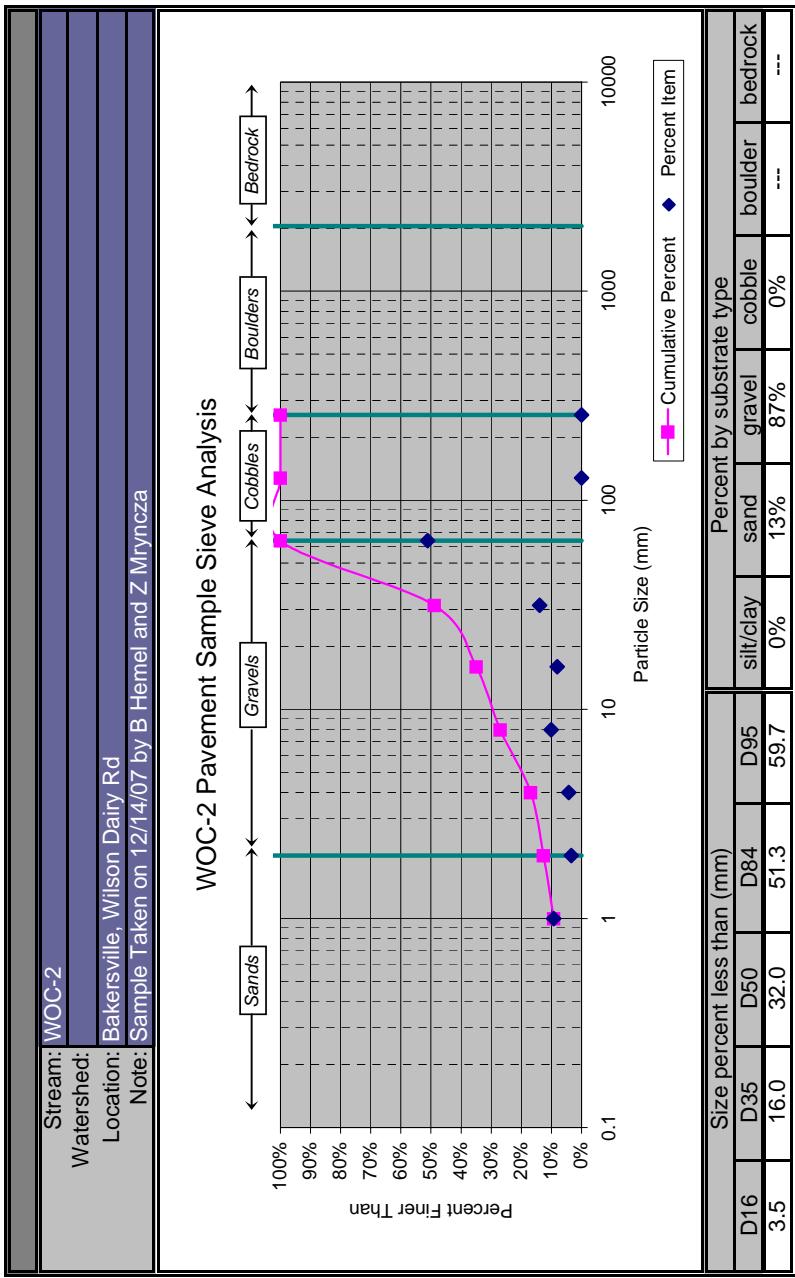


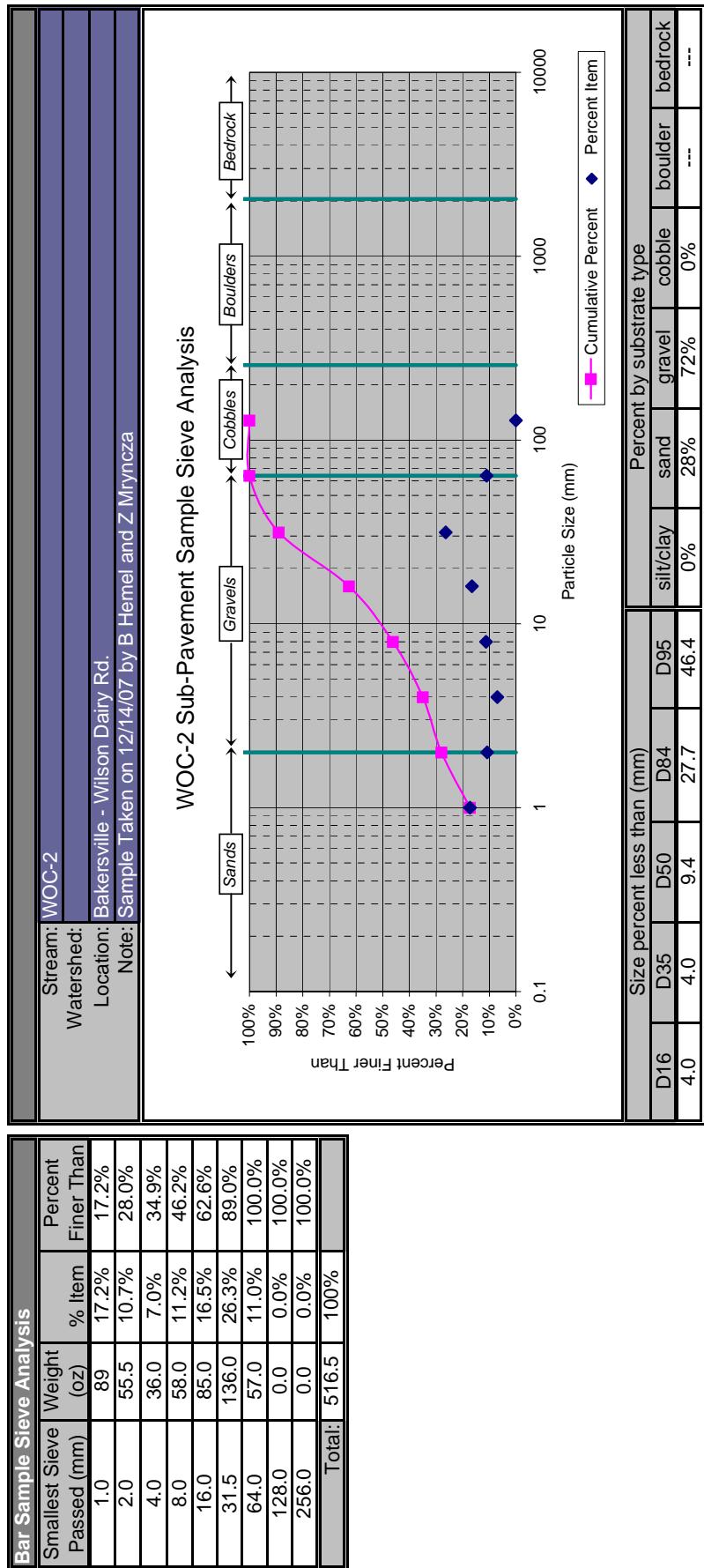


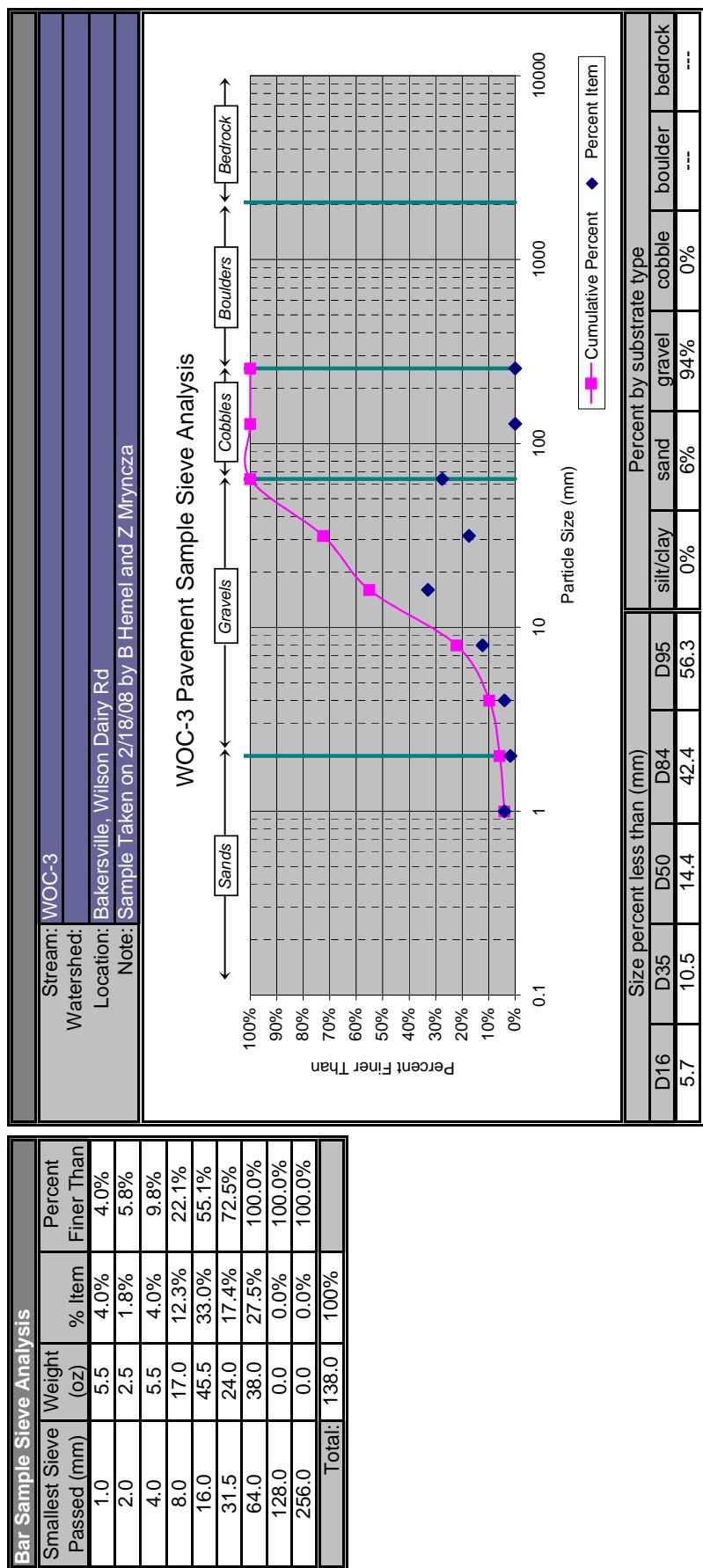


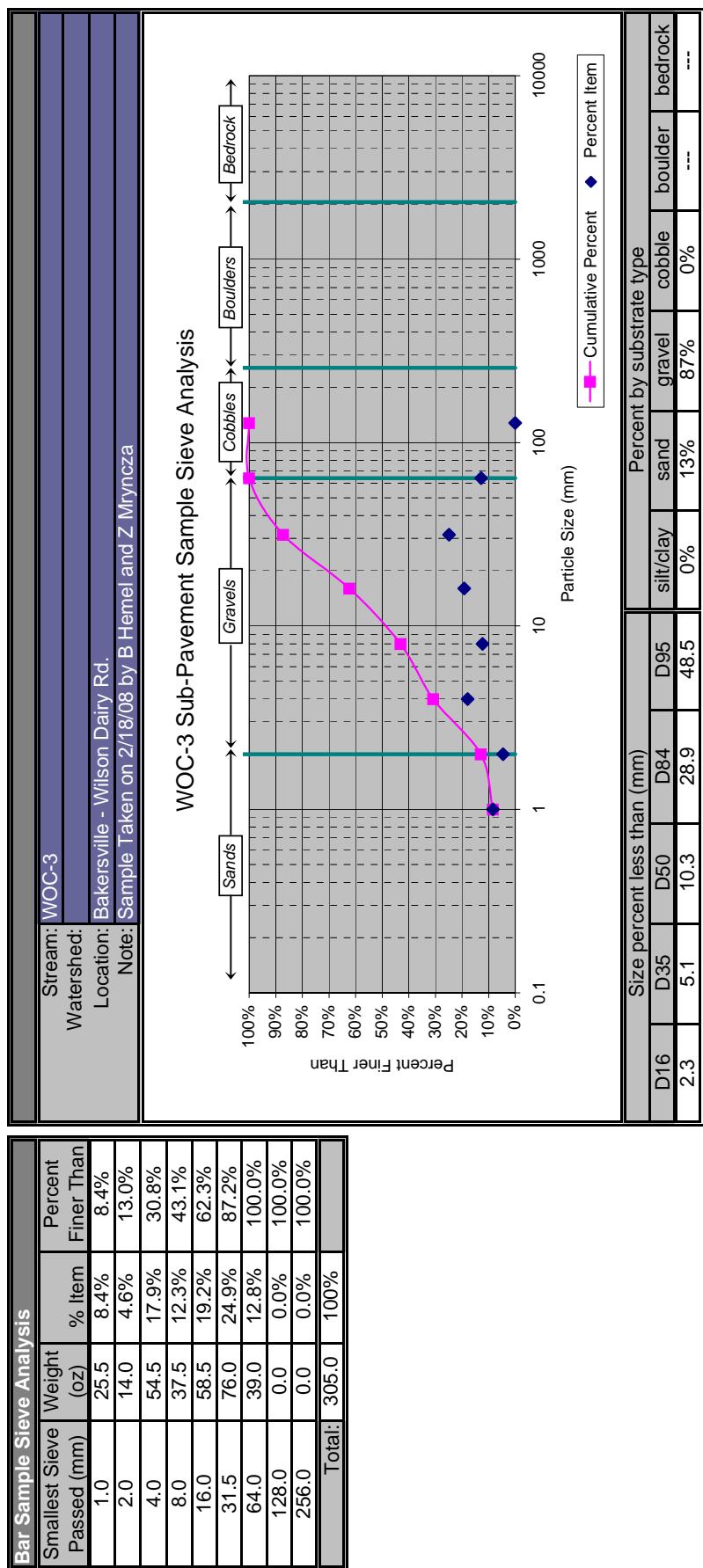


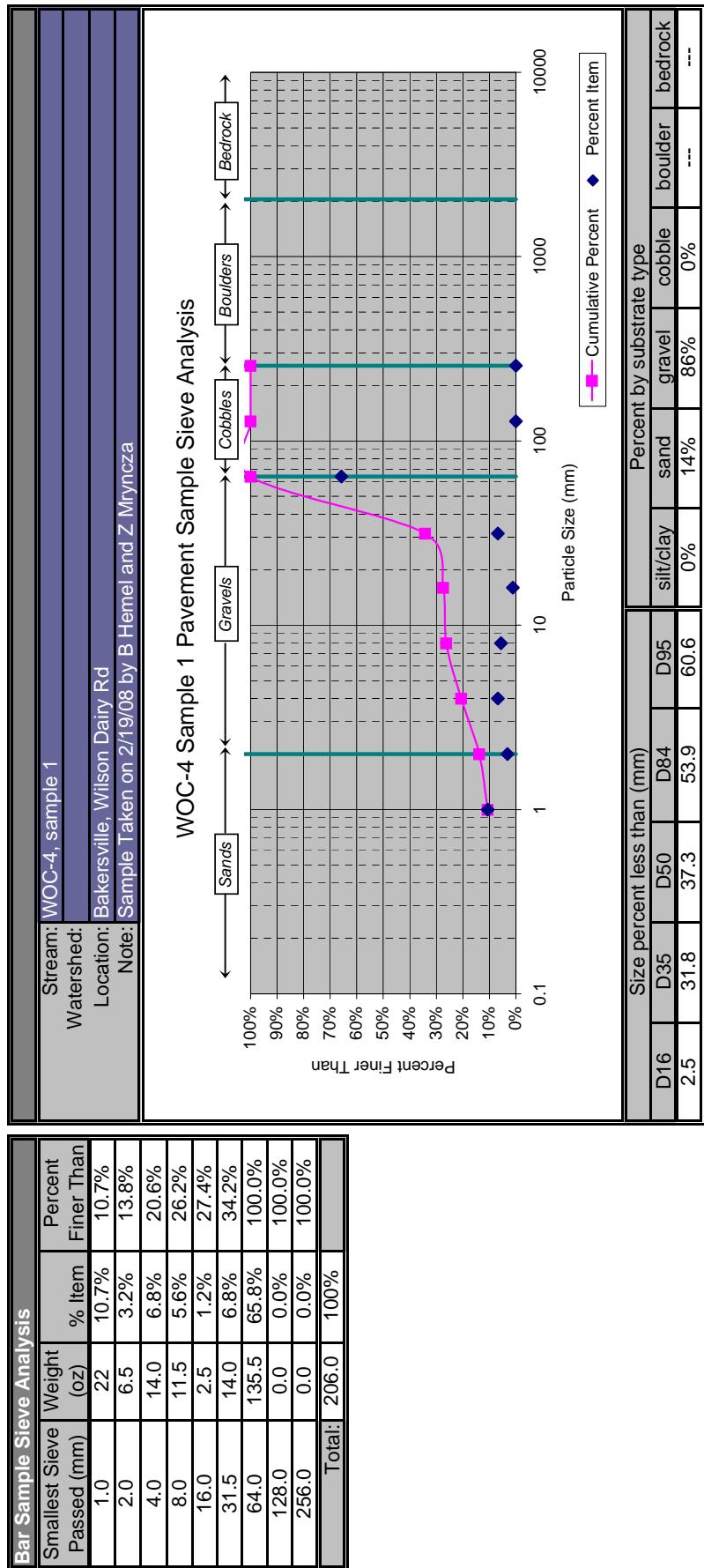
Bar Sample Sieve Analysis				
Smallest Sieve Passed (mm)	Weight (oz)	% Item	Percent Finer Than	
1.0	36	9.2%	9.2%	
2.0	13.5	3.4%	12.6%	
4.0	16.5	4.2%	16.9%	
8.0	39.5	10.1%	26.9%	
16.0	31.5	8.0%	35.0%	
31.5	54.5	13.9%	48.9%	
64.0	200.0	51.1%	100.0%	
128.0	0.0	0.0%	100.0%	
256.0	0.0	0.0%	100.0%	
Total:	391.5		100%	

