

DYE BRANCH STREAM RESTORATION PLAN

TOWN OF MOORESVILLE IREDELL COUNTY, NORTH CAROLINA



NORTH CAROLINA ECOSYSTEM ENHANCEMENT PROGRAM



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Dye Branch Stream Restoration Plan

Town of Mooresville Iredell County, North Carolina

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Prepared For:

Ecosystem Enhancement Program

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1.0 Introduction

1.1 Project Description

The proposed Dye Branch stream restoration project is located within the City Limits of Mooresville, North Carolina. Mulkey, Inc. (Mulkey) was contracted through the North Carolina Ecosystem Enhancement Program (EEP) to provide design and construction management services as part of an On-Call Services Agreement. This urban stream restoration project covers a portion of Dye Branch and one of its tributaries, Cemetery Branch, situated immediately east of the Mooresville downtown area. Specifically, the project begins along Dye Branch at the culvert outlet under Center Avenue and extends downstream nearly 3,500 linear feet to the last residential property at the southern end of McLelland Avenue. The proposed restoration of Cemetery Branch begins immediately downstream of the Church Street culvert and extends approximately 1,000 linear feet to its confluence with Dye Branch. The two combined streams total approximately 4,597 linear feet of existing stream channel. This does not include the length of the culverts. Figure 1 denotes the project area associated with both stream channels and includes directions to the project site.

These segments of Dye Branch and Cemetery Branch were selected for their excellent opportunities to restore natural stream functions, establish effective riparian buffers and restore overall healthy floodplain stability in this urbanized section of town. The Dye Branch project is entirely within urban confines, consisting primarily of residential areas and a city park. The landuse within and surrounding the project site is either periodically maintained or dominated by exotic, invasive vegetative species such as Chinese privet (Ligustrum sinense) and kudzu (Pueraria lobata). The lack of overall riparian vegetation, the condition of the existing vegetation and the excessive stormwater runoff from the surrounding urban areas has caused severe streambank erosion and poor water quality conditions. The restoration of Dye Branch and Cemetery Branch incorporates natural channel design methodologies and will total approximately 4,353 linear feet of stream channel, an overall decrease of nearly 244 linear feet of stream length. These efforts will utilize Priority II, III and IV stream restoration principles to reestablish the stream channels within their historical floodplains. The restoration effort will also include utility relocation and removal and/or eradication of exotic, invasive plants. No jurisdictional wetlands will be impacted as part of project implementation.

2.0 Goals and Objectives

The goals and objectives of this stream restoration plan will result in:

- Providing a stable system of stream channels that neither aggrades nor degrades while maintaining their dimension, pattern, and profile with the capacity to transport the watershed's water and sediment load;
- Improving the overall water quality and aquatic habitat by reducing sediment and waste inputs into the stream caused by bank erosion, mass-wasting, and stormwater runoff; and
- Improving the overall viability of the riparian vegetative communities through establishment of native species and elimination of invasive and exotic species.

3.0 General Watershed Information

Dye Branch and Cemetery Branch are situated within the Yadkin-Pee Dee River Basin. The site is within the US Geological Survey (USGS) hydrological unit code (HUC) 03040105 and the NC Division of Water Quality (NCDWQ) sub-basin 03-07-11. This sub-basin is known as the Upper Rocky River Watershed, covering approximately 277 square miles or 177,300 acres. Forests and pastureland account for approximately 90% of the land use within the sub-basin. The remaining ten percent is considered urban.

Dye Branch originates approximately 1,300 feet north of the project beginning from several intermittent drainages and culvert outlets. The stream flows in a southerly direction through the project area and empties into the Rocky River four miles downstream. The drainage area associated with the Dye Branch watershed covers nearly 0.6 square miles (384 acres). Cemetery Branch flows in a southeasterly direction to its confluence with Dye Branch approximately 1,000 linear feet downstream from the beginning of the project. The drainage area of the watershed of Cemetery Branch covers approximately 0.06 square miles (38.4 acres). The drainage areas associated with both streams are presented in Figure 2.

The dominant land use within the watershed is primarily urban, occupying approximately 85 percent of all land area within the watershed. Contrary to overall landuse in the Rocky River watershed, this portion of Dye Branch is exclusively classified as urban. The downtown area of Mooresville, which houses government complexes and commercial areas, including small businesses and restaurants, covers the northern-most section of the watershed. Residential neighborhoods and their yardscapes, as well as parks, are also included within the urban land use category, encompassing the majority of the land use in the watershed. Impervious surfaces and intensely maintained areas account for another ten percent of the land area. This large area of impervious surface can be attributed to the close proximity of parking lots adjacent to commercial and governmental buildings, as well as the presence of numerous secondary roadways in the immediate watershed area. Forest lands within the watershed are limited to small, narrow areas that account for the remaining percentage of the land use.

According to the North Carolina Department of Environment and Natural Resources (NCDENR), Dye Branch is currently classified as C (Secondary Recreation) waters according to the 1974 assessment (NCDENR, 2003). Cemetery Branch is not classified and therefore assumes the same classification as Dye Branch. According to the latest report issued by the NCDENR (2004), Dye Branch, from its source to its confluence with the Rocky River, is also currently listed as a 303(d) impaired stream within the 03-07-11 sub-basin. It is impaired for aquatic life with potential sources of pollution from urban runoff/storm sewers and a minor municipal point source (NCDENR, 2004).

Water quality information has been collected from two sampling sites along Dye Branch; one on SR 1147 approximately 2.5 miles downstream of the project area and the other on SR 1142 approximately 4 miles downstream of the site. The sampling site on SR 1147 received a North Carolina Biotic Index (NCBI) rating of "Fair" in 1985 and 1990. The sampling site located on SR 1142 was rated "Poor" in 2001. These ratings are based on the number of benthic macroinvertebrate taxa present in the intolerant groups Ephemeroptera, Plecoptera and

Trichoptera (EPTs) and the value of the NCBI. The ratings can range from Poor to Excellent and primarily reflect the influence of chemical pollutants (NCDENR, 2002).

Currently, there are 24 National Pollutant Discharge Elimination System (NPDES) dischargers within the 03-07-11 sub-basin, which includes portions of Mecklenburg and Cabarrus Counties. In recent years, one large industrial facility in the Dye Branch watershed which contributed waste to the Mooresville Waste Water Treatment Plant (WWTP) closed, nearly eliminating toxicity problems associated with that discharge. The Mooresville WWTP had only a few minor compliance problems between 1998 and 2001, most of which were resolved quickly. However, there is a significant amount of developed area in the Dye Branch watershed and the City of Mooresville will likely be required by NCDWQ to obtain an NPDES permit for municipal stormwater systems under the Phase II stormwater rules.

3.1 Current Property Ownership

The Dye Branch project site will be held in perpetuity under the strictures of a conservation easement. Approximately twenty-one individual landowners currently own and/or adjoin the land contained within this conservation easement. The majority of the acreage within the easement is owned by the Town of Mooresville. The remaining landowners, as documented by the Iredell County GIS/Mapping Department as of July 2005, are listed in Appendix A.

4.0 Existing Conditions

4.1 Existing Topography

The topography of the project site has been altered over the years by the increased urbanization of the downtown area. Within the project area and its vicinity, slopes have been graded, areas have been filled and the majority of the vegetation has been removed in order to make way for the city park, neighborhoods and other urban development. In all likelihood, the width of the floodplain has also been changed. The current floodplains of Dye Branch and Cemetery Branch vary in width above Cabarrus Avenue and narrow towards the terminus of the project. Elevations range across the project from a high of 850 feet above mean sea level at the upper limit, or beginning, to a low of 810 feet at the end.

4.2 Existing Natural Features

4.2.1 Geology

The Dye Branch Site is within the Piedmont physiographic province; specifically, the Southern Outer Piedmont Ecoregion (Griffith et al., 2002). It is underlain by the Charlotte Belt, a region consisting of intrusive, granitic rock, which formed during the Permian and Pennyslvanian Periods (265 to 325 million years ago) (NCDLR, 1985).

4.2.2 Soils

Soils found at the Dye Branch Site lie within the Felsic Crystalline System of the western Piedmont (Daniels et al., 1999). According to the Iredell County Soil Survey, Chewacla, Cecil fine sandy loam and Colfax sandy loam are the soils underlying the project area (Figure 3). The Chewacla soils are deep, somewhat poorly drained soils which have formed from recent alluvium on nearly level floodplains along streams that drain from the Mountains and Piedmont physiographic provinces. The Cecil soils are eroded, well-drained soils located on 6 to 15 percent slopes bordering drainageways. The Colfax soils are somewhat poorly drained upland soils along drainageways with 2 to 6 percent slopes.

Based on the Soil Survey of Iredell County, Chewacla and Colfax soils comprise the floodplain portion of the site, while the adjacent uplands consist mainly of Cecil soils. Chewacla soils are classified by the Natural Resources Conservation Service (NRCS) as fine-loamy, mixed, active, thermic Fluvaquentic Dystrudepts. Colfax soils are classified as fine-loamy, mixed, subactive, thermic Aquic Fragiudults. Chewacla and Colfax soils are classified as Hydric B soils because their composition is not entirely hydric, but retain a hydric status due to inclusions of Hydric A soils. These inclusions are most commonly Wehadkee and Worsham soils.

4.3 Existing Hydrologic Features

Mulkey surveyed the existing conditions at the project site by using total station survey equipment with GPS survey grade receivers. Existing condition surveys included longitudinal profiles, cross sections, pebble counts, and bar samples to determine the current state of the stream channels. Existing longitudinal profiles were conducted by identifying each stream feature (riffle, run, pool, or glide) and surveying specific points at those features. These specific locations included top of bank, bankfull, waters edge or surface, and thalweg. In addition, 10 cross sections on Dye Branch and four along Cemetery Branch were selected and surveyed at representative stream features throughout the project. These cross section helped to fully characterize the dimension of the existing channels (Figure 4 and Appendix B). Following the completion of the existing channel surveys, pebble counts were conducted at specific cross section locations as well as a bar sample analysis. Data pertaining to each stream channel are discussed in the following sections.

4.3.1 Jurisdictional Streams

According to the North Carolina Administrative Code, Dye Branch and Cemetery Branch both meet the jurisdictional definition for perennial streams. Perennial streams have water flowing in a well-defined channel for a majority of the year (greater than 90 percent of the time). Another stream channel was identified in the project area whose confluence is approximately 500 feet downstream of the confluence of Dye Branch and Cemetery Branch; however, it meets only the jurisdictional definition of an intermittent stream. Intermittent streams contain water for only part of the year, typically during winter and spring when the aquatic bed is below the water table (NCAC, 1999).

4.3.1.1 Dye Branch

Dye Branch flows in close proximity to downtown Mooresville. The substantial amount of impervious surface and lack of vegetation throughout the watershed has contributed to the flashy flood conditions and actively eroding streambanks of the existing stream channel. Little to no riparian buffer exists along the stream within the project area, which has further exacerbated the destabilization of the stream.

The existing Dye Branch channel within the project area has been separated into three reaches. The first reach begins at the culvert outlet under Center Avenue and ends at the McLelland Avenue culvert. The second reach begins at the McLelland Avenue culvert outlet and ends at the Cabarrus Avenue culvert and the third reach begins at the Cabarrus Avenue culvert outlet and ends at the last residential property on Cabarrus Avenue. The slope along Dye Branch ranges from 0.0060 ft/ft (or 0.6%) in its upper reach to an average slope of 0.0110 ft/ft (or 1.1%) in the lower reach. Existing profile information for Dye Branch can be found in Appendix B. Dye Branch is classified as an unstable E4 channel along the upper two reaches of

the project according to the Rosgen stream classification system (Rosgen, 1994). It transitions to a G4c stream type as the slope increases through the lower reach.

The bank height ratios also vary between the reaches. Bank height ratios note the difference between the bankfull elevation and the lowest stream bank. Commonly, stable channels exhibit bank height ratios between 1.0 and 1.3; however, these numbers may increase based on stream classification and overall entrenchement. The existing ratios were approximately 1.0 along the upper two reaches. As for the lower reach, Mulkey observed ratios ranging up to 5.0 further denoting the overall instability of this reach. A summary of the cross section data used to determine these classifications is presented in Table 1 and existing cross section views are presented in Appendix B. Additional information including existing pattern data for Dye Branch can be found with all the morphological data in Appendix C.

The composition of the stream bed and banks is an important facet of stream character, influencing channel form and hydraulics, erosion rates and sediment supply. The stream bed along Dye Branch was characterized using two protocols, the modified Wolman Pebble Count (Rosgen, 1993) and the bar sample analysis. The bar sample analysis provides data for both comparison purposes and sediment transport validations.

According to the modified Wolman Pebble Count procedure, the average d₅₀ (50% of the sampled population is equal to or finer than the representative particle diameter) is approximately 5.0 mm for Dye Branch, which falls into the fine gravel size category. Pebble counts were taken at 10 locations along Dye Branch. The locations included 5 riffles, 3 runs, 1 glide and 1 pool cross section. To provide a more detailed picture of the pebble counts, counts were taken within specific areas of the stream channel. Samples taken between bankfull elevations were categorized as "Classification" samples and those taken below the water surface were used as the "Wetted Perimeter" samples. The classification samples determine the stream's material size as it relates to bankfull events and its overall stream material classification. The wetted perimeter samples are used to describe the movement of sediment within the active bed. The particle size distribution data which includes the classification, wetted perimeter, and bar sample are presented in Appendix D.

The stability rating of the existing Dye Branch channel was determined by using the Pfankuch Channel Stability and Bank Erosion Hazard Index (BEHI) Forms. All three reaches associated with Dye Branch were assessed. The Pfankuch rating for the Dye Branch channel was estimated to be between 114 and 125, which ranks as "Poor" according to the rating system established for an E4 and G4c Rosgen stream types. The BEHI rating was "Extreme" for all three reaches. These stream channel stability evaluations can be found in Appendix E.

4.3.1.2 Cemetery Branch

Cemetery Branch was classified as an unstable E4 stream. The average slope of this channel is 0.0190 ft/ft (or 1.9%). The streambanks associated with this tributary have been destablilized by its urban surroundings, lack of vegetation and ongoing flow regimes. A summary of the cross section data used to determine this classification is also presented in Table 1 along with the data for Dye Branch. Existing cross section views are presented in Appendix B. Additional information including existing pattern data for Cemetery Branch can be found with all the morphological data in Appendix C.

According to the modified Wolman Pebble Count procedure, the average d₅₀ for the stream classification was approximately 6.0 mm, which falls into the fine gravel size category (Appendix D). The Pfankuch Channel Stability rating for Cemetery Branch was estimated to be 117, which is considered "Poor" for an E4 Rosgen stream type. The BEHI evaluation conducted on Cemetery Branch determined that the channel has "Extreme" bank erosion potential.

Table 1. Summary of Existing Cross Sections - Dye Branch and Cemetery Branch

Cross Section	Station No.	Morph. Feature	Bankfull Area (ft²)	Ent. Ratio	W/D Ratio*	Wetted Perimeter (ft)	Hydraulic Radius (ft)	Stream Class,*
1	1+53	Riffle	14.3	2.6	14.2	16.2	0.88	C4
2	2+10	Run	18.2	1.9	12.2	17.1	1.1	[88]
3	5+61	Riffle	19.7	3.2	7.9	15.6	1.3	E4
4	8+73	Run	19.4	>5	6.5	14.5	1.3	
5	10+13	Riffle	18.1	>5	7.0	14,4	1.3	E4
6	15+71	Riffle	22.9	>5	6.2	15.6	1.5	**
7	26+22	Pool	20.8	1.5	9.5	17.2	1.2	523
8	26+42	Glide	21.3	2.5	27	26.1	0.8	57
9	26+99	Run	20.3	1.9	74.6	38.3	0.5	
10	31+91	Riffle	17.4	1.5	12,5	17.1	1.0	G4c
Cemetery	4+68	Pool	14.6	>5	1.2	15.3	0.9	
Cemetery	4+71	Glide	7.1	3.1	10.5	10	0.7	148
Cemetery	9+08	Riffle	6.8	2.0	7.0	9.0	0.8	E4
Cemetery	9+18	Run	8.3	4.2	4.8	8.8	0.9	27

*Notes: Ent. Ratio is "Entrenchment Ratio"

W/D Ratio is "Width/Depth Ratio"

Stream classification is only viable along riffle sections.

4.3.2 Jurisdictional Wetlands

Jurisdictional wetland determinations were performed using the three-parameter approach as prescribed in the 1987 Corps of Engineers Wetlands Delineation Manual (Environmental Laboratory, 1987). One jurisdictional wetland exists within the boundaries of the project site. This wetland is located along the left side of Cemetery Branch approximately 500 feet downstream of the Church Street culvert. The wetland area totals approximately 0.098 acres and will likely be contained within the permanent conservation easement, once it is finalized. Wetland determination forms for the Dye Branch site are presented in Appendix F. The wetland covers nearly 0.098 acres and is characterized as a small depressional area adjacent to Cemetery Branch. It is dominated by herbaceous species that are mowed on a continuous basis. The wetland provides only modest habitat, very limited water storage capacity, and based on low opportunity, plays only a minor role in improving water quality at the site. This wetland will not be impacted by the enhancement of the Cemetery Branch channel and does not have an USACE Action ID Number appointed to it.

4.4 Existing Plant Communities

The vegetative communities found within the project area can be characterized by two major groupings. These groupings include Urban/Disturbed Land and Piedmont Bottomland Forest (Figure 5). Each plant community with its distinct assemblage of plants arose in response to diverse topography and the influences of changing land uses over time. Scientific names are presented along with the common names the first time the species is cited, but subsequent textual references to the same species will be limited only to its common name.

4.4.1 Urban/Disturbed Land

The urban/disturbed land is the most dominant vegetative community, where it accounts for approximately 85% of the total land area within the project area. The upper reach of the project is dominated by kudzu (*Pueraria lobata*), covering essentially the entire floodplain of Dye Branch. Most of middle reach, situated between Mc Lelland Road and Cabarrus Avenue, is within the City Park confines and is periodically maintained to the top of the stream bank. This area is dominated by fescue (*Festuca* spp.) along the entire left side of the stream and approximately 1,300 feet downstream from McLelland Road along the right side of the channel. Further downstream, the right side of the channel is primarily forested to Cabarrus Avenue. The lower reach of the project consists of residential yardscapes dominated by fescue and Chinese privet (*Ligustrum sinese*) along the left side of the stream, facing downstream. The right side is forested.

Cemetery Branch also lies within the City Park confines. The majority of the banks surrounding this channel consist primarily of fescue and other weeds which are maintained on a periodical basis.

4.4.2 Piedmont Bottomland Forest

Vegetation found in this community is consistent with the Schafale and Weakley's (1990) Piedmont Bottomland Forest classification. This vegetative community exists along the forested portion of the project site along the right side of Dye Branch above Cabarrus Avenue and continues along the right side to the end of the project. This community is also present along Cemetery Branch approximately 100 feet downstream of the Church Street culvert and extends approximately 300 feet along the left side of the channel. Dominant species found within this vegetative community include red maple (Acer rubrum), black willow (Salix nigra), sycamore (Platanus occidentalis), yellow poplar (Liriodendron tulipifera), box elder (Acer negundo), Chinese privet (Ligustrum sinense) and giant cane (Arundinaria gigantea). Piedmont Bottomland Forests are generally situated on floodplain ridges and terraces other than active levees adjacent to the stream channel. They are underlain by various alluvial soils, including the Chewacla and Congaree series. These communities are flooded; however, they are seldom disturbed by flowing water. Bottomland forests are believed to form a stable climax forest, having an uneven aged canopy with primarily gap phase regeneration, although the possibility of unusually deep and prolonged flooding may make widespread mortality more likely than in uplands (Schafale and Weakley, 1990).

4.5 Invasive Plant Species

Invasive, or non-native species, are the dominant plant species within the project area. Extensive quantities of Chinese privet and kudzu were observed along the stream banks, floodplain, and throughout the project site.

4.6 Threatened and Endangered Species

According to the US Fish and Wildlife Service (USFWS), neither threatened nor endangered species are known to occur in Iredell County. However, one threatened due to similarity of appearance (T S/A) species and three federal species of concern (FSC) have been documented for Iredell County. Information regarding these federally listed species of concern can be found in Table 2.

Table 2. Federally Listed Species

Common Name	Scientific Name	Federal Status	State Status	Habitat Requirements	Suitable Habitat	Biological Conclusion
Alleghany woodrat	Neotoma magister	FSC	SC	A small mammal found in rocky places and abandoned buildings in deciduous or mixed forests in the northern mountains and adjacent Piedmont.	No	Not Applicable
Bog turtle	Clemmys muhlenbergii	T(S/A)	Ť	A turtle found in bogs, wet pastures, and wet thickets.	No	Not Applicable
Heller's trefoil	Lotus helleri	FSC	A vascular plant found in open woods over clay soils and roadsides.		No	Not Applicable
Tall Delphinium FSC		FSC*	4	A vascular plant found in rich woods (and edges of woods), rocky slopes, semi-open woodlands, glades and prairie openings.	No	Not Applicable

SC—Special Consern

4.7 Environmental Issues

Federal, state, and local databases were searched using a designated one-mile radius to determine whether the study area or neighboring areas have a regulatory history of environmental problems that could have an adverse impact on the study area. These databases included the following:

- National Priorities List (NPL);
- Resource Conservation and Recovery Information System (RCRIS) which includes information on Treatment, Storage, and/or Disposal (TSD);
- Comprehensive Environmental Response, Compensation, and Liability Information System (CERCLIS);
- Resource Conservation and Recovery Act Information System Small and Large Quantity Generator and/or Transporter (RCRA);
- Emergency Response Notification System (ERNS);

SR-T-Significantly Rare and Is Proposed for Threatened Status

^{*}Historic record - the species was last observed in the county more than 50 years ago

- State Inactive Hazardous Site Program List, known as the State Priorities List (SPL);
- State Landfills (Landfills);
- Leaking Underground Storage Tanks (LUST);
- Owners of Underground Storage Tanks (UST);
- Delisted NPL;
- RCRA Administration Action Tracking System (RAATS);
- Hazardous Materials Incident Report System (HMIRS);
- PCB Activity Database (PADS);
- Facilities Index System (FINDS);
- Toxic Release Inventory System (TRIS);
- Federal Superfund Liens (NPL Liens);
- State of North Carolina Hazardous Substance Disposal Site (NC HSDS);
- Toxic Substances Control Act identifying Chemical Substance Inventory List (TSCA);
- Records of Decision (ROD);
- Superfund (CERCLA) Consent Decrees (CONSENT); and
- Former Manufactured Gas Sites (Coal Gas).

A copy of the EDR report is provided in Appendix G. EDR did not report any on-site sources of potential contamination. However, EDR listed several sites of potential contamination within a one-half mile surrounding the study area. Those sites include seven LUST sites, six of which are within the Dye Branch drainage area. The LUST sites within Dye Branch drainage area are: Mooresville Town Library, 121 East Catawba Ave.; Burlington Mills, 476 South Main St. (2 sites); Bills Exxon, 204 South Main St.; Glaspy's Auto Service, 152 South Main St.; Shepherd's, 126 East Center Avenue; and Mooresville Amoco Service, 151 South Broad St. One of the sites at Burlington Mills, Bills Exxon, Glaspy's Auto Service and Mooresville Amoco Service have not been closed out, which indicates reports on the ongoing clean up process are still being generated.

The Mulkey team conducted a cursory investigation for any Recognized Environmental Concerns (RECs) throughout the site. The investigation included only a visual scan of the property. RECs are characterized as the presence or likely presence of any hazardous substances or petroleum products on a property under conditions that indicate an existing release, a past release, or a material threat of a release of any hazardous substances or petroleum products into structures on the property or into the ground, groundwater, or surface water of the property (ASTM E1527-00). None were observed as part of the existing conditions survey.

A building containing a men's and women's bathroom is located along the middle reach in Glenwood Memorial Park. No other buildings, sheds or other structures were observed in the project area.

4.8 Cultural Resources

Mulkey conducted a review of properties determined eligible for the National Register of Historic Places at the State Historic Preservation Office (SHPO) for the study area and surrounding areas. According to the files, two locations have been placed on the National Register within a one-mile radius of the study area. Those locations include the Mooresville Historic District and Broad Street Row. The Mooresville Historic District lies approximately one third-mile northwest of the project area and extends northeast from NC 152 for approximately 0.5 miles encompassing both Broad and Main Streets. Broad Street Row is located approximately one quarter-mile west of the project area along Broad Street between Wilson Avenue and NC 152. In addition, Mulkey contacted the North Carolina State Archaeological Office to determine if documented archaeological sites occur at or near the project area. No sites were identified within a one-mile radius of the project area.

4.9 Utility Realignment

The City of Mooresville has agreed to realign the sewer line that currently exists inside the project area between Center Avenue and the confluence of Dye and Cemetery Branch (upper and middle reaches). The proposed realignment includes relocating the sewer line outside of the floodprone area along the right side of the stream (looking downstream) in order to position it outside the buffer requirement for stream restoration. Three crossings along these two reaches currently exist. The existing crossing on the upper reach will be abandoned and the remaining two crossings on the middle reach will be relocated to intersect the channel only underneath the proposed riffle sections. Reason being, riffle sections are generally the most stable sections of a channel. Aggradation and degradation processes do occur as part of maintaining the dynamic equilibrium within the active streambed; however, grade control will be implemented to insure these processes are minimized to the extent practicable through these areas. Mulkey will incorporate the crossings in the design of Dye Branch and to the extent practicable will set the elevation of the stream above the sewer line so that the crossing will run subsurface to the channel.

5.0 Natural Channel Design

5.1 Reference Reach Analyses

Four reference reaches have been identified for use on the Dye Branch stream restoration project. All four reference reaches, Derita Branch, UT to Lake Jeanette, UT to SW Prong Beaverdam Creek and UT to Mine Creek, were chosen because they represent the stable, urban, piedmont stream type.

5.1.1 Derita Branch

Derita Branch is situated in Mecklenburg County, approximately 2.5 miles north of Charlotte on the northside of SR 2480 (Figure 6). Derita Branch is characterized as a first order, perennial stream and classifies as an urban E4 stream type. Specific morphological data for this reference reach are given within the morphological table found in Appendix C. Its watershed is approximately 0.25 square miles (166 acres) and encompasses an urban neighborhood and commercialized property. Common riparian species found along this stream corridor include American holly (Ilex opaca), red maple, sweetgum (Liqiudambar styraciflua), hackberry (Celtis laevigata), flowering dogwood (Cornus florida), water oak (Quereus nigra), white oak (Quereus alba), black cherry (Prunus serotina) and poison ivy (Toxicodendron radicans).

5.1.2 Unnamed Tributary to Lake Jeanette

UT to Lake Jeanette is situated in Guilford County, approximately 0.5 miles upstream of the SR 2348 crossing of Lake Jeanette (also referred to as Richland Lake) (Figure 7). UT to Lake Jeanette is characterized as a second order, perennial stream and classifies as a rural C5 stream type. Specific morphological data for this reference reach are given within the morphological table found in Appendix C. Its watershed is also approximately 0.25 square miles (166 acres) and encompasses a relatively low density suburban neighborhood within the City of Greensboro. Riparian species commonly found along this stream corridor include of American holly, red maple, American Beech (Fagus grandifolia), ironwood (Carpinus caroliniana) flowering dogwood, white oak and yellow poplar.

5.1.3 Unnamed Tributary to Southwest Prong Beaverdam Creek

UT to SW Prong Beaverdam Creek is located in Wake County, immediately upstream of the intersection of Lake Boone Trail and Runnymeade Road (Figure 8). UT to SW Prong Beaverdam Creek is characterized as a first order, perennial stream and classifies as an urban C5 stream type. Specific morphological data for this reference reach are given within the morphological table found in Appendix C. Its watershed covers approximately 0.28 square miles (180 acres) and encompasses an older urban neighborhood in the City of Raleigh. Common species located along the riparian zone of this stream include tag alder (Alms serrulata), red maple, river birch (Betula nigra), sweetgum, flowering dogwood, tulip poplar, giant cane, poison ivy, jewelweed (Impatiens campensis) and bamboo (Phyllostachys aurea).

5.1.4 Unnamed Tributary to Mine Creek

UT to Mine Creek is located in Wake County, along the east side of North Hills Drive in Raleigh (Figure 9). UT to Mine Creek is characterized as a first order, perennial stream and classifies as an urban B4/1 stream type. Specific morphological data for this reference reach are given within the morphological table found in Appendix C. Its watershed covers approximately 0.17 square miles (109 acres) and encompasses an older residential area in the City of Raleigh. Common species located along the riparian zone of this stream include sycamore, river birch, sweetgum, flowering dogwood, tulip poplar, poison ivy, and jewelweed (*Impatiens campensis*).

5.2 Sediment Transport Analyses

Sediment plays a major role in the influence of channel stability and morphology (Rosgen, 1996). A stable stream has the capacity to move its sediment load without aggrading or degrading. Sediment analyses are generally divided into measurements of bedload and suspended sediment (washload), changes in sediment storage, size distributions and source areas. Washload is normally composed of fine sands, silts and clay transported in suspension at a rate that is determined by availability and not hydraulically controlled. Bedload is transported by rolling, sliding, or hopping (saltating) along the bed. At higher discharges, some portion of the bedload can be suspended, especially if there is a sand component in the bedload. Bed material transport rates are essentially controlled by the size and nature of the bed material and hydraulic conditions (Hey and Rosgen, 1997).

Two measures are used to calculate sediment loads for natural channel design projects: (1) sediment transport competency and (2) sediment transport capacity. Competency is a stream's ability to move particles of a given size. It is expressed as a measure of force (lbs/ft²). Capacity is a stream's ability to move a quantity of sediment and is a measurement of stream power,

expressed in units of lbs/ft-sec. These analyses are conducted to ensure that the designed stream beds including Dye Branch and Cemetery Branch do not aggrade or degrade during bankfull conditions. Brief descriptions of these two analyses are presented in the following subsections. Entrainment and velocity calculation sheets used for these analyses are presented in Appendix H and I, respectively. The locations of the sediment sampling points are depicted in Figure 4.

5.2.1 Sediment Competency Analysis

The critical dimensionless shear stress (τ^*_{ci}) is the measure of force required to initiate general movement of particles in a bed of a given composition. This calculation is part of several calculations used to determine aggradation/degradation along the stream channel. For shear stresses exceeding this critical value, essentially all grain sizes are transported at rates in proportion to their presence in the bed (Wohl, 2000). For gravel-bed streams, the critical dimensionless shear stress is generally calculated using surface and subsurface particle samples from representative riffle sections. The critical dimensionless shear stress calculation is presented below.

$$\tau^*_{ci} = 0.0834 \left(\frac{d_i}{d_{50}} \right)^{-0.872}$$
 where, $\tau^*_{ci} = \text{critical dimensionless shear stress}$ (lbs/ft²)

 $d_i = \text{median particle size of riffle bed surface (mm)}$
 $d_{50} = \text{median particle size of subsurface sample (mm)}$

Note that d_i and d_{50} values were empirically determined by in situ measurements. Based on the d_i of 6.0 mm and the d_{50} of 2.8 mm in reach 1, the critical dimensionless shear stress was calculated to be approximately 0.0429 lbs/ft² utilizing the calculation above. This critical dimensionless shear stress is used as part of the aggradation analysis presented in the following section.

The shear stress placed on the sediment particles is the force that entrains and moves the particles. The critical shear for the proposed channel has to be sufficient to move the D_{84} of the bed material. The critical shear stress was calculated and plotted on the Modified Shield's curve to determine the approximate size of particles that will be moved (Rosgen, 2001).

Based on the Modified Shield's curve, particles ranging from 20 mm to 90 mm could be moved within reach one of the Dye Branch channel, with an average moveable size of 40 mm. The largest particle found on the depositional bars was 24 mm. The D_{84} and D_{100} in this reaches are 10 mm and 22 mm, respectively. The middle and lower reaches of Dye Branch can move particles ranging from 30 mm to 100 mm, with and average moveable particle size of 65 mm. The largest particle found on depositional bars in these reaches was 45.7 mm. The D_{84} and D_{100} of the reach were 9.3 mm and 150 mm, respectively. Therefore, the proposed design has sufficient shear stress to move the bedload associated with all three reaches Based on Shield's curve, Cemetery Branch can move particles ranging from 45 mm to 180 mm. The D_{84} and D_{100} of Cemetery Branch are 10.2 and 15.0 mm, respectively.

Mulkey also utilitized another method to calculate critical shear stress for each reach studied as taught by Dave Rosgen, PhD., PH, with Wildland Hydrology, Inc. However, when this method

was used to calculate the shear stress of the proposed design, the middle and lower reaches of Dye Branch indicated instability. When the dimensions of reaches two and three were adjusted to create a "stable" entrainment; width/depth (W/D) ratios were out of the range observed in stable channels. Since the Shield's curve calculations indicate that all reaches are capable of moving their supplied sediment only the results from the Sheild's curve analysis were considered appropriate for these reaches.

5.2.2 Sediment Transport Capacity

Stream power was calculated for both the existing and design channel conditions to determine the effect of the restoration on sediment transport capacity. A stream's capacity is defined as the maximum load a stream can transport at a given time. The capacity of a stream to move sediment is directly related to velocity and stream power. The existing channel exhibited an excess of stream power as noted by the mass wasting of banks and excessive bank height ratios. By adjusting width-to-depth ratios and providing a floodplain at the bankfull stage, the proposed design reduces both stream power and velocity; thereby, reducing capacity to only that needed to move the sediment supplied by the watershed.

5.2.3 Aggradation/Degradation Analysis

New channel construction associated with natural channel design projects generally includes the design and layout of a channel with increased length and sinuosity and reduced slope as compared with the existing channel. However, there are some situations where the existing channel exhibits excessive and unstable patterns. The new channel design in these cases will result in an increase in slope and a decrease in channel length. The data associated with these channels must prove that the adjusted channel slope will not cause the stream to aggrade or degrade. The upper portion of Dye Branch maintains a relatively stable profile; therefore the proposed design will only slightly decrease the channel's slope (0.00415 ft/ft), and improve its dimension and pattern. The middle portion of Dye Branch was designed to have a slightly greater slope (0.0094 ft/ft) than the existing channel (0.008 ft/ft) due to the shorter length of the new channel alignment. The proposed design for the lower portion of Dye Branch will result in a new and slightly shorter channel with less slope (0.0102 ft/ft) than the existing channel (0.0110 ft/ft) and a lower width/depth ratio. The proposed width/depth ratios were adjusted in conjunction with the slope to ensure that the proposed stream will transport its sediment over time without aggrading or degrading.

Calculations of critical depth are required. These calculations represent the need to transport large sediment particles, usually defined as the largest particle of the riffle sub-pavement sample. As a result, critical depth can be compared with the design mean riffle depth in order to verify that the design stream has sufficient competency to move large particles without causing the thalweg to aggrade or degrade. The calculation for critical water depth is shown below.

$$d_{\sigma} = \frac{1.65 (\tau^*_{ci})D_i}{S}$$
 where, $d_{\sigma} = \text{critical water depth (ft)}$
 $\tau^*_{ci} = \text{critical dimensionless shear stress}$
 (lbs/ft^2)
 $D_i = \text{largest particle of bar or subpavement sample (ft)}$
 $S = \text{average channel slope (ft/ft)}$

5.2.4 Sediment Transport Summary

Based on the calculations for competency, aggradation, degradation and capacity, bankfull conditions in the design channel will entrain particles ranging from 15 to 110 mm. The D_{100} of Dye Branch is approximately 64 mm. The design channel is predicted to remain stable over time based on the establishment of proper dimension, pattern and profile and an active floodplain. The addition of riparian vegetation will further enhance the long term stability of the entire system.

5.3 Proposed Design

Design methodologies are based on natural channel design concepts outlined by Rosgen (1994, 1996, 1998). These methodologies include existing and reference reach channel surveys, data interpretations and geomorphological comparisons of all channel features. Based on field observations and preliminary ideas, the project will attempt to implement restoration similar to Priority Levels II and III. The Priority Level II Restoration involves construction of a new channel with a floodplain bench at the bankfull elevation. This will be implemented along the the entire portion of the Dye Branch stream channel. The Priority Level III Restoration will involve the reconstruction or installation of additional bankfull benches within the existing channel confines. This restoration type will be implemented along Cemetery Branch. A summary of the existing and proposed streams at the project site is outlined in Table 3. A Conceptual Design for Dye Branch can be found in the Attachments section.

Table 3. Dye Branch Stream Restoration Summary

Stream	Priority Level	Type	Existing Length of Channel* (If)	Proposed Length of Channel* (lf)
Dye Branch	II	Restoration	3628.51	3353.89
Cemetery Branch	ш	Restoration	968.28	998.64
		Total	4596.79	4352.53

^{*} Lengths do not include culverts.

5.3.1 Dye Branch

It is anticipated that Priority Level II Restoration design measures will be applied to approximately 3,353 linear feet of Dye Branch, the entire length of project along the main channel (Appendix J). This restoration will transform the stream from an unstable E4/G4c stream type to a stable C4 stream type. The upper reach, from the project's beginning at Station 0+00 to Station 6+25 averages a slope of 0.0042 ft/ft (or 0.4%), which is the flattest of the three sections of channel. Cross vanes, j-hook vanes, single arm rock vanes and rootwads will be used along this segment to provide overall stability and grade control. Bankfull cross sectional areas average 24.1 square feet for riffles and 36.4 square feet for pools and are also found in Appendix J. The upper reach stream channel will contain floodplain benches and improved meander pattern, which will help reduce stream velocities.

The middle reach, which exhibits a slope of 0.0094 ft/ft (or 0.9%), will provide a gradual transition between the upper and the lower reaches. Bankfull cross sectional areas associated with the middle reach average 20.0 square feet for riffles to 29.0 square feet for pools. The subsequent decrease in overall areas as compared with the upper reach is due to the increased slope. Approximately 630 ft of new channel will excavated from Station 14+60 to Station

20+90 in order to further stabilize the stream. The remainder of this reach will utilize floodplain benches and radius improvements. Structures used through this section will include cross vanes, j-hook vanes, and single arm rock vanes. Rootwads will be installed at specific areas to relieve stress from outside bends and to provide natural habitat for aquatic life.

The lower reach of Dye Branch, extending from Station 22+90 to Station 35+22, exhibits slopes averaging 0.0102 ft/ft (or 1.0%), which are the steepest throughout the project. Due to this increase of slope, the bankfull cross sectional areas have decreased as the stream flows from the upper to the lower reach. The bankfull cross sectional areas associated with the lower reach average 18.8 square feet for riffles and 29.0 square feet for pools. This reach will also utilize cross vanes, j-hooks, single arm vanes, and rootwads. In addition to the structures, floodplain benches and improvements to the overall pattern of the channel will aid in decreasing velocities and further stabilize the stream.

5.3.2 Cemetery Branch

Stream restoration associated with Cemetery Branch will be exclusively Priority Level III Restoration. This restoration will change the stream from an unstable E4 stream type to a stable B4 stream type. The restoration will begin approximately 40 ft downstream of the Church Street culvert and extend approximately 1,000 linear ft to its confluence with Dye Branch. Bankfull cross sectional areas proposed for this stream channel are 7.0 square feet for riffles and 10.3 square feet for pools. Cross vanes, single arm rock vanes and rootwads will be installed to provide grade control and improve overall channel stability. Minor pattern improvements are also proposed.

5.4 Proposed Construction Sequence

Construction of the project will be carried out in three phases to ensure adequate implementation of sedimentation controls, channel stability, and maximum vegetation survival. During the first phase, primary construction access roads, spoil areas, and staging areas will be established. During the second phase, the majority of the restoration activities will take place along both Dye Branch and Cemetery Branch. These will include establishing the proper dimension, pattern, and profile along each of the channels followed by structure installation. The consequent filling of the abandoned channels will also be completed as part of the second phase. Disturbed banks will be seeded, mulched, and matted immediately upon completion of any grading. The final phase will involve minor grading, site preparation (sub-soiling), removal of temporary access roads and staging areas, and the installation of plant material.

Initially, the primary construction access roads, spoil areas, and the staging areas will be established throughout the entire Dye Branch Stream Restoration Site. Once these areas have been established, erosion and sedimentation control devices will be installed. Also, temporary fencing will be installed around the project site.

The second phase of the project will involve construction of new channels and placement of structures for Dye Branch and Cemetery Branch. These structures will provide stability and habitat for the stream channel and will include cross vanes, j-hook vanes, single-arm rock vanes, and rootwads. Construction of the new channel must be staged to ensure the most economical use of equipment and materials, and to ensure that sedimentation controls and channel stability efforts are maximized. As the majority of the construction will occur within the existing channel, the stream's water will be pumped around the construction.

The new Dye Branch channel will be constructed from Center Street to McLelland Avenue (Station 0+00 to Station 6+25). Special stilling basins will be utilized to filter any groundwater that accumulates within the proposed channel. Pumping the perennial flow and filtering the groundwater will further ensure superior sediment control since groundwater difficulties are anticipated. Spoil generated from excavation of the new channel will eventually be used to fill the existing stream channel downstream of McLelland Avenue. The majority of the excavation spoil from upstream of McLelland Avenue will be stockpiled on the Town of Mooresville's property at the southern end of McLelland Avenue as detailed on the erosion control plans, to reduce material-handling time and to minimize compaction of the substrate.

Between McLelland Avenue and Cabarrus Street (Station 7+50 to Station 22+00), the channel will be constructed in much the same manner as the upstream portion. Perennial flows will be pumped from the culvert at McLelland Avenue to below Station 14+60 where the proposed channel departs from the existing channel. All required grading and structure installation will occur upstream of Station 14+60 prior to construction of the new location channel. Once this segment is complete, the new location segment of channel will be constructed while the flow remains in the existing channel. Again, all groundwater seepage into the proposed channel will be pumped into special stilling basins for filtering. All spoil material will be stockpiled on the east side of the existing channel near the basketball courts as detailed on the erosion control plans, to reduce material-handling time and to minimize compaction of the substrate.

Once the water is diverted into the new location segment of Dye Branch, filling of the old channel will commence. Approximately one quarter-acre of area will be graded to resemble that of a vernal pool. The unnamed, intermittent tributary will be routed into this depressional area to provide a hydrologic source. At the downstream limit of the depression, a small channel will be constructed to allow water to flow out of the depression in times of excessive rainfall and to prevent stagnation.

The final leg of main channel construction is below Cabarrus Street (Station 22+90 to Station 35+22). Due to very limited access and extremely unstable vertical banks, all equipment will have to enter the construction area from the lower limit of the project. Most of the channel work will occur with equipment in the channel. However, to minimize any potential negative impacts to the water quality and to minimize sedimentation, all flow will be pumped from the outlet of the culvert under Cabarrus Street to downstream of the construction limits. Large amounts of debris consisting of broken concrete, tires, and miscellaneous rubbish will be removed and hauled off site to a permitted landfill. Any excavated material from the segment of stream channel will be utilized to construct bankfull benches along the left bank (facing downstream).

The new Cemetery Branch channel will be constructed from Station 0+40 to the new Dye Branch channel while pumping all flow around the construction area. Bankfull benches will be constructed along areas with steep unstable banks. Every attempt will be made to utilize all excavated material on-site; however, due to limited filling of old channels some material may have to be hauled off-site. North Carolina State University will have constructed a diversion structure at the upstream limit of Cemetery Branch. This structure will not be disturbed during construction.

The final phase of the construction process will involve minor grading and sub-soiling of the site, removal and amelioration of temporary access roads, and removal of erosion and sedimentation control measures as the site is stabilized. The sub-soiling will be done to mitigate soil compaction of by heavy equipment and urbanization and to create micro-topographic features adjacent to the stream channel. Removal of temporary access roads and staging areas will start at the beginning of the project and proceed downstream. This will allow the removal of all temporary materials and the renovation of disturbed areas. Following the final grading activities, native trees and shrubs will be planted at the site during the dormant season.

6.0 Flood Analyses

Portions of the Dye Branch Site, including the channel of Dye Branch and its immediate floodplain are located within the Federal Emergency Management Association's (FEMA) 100year flood boundary, as depicted on Figure 10 (FEMA, 1980). These areas are inundated by the 100-year flood where Base Flood Elevations (BFE) have been determined, but no floodway. Section 60.3 (c)(10) of the National Flood Insurance Program (NFIP) regulations at 44 Code of Federal Regulations (CFR) states that a community shall "require until a regulatory floodway is designated, that no new construction, substantial improvements, or any other development (including fill) shall be permitted within Zones A1-30 and AE on the community's FIRM, unless it is demonstrated that the cumulative effect of the proposed development, when combined with all other existing and anticipated development, will not increase the water surface elevation of the base flood more than one foot at any point within the community". Although there are no regulatory floodways designated for any portion of the Dye Branch site, hydraulic models for both existing and proposed conditions were developed using FEMA's 100-year discharge. Using FEMA's discharge and the existing topography, a model was developed to analyze existing water surface elevations (WSEL) versus the mapped elevations. The existing conditions model shows WSEL higher than the FEMA model. Discrepancies in WSEL can be attributed to the original 1980 FEMA model having distinctly lower inverts than the surveyed inverts taken in early 2005. In order to ensure compliance with federal regulations, a set of design discharges were formulated and included in both the existing and proposed conditions models to determine if there was an increase or decrease in WSEL using the new survey data.

Design discharges were determined using the U.S. Army Corps of Engineers' Hydrologic Modeling System (HEC-HMS). HEC-HMS is a computer program designed to simulate the surface runoff response of a river basin to precipitation by representing the basin as an interconnected system of hydrologic components. In order for the model to predict the peak discharges, the following information must be known:

- Drainage Areas
- Rainfall Totals and Temporal Distribution
- Time of Concentration/Lag Times
- Soil Conservation Service (SCS) Curve Numbers
- Stream and Reservoir Routings

Limits of flooding were determined using HEC-RAS software from the US Army Corps of Engineers Hydrologic Engineering Center. Water surface profiles for the 2-year, 5-year, 10-

year, 25-year, 50-year, and 100-year storm events were computed. These models show that there is no increase in base flood elevation due to the restoration of Dye Branch, specifically; all of the studied cross sections showed a decrease in WSEL. Data from the 50-year and 100-year storm events is included in Table 4.

Table 4. Flood Analyses for the 50-Year and 100-Year Storm Events.

***		W
Dve	Branch	Profile: 50 vr

6. M.	OTT	Wate	er Surface Ele	vation
Station (proposed)	Q Total (cfs)	Existing (ft)	Proposed (ft)	Difference (ft)
0.68	850	803.37	802	-1.37
411.87	850	805.98	805.03	-0.95
776.83	850	808.28	807,9	-0.38
1073	850	811.82	810.95	-0.87
1284.09	.850	814.84	813.76	-1.08
1341.72	Culvert			
1383.64	700	822.46	822.44	-0,02
1461.36	700	822.49	822.45	-0.04
1833.18	700	822.55	822.5	40.05
2231.02	700	822.6	822,48	-0.12
2529.54	700	824.08	823,93	-0.15
2764.51	700	826.56	826.37	-0.19
2969.73	700	828.37	827.67	-0.70
3035.08	700	829.39	828	-1.39
3103.58	Culvert			
3161.46	700	832.01	831.87	-0.14
3235.01	700	831.99	831.87	-0.12
3628.84	700	833.24	832.52	-0.72
3759.36	700	833.74	833.1	-0.64

Station	Q	Water Surface Elevation			
(proposed)	Total (cfs)	Existing (ft)	Proposed (ft)	Difference (ft)	
0.68	1000	803.78	802.36	-1.42	
411.87	1000	806.41	805.4	-1.01	
776.83	1000	808.78	808.33	+0.45	
1073	1000	812.3	811.38	-0.92	
1284.09	1000	815.87	814.15	-1.72	
1341.72	Culvert				
1383.64	750	822.61	822.55	-0.06	
1461.36	750	822.64	822.56	-0.08	
1833.18	750	822.7	822.61	-0.09	
2231.02	750	822.76	822.6	-0.16	
2529.54	750	824.29	824.04	-0.25	
2764.51	750	826.66	826.51	-0.15	
2969.73	750	828.46	827.78	-0.68	
3035,08	750	829.52	828.11	-1.41	
3103.58	Culvert				
3161.46	750	832.11	831.95	-0.16	
3235,01	750	832.08	831.95	-0.13	
3628.84	750	833.4	832.65	-0.75	
3759.36	750	833.91	833.23	-0.68	

7.0 Typical Drawings

Seven different structure types made of natural materials will be utilized as part of the design sequence. These structures include single-arm rock vanes, j-hook rock vanes, cross vanes, rootwads, step pools, constructed riffles, and double log drop structures. Details for these structures can be found in Appendix K.

7.1 Single-Arm Rock Vane

These structures are designed to dissipate the secondary circulation cells which cause stress in the near bank region. They also force the thalweg away from the bank and towards the middle of the channel. These structures are placed on the outsides of meander bends. Footer rocks are placed on one side of the channel bottom for stability. More rocks are then placed at an angle to the stream bank, gradually inclining in elevation until they are located at the proposed bankfull elevation. At the point at which the structure reaches the bankfull elevation, rocks are placed perpendicular to the rock vane arm and embedded into the bank. These additional rocks provide a linkage to the existing stream bank as well as providing added protection during heavy flows.

7.2 J-Hook Rock Vanes

These structures are also designed to dissipate the secondary circulation cells which cause stress in the near bank region. They also force the thalweg away from the bank and towards the

middle of the channel. Similar in design to single-arm rock vanes, these structures are placed on the outsides of meander bends. Footer rocks are placed on one side of the channel bottom for stability. More rocks are then placed at an angle to the stream bank, gradually inclining in elevation until they are located above the bankfull surface directly adjacent to the stream bank. Additional rocks are placed in the channel to give the structure a "J" shape. These extra rocks are added to maintain the pool and provide additional fish habitat.

7.3 Cross Vanes

These structures serve to maintain the integrity and composition of the riffle while promoting scour along the center of the channel, away from the adjacent banks. The design shape is roughly that of the letter "U" with the apex situated on the upstream side in the riffle section. Footer rocks are placed in the channel bottom for stability. Rocks are then placed on the top of these footer rocks in the middle of the channel at approximately the same elevation as the designed stream bed. Rocks are then placed at an angle to the stream bank on either side of the channel. These rocks gradually incline to the bankfull elevation. Water flowing downstream is forced over these rocks towards the middle of the channel on either side of the structure, effectively scouring a pool immediately downstream. Cross vanes are used primarily for stabilization and grade control, but the structures also provide habitat for fisheries and other aquatic wildlife.

7.4 Root Wads

The objectives of these structures are to: provide in-stream and overhead cover for aquatic organisms, including fish; provide shade, detritus and terrestrial insect habitat; and provide minimal protection of the stream bank from erosion. Generally, a footer log and boulder are placed on the channel bottom and abut the stream bank along the outside of the meander bend. This provides support for the rootwad and stability (minimal) to the stream bank. A large tree rootwad (or root-ball) is then placed on the stream bank with additional boulders and rocks on either side for stability. Flowing water is deflected away from the bank and towards the center of the channel.