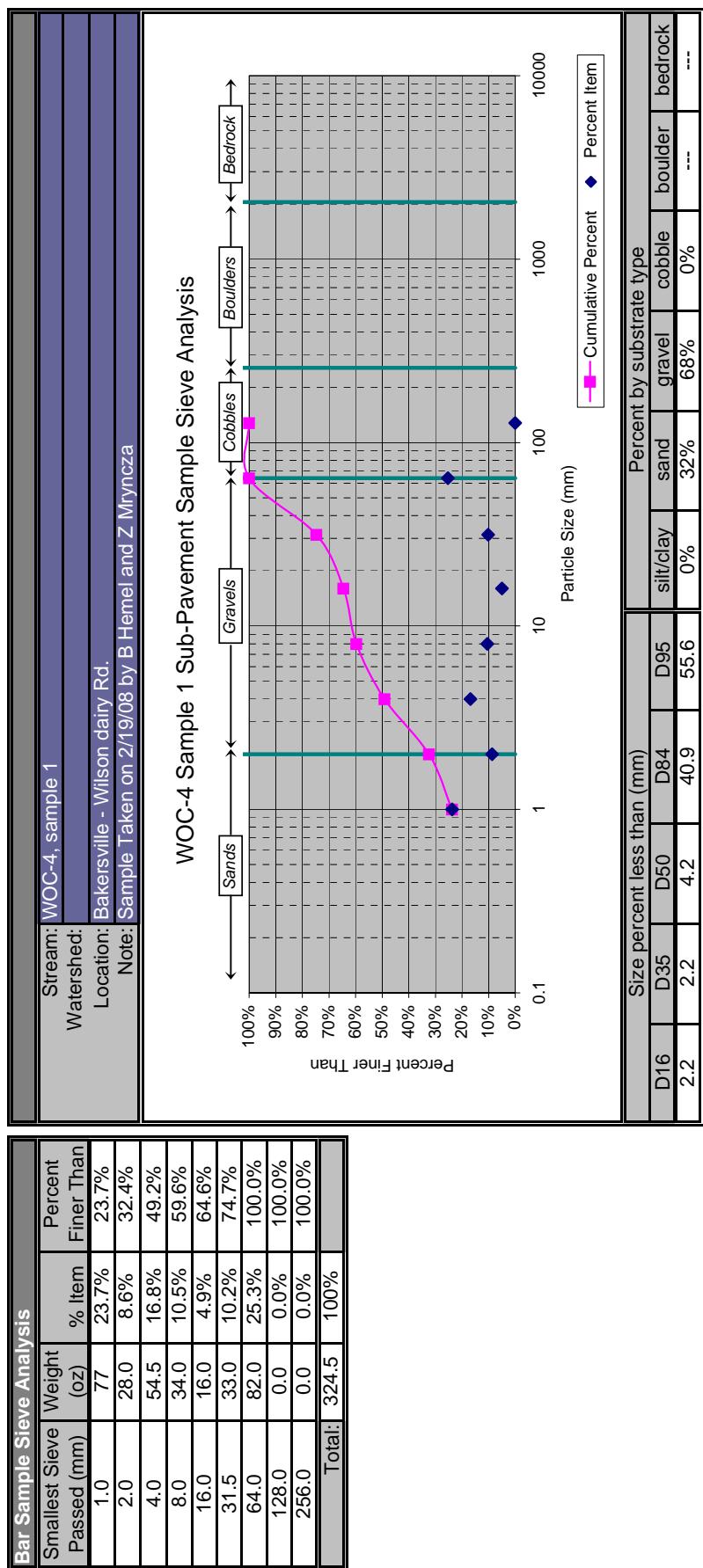


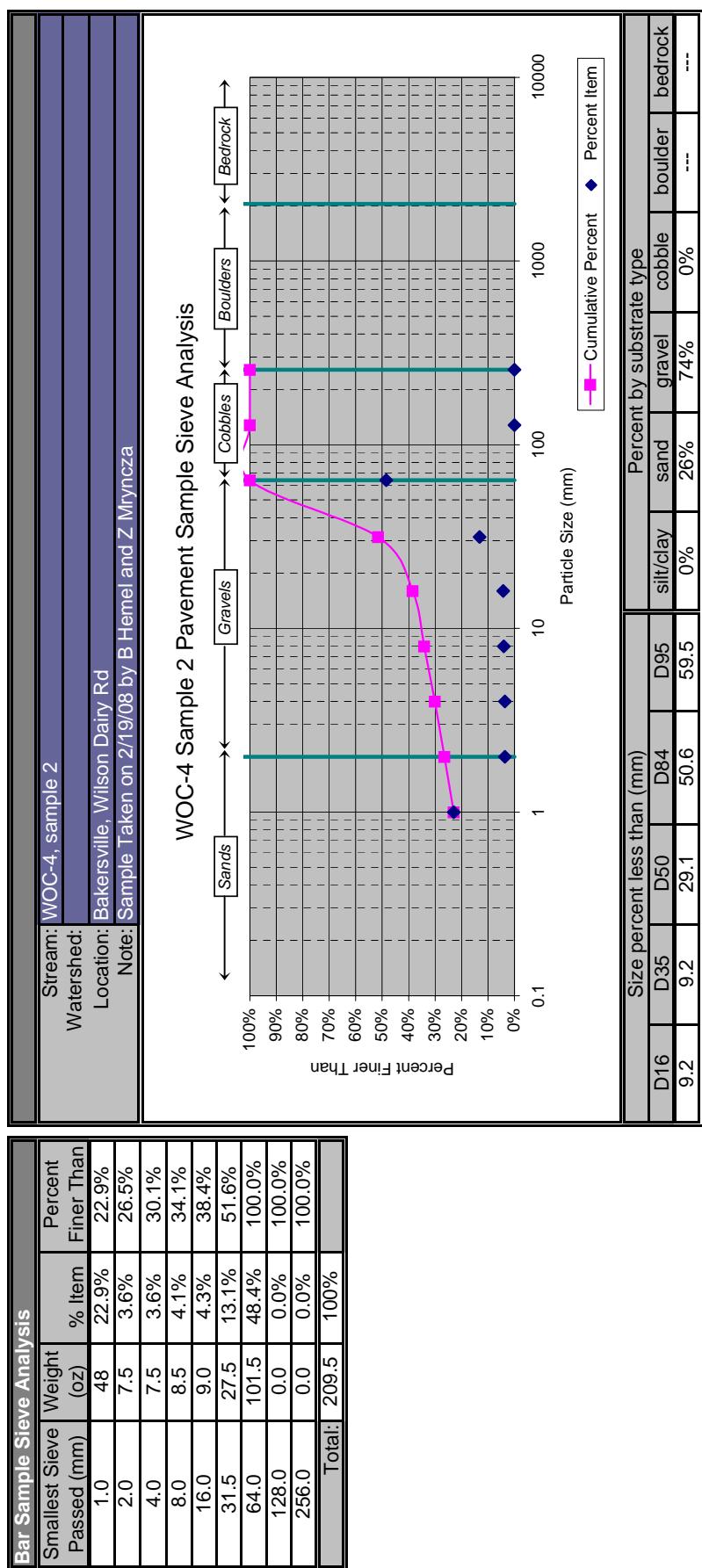




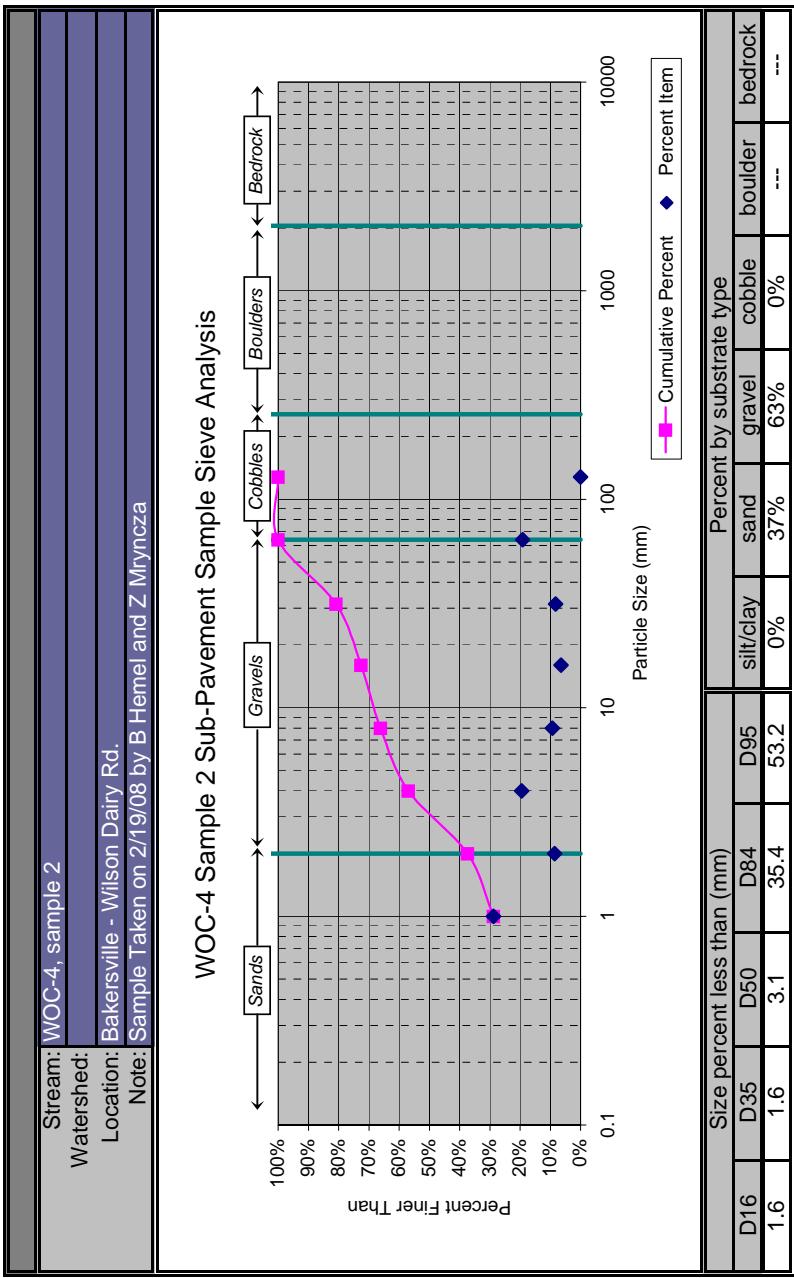


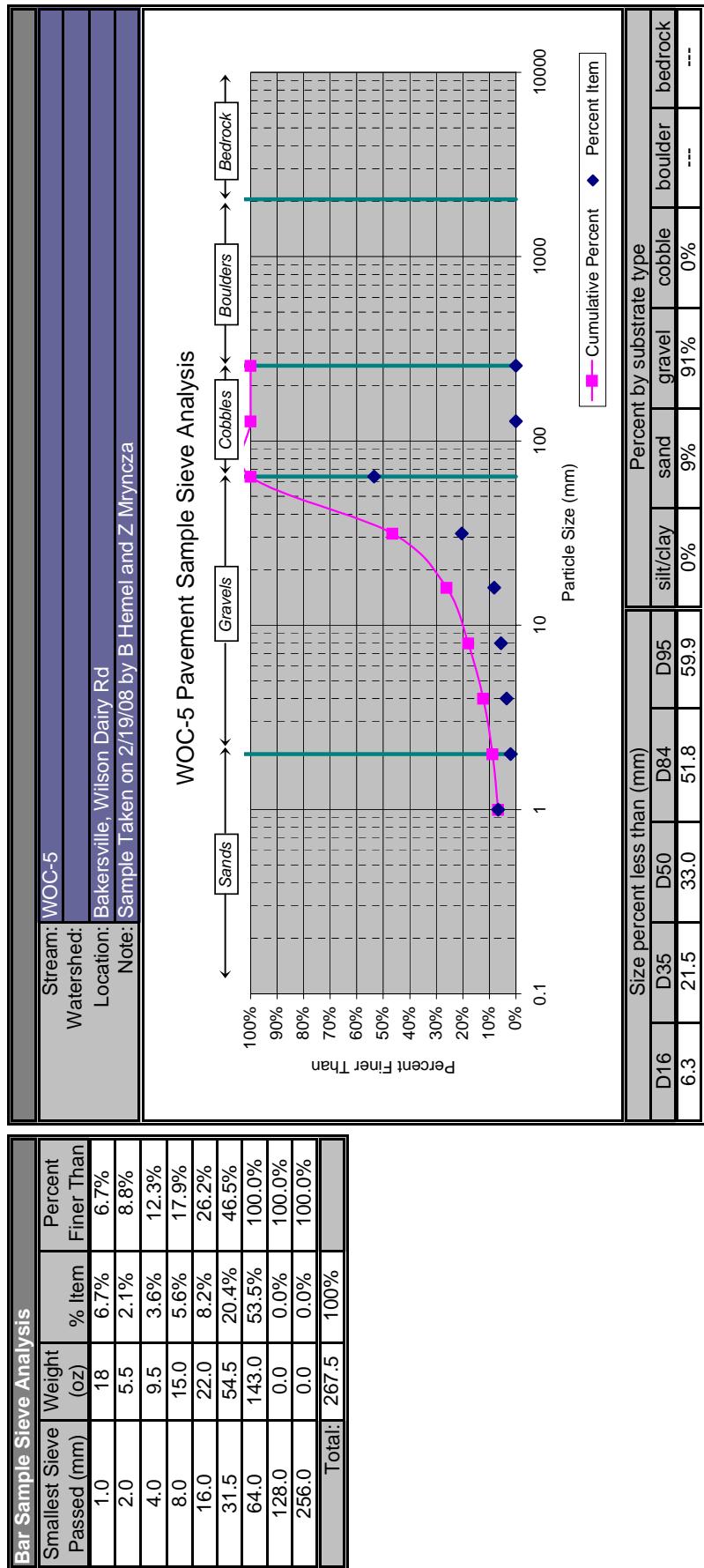


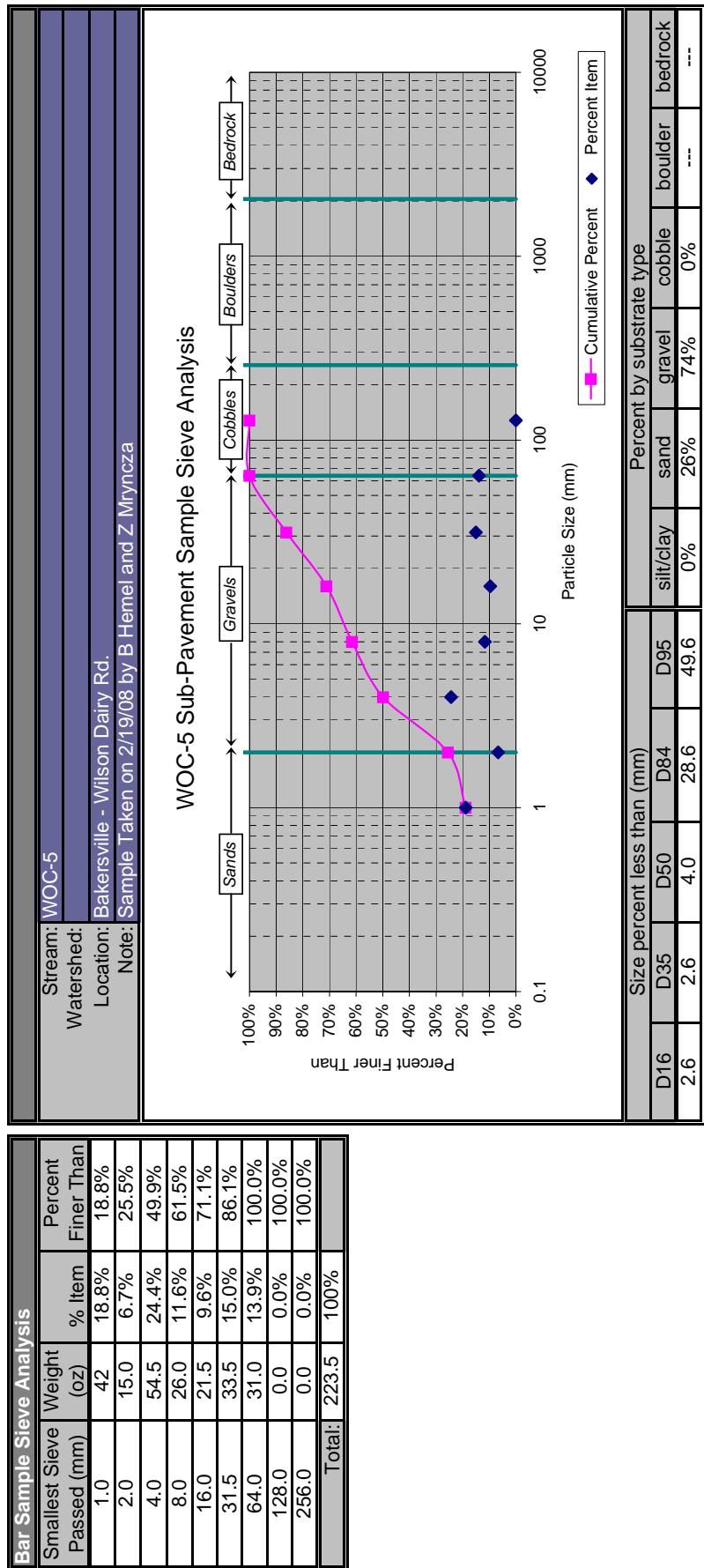




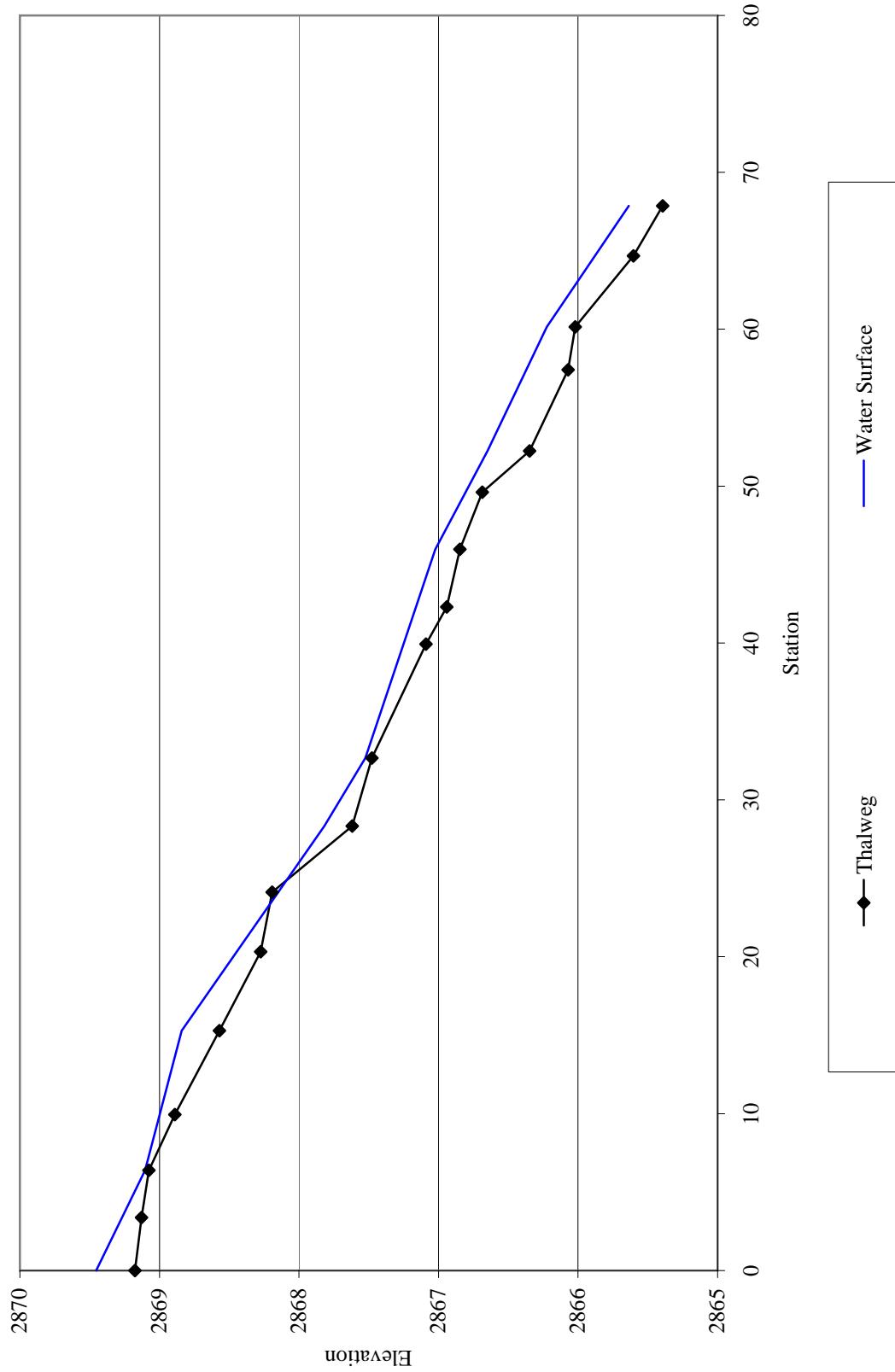
Bar Sample Sieve Analysis				
Smallest Sieve Passed (mm)	Weight (oz)	% Item	Percent Finer Than	
1.0	80.5	28.8%	28.8%	
2.0	24.0	8.6%	37.4%	
4.0	54.5	19.5%	56.9%	
8.0	26.0	9.3%	66.2%	
16.0	18.0	6.4%	72.6%	
31.5	23.0	8.2%	80.9%	
64.0	53.5	19.1%	100.0%	
128.0	0.0	0.0%	100.0%	
256.0	0.0	0.0%	100.0%	
Total:	279.5		100%	