7.5 Step Pool Structures

Step pool structures are used primarily for grade control. They are implemented in cases involving significant slope changes, or drops, over short distances. Step pool structures are designed using a combination of small plunge pools in a stair-step fashion similar to a series of "nested" cross vanes. The construction implementation of these structures is similar with that of the cross vane, whereby footer rocks are placed in the channel bottom for stability. Rocks are then placed on the top, and slightly upstream of these footer rocks to create a series of stepped, alternating pools. Each pool is created by placing the header rocks in the middle of the channel at approximately the same elevation as the designed stream bed. Other header rocks are then placed at an angle to the stream bank on either side of the channe, with the rocks gradually inclining to the bankfull elevation. Water flowing downstream is forced over this system of steps and consequently alternates back and fourth across the centerline of the channel, effectively maintaing the scour pool at the bottom of each step. Like cross vanes, step pools also provide bank stabilization along both sides of the channel as well as habitat for fisheries and other aquatic wildlife.

7.6 Constructed Riffles

Constructed riffles provide an alternative mechanism for establishing grade control along the steeper sections of a channel. They are designed to house a thick laver of native bed material, and in some cases gravel or surge stone, installed in the bed at a riffle location. Generally, constructed riffles exhibit a boulder or log sill at both the upstream and downstream end location to serve as grade control. These sills are vertically keyed into the streambed using geotextile fabric overlain with the riffle bed material to prohibit scour and undermining. Rip rap toe protection is also installed along the horizontal length of each constructed riffle against the left and right edge-of-waters for further scour protection. Bedload and sediment transport capabilities are maintained throughout the reach resulting in a stable riffle section.

7.7 Double Log Drop Structures

These structures are used to create habitat diversity while providing grade control in a situation where the streambed has a relatively small drop over a relatively short distance. Double log drop structures are designed using a set of small plunge pools in a stepped fashion created by a pair of angled log weirs. Similar to step pools, footer rocks are placed in the channel bottom at the downstream end of the structure for stability. Rocks and rebar pins are used to secure the logs in place. The logs are installed to create a series of two stepped, alternating pools. A rootwad is generally installed in the streambank at the lower pool to help deflect the stream flow to the middle of the channel. Water flowing downstream is forced over a pair of small steps while alternating back and fourth across the centerline of the channel, effectively maintaing scour pools at the bottom of each step. Native hardwood trees are used for the logs and rootwads for this structure. Geotextile fabric is used to vertically key the logs into the streambed. Double log drop structures are another design concept used to provide habitat for fisheries and other aquatic wildlife while serving ultimately as grade control.

8.0 Stream Riparian Planting Plan

The planting plan for the riparian and upland buffers of the Dye Branch site will provide post-construction erosion control and riparian habitat enhancement. The planting plan will also attempt to blend existing vegetative communities into recently restored areas. Plantings in the buffer areas will include native species appropriate for the Piedmont physiographic province and the project site. Plants within the floodplain will be flood tolerant species, which can accommodate periodic flooding events throughout the year. A variety of trees and shrubs will be planted to provide cover and habitat for wildlife as well as soil stabilization.

Tree and shrub species will be planted in specific planting zones. These planting zones will accommodate plant species which have specific requirements for growth. Hydrology and topography are main factors that dictate a plant's ability to survive and to thrive following planting. These planting zones will be created around these requirements and will include the following zones: Zone 1 (Stream Banks), Zone 2 (Riparian Buffer), Zone 3 (Wetlands), and Zone 4 (Upland Buffers). A list of species in each Zone can be found in Table 5.

Table 5. Recommended Plant Species and Planting Zones.

Planting	Zone	Recommended	Plant Species A
Zone	Description	Scientific Name	Common Name
1	Stream Banks	Alnus serrulata Betula nigra Cephalanthus occidentalis Cornus amonum Hibiscus mosheutos Lindera benzoin Salix nigra Salix sericea Sambucus canadensis	Tag alder River birch Buttonbush Silky dogwood Marsh mallow Spicebush Black willow Silky willow Elderberry
2	Riparian Buffer	Betula nigra Fraxinus pennsylvanica Lindera benzoin Plantanus occidentalis Quercus nigra Quercus phellos Sambucus canadensis	River birch Green ash Spicebush Sycamore Water oak Willow oak Elderberry
3	Wetlands	Alnus serrulata Cephalanthus occidentalis Cornus amomum Fraxinus pennsylvanica Hibiscus mosheutos Salix nigra Salix sericea	Tag alder Buttonbush Silky dogwood Green ash Marsh mallow Black willow Silky willow
4	Vernal Pools	Boehmeria cylindrica Carex lurida Carex intumescens Cyperus strigosus Eleocharis obtusa Eupatorium fistulosum Juncus coriaceus Juncus effuses Saururus cernuus	False nertle Lurid sedge Bladder sedge Umbrella sedge Blunt spike-rush Joe-pye weed Leathery rush Soft rush Lizard's tail
5	Upland Buffer	Carya tomentosa Cornus florida Diospryos virginiana Ilex opaca Juniperus virginiana Pinus echinata Pinus strobus Pinus virginiana Prunus serotina Quercus alba Quercus falcata	Mockernut hickory Flowering dogwood Persimmon American holly Eastern red cedar Shortleaf pine White pine Virginia pine Black cherry White oak Southern red oak

A List is alphabetized by scientific name within each planting zone.

Shrubs and trees with extensive, deep rooting systems will assist in stabilizing the banks in the long term. Native grasses, transplants, and live stakes will be utilized at the site for immediate stabilization as well as erosion control matting along the newly created stream banks. Vegetation will be planted in a random fashion in an effort to mimic natural plant communities. Colonization of local herbaceous vegetation will inevitably occur, which will provide additional soil stability. Tree species will be planted as bare root stock on random eight-foot centers at a

frequency of 680 stems per acre. Shrub species will be dispersed among these tree species also on random eight-foot centers. Larger plant stock will be established in areas immediately adjacent to channel structures. These areas will also receive much denser plantings in order to expedite the stabilization of the soil through greater rooting mass. Planting stock will be culled to remove inferior specimens, so only healthy, viable stock will be planted at the project site. Planting of species will utilize dormant plant stock and will be performed to the extent practicable between December 1st and March 15th.

8.1 Invasive Species Management

Invasive species control at the project site will be focused on effectively eliminating kudzu (Pueraria lobata) and Chinese privet (Ligustrum sinense) from the riparian areas along Dye Branch and Cemetery Branch. Eliminating these invasive species will provide long-term benefits for existing plant species and those that will be established. Controlling these species will likely involve both mechanical and chemical control mechanisms. The Town of Mooresville will oversee and maintain the invasive species aspect.

Kudzu is predominantly found along the portion of Dye Branch between Center Avenue and McLelland Avenue. This particular area accounts for approximately 4 acres of kudzu infestation. The remaining portion of the kudzu is found along the forested area adjacent to Cemetery Branch. Chinese privet is most prevalent along the lower reach of Dye Branch, below Cabarrus Avenue.

Kudzu can be controlled by utilizing chemical applications of clopyralid herbicide during its most active periods of growth, which usually occur during the months of June and July. The most effective period to apply clopyralid herbicide is just prior to or during its blooming period. Application rates range from two thirds to one and one third pints per acre.

Chinese privet is generally difficult to control due its growth habit and waxy leaf surface. Initially, mechanical control of this species is the best method. Mechanical control will significantly reduce the plant's stature, whereby stimulating a cluster of young growth, which provide an easier, more effective herbicide application. Mechanical control of this species should be done in early spring or late fall. Applications of 4 to 6 pints per acre of imazapyr herbicide during the active growing season will provide effective control of Chinese privet.

9.0 Stormwater Wetland

In an effort to improve water quality at the project site, North Carolina State University (NCSU) was contracted to construct stormwater treatment wetlands. These wetlands will be situated immediately south of Cemetery Branch and just west of Dye Branch, in what currently is a mowed and maintained field. A diversion structure containing a weir, will be located immediately downstream of the Church Street culvert. It will control the stormwater entering the wetlands at a rate up to 8 cubic feet per second. Once the weir reaches it capacity the water will overflow into Cemetery Branch. This will only remove a very small amount of flow equivalent to the first inch (1") of rainfall; therefore, the bankfull peak discharge of Cemetery Branch will not be affected. Downstream of the diversion structure, an energy dissipater is proposed to lower velocities out the the weir. This dissipater is designed to accommodate the entire 10-year peak flow as the flow to the stormwater wetland system may periodically be shut off for maintenance.

The water that enters the wetlands will be filtered through three "wetland cells" connected by conveyance pipe. Once the water is filtered through the cells it will flow into a small v-ditch and be directed into Dye Branch. This process will have no affect on the bankfull discharge of Dye Branch due to the peak discharge from the wetland being small relative to that of Dye Branch.

10.0 Stream Monitoring Plan

Monitoring will determine the degree of success the mitigation project has achieved in meeting the objectives of providing proper channel functions and increased habitat quality. This monitoring data will provide the EEP and resource agencies with evidence that the goals of the Dye Branch project have been met. Monitoring of the site will include an assessment of geomorphology and riparian vegetation at least once each year for a total of five years adhering to the USACE Stream Mitigation Guidelines. Monitoring reports will be submitted annually to the EEP by December of each year. The monitoring reports will follow the most current EEP Monitoring Report Template and include detailed analysis of the new stream and floodplain, plant survivability, photos, and photo location points as well as a description of any problems and recommendations for remedial measures. Photo point locations are shown on Figure 4 and pre-construction photos of these areas can be found in Appendix A. In the event that success criteria are not met, remedial measures will be installed to achieve success, as directed by the EEP.

Upon completion of the project, an as-built channel survey will be conducted. The survey will document the dimension, pattern, and profile of the restored channel. Permanent cross sections will be established at an approximate frequency determined by the EEP. The locations will be selected to represent approximately 50% riffle and 50% pool areas. The as-built survey will include photo documentation at all cross sections, a plan view diagram, a longitudinal profile, vegetation information and pebble counts. The as-built plan will serve as a reference for demonstrating and quantifying the magnitude and frequency of problem events.

10.1 Stream Channel Assessment

During the first-year Mulkey will evaluate the restored portion of Dye Branch and Cemetery Branch in regard to overall channel stability. Since streams are considered as "active" or "dynamic" systems, restoration is achieved by allowing the channel to develop a stable dimension, pattern, and profile such that, over time, the stream features (riffle, run, pool, and glide) are maintained and the channel does not aggrade or degrade. Minor morphologic adjustments from the design stream are anticipated based on the correlation of reference reach data, excessive sediment deposition from upstream sources, and on-going changes in land use within the watershed in addition to the effects of extraordinary meteorological events.

10.2 Vegetation Success

Vegetation requirements state that 260 stems/acre must be viable for success after the five year monitoring period. Should the performance criteria outlined above not be met during the monitoring period, Mulkey will provide the EEP with a remediation proposal, detailing corrective actions and/or maintenance actions proposed, and an implementation schedule. Upon review and approval/modification of proposed corrective measures by the EEP and the

regulatory agencies, Mulkey will oversee the implementation of the necessary corrective measures.

10.3 Monitoring Data

Monitoring data for each monitoring year will consist of the following:

 Stream Channel Assessment Channel stability

2. Vegetation Data

Number of stems/acre of woody species
Percent of survival of planted woody species
Species composition, including non-dominants
Quantitative measure of noxious species
Overall condition of the planted species
Photo reference locations of each plot

10.4 Reporting

The first-year monitoring reports will be submitted to the EEP's designated representative for coordination with the appropriate regulatory agencies on an annual basis. The first-year of monitoring will have two submittals, one being the As-Built drawings and the second being the First Year Annual Monitoring Report, which will follow the most current EEP Monitoring Template. It is understood that the EEP will coordinate any necessary monitoring report submittals with the regulatory agencies. If monitoring reports indicate any deficiencies in achieving the success criteria on schedule, a remedial action plan will be included in the annual monitoring reports. Mulkey will be available to coordinate any agency site visits, both before and after restoration activities have been completed. Vegetative monitoring will be conducted during the summer months of each monitoring year.

10.5 Exotic/Invasive Species

Invasive species will be identified and controlled so that none become dominant species or alter the desired community structure of the site. Specific areas have already been identified to contain invasive plants. Invasive species within these areas will be controlled using the most appropriate means that is suitable to EEP.

11.0 Stream Performance Criteria

Based on the Classification Key for Natural Rivers (Rosgen, 1996), restoration activities will ultimately result in the classification of a C-stream type for Dye Branch and a B-stream type for Cemetery Branch. The C-stream types are slightly entrenched, meandering, gravel dominated, riffle-pool channels with well developed floodplains. Pool to pool spacing for this stream type averages five-to-seven bankfull channel widths in length. The stream banks are generally composed of sand and gravel material, with stream beds exhibiting little difference in pavement and sub-pavement material composition. Rates of lateral migration are influenced by the presence and condition of riparian vegetation. The C-stream type, is best characterized by the presence of point bats and other depositional features, it is very susceptible to shifts in both lateral and vertical stability caused by direct channel disturbance and changes in the flow and sediment regimes of the contributing watershed. As a result, stream success criteria will be

based on overall stability. It is expected that channel adjustment will occur throughout the restored reaches; however, excessive adjustment and potential stream instability will be judged to be occurring if the width/depth ratio is measured to be greater than 18, the bank height ratio is greater than 1.4; radius of curvature ratio is less than 1.5, or the development of head cuts occur. These limits are established based on reference reach data for C stream types in North Carolina.

The B-stream types are moderately entrenched, have a lower sinuosity and less developed floodplain than the C-stream type and are usually confined to narrow valleys. The B-stream type exhibits a width/depth ratio greater than 12 and a pool to pool spacing between four-and-five bankfull widths in length. Both streambank erosion rates and aggradation/degradation processes are usually low. The bed morphology is dominated by "rapids", produced from debris constriction and a confining valley.

12.0 References

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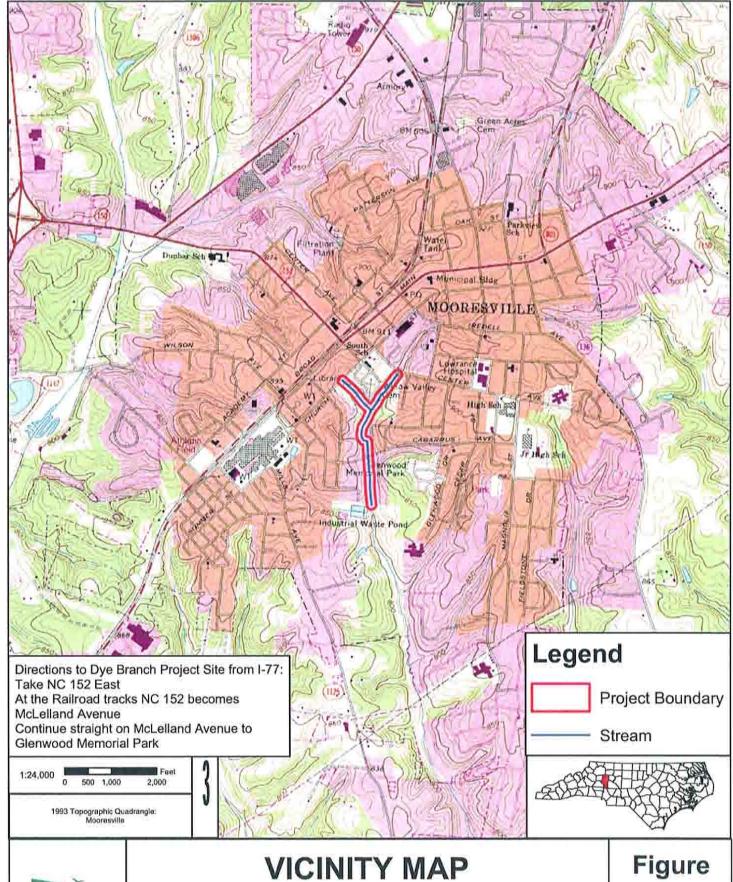
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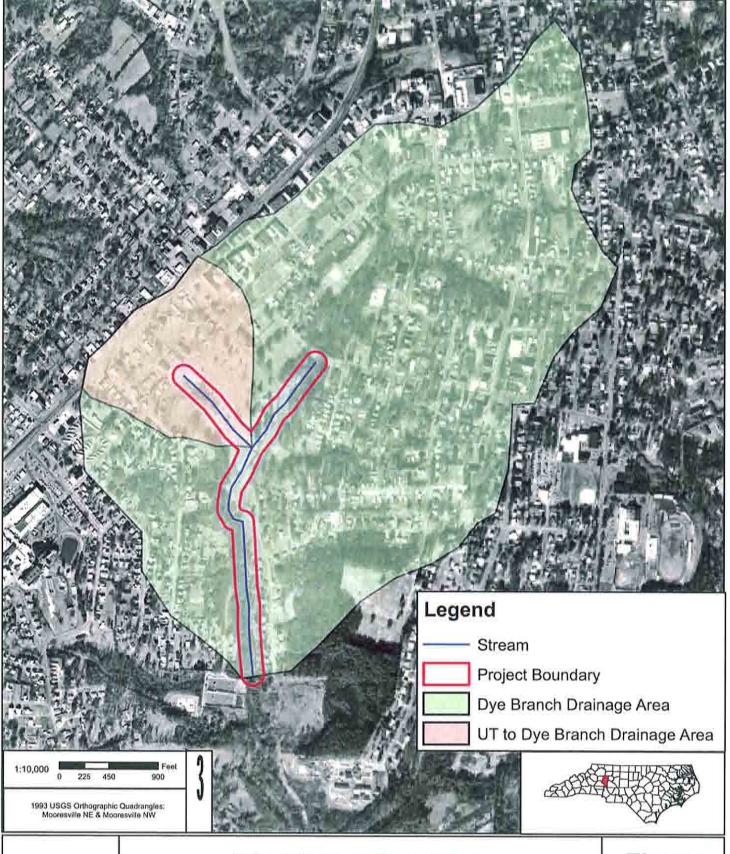
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DYE BRANCH STREAM RESTORATION IREDELL COUNTY, NORTH CAROLINA



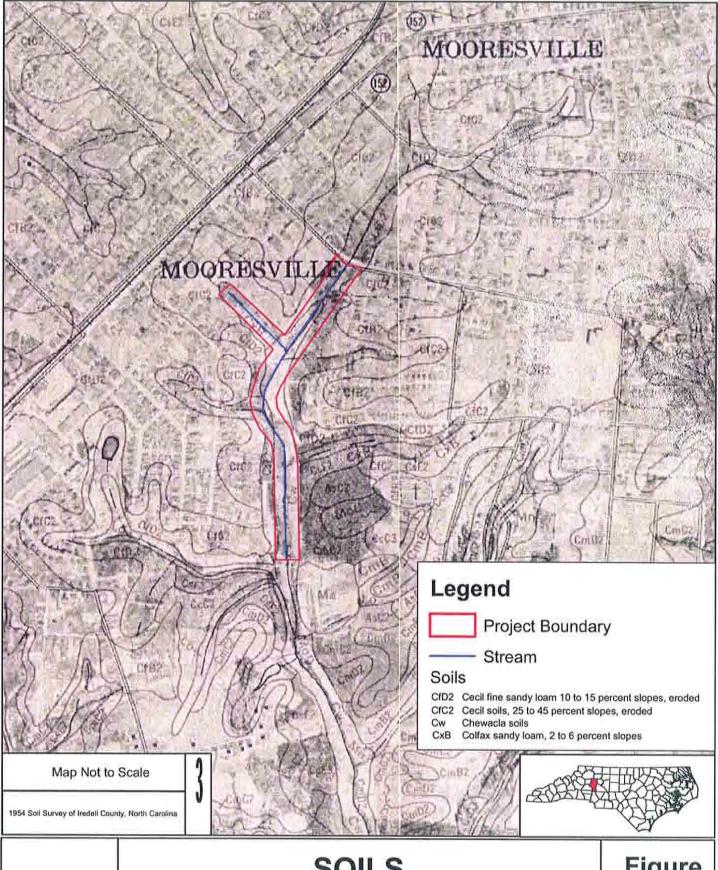


DRAINAGE AREA

DYE BRANCH STREAM RESTORATION IREDELL COUNTY, NORTH CAROLINA

Figure

2

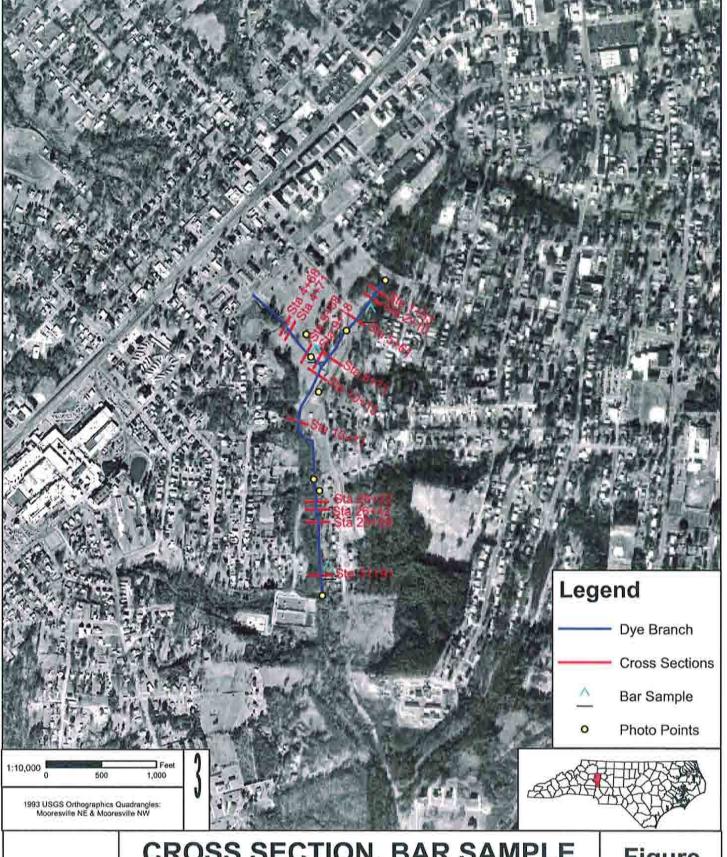




SOILS

DYE BRANCH STREAM RESTORATION IREDELL COUNTY, NORTH CAROLINA

Figure



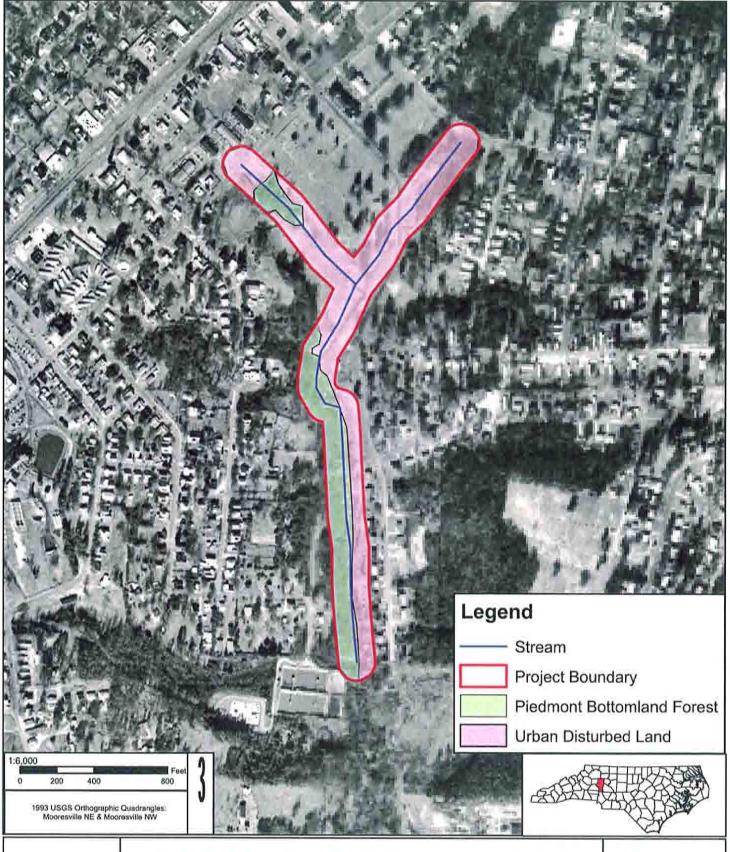


CROSS SECTION, BAR SAMPLE AND PHOTO POINT LOCATIONS

DYE BRANCH STREAM RESTORATION IREDELL COUNTY, NORTH CAROLINA

Figure

4



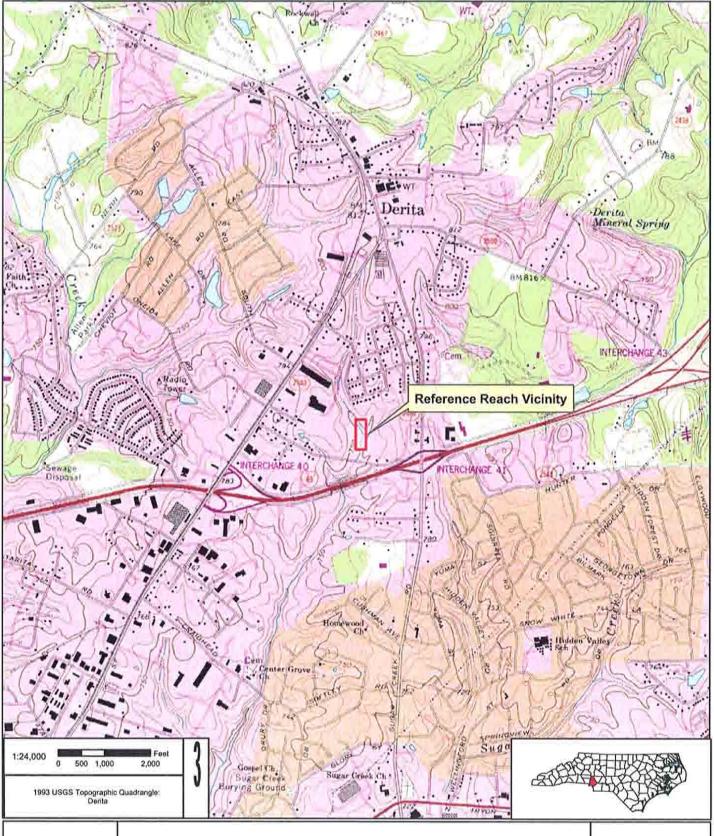


VEGETATIVE COMMUNITIES

DYE BRANCH STREAM RESTORATION IREDELL COUNTY, NORTH CAROLINA

Figure

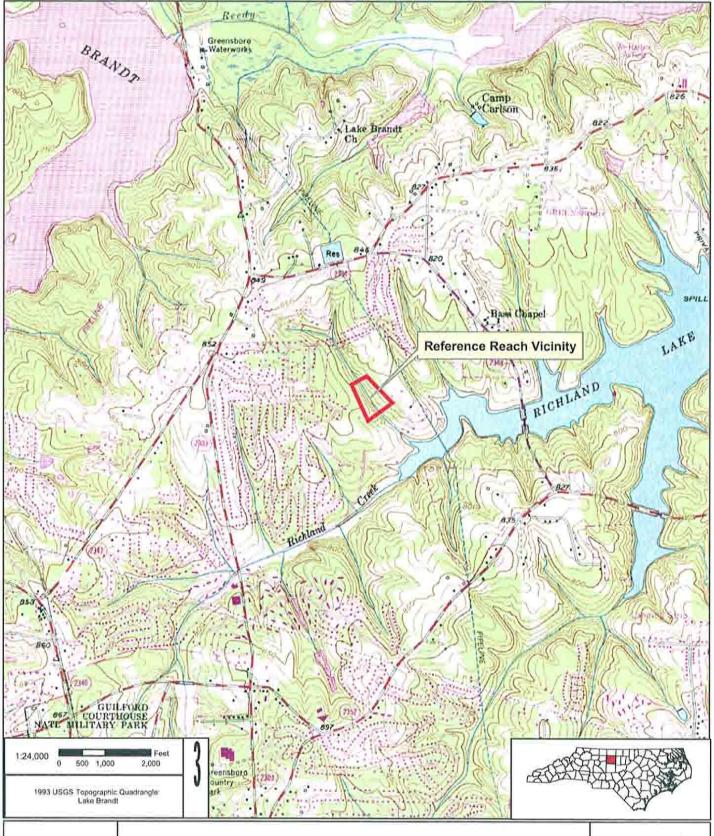
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DERITA BRANCH
MECHLENBURG COUNTY, NORTH CAROLINA