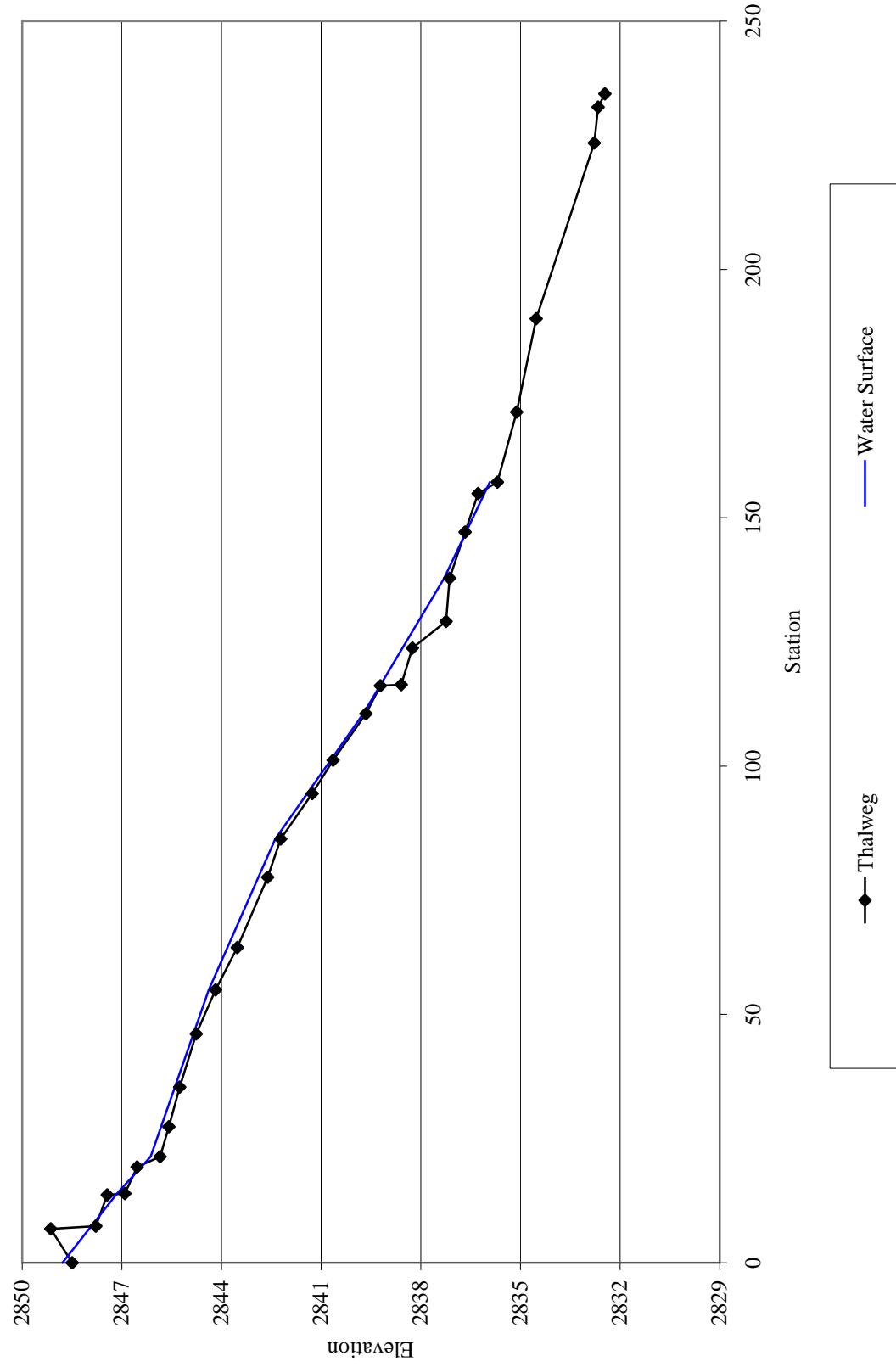




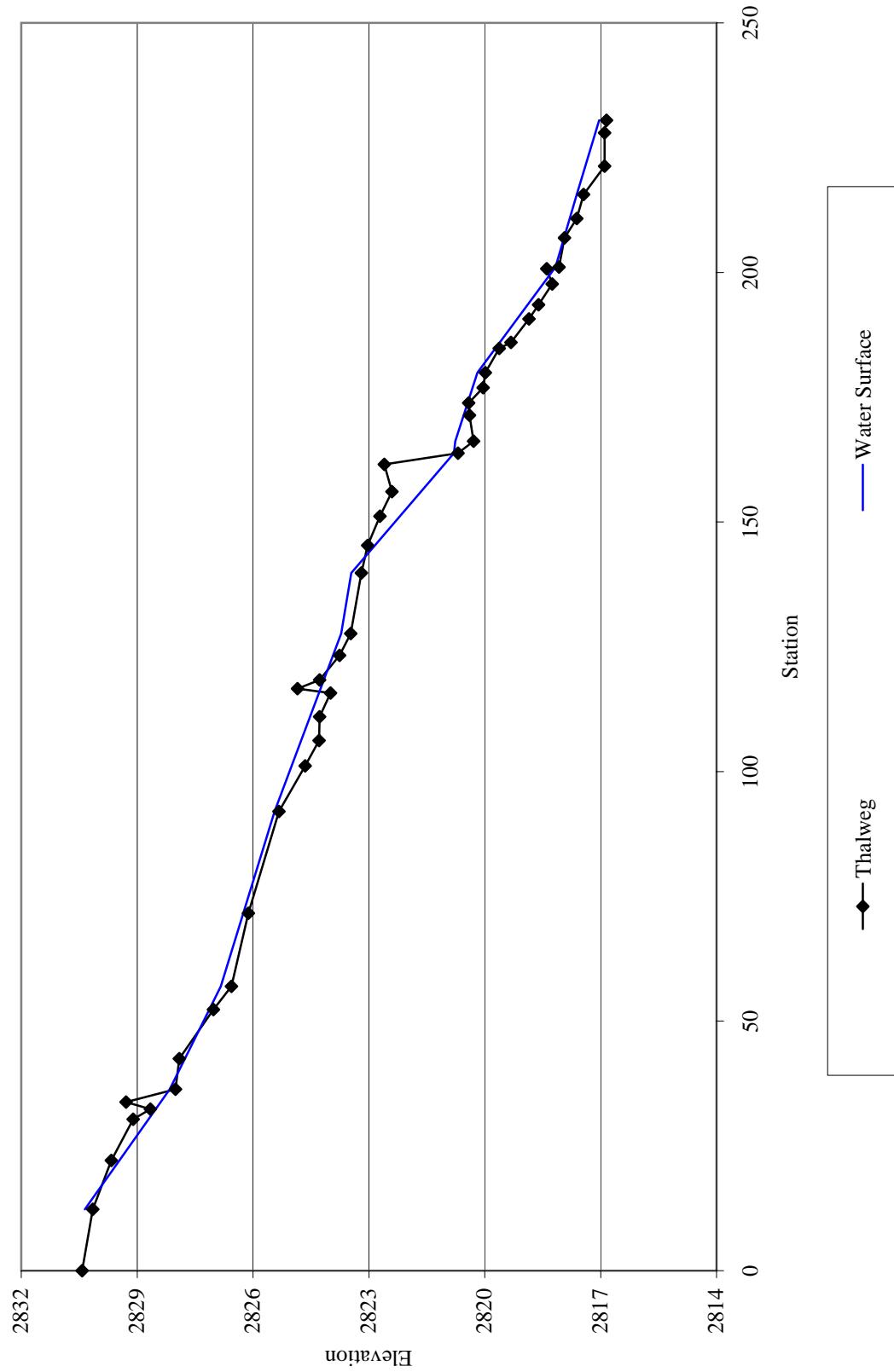
## Longitudinal Profile For XS-R



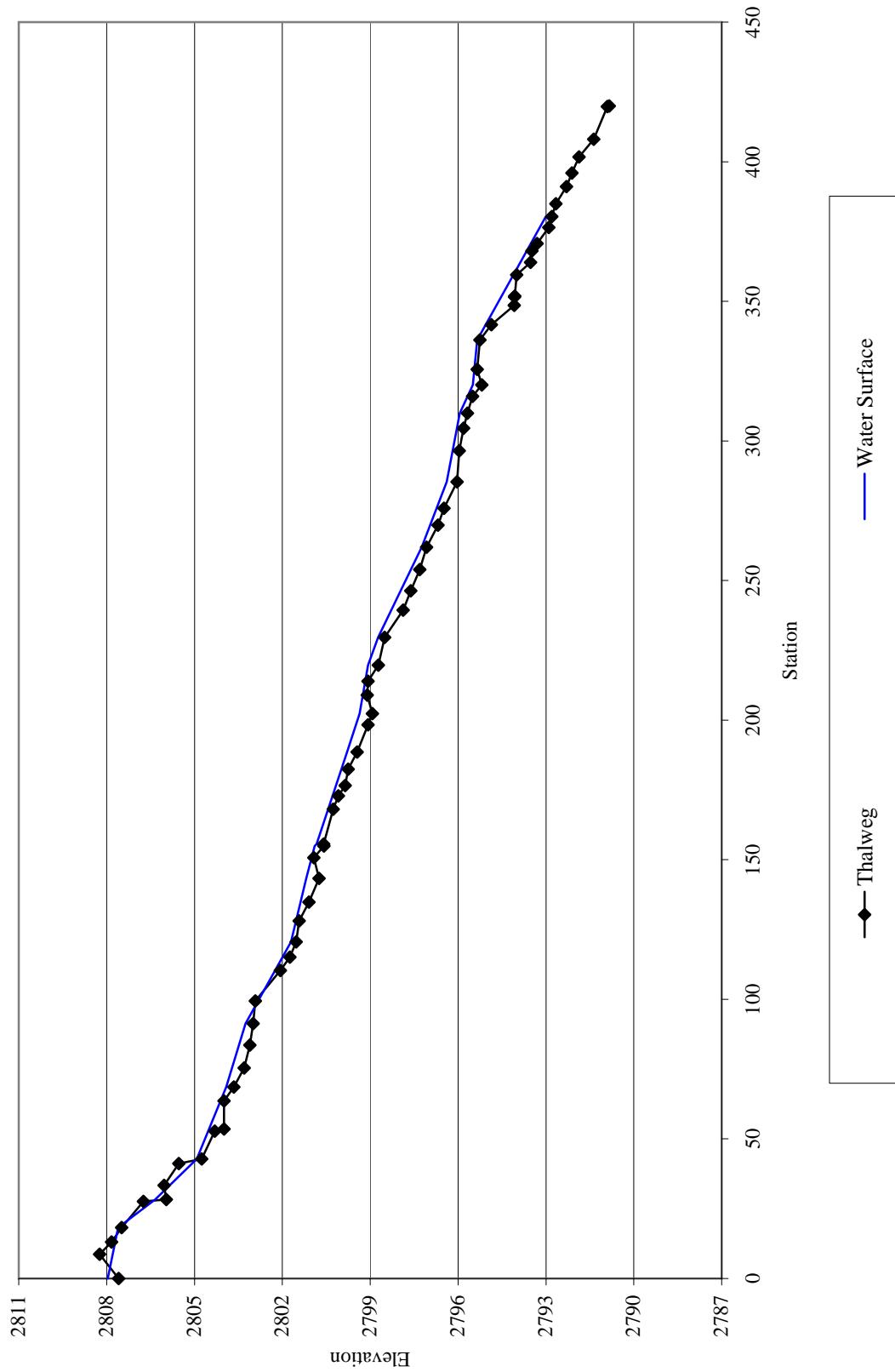
## Longitudinal Profile For XS-2



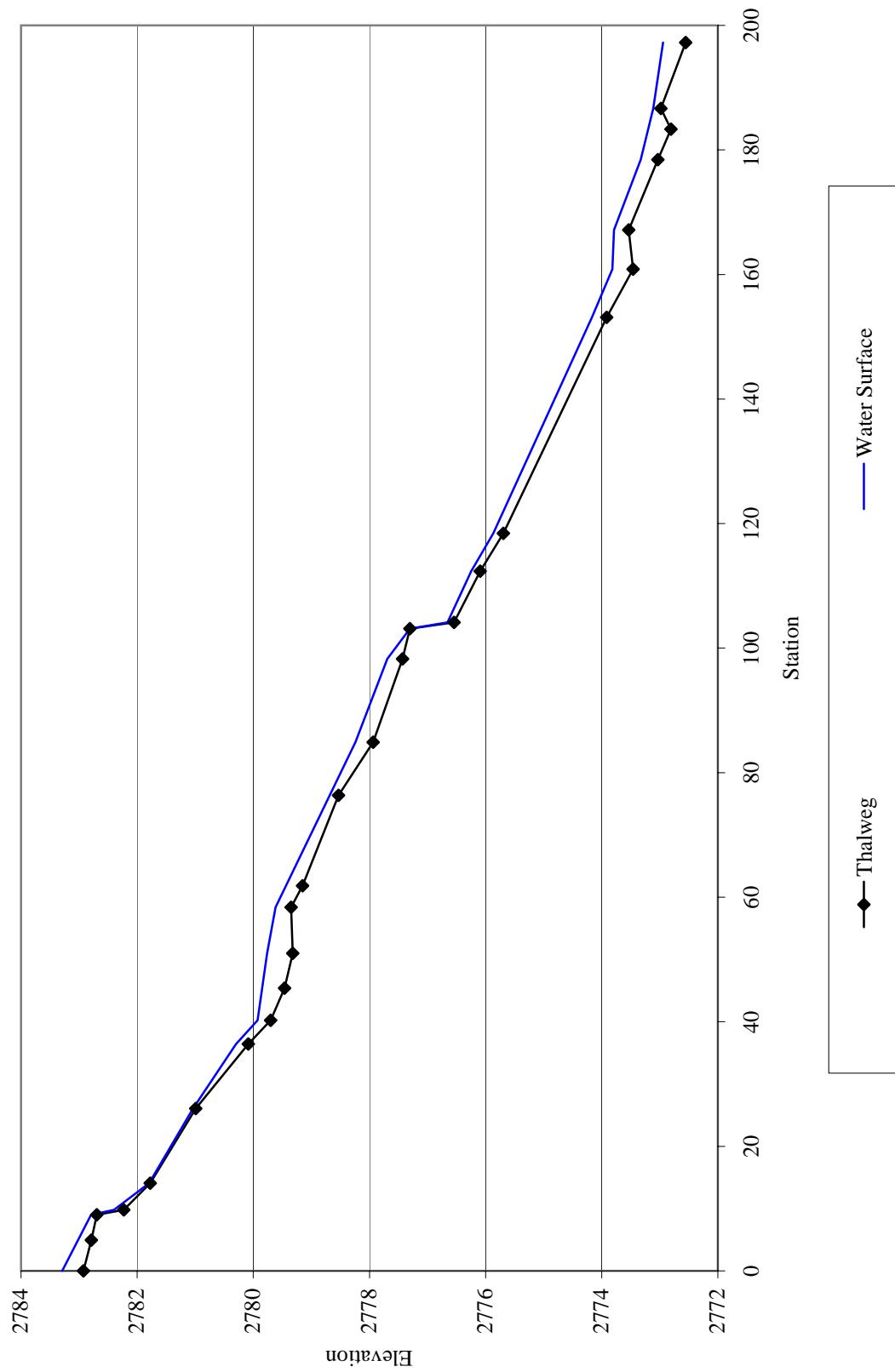
### Longitudinal Profile For XS-3



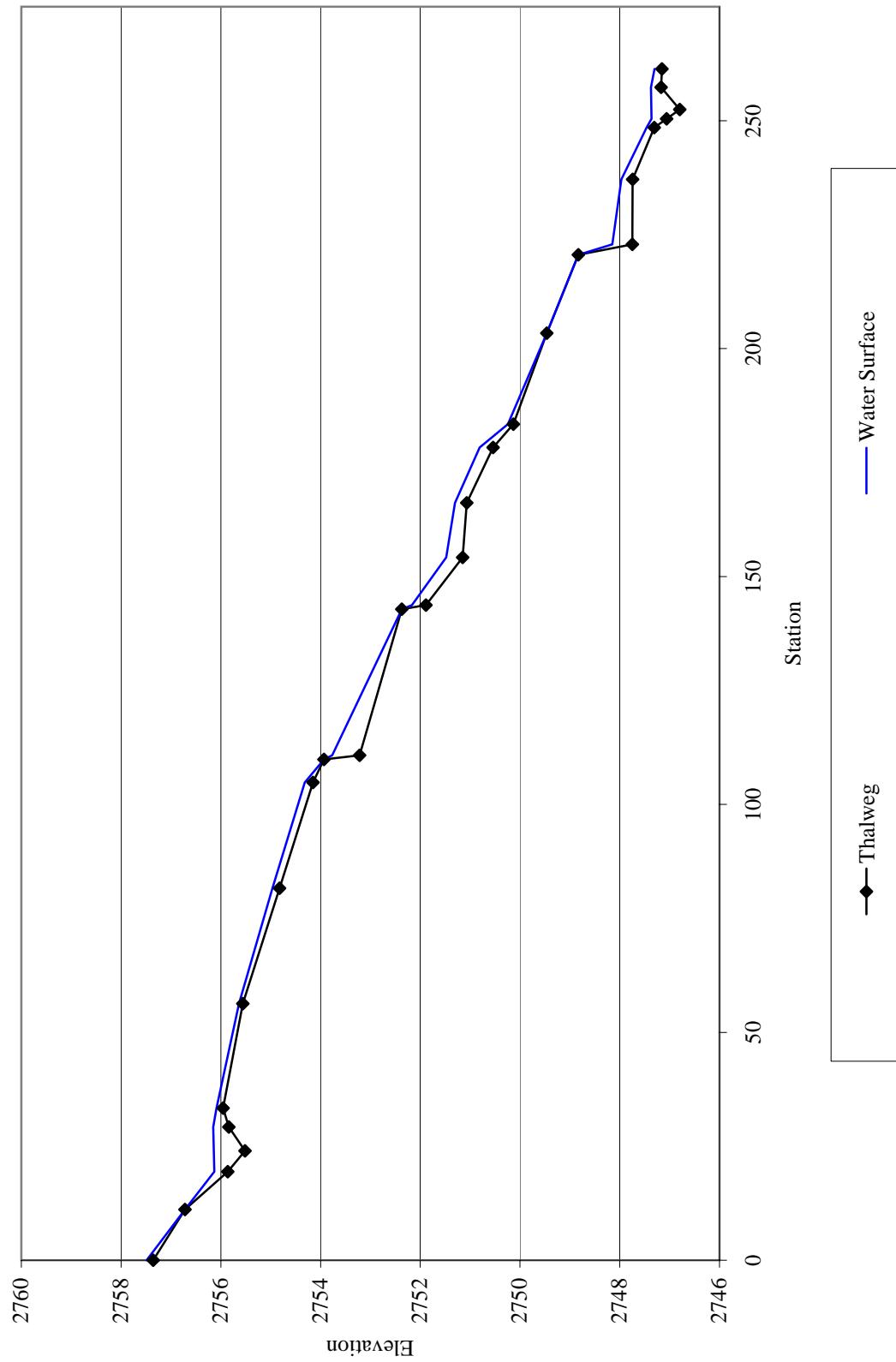
## Longitudinal Profile For XS-6 and XS-7



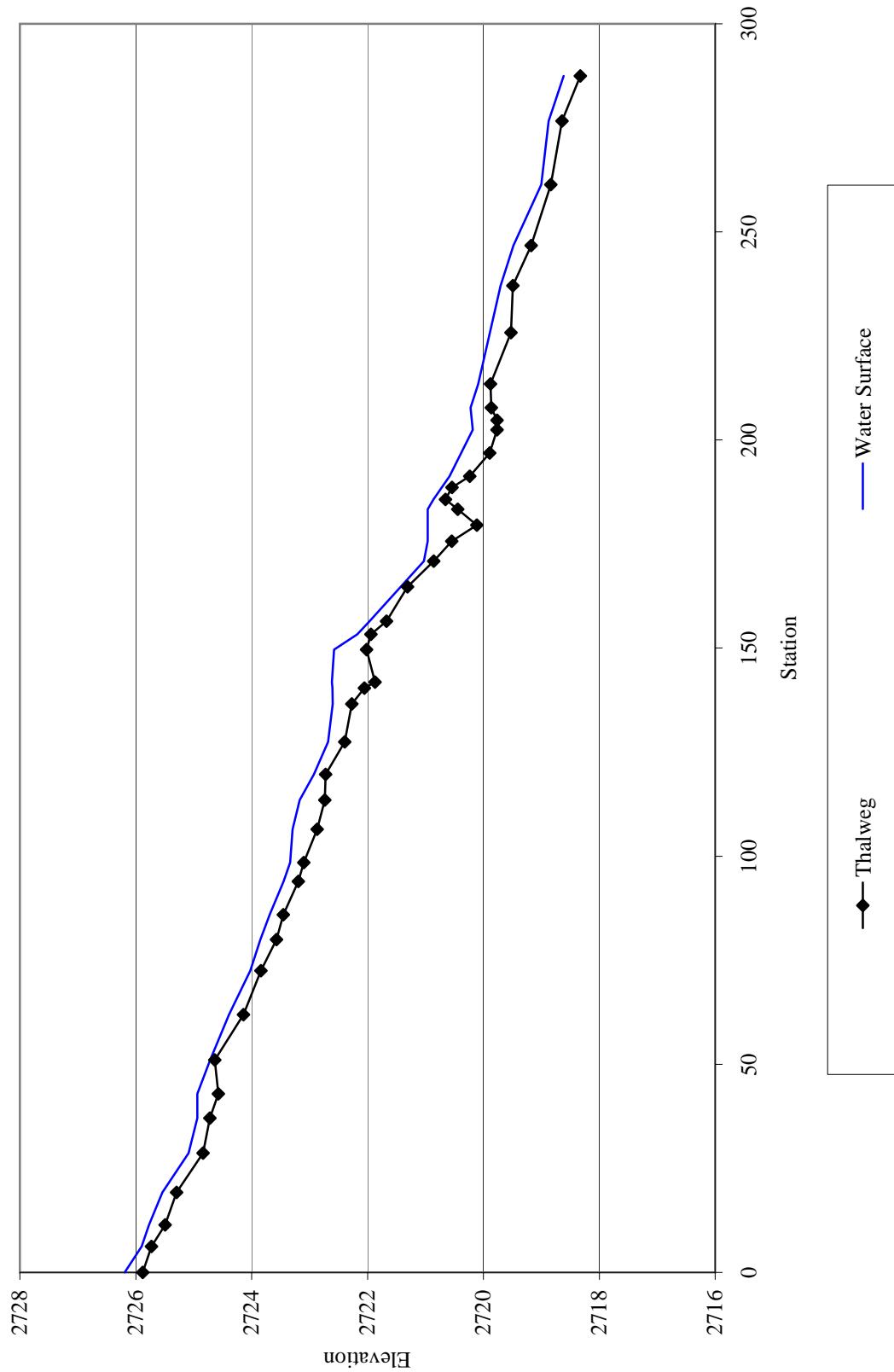
### Longitudinal Profile For XS-8 and XS-9