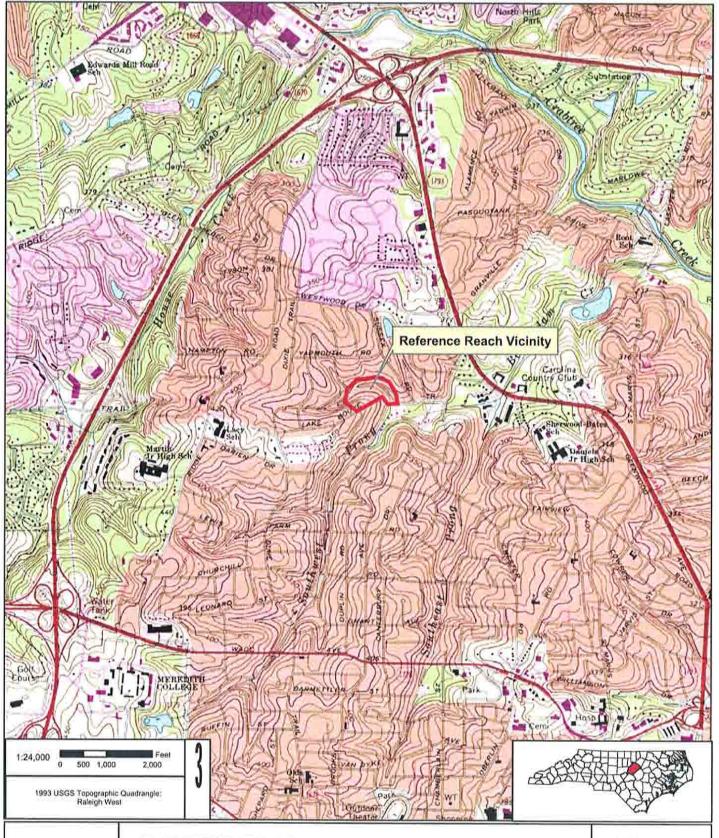
Figure





UT TO LAKE JEANETTE
GUILFORD COUNTY, NORTH CAROLINA

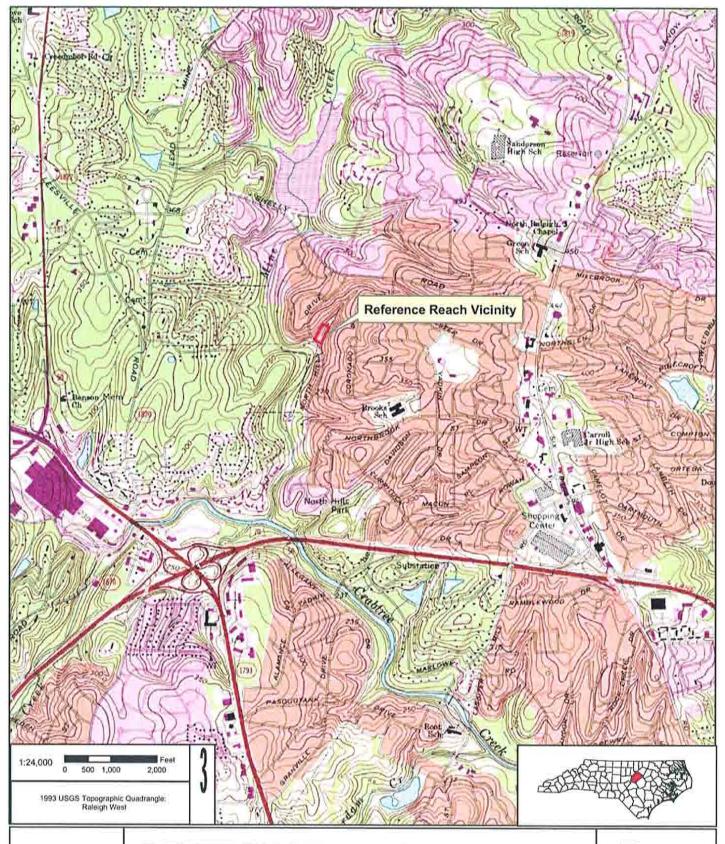
Figure





UT TO SW PRONG BEAVERDAM CREEK WAKE COUNTY, NORTH CAROLINA

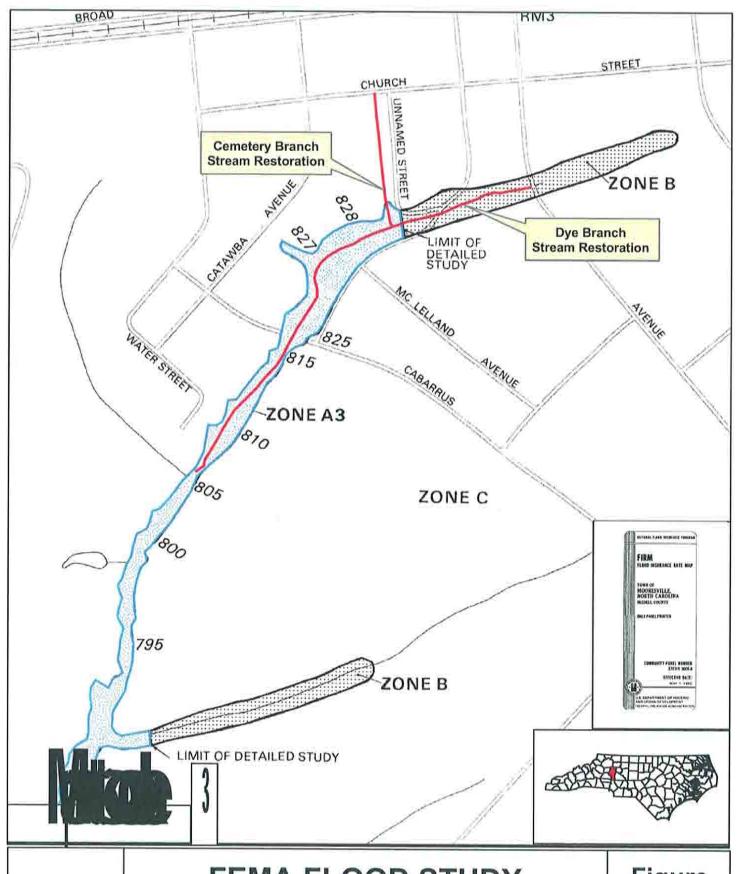
Figure





UT TO MINE CREEK
WAKE COUNTY, NORTH CAROLINA

Figure

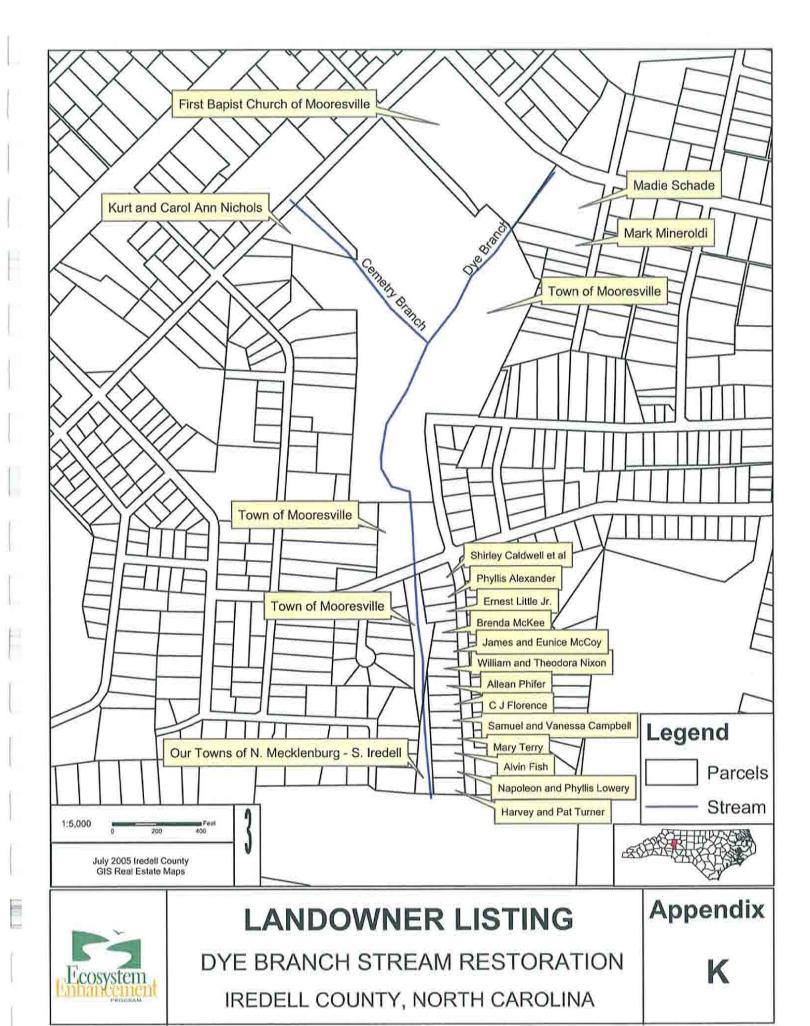


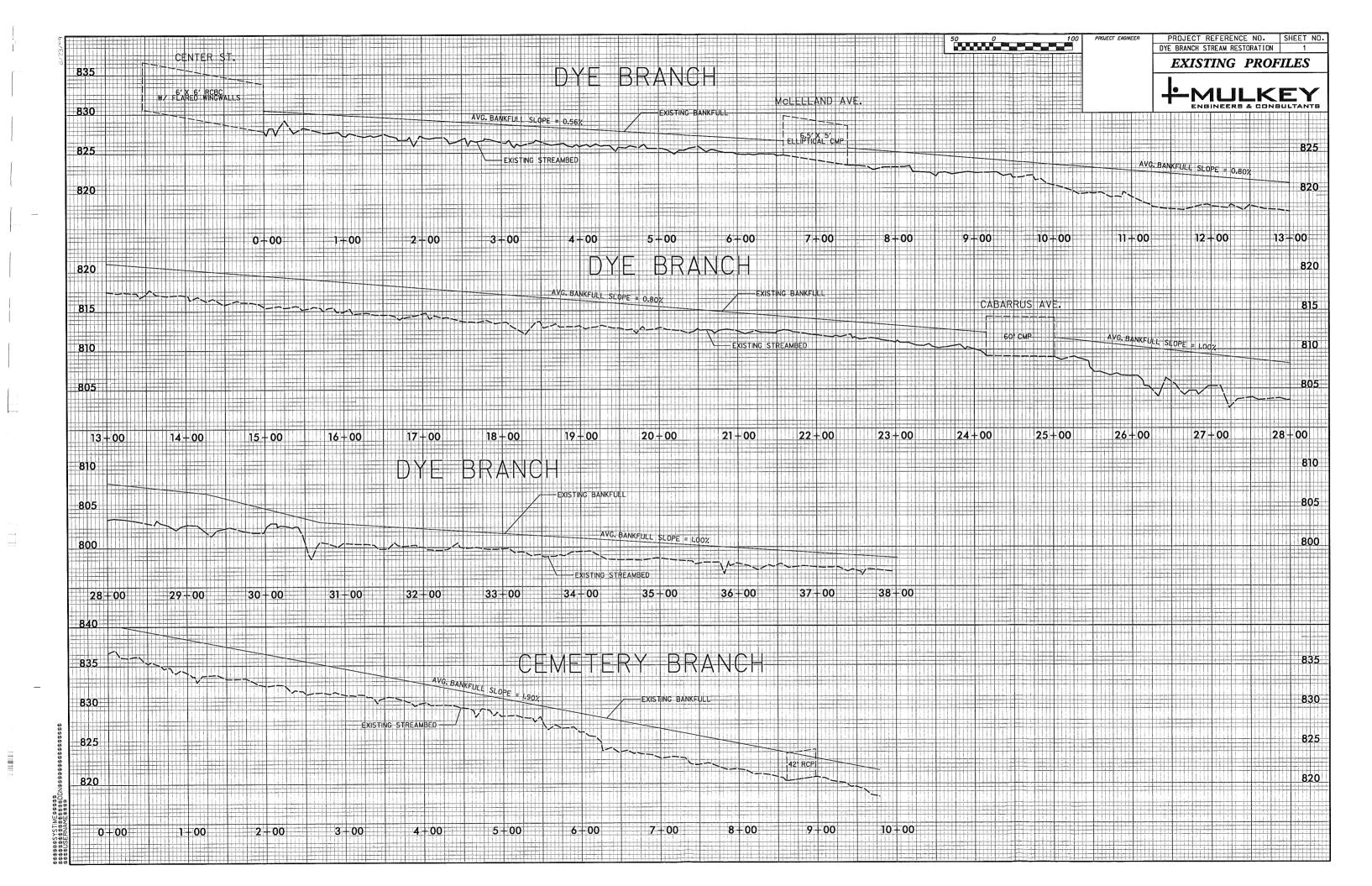


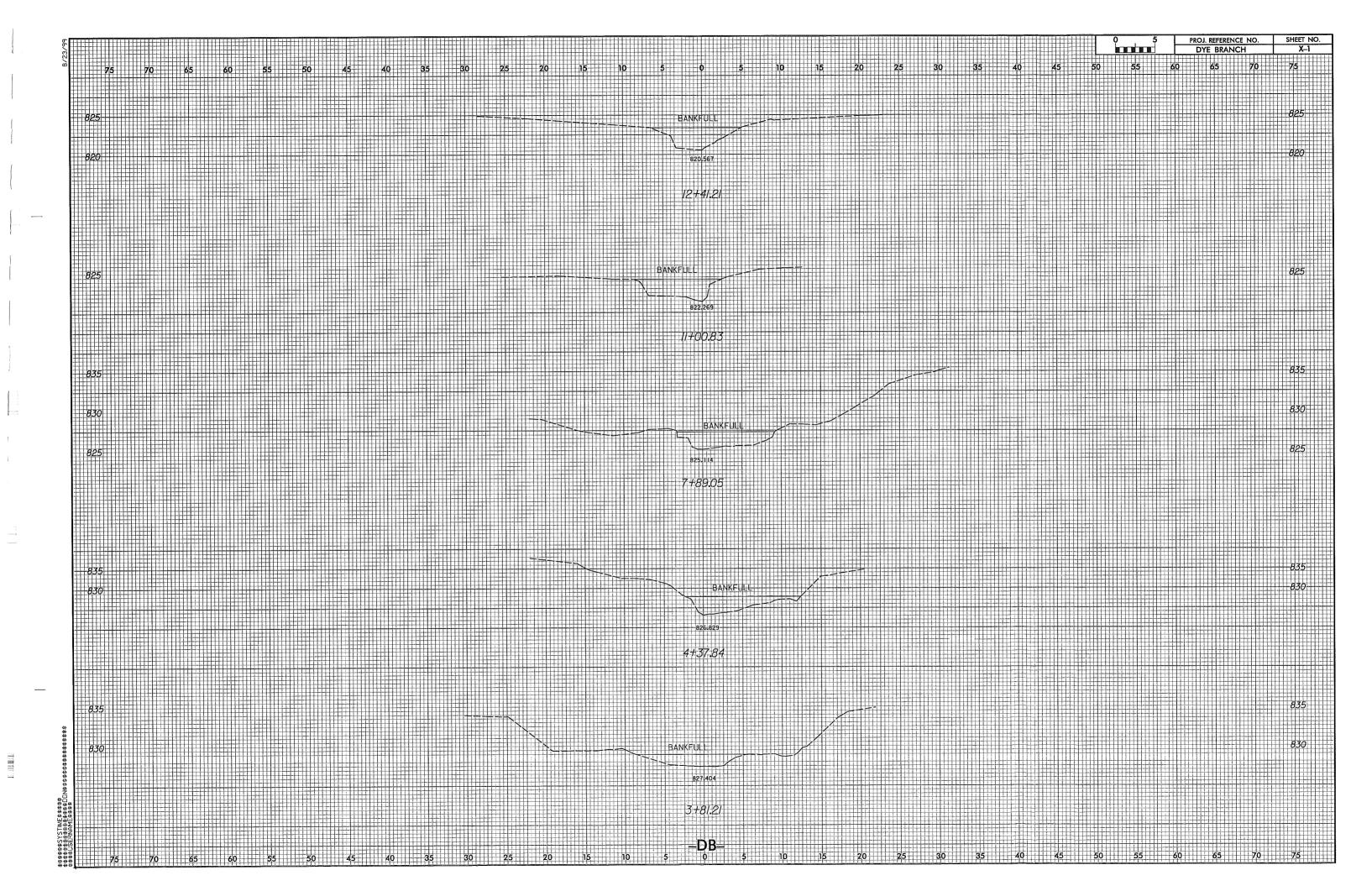
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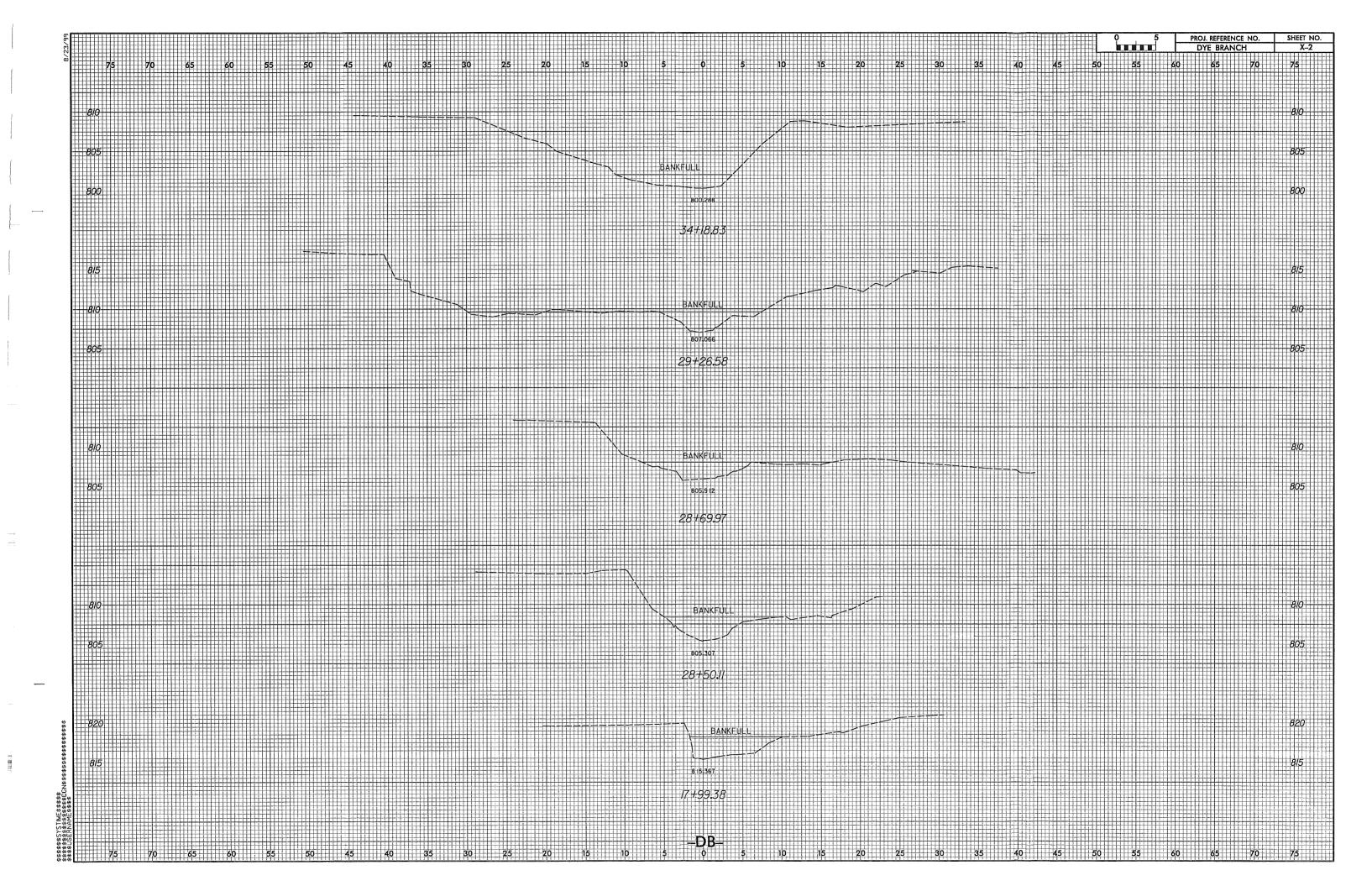
DYE BRANCH STREAM RESTORATION IREDELL COUNTY, NORTH CAROLINA

Figure









Cemetery Branch

Restoration Site: USGS Gage Station: Reference Reach:

Derita Branch, UT to Lake Jeanette, UT to SW Prong Benverdam Mulkey 5/27/2005

Surveyors: Date: Weather:

/ariables		Existing Channel		Proposed Reach		Reference Reach Derita Branch	Reference Reach UT to Lake Jeanette	Reference Reach UT SW Prong Byd
. Stream Type		Unstable E4		C4	_	E4	C4	C5
. Drainage Area (sq. mi)		0.06		0.06		0.250	0.25	0.28
Bankfull Width (Wbkf) ft	Mean:	6.98	Mean:	10.0	Mean:	11.25	9.50	11.77
C ASSESSMENT MANAGEMENT OF CONTRACT OF CON	Minimum:	10100	Minimum:	1,9659	Minimum:	11160	8.90	9.90
	Maximum:		Maximum:		Maximum:		12.10	14.10
Bankfull Mean Depth (dbkf) ft	Mean:	0.97	Mean:	0.7	Mean:	1.63	0.80	0.80
. Dankion Mean Depar (doki) ii	Minimum:	U.57	Minimum:	9.6		1.03		
					Minimum:		0.70	0.70
TO ALSO IN SECURITION OF THE SECOND OF THE S	Maximum:	475	Maximum:		Maximum:		0.80	1.00
. Width/Depth Ratio (Wbkf/dbkf)	Mean;	7,19	Mean:	14.3	Mean:	6.89	11.70	14.97
	Minimum:		Minimum:		Minimum:			
	Maximum:		Maximum:		Maximum:			
Bankfull Cross-Sectional Area (Abkf) sq ft	Mean:	6.76	Mean:	7.0	Mean:	18.35	7.70	9.38
	Minimum:		Minimum:		Minimum:		6.80	7.80
	Maximum:		Maximum:		Maximum:		8.40	10.50
. Bankfull Mean Velocity (Vbkf) fps	Mean:	7.2	Mean:	6.2	Mean:	5.86	4.55	4.80
	Minimum:	6.6	Minimum:	5.5	Minimum:	5.27		4.10
	Maximum:	7.8	Maximum:	6.7	Maximum:	6.98		5.20
Bankfull Discharge (Obkf) cfs	Mean:	49.0	Mean:	43.1	Mean:	107,4	35	45
	Minimum:	44.3	Minimum:	38.4	Minimum:	96.7		38.00
	Maximum:	52.8	Maximum;	46.6	Maximum:	128.1		46.00
. Maximum Bankfull Depth (dmax) It	Mean:	1,52	Mean:	1.1	Mean:	2.4	1,30	1.28
Control of the Contro	Minimum:	1000	Minimum:	0.8	Minimum:	70	1.20	1.00
	Maximum:		Maximum:	1.6	Maximum:		1.30	1.70
0. Ratio of Low Bank Height to Maximum	Mean:	1,49	Mean:	1.0	Mean:	1.2	1,00	1.00
Bankfull Depth (lbh/dmax)	Minimum:	1,40		1.00		106	1,00	1:00
Denistan Dapin (tolvennix)	Maximum:		Minimum:		Minimum:			
1 Width of Flood Prope War All Calls		11.0	Maximum:	00.0	Maximum:	400.0	05.00	60.00
Width of Flood Prone Area (Wfpa) It	Mean;	14.2	Mean:	28.0	Mean:	100.0	25.00	90.00
	Minimum:		Minimum:		Minimum:		19.00	
THE RESERVE THE PROPERTY OF THE PERSON OF TH	Maximum:		Maximum:		Maximum:		36.00	
2. Entrenchment Ratio (W/pa/Wokl)	Mean:	2.0	Mean:	2.8	Mean:	8.9	3.80	7.65
	Minimum:	0.0	Minimum:		Minimum:			
	Maximum:	0.0	Maximum:		Maximum:			
3. Meander Length (Lm) It	Mean:	42.0	Mean:	55.2	Mean:	79.0	50.2	71.0
Contract Contract Contract Contract	Minimum:	13.6	Minimum:	46.0	Minimum:	29.0	26.0	33.0
	Maximum:	71.0	Maximum:	64.4	Maximum:	155.0	69.0	144.0
4. Ratio of Meander Length to Bankfull Width	Mean:	6.0	Mean:	6.0	Mean:	7.0	5.28	6.03
(Lm/Wbkf)	Minimum:	2.0	Minimum:	4.6	Minimum:	2.6	2.92	2.80
(City Hotel)	Maximum:	10.2						
5. Radius of Curvature (Rc) It			Maximum:	6.4	Maximum:	13.8	5.70	12.24
5. Hadius of Corvature (HC) If	Mean;	19.6	Mean:	27.6	Mean:	36.8	9.70	18.00
	Minimum:	3.9	Minimum:	18.4	Minimum:	25.5	5.00	11.10
	Maximum:	37.0	Maximum:	36.8	Maximum:	48.0	22.00	38.00
Ratio of Radius of Curvature to Bankfull	Mean:	2,8	Mean:	2.8	Mean;	3.3	1.02	1,53
Width (Rc/Wbkf)	Minimum:	0.6	Minimum	1.8	Minimum:	2.3	0.56	0.94
	Maximum:	5.3	Maximum:	3.7	Maximum:	4.3	1.82	3.23
7. Belt Width (Wblt) ft	Mean:	10.8	Mean	32.2	Mean:	41.0	33	71
	Minimum:	5.3	Minimum:	23.0	Minimum:	28.3	26	30
	Maximum:	22.6	Maximum:	41.4	Maximum:	53.7	40	119
Meander Width Ratio (Wbit/Wbkf)	Mean	1.5	Mean:	3.2	Mean:	3.6	3.47	6.03
12. ACCUPATION OF THE PROPERTY	Minimum	0.8	Minimum:	2.3	Minimum:	2.5	267.0	2.55
	Maximum:	3.2	Maximum:	4,1	Maximum:	4.8		10.11
1. Sinuosity (Stream length/valley distance)	Mean:	1.14	Mean:	1.14	Mean:	1.15	1.39	2.22
(K)	Minimum		Minimum		Minimum:	1119	100	-
ACM	Maximum:		Maximum:		Maximum:			
2. Valley Slope (ft/ft)	Moan:	0.0217	Mean:	0.0217	Mean:	0.0077	0.0076	0.0300
E. Yalley Stope (lett)	Minimum:	0.0217	Minimum	0.0217		0.0077	0.0076	0.0300
					Minimum:			
2 Average Mater Profess Class	Maximum:	0.0100	Maximum:	0.0400	Maximum:	0.0007	2.4454	0.0430
3. Average Water Surface Slope	Mean:	0.0190	Mean:	0.0190	Mean:	0.0067	0.0057	0.0130
for Reach (Savg)	Minimum:		Minimum:		Minimum:			
	Maximum:		Maximum:	MHI WAAAAA	Maximum:	17,400,000		
Pool Slope (Spool) ft/ft	Mean	0.0110	Mean:	0.0019	Mean:	0.0000	0.0005	0.0011
	Minimum:	0.0010	Minimum:	0.0000	Minimum:	0.0000	10 may 1/2 m 2 m 2 m 2 m 2 m 2 m 2 m 2 m 2 m 2 m	0.0000
	Maximum:	0.0280	Maximum:	0.0038	Maximum:	0.0000		0.0030
5. Ratio of Pool Slope to Average Slope	Mean:	0.579	Mean:	0.100	Mean:	0.000	0.08	0.08
(Spool/Savg)	Minimum:	0.053	Minimum:	0.000	Minimum:	0.000		0.00
U. J. O. J. C. L.	Maximum:	1.474	Maximum:	0.200	Maximum:	0.000		0.23
Maximum Pool Depth (dpool) ft	Mean	2.6	Mean	2.0	Mean:	3.2	2.90	2.40
V. MORANISM I STARTARDA MARISM II	Minimum:	(7)E)	Minimum:	700	Minimum:	170.50	2.40	1.80
	Maximum:		Maximum		Maximum:		2.90	2.90
7. Ratio of Maximum Pool Depth to Bankfull	Mean:	2.7	Mean;	2.9	Mean:	2.0		3.00
				2.0		2.0	3.63	
Mean Depth (dpool/dbkf)	Minimum:	0.0	Minimum:		Minimum:	0.0		2.25
	Maximum:	0.0	Maximum:	- Suita	Maximum:	0.0		3.63
S. Pool Width (Wpool) ft	Mean:	13.1	Mean	14.0	Mean:	15.6	10.70	9.90
	Minimum:		Minimum:		Minimum:	1125487.8	8.00	9.10
	Maximum:		Maximum		Maximum:		20.70	10.50
9, Ratio of Pool Width to Bankfull Width	Mean	1.9	Mean:	1.4	Mean:	7.4	1.13	0.84
(Wpool/Wbkl)	Minimum:	0,0	Minimum:	(*/677)	Minimum:	0.0	11-130	0.77
4 - F	Transmitter and the same	×14	Maximum:		Maximum:	0.0		0.89

Cemetery Branch

Restoration Site: USGS Gage Station: Reference Reach: Surveyors: Date: Weather:

Derita Branch, UT to Lake Jeanette, UT to SW Prong Beaverdam Mulkey 5/27/2005

PETER		Emission Character		Branch and Branch	_	Reference Reach Derita Branch	Reference Reach	Reference Reach
Variables		Existing Channel		Proposed Reach			UT to Lake Jeanette	UT SW Prong Bydn
30. Bankfull Cross-sectional Area at Pool	Mean:	14.7	Mean:	10.3	Mean:	29.8	10.75	13.50
(Apool) sq It	Minimum		Minimum:		Minimum.		9.90	11.40
	Maximum:		Maximum:		Maximum:	2000	11.60	16.00
Hatio of Pool Area to Bankfull Area	Mean:	2.2	Mean:	1.5	Mean:	1.6	1.40	1.44
(Apool/Abkf)	Minimum:	0.0	Minimum:		Minimum:	2400		13.000
	Maximum:	0.0	Maximum:		Maximum:			
32. Pool to Pool Spacing (p-p) ft	Mean:	86.0	Moan:	27.6	Mean:	140.8	40.20	36.50
	Minimum	22.8	Minimum:	18.4	Minimum.		20.7	.18
	Maximum:	228.2	Maximum:	32.2	Maximum:		54.80	58.00
33. Ratio of Pool-to-Pool Spacing to Bankfull	Mean:	12.3	Mean:	2.8	Mean:	12.5	4.23	3.10
Width (p-p/Wbkf)	Minimum:	3.3	Minimum:	1.8	Minimum:	0.0	2.2	1.53
The second secon	Maximum:	32.7	Maximum:	3.2	Maximum:	0.0	5.80	4.93
34. Pool Length (Lp) It	Mean:	8.2	Mean:	20.7	Mean:	24.0	N/A	10.50
	Minimum	4.7	Minimum:	13.8	Minimum:	15.1		3.5
	Maximum:	11.9	Maximum:	27.6	Maximum:	32.8		30.00
5. Ratio of Pool Length to Bankfull Width	Mean:	1.2	Mean:	2.1	Mean:	2.1	N/A	0.89
(Lp/Wbkf)	Minimum:	0.7	Minimum:	1.4	Minimum:	1.3		0.30
	Maximum:	1.7	Maximum:	2.8	Maximum:	2.9		2.55
66. Riffle Slope (Sriff) ft/ft	Mean:	0.0340	Mean:	0.0475	Mean:	0.0160	N/A	0.04
on a more entered a construction of	Minimum:	0.0120	Minimum:	1919,110	Minimum:	0.0064	F.8355%	0.022
	Maximum:	0.0880	Maximum:		Maximum:	0.0290		0.05
7. Ratio of Riffle Slope to Average Slope	Mean:	1,789	Mean:	2.5	Mean:	2.4	N/A	2.69
(Sriff/Savg)	Minimum:	0.632	Minimum:	500	Minimum:	1.0	130	1.69
formonal	Maximum:	4.632	Maximum:		Maximum:	4.3		4.00
88. Maximum Riffle Depth (driff) It	Mean:	1.5	Mean:	1.1	Mean:	2.40	1.30	1,30
, waxiiigii riiiio capii (diii) ii	Minimum:	1.0	Minimum:	10.1	Minimum:	6.40	1.2	1.50
	Maximum:		Maximum:		Maximum:		1.30	1.70
39. Ratio of Maximum Riffle Depth to Bankfull	Mean:	1,6	Mean:	1.6	Mean:	1.5	1.63	1.63
		0.0		1.0	Minimum.	0.0		1.25
Mean Depth (driff/dbkf)	Minimum: Maximum:	0.0	Minimum:		Maximum:	0.0	1.71	2.13
6 6 6 76 78			Maximum:	0.0150				
0. Run Slope (Srun) IVII	Mean:	0.0080	Mean:	0.0150	Mean:	0.0071	N/A	0.01
	Minimum:	0.0000	Minimum:	0.0050	Minimum:	0.0018		0.003
	Maximum:	0.0320	Maximum:	0.0250	Maximum:	0.0114		0.02
Ratio of Run Slope to Average Slope	Mean:	0.421	Mean:	0.789	Mean:	1.054	N/A	0.69
(Srun/Savg)	Minimum	0.000	Minimum:	0.263	Minimum:	0.275		0.23
	Maximum:	1.684	Maximum:	1,316	Maximum:	1.703		1.31
2. Maximum Run Depth (drun) ff	Mean:	2.2	Mean:	1.4	Mean:	2.7	N/A	1.60
	Minimum:		Minimum:		Minimum:			1.4
	Maximum;		Maximum:		Maximum:			1.70
3. Ratio of Run Depth to Bankfull Mean Depth	Mean:	2.2	Mean:	2.0	Mean:	1.7	N/A	2.00
(drun/dbkl)	Minimum:	0.0	Minimum		Minimum.			1.75
	Maximum:	0.0	Maximum:		Maximum:			2.13
4. Slope of Glide (Sglide) ft/ft	Meant	0.0010	Mean:	0.0060	Mean:	0.0065	N/A	0.00
	Minimum:	0.0009	Minimum:	0.0000	Minimum:	0.0006		0
	Maximum:	0.0010	Maximum:	0.0120	Maximum:	0.0124		0.01
5. Ratio of Glide Slope to Average Water	Mean:	0.051	Mean:	0.316	Mean:	0.969	N/A	0.12
Slope (Sglide/Savg)	Minimum	0.048	Minimum:	0.000	Minimum:	0.092		0
The state of the s	Maximum:	0.054	Maximum:	0.632	Maximum:	1.847		0.38
6. Maximum Glide Depth (dglide) ft	Mean:	1.5	Mean:	1.2	Mean:	2.4	N/A	1.55
AND DESCRIPTION OF THE PROPERTY OF THE PROPERT	Minimum:		Minimum:	, 7.4mil	Minimum:	1959		1.3
	Maximum:		Maximum:		Maximum:			1.80
7. Ratio of Glide Depth to Bankfull Mean Depth	Mean:	1.6	Mean:	1.7	Mean:	1.5	N/A	1.94
(dglide/dbkl)	Minimum	0.0	Minimum:	200	Minimum:	3.79	14.027	1.625
TOTAL TOTAL CONTROL OF THE PARTY OF THE PART	Maximum:	0.0	Maximum:		Maximum:			2.25

Materials:		Existing		Proposed	Refe	erence Reach	Reference Reach	Reference Reach
Particle Size Distribution of Channel Material						.5.2.07.		
D16		0.9		0.9		0.38		0.042
D35		1.2		1.2		0.7		0.3
D50		2.0		2.0		6		1.0
D84		8.0		8.0		10.7		17.0
D95		10.1	1	10.1		11.2		42.0
Particle Size Distribution of Bar Material	Pavement	Subpavement	Pavement	Subpavement	Pavement	Subpavement	Pavement	Pavement
D16	4.1	<0.1	4.1	< 0.1	7.8	<0.1	0.8	0.2
D35 D50	5.3	<0.1	5.3	<0.1	10	<0.1	1.7	1.9
D50	8.0	<0.1	8.0	<0.1	10.3	3	2.4	6.0
D84	10.2	7.1	10.2	7.1	10.9	11,3	6.9	22.0
D95	10.4	11.3	10.4	11.3	11.2	11.9	9.5	37.0
Largest Size Particle on Bar		88.9		88.9		1111711		45.0

Dye Branch

Reach 1

Restoration Site: USGS Gage Station: Reference Reach:

Derita Branch, UT to Lake Jeanette, UT to SW Prong Beaverdam Mulkey 5/27/2005

Surveyors: Date:

Weather:						Reference Reach	Reference Reach	Reference Reach
Variables		Existing Channel		Proposed Reach		Derita Branch	UT to Lake Jeanette	UT SW Prong Bydm
1. Stream Type		Unstable E4		C4		E4	C4	C5
2. Drainage Area (sq. mi)		0,6		0,6		0.250	0.25	0.28
3. Bankfull Width (Wokf) II	Mean:	12.5	Mean:	17.2	Mean:	11,25	9.50	11.77
	Minimum		Minimum:		Minimum:		8.90	9.90
V - V - PRIVATE ANTRE CAST - I WT ANTAINE	Maximum:		Maximum:		Maximum:		12.10	14.10
Bankfull Mean Depth (dbkf) fi	Mean:	1,58	Mean:	1.40	Mean;	1.63	0.80	0.80
	Minimum:		Minimum;		Minimum:		0.70	0.70
West Brook Barra Official Co.	Maximum:	70	Maximum:	100	Maximum:	0.00	0.80	1.00
Width/Depth Ratio (Wbkf/dbkf)	Mean: Minimum:	7.9	Mean: Minimum:	12.3	Mean: Minimum:	6.89	13.70	14.97
	Maximum:		Maximum:		Maximum:			
6. Bankfull Cross-Sectional Area (Abkf) sq ft	Mean:	19.7	Mean:	24.1	Mean:	18.35	7.70	9.38
	Minimum:	1511	Minimum:	6200	Minimum:	1,21,52	6.80	7.80
	Maximum:		Maximum:		Maximum:		8.40	10.50
7. Bankfull Mean Velocity (Vbkf) Ips	Mean:	5.6	Mean:	5.0	Mean:	5.86	4.55	4.80
	Minimum:	5.4	Minimum:	4.7	Minimum:	5.27		4.10
	Maximum:	5.9	Maximum:	5.3	Maximum:	6.98		5.20
B. Bankfull Discharge (Obkf) cfs	Mean:	110.6	Mean:	120.5	Mean;	107.4	35	45
	Minimum:	105.7	Minimum:	113.3	Minimum:	96.7	1	38.00
- V- 1 - V - V - V - V - V - V - V - V -	Maximum:	115.7	Maximum:	127.7	Maximum:	128.1		46.00
Maximum Bankfull Depth (dmax) II	Mean:	2.2	Mean:	2.1	Mean:	2.4	1,30	1.28
	Minimum:		Minimum;		Minimum: Maximum:		1.20	1.00
10. Date of Case Beat Hatability Maderille	Maximum: Mean:	1.1	Maximum: Mean:	1.0	Mean:	1.2	1.00	1.00
Ratio of Low Bank Height to Maximum Bankfull Depth (loh/dmax)	Minimum:	1-1	Minimum:	1.0	Minimum	1.6	1.00	1,00
Gabitan Dopar (tarromax)	Maximum:		Maximum:		Maximum:			
11. Width of Flood Prone Area (Wfpa) It.	Mean:	40.2	Mean:	48.0	Mean:	100.0	25.00	90.00
THE PERSON NAMED IN COMPANY OF THE PERSON NAMED IN	Minimum:	19/00/425	Minimum:	1.000	Minimum:	(56.27.27)	19.00	77.77.77
	Maximum:		Maximum:		Maximum:		36.00	
12. Entrenchment Ratio (Wlpa/Wbkf)	Mean:	3.2	Mean:	2.8	Mean:	8.9	3.80	7.65
	Minimum:		Minimum:		Minimum:			
	Maximum:	to Harrison	Maximum:		Maximum:			
13. Meander Length (Lm) It	Mean:	60.3	Mean:	51.2	Mean:	79.0	50.2	71.0
	Minimum:	20.6	Minimum:	26.2	Minimum:	29.0	26.0	33.0
	Maximum:	102.9	Maximum:	73.5	Maximum:	155.0	69.0	144.0
4. Ratio of Meander Length to Bankfull Width	Mean:	4.8	Mean:	3.0	Mean:	7.0	5.28	6.03
(Lm/Wbkf)	Minimum:	1.7	Minimum:	1.5	Minimum: Maximum:	2.6 13.8	2.92 5.70	2.80 12.24
15. Radius of Curvature (Rc) It	Maximum: Mean:	8.2 39.7	Maximum: Mean:	4.3 19.5	Mean:	36.8	9.70	18.00
15. Hadius of Curvatore (NC) It	Minimum:	16.1	Minimum:	12.3	Minimum:	25.5	5.00	11.10
	Maximum:	86.4	Maximum:	29.6	Maximum:	48.0	22.00	38.00
16. Ratio of Radius of Curvature to Bankfull	Mean:	3.2	Mean:	1.1	Mean:	3.3	1.02	1.53
Width (Rc/Wbkf)	Minimum	1.3	Minimum:	0.7	Minimum:	2.3	0.56	0.94
523 SANDAR WALLONSON	Maximum:	6.9	Maximum:	1.7	Maximum:	4.3	1.82	3.23
17. Belt Width (Wblt) ft	Mean:	14.8	Mean:	29.0	Mean:	41.0	33	71
	Minimum:	8.9	Minimum:	19.1	Minimum;	28.3	26	30
	Maximum:	25.3	Maximum:	40.3	Maximum:	53.7	40	119
18. Meander Width Ratio (Wblt/Wbkl)	Mean:	1,2	Mean:	1.7	Mean:	3.6	3.47	6.03
	Minimum	0.7	Minimum:	1.1	Minimum:	2.5		2.55
04 60 40 40 40 40 40 40 40 40 40 40 40 40 40	Maximum:	2.0	Maximum:	2.3	Maximum:	4.8	1.20	10.11
21. Sinuosity (Stream length/valley distance)	Mean: Minimum:	1.14	Mean; Minimum;	1.14	Mean: Minimum:	1.15	1.39	2.22
(K)	Maximum:		Maximum:		Maximum:			
22. Valley Slope (ft/ft)	Mean:	0.0064	Mean:	0.0064	Mean:	0.0077	0.0076	0.0300
ez. Velley Stope (littl)	Minimum:	0.0004	Minimum:	0.0004	Minimum:	0.0077	0.0070	0.0000
	Maximum:		Maximum:		Maximum:			
23. Average Water Surface Slope	Mean:	0.0056	Mean:	0.0052	Mean:	0.0067	0.0057	0.0130
for Reach (Savo)	Minimum:	1872354	Minimum:		Minimum:	23534.7	1222044	(540000)
	Maximum:		Maximum:		Maximum:			
24. Pool Stope (Spool) ft/ft	Mean:		Mean:	0.0006	Mean:	0.0000	0.0005	0.0011
	Minimum:		Minimum:	0.0000	Minimum:	0.0000		0.0000
	Maximum:		Maximum:	0.0012	Maximum:	0.0000		0.0030
25. Ratio of Pool Slope to Average Slope	Mean:		Moan:	0.1	Mean:	0.000	0.08	80.0
(Spool/Savg)	Minimum:		Minimum:	0,0	Minimum:	0.000		0.00
25 14 - 2-15 - 5-15	Maximum:		Maximum:	0.2	Maximum:	0.000	0.00	0.23
26. Maximum Pool Depth (dpool) ft	Mean:		Mean;	3,3	Mean: Minimum:	3.2	2.90	2.40
	Minimum: Maximum:		Minimum: Maximum:		Maximum:		2.40 2.90	1.80
27. Ratio of Maximum Pool Depth to Bankfull	Mean:	0.0	Mean:	2.4	Mean:	2.0	3.63	3.00
Mean Depth (dpool/dbkf)	Minimum	0.0	Minimum:	6.4	Minimum:	0.0	3.03	2.25
Court School Values and Male	Maximum:	0.0	Maximum:		Maximum:	0.0		3.63
28, Pool Width (Wpool) ft	Mean:	5.0	Mean:	24.0	Mean:	15.6	20.70	9.90
THE CONTRACTORS AND PROPERTY OF CO.	Minimum:		Minimum:	77.14	Minimum:	1 10 10	8.00	9.10
	Maximum:		Maximum:		Maximum:		10.70	10.50

29. Ratio of Pool Width to Bankfull Width (Wpool/Wbkf)

Maximum:

Mean: Minimum

Maximum:

1.4

Maximum:

Minimum:

Maximum:

1:4

0.0

Mean:

Maximum: Mean:

Minimum:

Maximum:

0.0

10.50 0.84

0.77

0.69

10.70 2.18

Reach 1

Restoration Site: USGS Gage Station: Reference Reach: Surveyors:

Derita Branch, UT to Lake Jeanette, UT to SW Prong Beaverdam Mulkey 5/27/2005

Date: Weather:

Variables		Existing Channel		Proposed Reach		Reference Reach Derita Branch	Reference Reach UT to Lake Jeanette	Reference Reach UT SW Prong Bydm
30. Bankfull Cross-sectional Area at Pool	Mean:		Mean:	32.9	Mean:	29.8	10.75	13.50
(Apool) sq ft	Minimum:		Minimum:	32.0	Minimum:	83.0	9,90	11.40
(dison) of it	Maximum:		Maximum:		Maximum:		11.60	16.00
31. Ratio of Pool Area to Bankfull Area	Mean:	0.0	Mean:	1.4		10		
(Appol/Abki)	Minimum:	0.0		1.9	Mean:	1.6	1.40	1.44
(Apool/Adki)			Minimum:		Minimum:			
AND THE PROPERTY OF THE PROPER	Maximum:	0.0	Maximum:		Maximum:	1777		
32. Pool to Pool Spacing (p-p) ft	Mean:		Mean:	47.7	Mean:	140.8	40.20	36.50
	Minimum:		Minimum:	39.8	Minimum:	178710	20.7	18
Name and the state of the state	Maximum:		Maximum:	55.7	Maximum:		54,8	58
33. Ratio of Pool-to-Pool Spacing to Bankfull	Mean:	0.0	Mean:	2.8	Mean:	12.5	4.23	3.10
Width (p-p/Wokf)	Minimum:	0.0	Minimum:	2.3	Minimum:	0.0	2.20	1.53
M A	Maximum:	0.0	Maximum:	3.2	Maximum:	0.0	5.80	4.93
34. Pool Length (Lp) ft	Mean:		Mean:	27.8	Mean:	24.0	N/A	10.50
24 1,000	Minimum:		Minimum:	15.9	Minimum:	15.1	W025A	3.50
	Maximum:		Maximum:	39.8	Maximum:	32.8		30.00
35. Ratio of Pool Length to Bankfull Width	Mean:	0.0	Mean:	1.6	Mean:	2.1	N/A	0.89
(Lp/Wbkf)	Minimum:	0.0	Minimum:	0.9	Minimum:	1.3	0.955	0.30
	Maximum:	0.0	Maximum:	2.3	Maximum:	2.9		2.55
36. Riffle Slope (Sriff) It/It	Moan:	0.0146	Mean:	0.0150	Mean:	0.0160	N/A	0.0350
so runte diope total ret	Minimum:	0.0027	Minimum:	0.0150	Minimum:	0.0160	N/A	
	Maximum:	0.0388	Maximum:					0.0220
2 B W - 1 B W - 6				0.0	Maximum:	0.0290		0.0520
37. Ratio of Riffle Slope to Average Slope	Mean:	2.615	Mean:	2.9	Mean:	2.385	N/A	2.69
(Sriff/Savg)	Minimum:	0.479	Minimum:		Minimum:	0.954		1,69
	Maximum:	6.921	Maximum:		Maximum:	4.331		4.00
8. Maximum Riffle Depth (driff) ff	Mean:	2.2	Mean:	2.1	Mean:	2.40	1.30	1.30
	Minimum:		Minimum:		Minimum:		1.20	1.00
	Maximum:		Maximum:		Maximum:		1.30	1.70
39. Ratio of Maximum Riffle Depth to Bankfull	Mean:	1.4	Mean:	1.5	Mean:	1.5	1.63	1.63
Mean Depth (driff/dbkf)	Minimum:	0.0	Minimum:		Minimum:	0.0	1.71	1.25
	Maximum:	0.0	Maximum:		Maximum:	0.0	1.63	2.13
40: Run Slope (Srun) It/fl	Mean:	0.0049	Mean:	0.0050	Mean:	0.0071	N/A	0.0090
	Minimum:	0.0008	Minimum:	0.0010	Minimum:	0.0018		0.0030
	Maximum:	0.0225	Maximum:	0.0100	Maximum:	0.0114		0.0170
41. Ratio of Run Slope to Average Slope	Mean:	0.875	Mean:	0.962	Mean:	1.054	N/A	0.69
(Srun/Savg)	Minimum:	0.142	Minimum:	0.192	Minimum:	0.275	1200	0.23
(Gidiz Gavg)	Maximum:	4.013	Maximum:	1.923	Maximum:			
42, Maximum Run Depth (drun) ft	Mean:	2.3	Mean:	2.3	Mean:	1,703	N/A	1.31
42, Maximum Hon Deput (Gron) II	Minimum:	2,3		6.0		:857	N/A.	1.6
			Minimum:		Minimum:			1.4
(2 P. 1 P. P. P. P. P. P. P.	Maximum:		Maximum:	72	Maximum:	- 12		1.7
43. Ratio of Run Depth to Bankfull Mean Depth	Mean:	1,5	Mean;	1.6	Mean:	1.7	N/A	2.00
(drun/dbkf)	Minimum:	0.0	Minimum:		Minimum:			1.75
ALCOHOLOGICA CONTRACTOR CONTRACTO	Maximum:	0.0	Maximum:		Maximum:			2.13
44. Slope of Glide (Sglide) ft/ft	Mean:		Mean:	0.0020	Mean:	0.0065	N/A	0.0016
	Minimum:		Minimum:	0.0000	Minimum:	0.0006		0.0000
	Maximum:		Maximum:	0.0040	Maximum:	0.0124		0.0050
15 Ratio of Glide Slope to Average Water	Mean:		Mean:	0.385	Mean:	0.969	N/A	0.12
Slope (Sglide/Savg)	Minimum:		Minimum:	0.000	Minimum:	0.092	TANEP.	0.00
The second secon	Maximum:		Maximum:	0.769	Maximum:	1.847		0.38
46. Maximum Glide Depth (dglide) fl	Moan:		Mean:	2.3	Mean:	2.4	N/A	1.55
The second of th	Minimum:		Minimum:	JE//E	Minimum:	079AT	1000	1.30
	Maximum:		Maximum:		Maximum:			1.80
47. Ratio of Glide Depth to Bankfull Mean Depth	Mean:	0.0	Mean:	1.6	A STATE OF THE PARTY OF THE PAR	+ 6	N/A	
(dolide/dbkf)	Minimum:	0.0		1.6	Mean:	1.5	N/A	1,94
(ugine/upkt)			Minimum:		Minimum:			1.63
]	Maximum:	0.0	Maximum:		Maximum:			2.25

Materials:		Existing		Proposed	Ref	erence Reach	Reference Reach	Reference Reach
Particle Size Distribution of Channel Material								
D16		<0.1		<0.1		0.38	N/A	0.042
D35		2.2		2.2		0.7	N/A	0.3
D50		4.5		4.5		6	N/A	1.0
D84		10		10		10.7	N/A	17.0
D95		10.5		10.5		11.2	N/A	42.0
Particle Size Distribution of Bar Material	Pavement	Subpavement	Pavement	Subpavement	Pavement	Subpayement	Pavement	Pavement
D16	2.6	<0.1	2.6	<0.1	7.8	<0.1	0.8	0.2
D35	4.7	<0.1	4.7	<0.1	10	<0.1	1.7	1.9
D50	6.0	2.8	6.0	2.8	10.3	3.0	2.4	6.0
D84	10	7.8	10	7.8	10.9	11.3	6.9	22.0
D95	10.5	10.6	10.5	10.6	11.2	11.9	9.5	37.0
Largest Size Particle on Bar		24		24				45.0

Reach 2

Restoration Site: USGS Gage Station: Reference Reach:

Derita Branch, UT to Lake Jeanette, UT to SW Prong Beaverdam Mulkey 5/27/2005

Surveyors: Date: Weather:

'ariables		Existing Channel		Proposed Reach		Reference Reach Derita Branch	Reference Reach UT to Lake Jeanette	Reference Reach UT SW Prong Byde
. Stream Type		Unstable E4		C4		E4	C4	C5
Drainage Area (sq. mi)		0.6		0.6		0.250	0.25	0.28
Bankfull Width (Wbkf) fi	Mean:	11.20	Mean;	16,1	Mean:	11.25	9.50	11,77
	Minimum:		Minimum:		Minimum:	THE CO.	8.90	9.90
The state of the s	Maximum:		Maximum:		Maximum:		12.10	14.10
Bankfull Mean Depth (dbkf) ft	Mean:	1.60	Mean:	1.24	Mean:	1.63	08.0	0.80
	Minimum:		Minimum:		Minimum:		0.70	0.70
	Maximum:		Maximum:		Maximum:		08.0	1.00
Width/Depth Flatio (Wbkf/dbkf)	Mean:	7.00	Mean:	13.0	Mean:	6.89	11.70	14.97
	Minimum:		Minimum:		Minimum:	2777	1.00	0.387
	Maximum;		Maximum:		Maximum:			
Bankfull Cross-Sectional Area (Abkf) sq ft	Mean:	18.10	Mean:	20.0	Mean:	18.35	7.70	9.38
Commission of the Commission American Commission Commis	Minimum:		Minimum:	(50,000,000)	Minimum:	70124	6.80	7.80
	Maximum:		Maximum:		Maximum:		8.40	10.50
Bankfull Mean Velocity (Vbkf) fps	Mean:	6.5	Mean:	6.2	Mean:	5.86	4.55	4.80
Delinial Modif Foldery (Font) ips	Minimum:	6.2	Minimum:	5.8	Minimum:	5.27	4.00	4.10
	Maximum:	6.9	Maximum:	6.6	Maximum:	6.98		
Basel III Disabilities (OHA) etc.		118.1					ne ne	5.20
Bankfull Discharge (Qbkf) cls	Mean:		Mean;	124.0	Mean:	107.4	35	45
	Minimum:	112.2	Minimum:	116.0	Minimum;	96.7		38.00
	Maximum:	124.8	Maximum:	132.0	Maximum:	128.1		46.00
Maximum Bankfull Dopth (dmax) ft	Mean:	2.8	Mean:	1.8	Mean:	2.4	1.30	1.28
	Minimum:		Minimum:	1.2	Minimum:		1.20	1.00
	Maximum:		Maximum:	2.4	Maximum:		1.30	1.70
). Ratio of Low Bank Height to Maximum	Mean:	1.00	Mean:	1.0	Mean:	1.2	1.00	1.00
Bankfull Depth (lbh/dmax)	Minimum:		Minimum:		Minimum:	Deg.	3014(8)	0.99823
	Maximum:		Maximum:		Maximum:			
. Width of Flood Prone Area (Wipa) II	Mean:	89.5	Mean:	0.08	Moan:	100.0	25.00	90.00
A CONTRACTOR OF THE PROPERTY O	Minimum:	100000	Minimum:		Minimum:	1.474.47	19.00	50.00
	Maximum:		Maximum:		Maximum:		36.00	
Entrenchment Ratio (Wfpa/Wbkf)	Mean:	8.0	Mean:	5.0	Mean:	8.9		7.65
Chiroficiation (Miles (0.0		9,0		0.0	3.80	7.65
	Minimum:		Minimum:		Minimum:			
	Maximum:		Maximum:		Maximum:			
Meander Length (Lm) (t	Mean:	79.7	Mean:	113.4	Меал:	79.0	50.2	71.0
	Minimum:	40.1	Minimum:	60.3	Minimum:	29.0	26.0	33.0
	Maximum:	172.7	Maximum:	152.5	Maximum:	155.0	69.0	144.0
. Ratio of Meander Length to Bankfull Width	Mean:	7.1	Mean:	7.0	Mean:	7.0	5,28	6.03
(Lm/Wbkf)	Minimum:	3.6	Minimum:	3.7	Minimum:	2.6	2.92	2.80
	Maximum:	15.4	Maximum:	9.5	Maximum:	13.8	5.70	12.24
. Radius of Curvature (Ro) It	Mean:	52.4	Mean:	39.9	Mean:	36.8	9.70	18.00
A CONTROL ON THE PROPERTY AND A STATE OF THE PARTY OF THE	Minimum:	14.5	Minimum:	27.8	Minimum:	25.5	5.00	11.10
	Maximum:	148.8	Maximum:	58.7	Maximum:	48.0	22.00	38.00
Ratio of Radius of Curvature to Bankfull	Mean:	4.7	Mean:	2.5	Mean:	3.3	1.02	1.53
Width (Rc/Wbkf)	Minimum:	1.3	Minimum:	1.7	Minimum:	2.3	0.56	0.94
TAXABLE CONT.	Maximum:	13.3	Maximum:	3.6	Maximum:	4.3	1.82	3.23
Belt Width (Wblt) ft	Mean:	24.3	Mean:	44.88	Mean:	41.0	33	71
Dell AARTH (AARTH) II		6.6		25.9				
	Minimum;		Minimum:		Minimum:	28.3	26	30
A DESCRIPTION OF THE PARTY OF T	Maximum:	56.9	Maximum:	58.2	Maximum:	53.7	40	119
Meander Width Ratio (Wblt/Wbkf)	Mean:	2.2	Mean:	2.8	Mean:	3.6	3.47	6.03
	Minimum:	0.6	Minimum:	1,6	Minimum:	2.5	14473	2.55
	Maximum:	5.1	Maximum:	3.6	Maximum:	4.8		10.11
Sinuosity (Stream length/valley distance)	Mean:	1.21	Mean:	1.30	Mean:	1.15	1.39	2.22
(K)	Minimum:		Minimum:		Minimum:		17.10.00.00	
	Maximum:		Maximum:		Maximum:			
. Valley Slope (ft/ft)	Mean:	0.0097	Mean:	0.0097	Mean:	0.0077	0.0076	0.0300
	Minimum:		Minimum:		Minimum:			200
	Maximum:		Maximum:		Maximum:			
. Average Water Surface Slope	Mean:	0.0080	Mean:	0.0094	Mean:	0.0067	0.0057	0.0130
for Reach (Savg)	Minimum:	201000000	Minimum:	ALL MANAGES	Minimum:	MINAME	WIW SHIP	om too.
and the state of t	Maximum:		Maximum:		Maximum:			
Pool Slope (Spool) It/II	Mean:	N/A	Mean:	0.0008	Mean:	0.0000	0.0005	0.0011
		NA					0.0005	0.0011
	Minimum:		Minimum	0.0000	Minimum:	0.0000		0.0000
	Maximum:		Maximum:	0.0015	Maximum:	0.0000		0.0030
Ratio of Pool Slope to Average Slope	Mean	N/A	Mean:	0.080	Mean:	0.000	80.0	80.0
(Spool/Savg)	Minimum:		Minimum:	0.000	Minimum:	0.000		0.00
	Maximum:		Maximum:	0.160	Maximum:	0.000		0.23
. Maximum Pool Depth (dpool) II	Mean:	N/A	Mean:	3.3	Mean:	3.2	2,90	2.40
	Minimum:		Minimum:		Minimum:		2.40	1.80
	Maximum:		Maximum:		Maximum:		2.90	2.90
Ratio of Maximum Pool Depth to Bankfull	Mean:	N/A	Mean:	2.7	Mean:	2.0	3.63	3.00
The state of the s	Minimum:	010		*15			5.00	
Mean Depth (dpool/dbkf)			Minimum:		Minimum:	0.0		2.25
I.V.	Maximum:		Maximum:		Maximum:	0.0		3.63

Reach 2

Restoration Site: USGS Gage Station: Reference Reach:

Derita Branch, UT to Lake Jeanette, UT to SW Prong Beaverdam Mulkey 5/27/2005

Surveyors: Date: Weather:

Variables		Existing Channel		Proposed Reach		Reference Reach Derita Branch	Reference Reach UT to Lake Jeanette	Reference Reach UT SW Prong Bydr
28. Pool Width (Wpool) ft	Mean:	N/A	Mean:	24.0	Mean:	15.6	20.70	9.90
	Minimum:	1900	Minimum:	2.40	Minimum:	13.0	8.00	9.10
	Maximum:		Maximum:		Maximum:		10.70	10.50
9. Ratio of Pool Width to Bankfull Width	Mean:	N/A	Mean:	1.5	Mean:	1.4	2.18	0.84
(Wpaol/Wbkf)	Minimum:	5250	Minimum:	1100	Minimum:	0.0	6110	0.77
	Maximum:		Maximum:		Maximum:	0.0		0.89
Bankfull Cross-sectional Area at Pool	Mean:	N/A	Mean:	29.0	Mean:	29.8	10.75	13.50
(Apool) sq ft	Minimum:		Minimum:	-27.61	Minimum:	55.00	9.90	11.40
MARKET MARKAN	Maximum:		Maximum:		Maximum:		11.60	16.00
1. Ratio of Pool Area to Bankfull Area	Mean:	N/A	Mean:	1.5	Moan:	1.6	1.40	1,44
(Apool/Abkl)	Minimum:	.1554.5	Minimum:	11,000	Minimum:	319	1509	3929
	Maximum:		Maximum:		Maximum:			
2. Pool to Pool Spacing (p-p) ft	Mean:	N/A	Mean:	48.3	Mean:	140,B	40.20	36.50
	Minimum:	7477	Minimum:	40.3	Minimum:	1,000	20.7	18
	Maximum:		Maximum:	56.4	Maximum:	1	54.80	58.00
3. Ratio of Pool-to-Pool Spacing to Bankfull	Mean:	N/A	Mean:	3.0	Mean:	12.5	4.23	3.10
Width (p-p/Wbkf)	Minimum:	134.70	Minimum:	2.5	Minimum:	0.0	2.2	1.53
account the burnership	Maximum:		Maximum:	3.5	Maximum:	0.0	5.80	4.93
4. Pool Length (Lp) It	Mean:	N/A	Mean:	24.2	Mean:	24.0	N/A	10.50
Access to the second state of the second state	Minimum:	Ameri	Minimum:	16.1	Minimum:	15.1	1307	3.5
	Maximum:		Maximum:	48.3	Maximum:	32.6		30.00
5. Ratio of Pool Length to Bankfull Width	Mean:	N/A	Mean:	1,5	Mean:	2.1	N/A	0.9
(Lp/Wbkf)	Minimum:	271533	Minimum:	1.0	Minimum:	1.3	1300	0.9
(ep. (Color)	Maximum:		Maximum:	3.0	Maximum:	2.9		2.5
6. Riffle Slope (Sriff) It/It	Mean:	0.0141	Moan:	0.0190	Mean:	0.0160	N/A	0.0350
or Thine Biops (Singlish	Minimum	0.0016	Minimum:	0.0100	Minimum:	0.0064	N/A	0.0220
	Maximum:	0.0419	Maximum:		Maximum:	0.0290		
7. Ratio of Riffle Slope to Average Slope	Mean:	1.758	Mean:	2.0	Mean:	2.385	N/A	0.0520 2.69
(Sriff/Savg)	Minimum:	0.198	Minimum:	2.0	Minimum:	0.954	1,000	
(Similary)	Maximum:	5.233	Maximum:		Maximum:	4.331		1.69
Maximum Riffle Depth (driff) it	Mean:	2.810	Mean:	1.8	Mean:	2.40	1.00	4.00
or maximum rame popul (dilit) ii	Minimum:	2,010	Minimum:	1.0	Minimum:	2.40	1.30	1.30
	Maximum:		Maximum:				1.2	1
9. Ratio of Maximum Riffle Depth to Bankfull	Mean:	1.8	Mean:	1.5	Maximum; Mean;	1.5	1.30	1.70
Mean Depth (driff/dbkf)	Minimum:	1.0	Minimum:	1,5		1.5	1.63	1.63
mean Debut formioned	Maximum:		Maximum:		Minimum: Maximum:	0.0	1.71	1.25
0. Run Slope (Srun) ft/ft	Mean:	0.0073	Mean:	0.0060	Mean:			2.13
or train stops (strain ten	Minimum:	0.0002	Minimum:	0.0020	Minimum:	0.0071	N/A	0.01
	Maximum:	0.0595	Maximum:	0.0100	Maximum:	0.0114		0.003
Ratio of Run Slope to Average Slope	Mean:	0.906	Mean:	0.638	Mean:		508	
(Srun/Savg)	Minimum:	0.019	Minimum:	0.213	Minimum:	1,054	N/A	0.69
(CONTROLLYM)	Maximum:	7.439	Maximum:	1.064	Maximum:			0.23
2. Maximum Run Depth (drun) ft	Mean:	2.84	Mean:	2.4	Mean:	1.703	N/A	1.31
se meaning contraction of the co	Minimum:	2.83	Minimum:	6.4	Minimum:	2.7	N/A	1.60
	Maximum:	2.85	Maximum:		Maximum:			1.4
3. Ratio of Run Depth to Bankfull Mean Depth	Mean:	1.78	Mean:	1.9	Mean:	1.7	61/4	1.70
(drun/dbkf)	Minimum:	1.77	Minimum:	1.8	Minimum:	197	N/A	2.00
N. S.	Maximum:	1.78	Maximum:		Maximum:			1.75
4. Slope of Glide (Sglide) ft/ft	Mean:	N/A	Mean:	0.0030		0.0005	AVA	2.13
2. September 1990 (September 1990)	Minimum:	14/4	Minimum:	0.0000	Mean; Minimum;	0.0065	N/A	0.00
	Maximum:		Maximum:	0.0000	Maximum:	0.0006 0.0124		0
5. Ratio of Glide Slope to Average Water	Mean:	N/A	Mean:	0.319			AU/A	0.01
Slope (Sqlide/Savg)	Minimum:	IVA	Minimum:		Mean:	0.969	N/A	0.12
Signa (Sullida Savar	Maximum:		Maximum:	0.000 0.638	Minimum: Maximum:	0.092		0
. Maximum Glide Depth (dglide) ft	Mean:	N/A	The second secon	2.0		1.847		0.38
y maximum Giloa Dahin (ollinga) ii	Minimum:	N/A	Mean:	2.0	Mean:	2.4	N/A	1,55
			Minimum:		Minimum:			1.3
7. Ratio of Glide Depth to Bankfull Mean Depth	Maximum:	AUA	Maximum:	1.0	Maximum:			1.80
	Mean:	N/A	Mean:	1.6	Mean:	1.5	N/A	1.94
(dglide/dbkf)	Minimum:		Minimum:		Minimum:	,		1.625
N.	Maximum:		Maximum:		Maximum:			2.25

Materials:		Existing		Proposed	Ref	erence Reach	Reference Reach	Reference Reach
Particle Size Distribution of Channel Material								
D16		0.15		0.15		0.38	N/A	0.042
D35		0.4		0.4		0.7	N/A	0.3
D50		3.3		3.3		6	N/A	1.0
D84		10.3		10.3		10.7	N/A	17.0
D95		13.7		13.7		11.2	N/A	42.0
Particle Size Distribution of Bar Material	Pavement	Subpavement	Pavement	Subpavement	Pavement	Subpavement	Pavement	Pavement
D16	4.2	<0.1	4.2	<0.1	7.8	<0.1	0.8	0.2
D35	6.8	0.1 - 2	6.8	<0.1	10	<0.1	1.7	1.9
D50	8.8	2.8	8.8	2.8	10.3	3	2.4	6.0
D84	12.4	7.8	12.4	7.8	10.9	11.3	6.9	22.0
D95	>16	10,6	>16	10.6	11.2	11.9	9.5	37.0
Largest Size Particle on Bar		45.7		45.7				45.0

Dye Branch

Reach 3

Restoration Site: USGS Gage Station: Reference Reach: Surveyors; Date: Weather;

Derita Branch, UT to Lake Jeanette, UT to SW Prong Beaverdam Mulkey 5/27/2005

arlables		Existing Channel		Proposed Reach		Reference Reach Derita Branch	Reference Reach UT to Lake Jeanette	Reference Reach
Stream Type		G4c		C4		E4	C4	C5
Drainage Area (sq. mi)		0.6		0.6		0.250	0.25	0.28
Bankfull Width (Wbkf) ft	Mean:	14.8	Mean:	15.0	Mean:	11.25	9.50	11.77
	Minimum:		Minimum:	1319	Minimum:	11.69		
	Maximum:						8.90	9.90
Description Description		40	Maximum:		Maximum:		12,10	14.10
Bankfull Mean Depth (dokf) ft	Mean:	1.2	Mean:	1.3	Mean:	1.63	0.80	0.80
	Minimum:		Minimum:		Minimum:		0.70	0.70
	Maximum:		Maximum:		Maximum:		0.80	1.00
Width/Depth Ratio (Wbkf/dbkf)	Mean:	12.5	Mean:	12.0	Mean:	6.89	11.70	14,97
	Minimum:		Minimum:		Minimum:	25020	72(6)	2557762
	Maximum		Maximum:		Maximum:			
Bankfull Cross-Sectional Area (Abkf) sq ft	Mean:	17.4	Mean;	18.8	THE RESERVE OF THE PERSON NAMED IN	10.05	7.74	
Programme Company of the Company of the	Minimum:	17.72	Minimum:	10.0	Mean:	18,35	7.70	9.38
					Minimum:		6.80	7.80
	Maximum:		Maximum:		Maximum:		8.40	10.50
Bankfull Mean Velocity (Vbkl) [ps	Mean:	6.7	Mean:	6.7	Mean:	5.86	4.55	4.80
	Minimum:	6.1	Minimum:	6.0	Minimum:	5.27	10,000	4.10
	Maximum:	7.2	Maximum:	7.3	Maximum:	6.98		5.20
Bankfull Discharge (Qbkf) cfs	Mean:	117.3	Mean:	126.4	Mean:	107.4	35	45
	Minimum:	105.4	Minimum:	112.5			35	
					Minimum:	96.7		38.00
Under an Best All Bases Co.	Maximum:	126.0	Maximum:	136.5	Maximum:	128.1		46.00
Maximum Bankfull Depth (dmax) ft	Mean:	2.4	Mean:	1.9	Mean:	2,4	1.30	1.28
	Minimum:		Minimum:		Minimum:	12162	1.20	1.00
	Maximum:		Maximum:		Maximum:		1.30	1.70
. Ratio of Low Bank Height to Maximum	Mean:	4.9	Mean:	1.0	Mean:	1.2	1.00	1.00
Bankfull Depth (lbh/dmax)	Minimum:	WIE	Minimum:	100	Minimum:	#5#E	1749	1.00
The state of the s	Maximum:		Maximum:					
Width of Flood Prone Area (WIpa) ft		20.0		E0.0	Maximum:	100.0	WW. 44	120100
width of Flood Frone Area (Wipa) fi	Mean:	22.0	Mean:	50.0	Mean:	100.0	25.00	90.00
	Minimum:		Minimum:		Minimum:		19.00	
	Maximum:		Maximum:		Maximum:		36.00	
Entrenchment Ratio (Wfpa/Wbkf)	Mean:	1.5	Mean:	3.3	Mean:	8.9	3.80	7.65
Character of the Annual Control of the Control of t	Minimum:		Minimum:	CTATE	Minimum:	(2007)	(3188)	,100
	Maximum:		Maximum:		Maximum:			
Meander Length (Lm) ft	Mean:	103.0		67.7		70.0		200
Meander rendin fruit it			Mean:	67.7	Mean:	79.0	50.2	71.0
	Minimum:	62.0	Minimum:	49.7	Minimum:	29.0	26.0	33.0
	Maximum:	156.9	Maximum:	93.2	Maximum:	155.0	69.0	144.0
Ratio of Meander Length to Bankfull Width	Mean:	7.0	Mean:	4.5	Mean:	7.0	5.28	6,03
(Lm/Wbkf)	Minimum:	4.2	Minimum:	3.3	Minimum:	2.6	2.92	2.80
	Maximum:	10.6	Maximum:	6.2	Maximum:	13.8	5.70	12.24
Radius of Curvature (Rc) ft	Mean;	42.1	Mean:	40.2	Mean:	36.8	9.70	
- Transper at a stranger when the	Minimum.	11.0		22.6				18.00
			Minimum:		Minimum:	25.5	5.00	11.10
	Maximum:	81.9	Maximum:	58.5	Maximum:	48,0	22.00	38.00
Ratio of Radius of Curvature to Bankfull	Mean:	2.9	Mean:	2.7	Mean:	3,3	1.02	1.53
Width (Rc/Wbkf)	Minimum:	0.7	Minimum:	1.5	Minimum:	2.3	0.56	0.94
	Maximum:	5.6	Maximum:	3.9	Maximum:	4.3	1.82	3.23
Belt Width (Wblt) ff	Mean:	30.6	Mean:	36.57	Mean:	41.0	33	71
AND THE PROPERTY OF THE PROPER	Minimum:	15.6	Minimum:	26.00	Minimum:	28.3	26	
	Maximum:	67.7	Maximum:	47.30				30
Meander Width Ratio (Wblt/Wbkt)	Mean:				Maximum:	53.7	40	119
Wieninger Wilder Haire (Well/Work)		2.1	Mean:	2.4	Mean:	3.6	3.47	6.03
	Minimum:	1.1	Minimum:	1.7	Minimum:	2.5	a consultation	2.55
	Maximum:	4.6	Maximum:	3.2	Maximum:	4.8		10.11
Sinussity (Stream length/valley distance)	Mean:	1.14	Mean:	1,20	Mean:	1.15	1.39	2.22
(K)	Minimum:		Minimum:	W - 12/2/2	Minimum:	10 MW	-1.00	De la Caracia
3/1	Maximum:		Maximum:		Maximum:			
Valley Slope (ft/ft)	Mean:	0.0125	Moan:	0.0125	Mean:	0.0077	0.0025	0.000
Tanty Globa (IDII)		V.V (25		0.0123		0.0077	0.0076	0.0300
	Minimum:		Minimum:		Minimum:			
A SECOND STATE OF THE SECO	Maximum:	- Otto -	Maximum:		Maximum:			
Average Water Surface Slope	Mean:	0.0110	Mean:	0.0102	Mean:	0.0067	0.0057	0.0130
for Reach (Savg)	Minimum:		Minimum:		Minimum:			
	Maximum:		Maximum:		Maximum:			
Pool Stope (Spool) ft/ft	Mean:	0.0071	Mean:	0.0010	Mean;	0.0000	0.0005	0.0011
	Minimum:	0.0004	Minimum:	0.0000	Minimum:	0.0000	5.000	0.0000
	Maximum:	0.0174						
Patts of Paul Claus to August 1997			Maximum:	0.0021	Maximum:	0.0000		0.0030
Ratio of Pool Slope to Average Slope	Mean:	0.650	Mean:	0,1	Mean:	0.000	0.08	0.08
(Spool/Savg)	Minimum:	0.038	Minimum	0.0	Minimum:	0.000		0.00
	Maximum:	1.584	Maximum:	0.2	Maximum:	0.000		0.23
Maximum Pool Depth (dpool) ft	Mean:	3.1	Mean:	3.3	Mean:	3.2	2.90	2.40
	Minimum		Minimum:		Minimum:	2.5	2.40	1.80
	Maximum:		Maximum:					
Dalla of Manhaman Book Brown & Book Brown		0.5			Maximum:		2.90	2.90
Ratio of Maximum Pool Depth to Bankfull	Mean	2.6	Mean:	2,6	Meant	2.0	3.63	3.00
Mean Depth (dpool/dbkf)	Minimum:	0.0	Minimum:		Minimum:	0.0		2.25
	Maximum:	0.0	Maximum:			0.0		