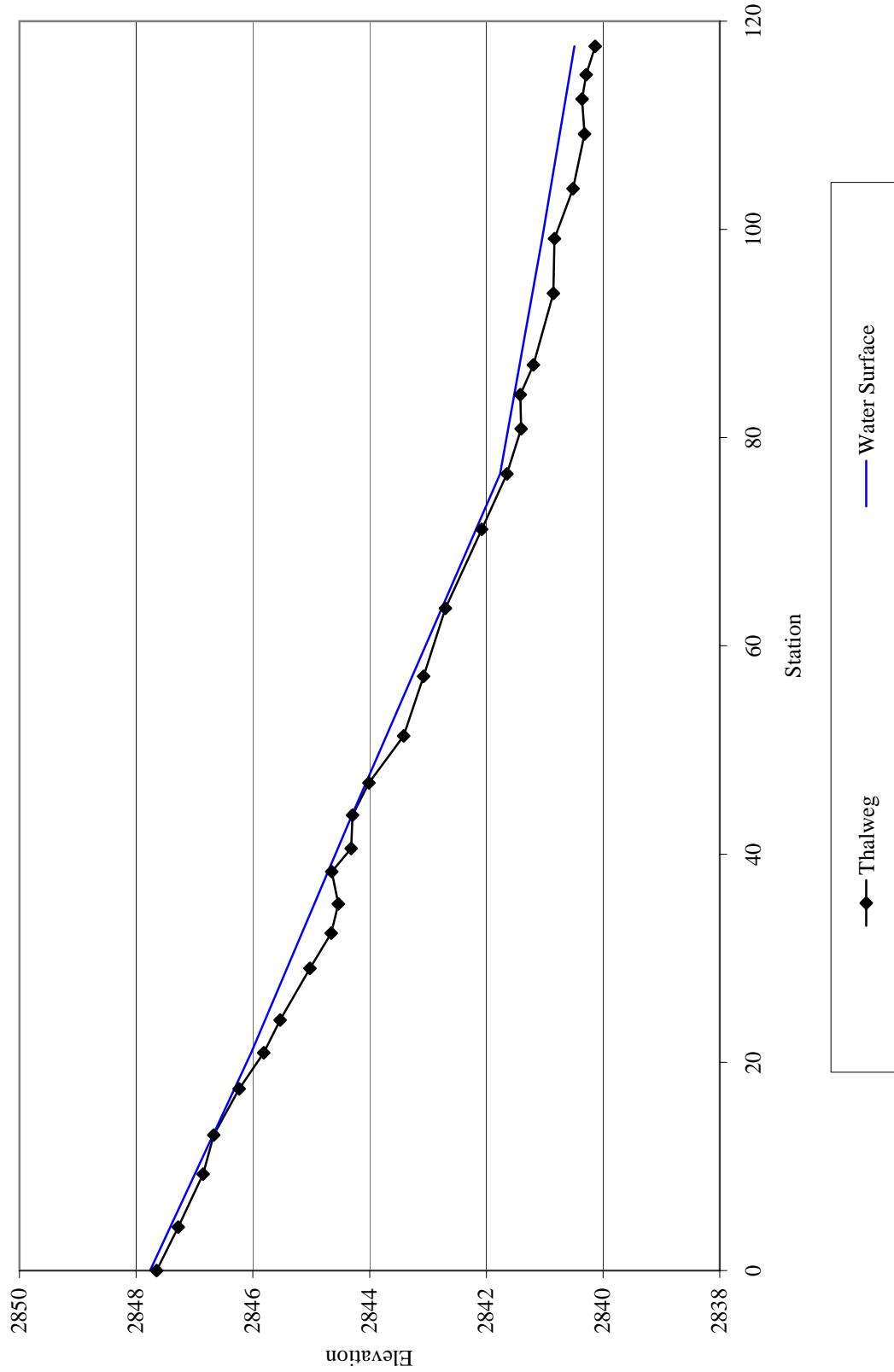
## Longitudinal Profile For XS-10



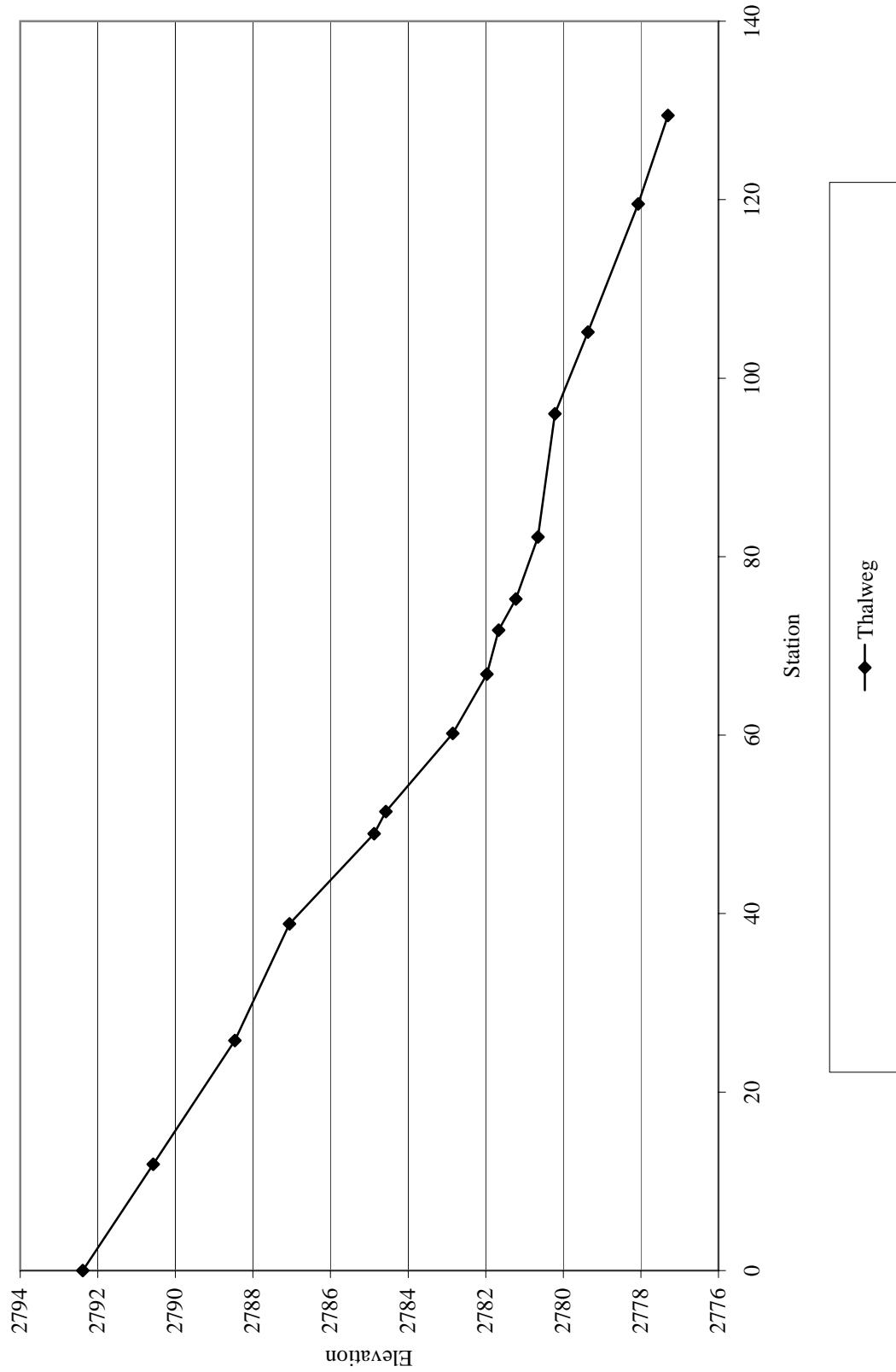
### Longitudinal Profile For XS-12 and XS-13



### Longitudinal Profile For XS-T1-1



### Longitudinal Profile For XS-T2





## Appendix E Reference Reach Data

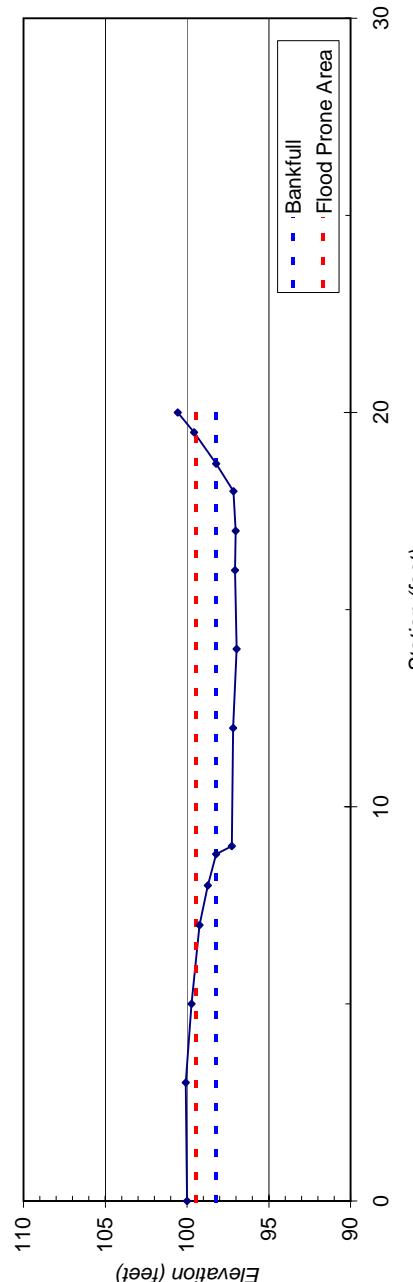


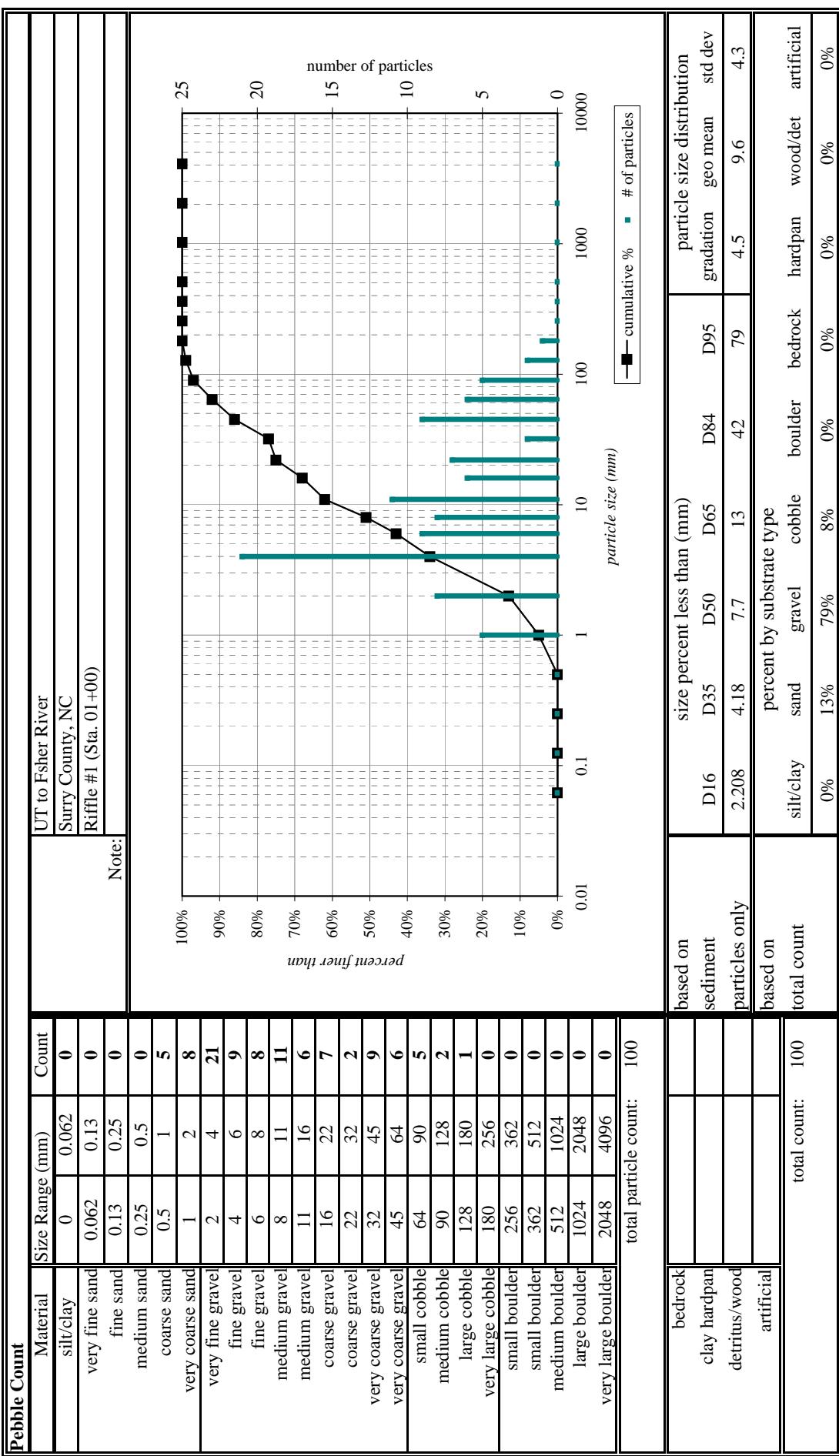


River Basin:	Yadkin
Watershed:	UT to Fisher River
XS ID	XS#1 Riffle
Drainage Area (sq mi):	0.38
Date:	6/9/2005
Field Crew:	G. Myrcza, A. Spiller

Station	Rod Ht.	Elevation	SUMMARY DATA
0.0	2.22	100.00	Bankfull Elevation:
3.0	2.15	100.07	Bankfull Cross-Sectional Area:
5.0	2.50	99.72	Bankfull Width:
7.0	2.98	99.24	Flood Prone Area Elevation:
8.0	3.49	98.73	Flood Prone Width:
8.8	4.00	98.22	Max Depth at Bankfull:
9.0	4.96	97.26	Mean Depth at Bankfull:
12.0	5.03	97.19	W / D Ratio:
14.0	5.25	96.97	Entrenchment Ratio:
16.0	5.16	97.06	Bank Height Ratio:
17.0	5.20	97.02	Slope (ft/ft):
18.0	5.06	97.16	Discharge (cfs)
18.7	4.00	98.22	42
19.5	2.65	99.57	B4c
20.0	1.66	100.56	

### Yadkin River Basin, UT to Fisher River, XS#1 Riffle



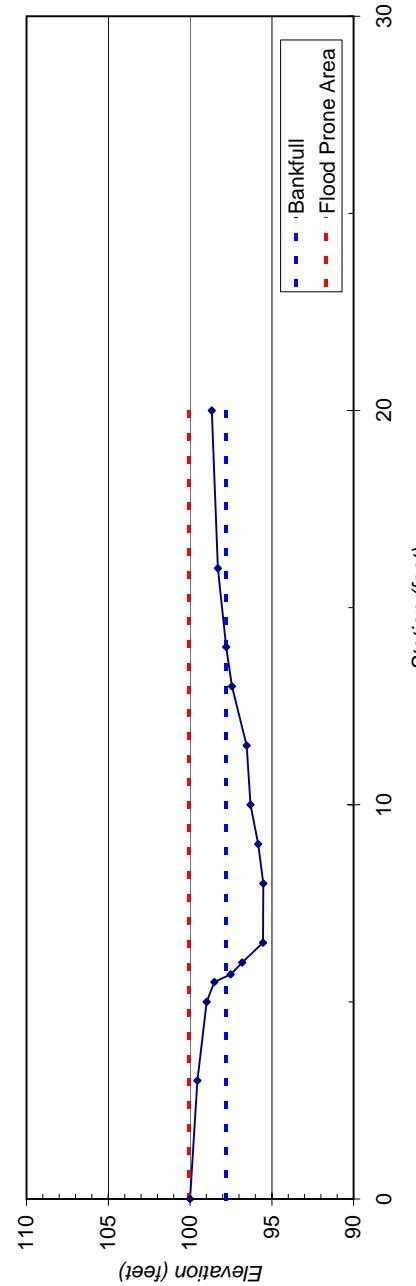


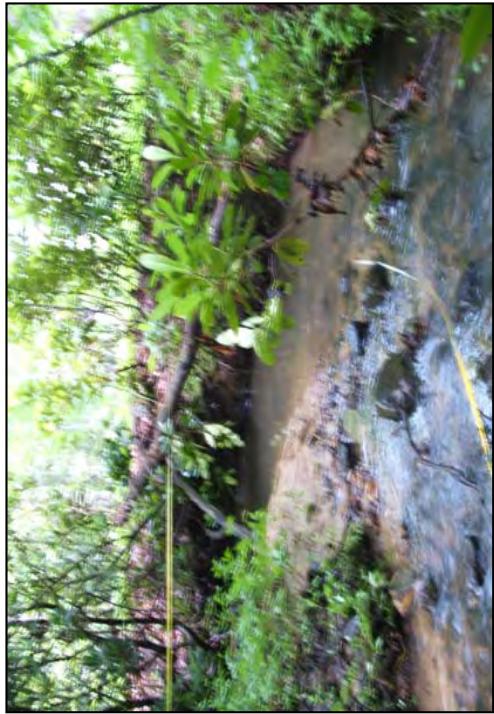


River Basin:	Yadkin
Watershed:	UT to Fisher River
XS ID	XS#3 Pool
Drainage Area (sq mi):	0.38
Date:	6/9/2005
Field Crew:	G. Myrcza, A. Spiller

Station	Rod Ht.	Elevation	SUMMARY DATA
0.0	1.33	100.00	Bankfull Elevation:
3.0	1.78	99.55	Bankfull Cross-Sectional Area:
5.0	2.35	98.98	Bankfull Width:
5.5	2.82	98.51	Flood Prone Area Elevation:
5.7	3.81	97.52	Flood Prone Width:
6.0	4.52	96.81	Max Depth at Bankfull:
6.5	5.79	95.54	Mean Depth at Bankfull:
8.0	5.82	95.51	W / D Ratio:
9.0	5.50	95.83	Entrenchment Ratio:
10.0	5.02	96.31	Bank Height Ratio:
11.5	4.80	96.53	Slope (ft/ft):
13.0	3.90	97.43	Discharge (cfs)
14.0	3.55	97.78	52
16.0	3.03	98.30	B4c
20.0	2.66	98.67	

**Yadkin River Basin, UT to Fisher River, XS#3 Pool**

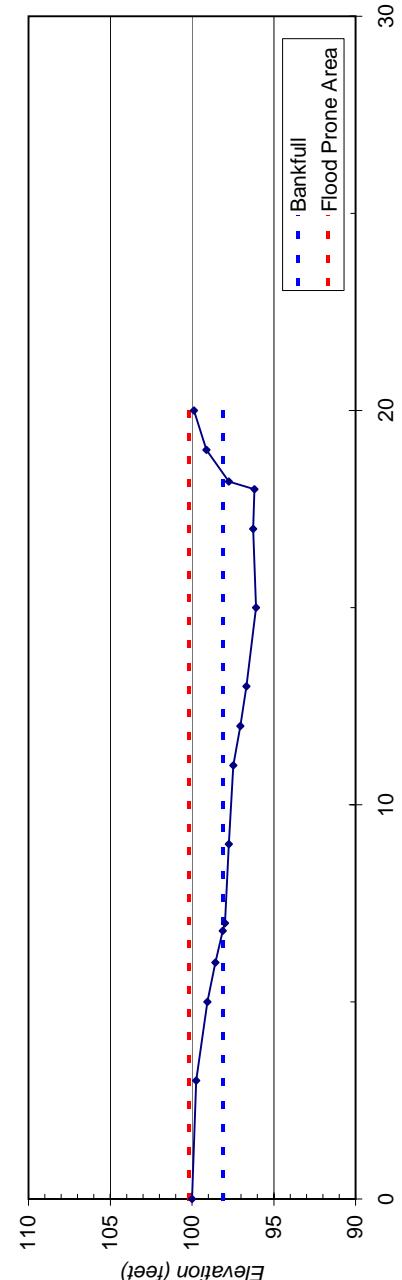




River Basin:	Yadkin
Watershed:	UT to Fisher River
XS ID	XS#2 Pool
Drainage Area (sq mi):	0.38
Date:	6/9/2005
Field Crew:	G. Myncza, A. Spiller

Station	Rod Ht.	Elevation	SUMMARY DATA
0.0	2.68	100.00	Bankfull Elevation:
3.0	2.94	99.74	Bankfull Cross-Sectional Area:
5.0	3.61	99.07	Bankfull Width:
6.0	4.10	98.58	Flood Prone Area Elevation:
6.8	4.56	98.12	Flood Prone Width:
7.0	4.70	97.98	Max Depth at Bankfull:
9.0	4.94	97.74	Mean Depth at Bankfull:
11.0	5.21	97.47	W / D Ratio:
12.0	5.64	97.04	Entrenchment Ratio:
13.0	6.00	96.68	Bank Height Ratio:
15.0	6.59	96.09	Slope (ft/ft):
17.0	6.42	96.26	Discharge (cfs)
18.0	6.50	96.18	56
18.2	4.93	97.75	B4c
19.0	3.56	99.12	
20.0	2.80	99.88	