Restoration Site: USGS Gage Station: Reference Reach: Surveyors:

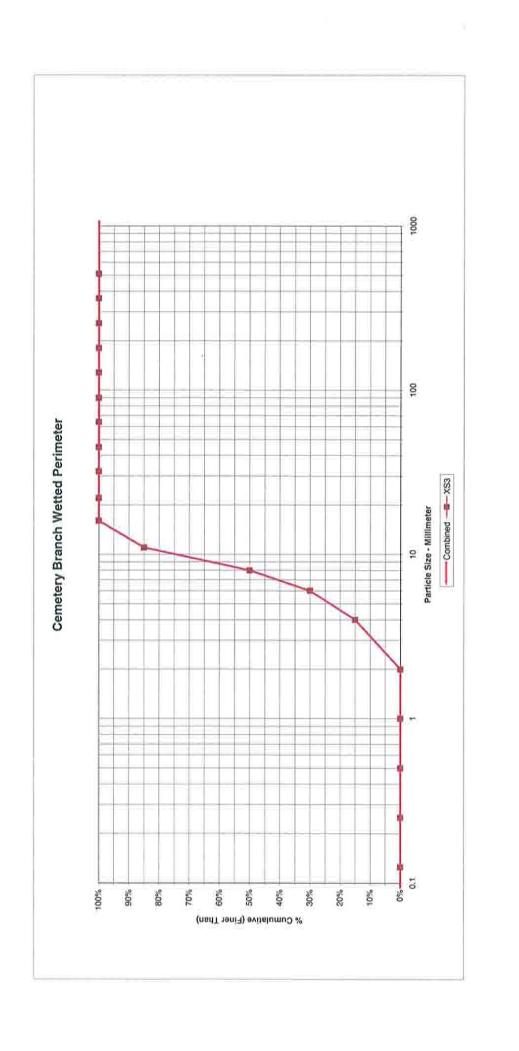
Reach 3

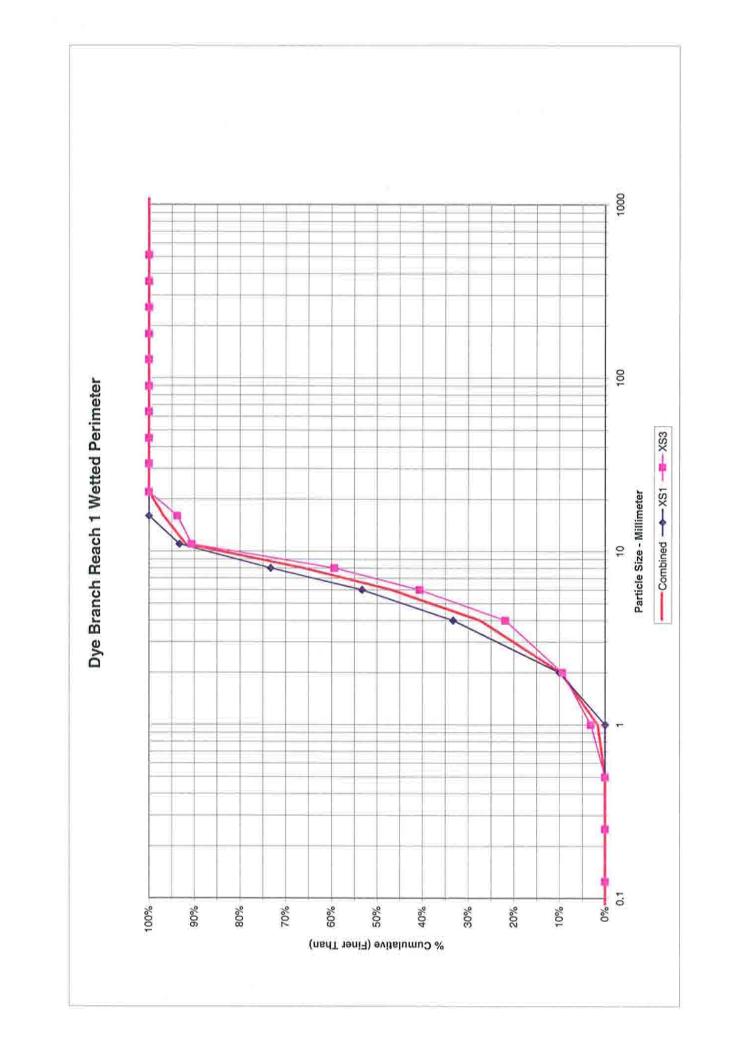
Derita Branch, UT to Lake Jeanette, UT to SW Prong Beaverdam Mulkey 5/27/2005

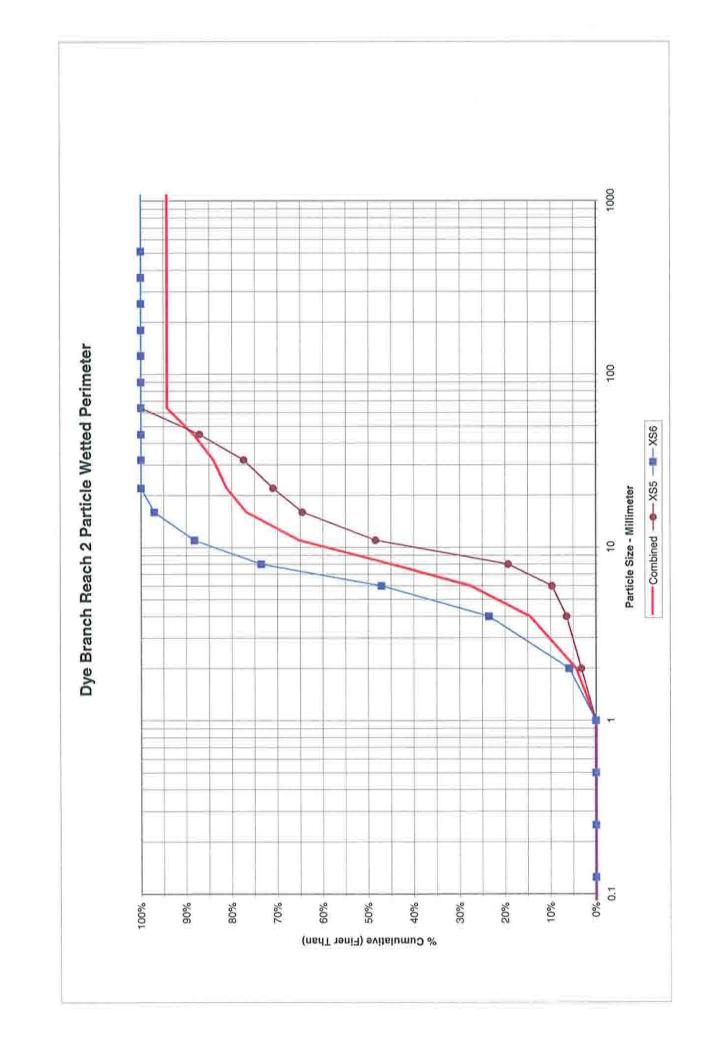
Date: Weather:

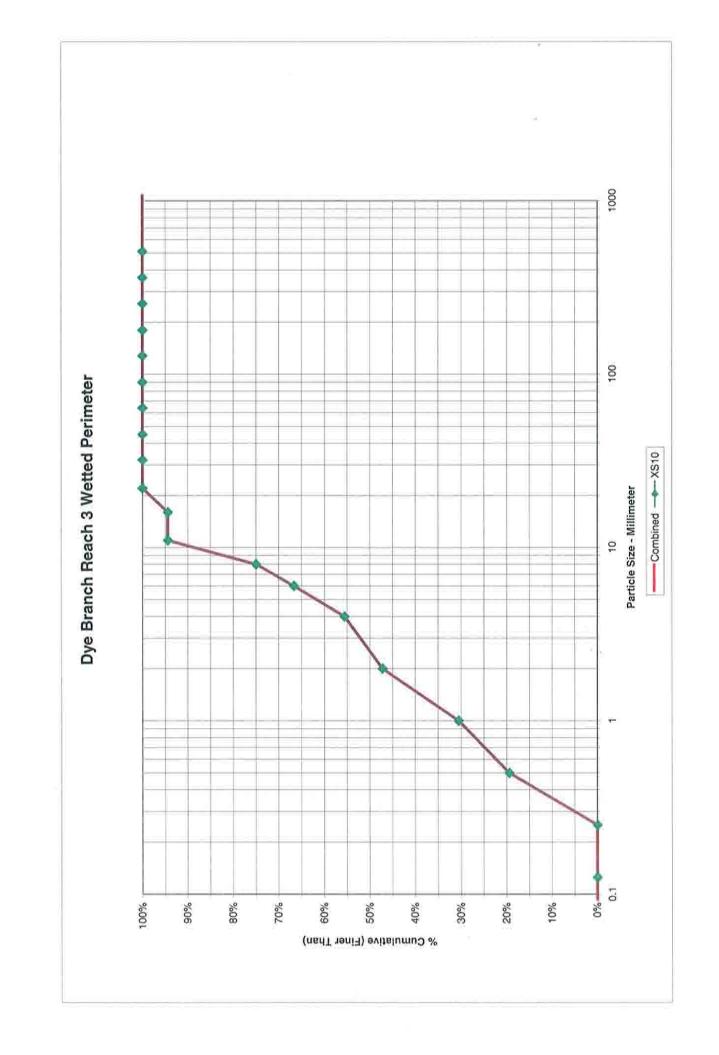
				Colorado de Colora		Reference Reach	Reference Reach	Reference Reach
ariables		Existing Channel	-1	Proposed Reach		Derita Branch	UT to Lake Jeanette	UT SW Prong Bydn
9. Pool Width (Wpool) ft	Mean; Minimum;	14.3	Mean: Minimum:	24,0	Mean: Minimum:	15.6	20.70 8.00	9.90 9.10
February Company of State of S	Maximum:	10	Maximum:	- 14	Maximum:		10.70	10.50
. Ratio of Pool Width to Bankfull Width	Mean: Minimum:	0.0	Mean:	1.6	Mean:	1.4	2.18	0.84
(Wpool/Wbkf)			Minimum:		Minimum:	0.0		0.77
	Maximum:	0.0	Maximum:		Maximum:	0.0	-272	0.89
Bankfull Cross-sectional Area at Pool	Mean:	20.8	Mean:	29.0	Mean:	29.8	10.75	13.50
(Apool) sq ft	Minimum:		Minimum:		Minimum:		9.90	11.40
	Maximum:		Maximum:		Maximum:		11.60	16.00
Ratio of Pool Area to Bankfull Area	Mean:	1.2	Mean:	1,5	Mean:	1.6	1.40	1.44
(Apool/Abkf)	Minimum:	0.0	Minimum		Minimum:			
	Maximum:	0.0	Maximum:	1755-TI	Maximum:			
Pool to Pool Spacing (p-p) ft	Mean:	162	Moan:	51	Mean:	141	40	37
	Minimum:	79	Minimum:	42	Minimum:	4114	21	18
	Maximum:	261	Maximum:	59	Maximum:		55	58
B. Ratio of Pool-to-Pool Spacing to Bankfull	Mean:	11.0	Mean:	3.4	Mean:	12.5	4.2	3.1
Width (p-p/Wbkf)	Minimum:	5.4	Minimum:	2.8	Minimum:	0.0	2.2	1.5
	Maximum:	17.7	Maximum:	3.9	Maximum:	0.0	5.8	4.9
Pool Length (Lp) ft	Mean:	24.8	Mean:	38.0	Mean:	24.0	N/A	10.5
	Minimum:	2.9	Minimum:	25.4	Minimum:	15.1	1000	3.5
	Maximum:	120.1	Maximum:	50.7	Maximum:	32.8		30.0
5. Ratio of Pool Length to Bankfull Width	Mean:	1.7	Mean:	2.5	Mean:	2.1	N/A	0.9
(Lp/Wbkf)	Minimum:	0.2	Minimum:	1.7	Minimum:	1.3	715A25	0.3
	Maximum:	8.1	Maximum:	3.4	Maximum:	2.9		2.5
Riffle Slope (Sriff) It/II	Mean:	0.0207	Mean:	0.0260	Mean:	0.0160	N/A	0.04
	Minimum.	0.0031	Minimum:		Minimum:	0.0064		0.022
	Maximum:	0.1214	Maximum:		Maximum:	0.0290		0.05
Ratio of Rillie Slope to Average Slope	Mean:	1.9	Mean:	2.6	Mean:	2.4	N/A	2.7
(Sriff/Savg)	Minimum:	0.3	Minimum:		Minimum:	1.0	1607	1.7
(omiowyg)	Maximum:	11.0	Maximum:		Maximum:	4.3		4.0
Maximum Riffle Depth (driff) ft	Moan:	2.4	The state of the s	10	Mean:		1.00	
Maximum Hillio Depth (dilit) II		6,4	Moan:	1.9		2,40	1.20	1.30
	Minimum: Maximum:		Minimum:		Minimum:		1.2	1
Control of the Burney Burney Burney Burney			Maximum:		Maximum:		1.30	1,70
P. Ratio of Maximum Rifle Depth to Bankfull	Mean:	2.0	Mean:	1.5	Mean:	1,5	1,5	1.6
Mean Depth (driff/dbkf)	Minimum:	0.0	Minimum:		Minimum:	0.0	1.7	1.3
	Maximum:	0.0	Maximum:		Maximum:	0.0	1.6	2.1
). Run Slope (Srun) ft/ft	Mean:	0.0081	Mean:	0.0090	Mean:	0.0071	N/A	0.01
	Minimum:	0.0010	Minimum:	0.0030	Minimum:	0.0018		0.003
	Maximum:	0.0384	Maximum:	0.0150	Maximum:	0.0114		0.02
. Ratio of Run Slope to Average Slope	Mean:	0.7	Mean:	0.9	Mean:	1.1	N/A	0.7
(Srun/Savg)	Minimum:	0.1	Minimum:	0.3	Minimum:	0.3	1.52.50	0.2
	Maximum:	3.5	Maximum:	1.5	Maximum:	1.7		1.3
Maximum Run Depth (drun) ft	Mean:	2.6	Mean:	2.0	Mean:	2.7	N/A	1.60
	Minimum.		Minimum:		Minimum:			1.4
	Maximum:		Maximum:		Maximum:			1.70
Ratio of Run Depth to Bankfull Mean Depth	Mean	2.2	Mean:	1.6	Mean:	1.7	N/A	2.0
(drun/dbkf)	Minimum:	0.0	Minimum:		Minimum:	N9n	MINGS I	1.8
	Maximum:	0.0	Maximum:		Maximum:			2.1
. Slope of Glide (Sglide) ft/ft	Mean:	0.0053	Mean:	0.0030	Mean:	0.0065	N/A	0.00
	Minimum:	0.0000	Minimum:	0.0000	Minimum:	0.0006		0
	Maximum:	0.0148	Maximum:	0.0060	Maximum:	0.0124		0.01
Ratio of Glide Slope to Average Water	Mean:	0.5	Mean:	0.3	Mean:	1.0	N/A	0.1
Slope (Sglide/Savg)	Minimum:	0.0	Minimum:	0.0	Minimum:	0.1	9000	0.0
CONTRACTOR MATERIAL M	Maximum:	1.3	Maximum:	0.6	Maximum:	1.8		0.4
Maximum Glide Depth (dglide) ft	Mean	2.4	Mean:	1.9	Mean:	2.4	N/A	1.55
Same Salan Albanda III	Minimum:	200	Minimum:	7.155	Minimum:	(663)	13051	1.3
	Maximum:		Maximum:		Maximum:			1.80
7. Ratio of Glide Depth to Bankfull Mean Depth	Mean:	2.0	Mean:	1.5	Mean:	1.5	N/A	
(dglide/dbkl)		0.0		1.5		1.5	N/A	1.9
(ohinasan)	Minimum: Maximum:	0.0	Minimum; Maximum;		Minimum:			1.6
M	Liviaximum:	0.0	IIV/8XIMUM)		Maximum:			2.3

Materials:		Existing	Proposed		Refe	rence Reach	Reference Reach	Reference Reach
Particle Size Distribution of Channel Material								
016		0.15		0.15		0.38	N/A	0.042
035		0.28		0.28		0.7	N/A	0.3
050		0.56		0.56		6	N/A	1.0
084		10.7		10.7		10.7	N/A	17.0
95		12.99		12.99		11.2	N/A	42.0
Particle Size Distribution of Bar Material	Pavement	Subpavement	Pavement	Subpavement	Pavement	Subpavement	Pavement	Pavement.
016	0.43	<0.1	0.43	< 0.1	7.8	<0.1	8.0	0.2
035	1.3	0.1 - 2	1.3	0.1 - 2	10	<0.1	1.7	1.9
050	2.6	2.8	2.6	2.8	10.3	3	2.4	6.0
084	9.3	7.8	9.3	7.8	10.9	11.3	6.9	22.0
95	10.7	10.6	10.7	10.6	11.2	11.9	9,5	37.0
argest Size Particle on Bar		45.7		45.7				45.0









Stream:	Cemetery Branch		Reach/Station:	Reach 1	Cross	Cross Section:	#3		Date:	6/1/2005 Crew:	Crew:	LT	
Erodib	Erodibility Variable/Value	/Value	Index	Bank Erosion Potential									
Bank Height/ Bankfull Height	Sankfull Height												
Bank Height	Bankfull									Bank Erosion Potential	n Potential		
(ft) A	五	A/B	4.6	Moderate				Very Low	Low	Moderate	High	Very High	Extreme
9.0	3.0	1.3			ď.	Bank Height/	Value	1.0-1.1	1.11+1.19	12-15	1.6-20	21-28	>2.8
O.	200	400				Bankfull Height	Index	1.6 - 1.9	20.39	4.0 - 5.9	6.0 - 7.9	8.6.9.0	10
Root Depth/Bank Height	mk Height					Root Depth/	Value	1.0 - 0.9	0.89 - 0.5	0.49 - 0.3	0.29 - 0.15	0,14 - 0,05	<0.05
Door Desert					ehe	Bank Height	Index	1.0 - 1.9	2.0-3.9	4.0 - 5.9	6.0 - 7.9	8.0 - 9.0	10
Moor Deput	C/A					Weighted	Value	100 - 80	79 - 55	54 . 30	29 - 15	14-5.0	0.5>
~ (o/)		1	10.0	Extreme		Root Density	Index	1.0 . 1.9	20.39	4.0 - 5.9	6.0 - 7.9	8.0 - 9.0	10
0.45	0.04					Roals Annla	Value	0 - 20	21 - 60	98-19	81 - 90	911-119	>119
0.13	0.04]				Dank Angre	Index	1.0-1.9	2.0 - 3.9	4.0 - 5.9	6.6 - 7.9	8.0 - 9.0	.10
Weighted Root Density	Density				7	Sueface Decreetion	Value	100 - 80	79 - 55	54 - 30	29-15	14.10	<10
C. C.					tine	race rangement	Index	1.0 - 1.9	20:39	4.0 - 5.9	6.0 - 7.9	8.0-9.0	10
(%) D	D*(C/A)	1	10.0	Extreme	Bank Materials	rials							
9.0	0.02				Bedrock (Be	Bedrock (Bedrock banks have very low bank erosion potential) Boulders (Banks composed of boulders have low bank erosion potential)	very low bank	erosion potent	tal)				
Bank Angle					Cobble (Sub	Cobble (Subtract 10 points. If sand/gravel matrix greater than 50% of bank material, then do not adjust)	f sand/gravel m	atrix greater th	an 50% of ba	ink material, t	hen do not ad	(inst)	
0							0				2		
Bank Angle (degrees)		1	8.9	High	Sand (Add 1) Silt/Clay (+)	Gravet (Add 3-10 points depending on percentage of bank material that is composed of sand). Sand (Add 10 points if sand is exposed to erosional processes). Silt/Clay (+ 0, no adjustment).	exposed to ero	sional process	material that a	s composed o	s sand)		
85.0													
					Stratification	TI.							
Surface Protection	100				Add 5-10 po	Add 5-10 points depending on position of unstable layers in relation to bankfull stage,	n position of un	stable layers ir	relation to b	ankfull stage.			
Protection		,											
8	_	1	1.9	Very Low	Total Score	415							
80.0					Very Low	Low Low	Moderate	High	Very High	Extreme			
Materials:			10.0		5-95	55 10-19.5	20 - 29.5	30 - 39.5	40 - 45	46 - 50			
			c										
Strattfication:			8.0										
TOTAL SCORE:	ORE:		5113	Ехтете									