### Yadkin River Basin, UT to Fisher River, XS#2 Pool

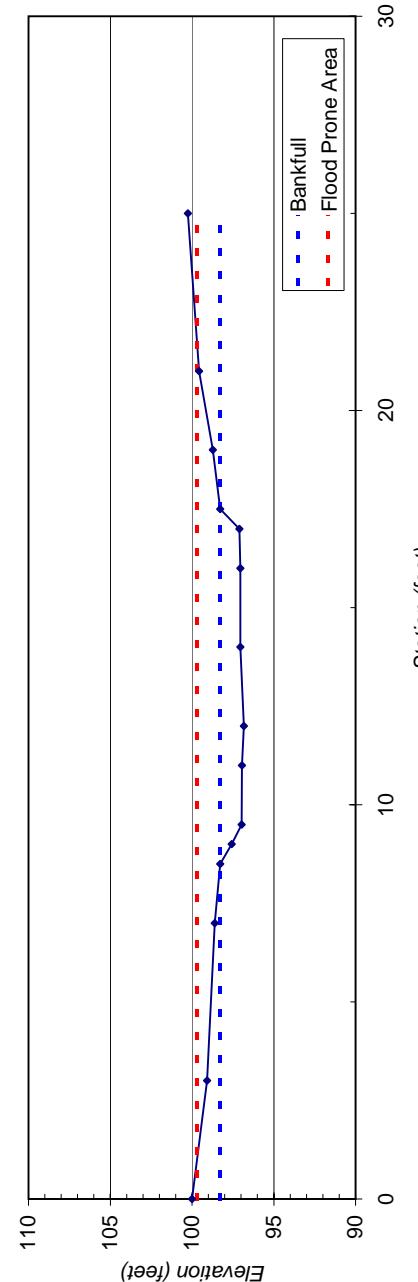


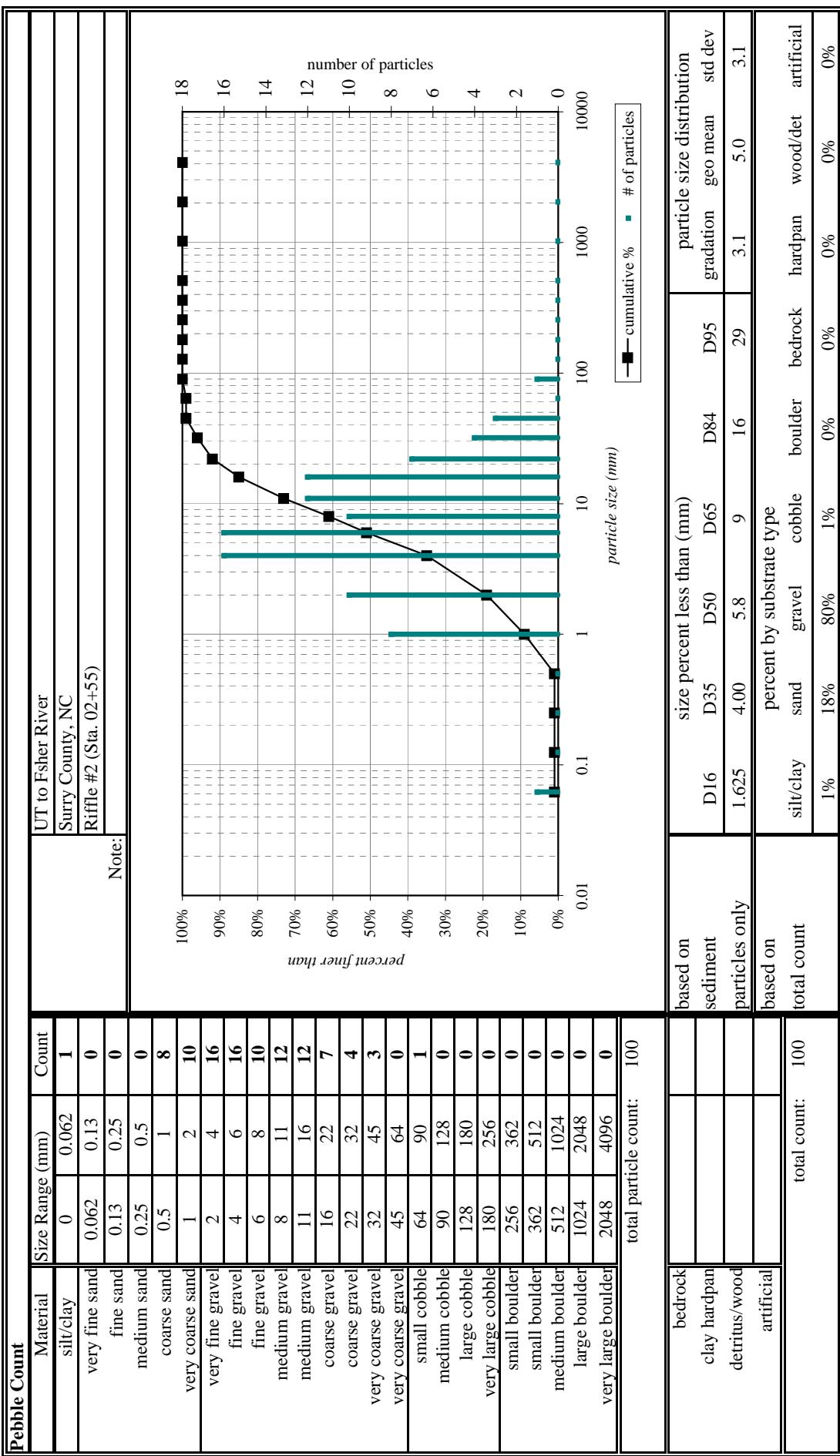


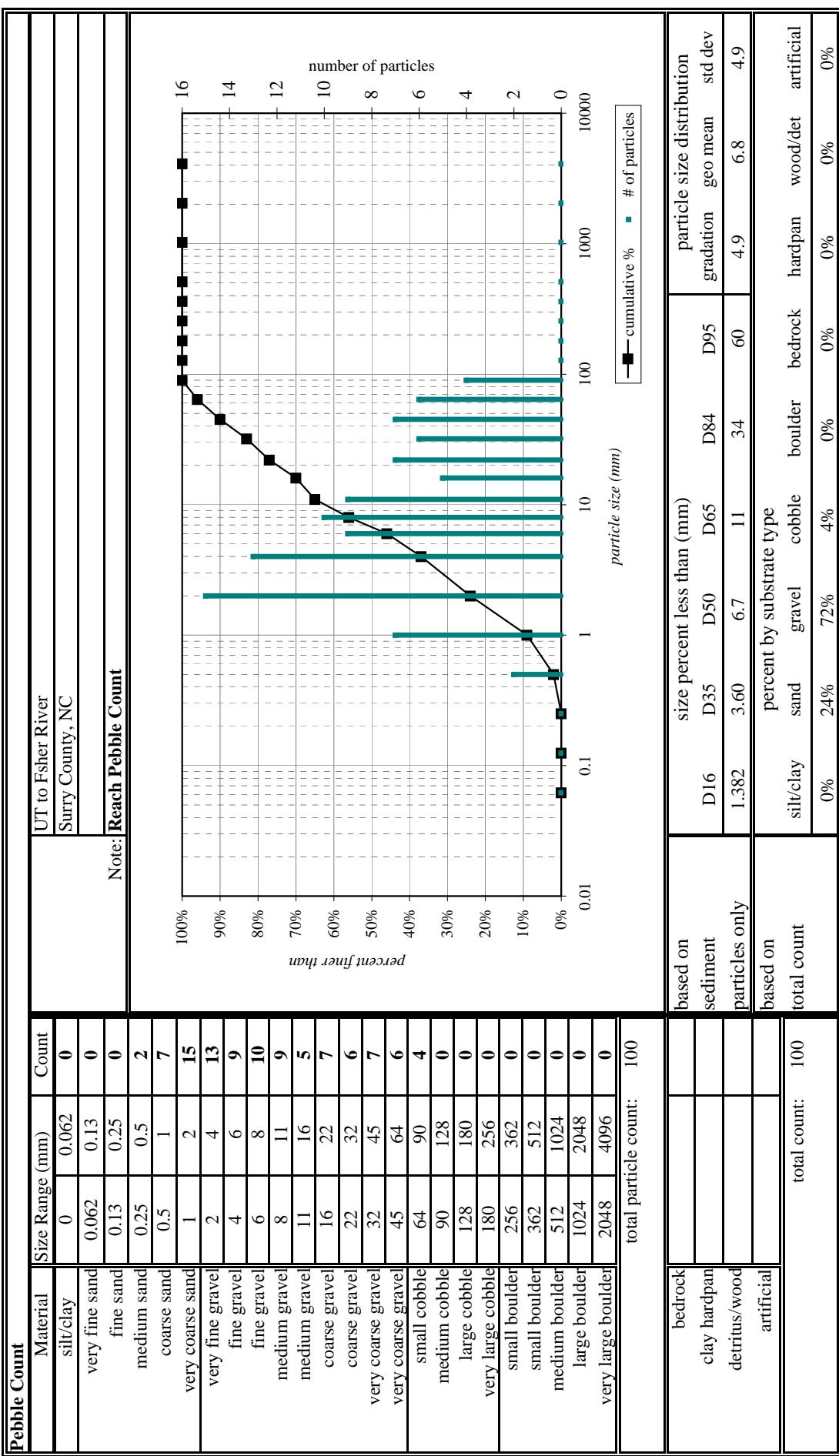
River Basin:	Yadkin
Watershed:	UT to Fisher River
XS ID	XS#4 Riffle
Drainage Area (sq mi):	0.38
Date:	6/9/2005
Field Crew:	G. Myrcza, A. Spiller

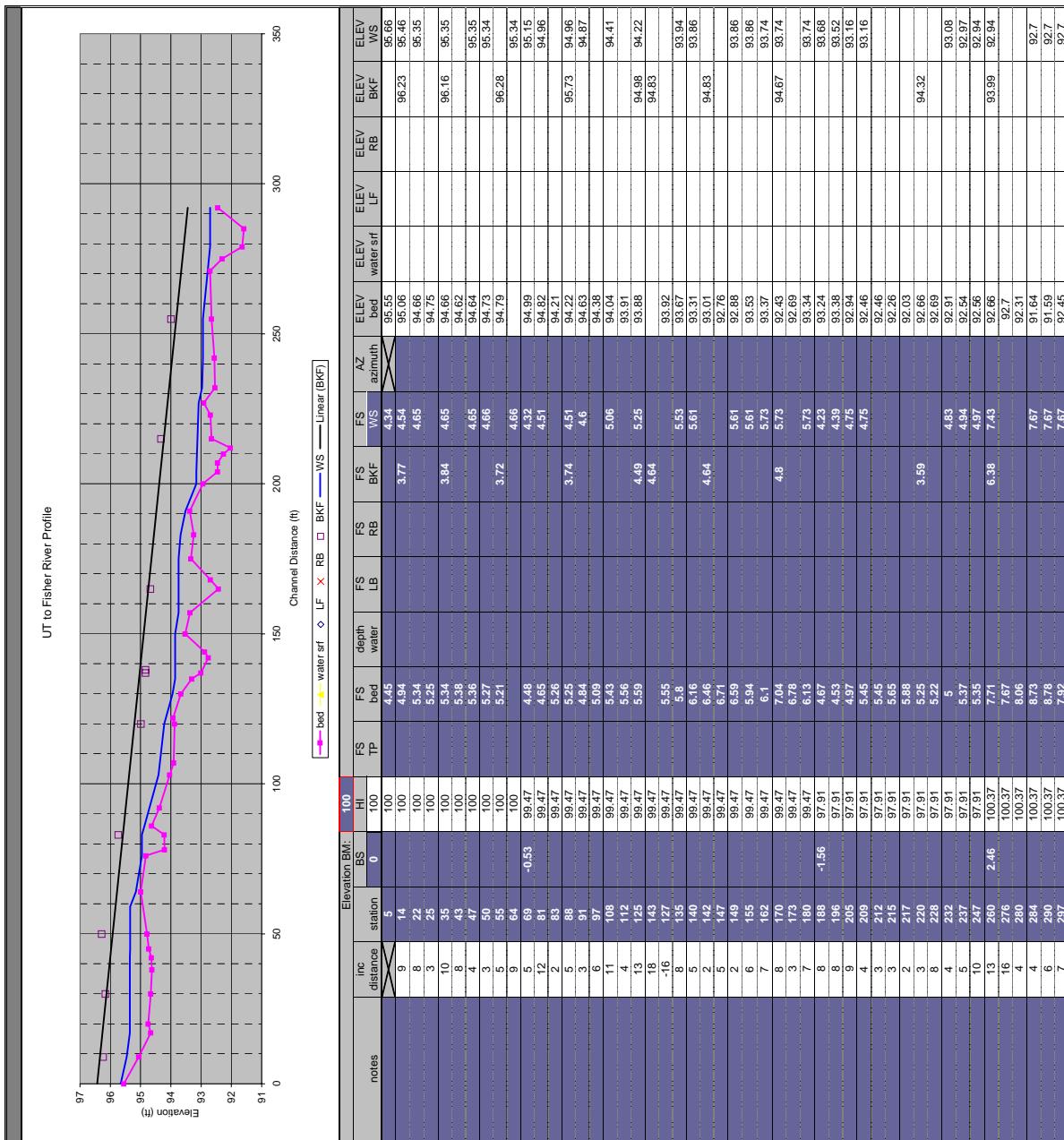
Station	Rod Ht.	Elevation	SUMMARY DATA
0.0	4.62	100.00	Bankfull Elevation:
3.0	5.54	99.08	Bankfull Cross-Sectional Area:
7.0	6.01	98.61	Bankfull Width:
8.5	6.34	98.28	Flood Prone Area Elevation:
9.0	7.04	97.58	Flood Prone Width:
9.5	7.66	96.96	Max Depth at Bankfull:
11.0	7.67	96.95	Mean Depth at Bankfull:
12.0	7.79	96.83	W / D Ratio:
14.0	7.58	97.04	Entrenchment Ratio:
16.0	7.57	97.05	Bank Height Ratio:
17.0	7.51	97.11	Slope (ft/ft):
17.5	6.34	98.28	Discharge (cfs)
19.0	5.90	98.72	
21.0	5.06	99.56	
25.0	4.37	100.25	

**Yadkin River Basin, UT to Fisher River, XS#4 Riffle**











River Basin:	French Broad
Watershed:	White Oak Creek, Existing Conditions
XS ID:	XS - R, Riffle
Drainage Area (sq mi):	0.5
Date:	8/26/2007
Field Crew:	B. Hemel, Z. Mryncza

SUMMARY DATA	
Bankfull Elevation:	2888.2
Bankfull Cross-Sectional Area:	5.1
Bankfull Width:	8.8
Flood Prone Area Elevation:	2869.1
Flood Prone Width:	11
Max Depth at Bankfull:	0.9
Mean Depth at Bankfull:	0.6
W / D Ratio:	15.2
Entrenchment Ratio:	1.3
Bank Height Ratio:	1.1

Station	Elevation
0.0	2881.13
1.8	2880.41
3.3	2879.98
4.6	2879.43
7.1	2878.10
8.1	2877.28
9.9	2875.73
10.9	2874.05
12.2	2872.99
13.3	2872.02
14.1	2871.11
15.6	2869.22
17.4	2868.20
18.2	2867.77
19.7	2867.91
21.6	2867.47
22.8	2867.39
24.1	2867.32
24.9	2867.31
26.0	2868.00
27.1	2869.07
29.0	2869.84
31.7	2870.53
34.3	2870.65
37.9	2870.04
40.9	2869.77
44.4	2870.12
46.7	2870.25

French Broad River Basin, White Oak Creek, Existing Conditions, XS - R, Riffle