CHANNEL STABILITY (PFANKUCH) EVALUATION AND STREAM CLASSIFICATION SUMMARY

Cemetery Branch Reach Location 6/23/2005 Observers LT Date EXCELLENT CATEGORY UPPER 1 Landform Slope Bank Slope Gradient <30% BANKS Mass Wasting No evidence of past or future mass wasting. 3 Debris Jam Potential Essentially absent from immediate channel area. 90%+ plant density. Vigor and variety suggest a deep dense soil binding root mass. Vegetative Bank Protection Channel Capacity Ample for present plus some increases. Peak flows contained, W/D ratio <7. LOWER BANKS 65%+ with large angular boulders. 12"+ common. Bank Rock Content Rocks and logs firmly imbedded. Flow pattern without cutting or deposition. Stable bed. Obstructions to Flow 2 Cutting Deposition Little or none. Infreq. raw banks less than 6". Little or no enclargement of channel or pt. bars. BOTTOM 10 Rock Angularity Sharp edges and corners. Plane surfaces rough. Surfaces dull, dark or stained. Gen. not bright. 11 Brightness 12 Consolidation of Particles Assorted sizes tightly packed or overlapping. No size change evident. Stable mater. 80-100% 4 13 Bottom Size Distribution 14 Scouring and Deposition <5% of bottom affected by scour or deposition. 6 Abundant Growth moss-like, dark green perennial. In swift water too. 15 Aquatic Vegetation TOTAL CATEGORY GOOD UPPER Landform Slope Bank Slope Gradient 30-40% BANKS Mass Wasting Infrequent. Mostly healed over. Low future potential. 6 Debris Jam Potential Present, but mostly small twigs and limbs Vegetative Bank Protection 70-90% density. Fewer species or less vigor suggest less dense or deep root mass. 6 LOWER Channel Capacity Adequate. Bank overflows rare, W/D ratio 8-15 BANKS Bank Rock Content 40-65%. Mostly small boulders to cobbles 6-12" 4 Some present causing crosive cross currents and minor pool filling. Obstructions newer and less firm. Obstructions to Flow Some, intermittently at outcurves and constructions. Raw banks may be up to 12". 6 Cutting Some new bar increase, mostly from coarse gravel. 8 Deposition BOTTOM 10 Rock Angularity Rounded corners and edges, surfaces smooth, flat. 2 11 Brightness Mostly dull, but may have <35% bright surfaces. 2 12 Consolidation of Particles Moderately packed with some overlapping. Distribution shift light. Stable material 50-80%. 8 13 Bottom Size Distribution Scouring and Deposition
 Aquatic Vegetation 12 5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools: Common. Algae forms in low velocity and pool areas. Moss here too. TOTAL CATEGORY FAIR UPPER 1 Landform Slope Bank slope gradient 40-60% 6 Mass Wasting BANKS Frequent or large, causing sediment nearly year long. Debris Jam Potential Moderate to heavy amounts, mostly larger sizes. Vegetative Bank Protection <50-70% density. Lower vigor and fewer species from a shallow, discontinuous root mass. 9 LOWER Channel Capacity Barely contains present peaks. Occasional overbank floods. W/D ratio 15 to 25. 3 20-40% with most in the 3-6" diameter class. 6 BANKS Bank Rock Content Obstructions to Flow Moder. Frequent, unstable obstructions move with high flows causing bank curting and pool filling. Significant, Cuts 12-24" high. Root mat overhangs and sloughing evident. Cutting Deposition 12 Moderate deposition of new gravel and course sand on old and some new bars BOTTOM 10 Rock Angularity Corners and edges well rounded in two dimensions. 11 Brightness Mixture dull and bright, i.e. 35-65% mixture range: 12 Consolidation of Particles Mostly loose assortment with no apparent overlap. 6 12 13 Bottom Size Distribution Moderate change in sizes. Stable materials 20-50% 14 Scouring and Deposition15 Aquatic Vegetation 30-50% affected. Deposits & scour at obstructions, constructions, and bends. Some filling of pools. 18 Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick TOTAL CATEGORY POOR UPPER Landform Slope Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same BANKS Mass Wasting 12 Debris Jam Potential Moderate to heavy amounts, predom. larger sizes. 8 Vegetative Bank Protection < 50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, LOWER Channel Capacity Inadequate. Overbank flows common. W/D ratio >25 4 BANKS Bank Rock Content <20% rock fragments of gravel sizes, 1-3" or less. Frequent obstructions cause crosion year-long. Sediment traps full, channel migration occurring. Almost continuous cuts, some over 24" high. Failure of overhangs frequent. Obstructions to Flow 8 Cutting Deposition 16 Extensive deposits of predominately fin particles. Accelerated bar development. 16 BOTTOM Well rounded in all dimensions, surfaces smooth. 10 Rock Angularity 4 11 Brightness Predominately bright, 65%+ exposed or scoured surfaces. 4 12 Consolidation of Particles No packing evident. Loose assortment easily moved 13 Bottom Size Distribution Marked distribution change. Stable materials 0-20%. 16 14 Scouring and Deposition More than 50% of the bottom is a state of flux or change nearly year-long. 24 15 Aquatic Vegetation 4 Perennial types scarce or absent. Yellow-green, short term bloom may be present. TOTAL 117 Sum of Totals for Excellent, Good, Fair, and Poor Ratings Stream Type 154 Reach Condition Table for _E4__ Stream Type Reach Condition GOOD FAIR Remarkst

POOR

Stream:	Dye Branch	ranch	Reach/Station:	Reach 1	Cro	Cross Section:		āŪĀ.	Date:	3/14/05 Crew;	Crew:	LT, MA	VfA
Erodib	Erodibility Variable/Value	/Value	Index	Bank Erosion Potential									
Bank Height/Bankfull Height	ankfull Height									Bant Greeten Betential	Potential		
Bank Height (ft) A	Bankfull Height (ft) B	A/B	4.6	Moderate				Very Low	Low	Moderate	High	Very High	Extreme
3.0	3.0	1.3				Bank Height/	Value	13.01	1,11-1,19	12-15	1.6 - 2.0	21-28	>2.8
4.0	3.0	C.I				Bankfull Height	Index	01-01	20-39	4.0 - 5.9	6.0 - 7.9	0.6 - 0.8	10
Root Depth/Bank Height	nk Height				əld	Root Depth/	Value	1.0 - 0.9	0.89 - 0.5	0.49 - 0.3	0.29-0.15	0.14 - 0.05	<0.05
Roor Depth	.,,,				shaV	Bank Height	Index	61-01	20.39	4.0-5.9	60-19	8.0 - 9.0	10
C⊗ C	C/A	1	10.0	Extreme	իրուծ	Root Density	Value	1.0 - 1.9	20-39	4.0-5.9	67 - 69	8.0.9.0	92
21.0	7000	0			dib	Roof Acolo	Value	0-20	21 - 60	08 - 19	81 - 90	911-119	>119
0.13	+0.0				ээ	Daily Might	Index	10:10	20-39	4.0 - 5.9	6.0-7.9	8.0 - 9.0	01
Weighted Root Denrify	Density	X =			S	Surface Protection	Value	100 - 80	79 - 55	54-30	29 - 15	14-10	01×
Root Density	D*(C/A)						Index	1.0 - 1.9	20-39	4.0 - 5.9	6.0 - 7.9	8.0 - 9.0	10
G(%)		1	10.0	Extreme	Bank Materials	sterials		,					
0.75	0.03				Bedrock (Boulders (Bedrock (Bedrock banks have very low bank crosion potential) Boulders (Banks composed of boulders have low bank erosion potential)	e very low bank f boulders have	erosion potent low bank erosi	ial) on potential)	207			
Bank Angle		:			Cobble (S	Cobble (Subtract 10 points. If sand/gravel matrix greater than 50% of bank material, then do not adjust)	f sand/gravel m	atrix greater th	ian 50% of b.	ank material, th	hen do not ac	finst)	
Bank Angle (degrees)			6.8	High	Gravel (A Sand (Ade Silt/Clay (Gravel (Add 5-10 points depending on percentage of bank material that is composed of sand) Sand (Add 10 points if sand is exposed to erosional processes) Silt/Clay (+ 0: no adjustment)	ending on perceis s exposed to ero	ntage of bank sional process	material that: es)	is composed o	f sand)		
85.0				ŝ	Stratification	tion							
Surface Protection	· ·				Add 5-10	Add 5-10 points depending on postition of unstable layers in relation to bankfull stage.	n position of un	stable layers in	relation to b	ankfull stage.			
Surface					1								
(%)			1.9	Very Low	Total Score	ore							
80.0					17.0	Very Low Low	Maderate	High	Ver High	Extreme			
Materials:			10.0		10	5-9.5 10-19.5	20 - 29.5	30 - 39.5	40 - 45	46 - 50			
Stratification:			8.0										
TOTAL SCORE:	ORE:		51.4	Extreme									
					-								

CHANNEL STABILITY (PFANKUCH) EVALUATION AND STREAM CLASSIFICATION SUMMARY

arc	on	Dye Branch Reach 1	
	3/14/2005	Observers LT & MA	
	CATEGORY	EXCELLENT	
JPPER	1 Landform Slope	Bank Slope Gradient <30%	2
BANKS	2 Mass Wasting	No evidence of past or future mass wasting.	3
	3 Debris Jam Potential	Essentially absent from immediate channel area.	2
	4 Vegetative Bank Protection	90%+ plant density. Vigor and variety suggest a deep dense soil binding root mass.	3
OWER	5 Channel Capacity	Ample for present plus some increases. Peak flows contained. W/D ratio <7.	1
BANKS	6 Bank Rock Content	65%+ with large angular boulders. 12"+ common.	2
	7 Obstructions to Flow	Rocks and logs firmly imbedded. Flow pattern without cutting or deposition. Stable bed.	2
	8 Cutting	Little or none. Infreq. raw banks less than 6".	4
	9 Deposition	Little or no enclargement of channel or pt, bars.	- 4
BOTTOM	10 Rock Angularity	Sharp edges and corners. Plane surfaces rough.	- 4
Carlo Transco	11 Brighmess	Surfaces dull, dark or stained. Gen. not bright.	1
	12 Consolidation of Particles	Assorted sizes tightly packed or overlapping.	.2
	13 Bottom Size Distribution	No size change evident. Stable mater. 80-100%	- 4
	14 Scouring and Deposition	<5% of bottom affected by scour or deposition.	6
	15 Aquatic Vegetation	Abundant Growth moss-like, dark green perennial. In swift water too.	1
		TOTAL	_
	CATEGORY	GOOD	4
JPPER	1 Landform Slope	Bank Slope Gradient 30-40%	6
BANKS	2 Mass Wasting	Infrequent. Mostly healed over. Low future potential.	4
	3 Debris Jam Potential	Present, but mostly small twigs and limbs.	6
	4 Vegetative Bank Protection	70-90% density. Fewer species or less vigor suggest less dense or deep root mass.	2
LOWER	5 Channel Capacity	Adequate. Bank overflows rare. W/D ratio 8-15	4
BANKS	6 Bank Rock Content	40-65%. Mostly small boulders to cobbles 6-12"	4
	7 Obstructions to Flow	Some present causing erosive cross currents and minor pool filling. Obstructions newer and less firm.	6
	8 Cutting	Some, intermittently at outcurves and constructions. Raw banks may be up to 12".	8
	9 Deposition	Some new bar increase, mostly from coarse gravel.	
BOTTOM	10 Rock Angularity	Rounded corners and edges, surfaces smooth, flat.	2
	11 Brightness	Mostly dull, but may have <35% bright surfaces.	4
	 Consolidation of Particles 	Moderately packed with some overlapping.	8
	13 Bottom Size Distribution	Distribution shift light. Stable material 50-80%.	13
	14 Scouring and Deposition	5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools	2
	15 Aquatic Vegetation	Common. Algae forms in low velocity and pool areas. Moss here too. TOTAL	-
		FAIR	_
mnen	CATEGORY	Bank slope gradient 40-60%	6
UPPER	1 Landform Slope	Frequent or large, causing sediment nearly year long.	9
BANKS	2 Mass Wasting		-
	3 Debris Jam Potential	Moderate to heavy amounts, mostly larger sizes. <50-70% density. Lower vigor and fewer species from a shallow, discontinuous root mass.	9
	4 Vegetative Bank Protection	Barely contains present peaks. Occasional overbank floods. W/D ratio 15 to 25.	3
LOWER	5 Channel Capacity	20-40% with most in the 3-6" diameter class.	6
BANKS	6 Bank Rock Content	Moder. Frequent, unstable obstructions move with high flows causing bank cutting and pool filling.	6
	7 Obstructions to Flow	Moder. Frequent, unstable obstructions move with high nows existing same cutting and post timing.	1
	8 Cutting	Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident. Moderate deposition of new gravel and course sand on old and some new bars.	i
	9 Deposition	Moderate deposition of new graver and course sand on old and some new bars.	
BOTTOM	10 Rock Angularity	Corners and edges well rounded in two dimensions.	2
	11 Brightness	Mixture dull and bright, i.e. 35-65% mixture range.	i
	12 Consolidation of Particles	Mostly loose assortment with no apparent overlap.	
	13 Bottom Size Distribution	Moderate change in sizes. Stable materials 20-50%	1.
	14 Scouring and Deposition	30-50% affected. Deposits & scour at obstructions, constructions, and bends. Some filling of pools.	1
	A P. L. Company of Paris, and Company of the Compan	Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick.	
	15 Aquatic Vegetation	TOTAL	
		TOTAL,	
TIDDIFP	CATEGORY	POOR	
UPPER	CATEGORY 1 Landform Slope	POOR Bank slope gradient 60%+	
UPPER BANKS	CATEGORY 1 Landform Slope 2 Mass Wasting	POOR Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same,	
	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential	POOR Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same. Madesage to be any amounts, predom, larger sizes.	
BANKS	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential 4 Vegetative Bank Protection	POOR Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same. Moderate to heavy amounts, predom, larger sizes. <50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass,	
BANKS LOWER	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential 4 Vegetative Bank Protection 5 Channel Capacity	POOR Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same, Moderate to heavy amounts, predom, larger sizes. <50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, Inadequate. Overbank flows common. W/D ratio >25	
BANKS LOWER	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential 4 Vegetative Bank Protection 5 Channel Capacity 6 Bank Rock Content	POOR Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same, Moderate to heavy amounts, predom. larger sizes. <50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, Inadequate. Overbank flows common. W/D ratio >25 <20% rock fragments of gravel sizes, 1-3" or less.	
BANKS LOWER	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential 4 Vegetative Bank Protection 5 Channel Capacity 6 Bank Rock Content 7 Obstructions to Flow	POOR Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same, Moderate to heavy amounts, predom, larger sizes. <50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, Inadequate. Overbank flows common. W/D ratio >25 <20% rock fragments of gravel sizes, 1-3" or less. Frequent obstructions cause crossion year-long. Sediment traps full, channel migration occurring.	
BANKS LOWER	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential 4 Vegetative Bank Protection 5 Channel Capacity 6 Bank Rock Content 7 Obstructions to Flow 8 Cutting	Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same. Moderate to heavy amounts, predom. larger sizes. <50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, Inadequate. Overbank flows common. W/ID ratio >25 <20% rock fragments of gravel sizes, 1-3" or less. Frequent obstructions cause crossion year-long. Sediment traps full, channel migration occurring. Almost continuous cuts, some over 24" high. Failure of overhangs frequent.	
BANKS LOWER BANKS	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential 4 Vegetative Bank Protection 5 Channel Capacity 6 Bank Rock Content 7 Obstructions to Flow 8 Cutting 9 Deposition	Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same. Moderate to heavy amounts, predom. larger sizes. <50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, Inadequate. Overbank flows common. W/ID ratio >25 <20% rock fragments of gravel sizes, 1-3" or less. Frequent obstructions cause crosion year-long. Sediment traps full, channel migration occurring. Almost continuous cuts, some over 24" high. Failure of overhangs frequent. Fixtensive deposits of predominately fin particles. Accelerated bar development.	
BANKS LOWER BANKS	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential 4 Vegetative Bank Protection 5 Channel Capacity 6 Bank Rock Content 7 Obstructions to Flow 8 Cutting 9 Deposition 10 Rock Angularity	Bank slope gradient 60%+ Frequent of large, causing sediment nearly year long or imminent danger of same. Moderate to heavy amounts, predom. larger sizes. <50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, Inadequate. Overbank flows common. W/D ratio >25 <20% rock fragments of gravel sizes, 1-3" or less. Frequent obstructions cause crossion year-long. Sediment traps full, channel migration occurring. Almost continuous cuts, some over 24" high. Failure of overhangs frequent. Extensive deposits of preduminately fin particles. Accelerated bar development. Well rounded in all dimensions, surfaces smooth.	
BANKS LOWER BANKS	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential 4 Vegetative Bank Protection 5 Channel Capacity 6 Bank Rock Content 7 Obstructions to Flow 8 Cutting 9 Deposition 10 Rock Angularity 11 Brightness	Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same, Moderate to heavy amounts, predom, larger sizes. <50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, Inadequate. Overbank flows common: W/D ratio >25 <20% rock fragments of gravel sizes, 1-3" or less. Frequent obstructions cause crossion year-long. Sediment traps full, channel migration occurring. Almost continuous cuts, some over 24" high. Failure of overhangs frequent. Extensive deposits of predominately fin particles. Accelerated bar development. Well rounded in all dimensions, surfaces smooth. Predominately bright, 65%+ exposed or scoured surfaces	3
BANKS LOWER BANKS	CATEGORY 1 Landform Slope 2 Mass Wasting 3 Debris Jam Potential 4 Vegetative Bank Protection 5 Channel Capacity 6 Bank Rock Content 7 Obstructions to Flow 8 Cutting 9 Deposition 10 Rock Angularity 11 Brightness 12 Consolidation of Particles	Bank slope gradient 60%+ Frequent or large, causing sediment nearly year long or imminent danger of same. Moderate to heavy amounts, predom, larger sizes. <50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, Inadequate. Overbank flows common: W/D ratio >25 <20% rock fragments of gravel sizes, 1-3" or less. Frequent obstructions cause crosion year-long. Sediment traps full, channel migration occurring. Almost continuous curs, some over 24" high. Failure of overhangs frequent. Extensive deposits of predominately fin particles. Accelerated bar development. Well rounded in all dimensions, surfaces smooth. Predominately bright, 65%+ exposed or scoured surfaces No packing evident. Loose assortment easily moved	3
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Remarks:

FAIR POOR

Stream:	Dye Branch	ranch	Reach/Station:	Reach 2	×	Cross Section:		*****	Date:	3/14/05 Crew:	Crew:	LT,MA	MA
Erodibi	Erodibility Variable/Value	/Value	Index	Bank Erosion Potential									
Bank Height/Bankfull Height	mkfull Height									Back Perceion Decouried	Determinal		
Bank Height (ff) A	Bankfull Height (ft) B	A/B	4.6	Low				Very Low	Low	Moderate	High	Very High	Extreme
0.0	0+				1	Bank Height/	Value	1.0-1.1	111-119	12-15	1.6-20	21-28	>2.8
0.4	0.6	2				Bankfull Height	Index	1.0 - 1.9	2.0 - 3.9	4.0 - 5.9	60.19	80.90	10.
Root Depth/Bank Height	k Height				əld	Root Depth/	Value	10.09	50-680	0.49 - 0.3	0.29 - 0.15	0.14 0.05	<0.05
The Control of					lsize	Bank Height	Index	1.0 - 1.9	2.0-3.9	4.0 - 5.9	6,0-7.9	8.0 - 9.0	10
Moor Deput	C/A				ΛÝ	Weighted	Value	100 - 80	79 - 55	54:30	29 - 15	14 - 5.0	<5.0
26/			10.0	Extreme	illic	Root Density	Index	1.0 - 1.9	2.0-3.9	4.0 - 5.9	6.0 - 7.9	8.0 9.0	10.
200	0.04				lib	Beat, Ande	Value	0-20	23 - 60	61 - 80	81 - 90	911-116	>119
50.0	0.01				Ero	Dank Angie	Index	1.0 - 1.9	20-39	4.0 - 5.9	6.0 - 7.9	8.0~9.0	10
Weighted Root Density	tensity	9				Surface Protection	Value	100 - 80	79-55	\$.30	29 - 15	14 - 10	<10
Root Density							Index	1.0.1.9	20-3.9	4.0 - 5.9	6.0 - 7.9	8.0 - 9.0	10
(%) D	D-(C/A)		10.0	Ехиете	Bank	Bank Materials Bedrock (Bedrock banks have very low bank erosion potential)	very low bank	crosion poten	tial)				
0.6	0.01	l			Boulc	Boulders (Banks composed of boulders have low bank erosion potential)	f boulders have	low bank eros	ton potential				
Bank Angle					Cobb	Cobble (Subtract 10 points. If sand/gravel matrix greater than 50% of bank material, then do not adjust)	f sand/gravel m	arrix greater t	han 50% of b	ank material, t	then do not at	ijnst)	
Bank Angle (degrees)			5.9	Moderate	Sand Silt/C	Gravel (Add 5-10 points depending on percentage of bank material that is composed of sand) Sand (Add 10 points if sand is exposed to erosional processes) Silt/Clay (+ 0: no adjustment)	nding on perces exposed to ero	ntage of bank sional process	material that es)	s composed c	of sand)		
80.0					Strati	Stratification							
Surface Protection Surface	- in-				Add	Add 5-10 points depending on position of unstable layers in relation to bankfull stage.	n position of un	stable layers in	relation to b	ankfull stage.			
Protection		4			L								
(%)			9.0	Very High	Tota	Total Score Very Low	Moderate	High	Ver High	Extreme			
Materials:			10:0			5-9.5 10-19.5	20 - 29.5	30 - 39.5	40 - 45	46 - 30			
Stratification:			8.0		-								
TOTAL SCORE:	ORE:		57.5	Ехиете									
					_								

CHANNEL STABILITY (PFANKUCH) EVALUATION AND STREAM CLASSIFICATION SUMMARY

Dye Branch Reach 2 Reach Location 3/14/2005 Observers LT, MA Date EXCELLENT CATEGORY UPPER Landform Slope Bank Slope Gradient < 30% BANKS No evidence of past or future mass wasting. Mass Wasting Debris Jam Potential Essentially absent from immediate channel area. 90%+ plant density. Vigor and variety suggest a deep dense soil binding root mass. Vegetative Bank Protection Channel Capacity LOWER Ample for present plus some increases. Peak flows contained. W/D ratio <7. 65%+ with large angular boulders, 12"+ common. BANKS Bank Rock Content Rocks and logs firmly imbedded. Flow pattern without cutting or deposition. Stable bed. 2 Obstructions to Flow Little or none. Infreq. raw banks less than 6". Cutting Deposition Little or no enclargement of channel or pt. bars BOTTOM 10 Rock Angularity Sharp edges and corners. Plane surfaces rough. Surfaces dull, dark or stained. Gen. not bright. 11 Brightness 12 Consolidation of Particles Assorted sizes tightly packed or overlapping. No size change evident. Stable mater. 80-100% 13 Bottom Size Distribution 14 Scouring and Deposition <5% of bottom affected by scour or deposition. 6 15 Aquatic Vegetation Abundant Growth moss-like, dark green perennial. In swift water too. TOTAL GOOD CATEGORY UPPER Landform Slope Bank Slope Gradient 30-40% 6 BANKS Mass Wasting Infrequent. Mostly healed over. Low future potential. Debris Jam Potential Present, but mostly small twigs and limbs. 70-90% density. Fewer species or less vigor suggest less dense or deep root mass. Vegetative Bank Protection 6 LOWER Channel Capacity Adequate. Bank overflows rare. W/D ratio 8-15 2 40-65%. Mostly small boulders to cobbles 6-12" 4 BANKS Bank Rock Content Some present causing crosive cross currents and minor pool filling. Obstructions newer and less firm. Obstructions to Flow 6 Cutting Some, intermittently at outcurves and constructions. Raw banks may be up to 12". 8 Deposition some new bar increase, mostly from coarse gravel. 10 Rock Angularity Rounded corners and edges, surfaces smooth, flat. 2 11 Brightness Mostly dull, but may have <35% bright surfaces. 2 Moderately packed with some overlapping. 12 Consolidation of Particles Distribution shift light. Stable material 50-80%. 13 Bottom Size Distribution 5-30% affected. Scour at constrictions and where grades steepen. Some deposition in pools 12 14 Scouring and Deposition 15 Aquatic Vegetation Common. Algae forms in low velocity and pool areas. Moss here too. TOTAL CATEGORY FAIR HPPER 1 Landform Slope Bank slope gradient 40-60% 6 Frequent or large, causing sediment nearly year long. BANKS Mass Wasting Debris Jam Potential Moderate to heavy amounts, mostly larger sizes. <50-70% density. Lower vigor and fewer species from a shallow, discontinuous root mass. 9 Vegetative Bank Protection LOWER Channel Capacity Barely contains present peaks. Occasional overbank floods. W/D ratio 15 to 25. 6 BANKS Bank Rock Content 20-40% with most in the 3-6" diameter class. Moder. Frequent, unstable obstructions move with high flows causing bank cutting and pool filling. Obstructions to Flow Significant. Cuts 12-24" high. Root mat overhangs and sloughing evident. 12 Cutting Moderate deposition of new gravel and course sand on old and some new bars Deposition BOTTOM 10 Rock Angularity Corners and edges well rounded in two dimensions. 11 Brightness Mixture dull and bright, i.e. 35-65% mixture range. à 12 Consolidation of Particles 6 Mostly loose assortment with no apparent overlap. 12 Moderate change in sizes. Stable materials 20-50% 13 Borrom Size Distribution 30-50% affected. Deposits & scour at obstructions, constructions, and bends. Some filling of pools. Scouring and Deposition
 Aquatic Vegetation 18 Present but spotty, mostly in backwater. Seasonal algae growth makes rocks slick. TOTAL CATEGORY POOR Bank slope gradient 60%+ UPPER Landform Slope Frequent or large, causing sediment nearly year long or imminent danger of same. 12 BANKS Mass Wasting Debris Jam Potential 8 Moderate to heavy amounts, predom, larger sizes. 50% density. Fewer species and less vigor indicate poor, discontinuous and shallow root mass, Vegetative Bank Protection LOWER Channel Capacity Inadequate. Overbank flows common. W/D ratio >25 <20% rock fragments of gravel sizes, 1-3" or less. BANKS Bank Rock Content Obstructions to Flow Frequent obstructions cause erosion year-long. Sediment traps full, channel migration occurring. Almost continuous cuts, some over 24" high. Failure of overhangs frequent Cutting 16 Extensive deposits of predominately fin particles. Accelerated bar development. 16 Deposition BOTTOM 10 Rock Angularity Well rounded in all dimensions, surfaces smooth. 11 Brightness Predominately bright, 65% * exposed or scoured surfaces 12 Consolidation of Particles No packing evident. Loose assortment easily moved 8 16 13 Bottom Size Distribution Marked distribution change. Stable materials 0-20%. 14 Scouring and Deposition 15 Aquatic Vegetation 24 More than 50% of the bottom is a state of flux or change nearly year-long. Perennial types scarce or absent. Yellow-green, short term bloom may be present. TOTAL 125 Sum of Totals for Excellent, Good, Fair, and Poor Ratings Stream Type Reach Condition Table for Reach Condition Stream Type GOOD

Remarks

FAIR

POOR

Stream:	Dye Branch	ranch	Reach/Station:	Reach 3	O	Cross Section:			Date:	3/14/05 Crew:	Crew;	LT, MA	WA
Erodibi	Erodibility Variable/Value	/Value	Index	Bank Erosion Potential									
Bank Heggit/ Bankfull Heggit	mkţuli Hegbi				L					Bank Erosion Potential	n Potential		
Bank Height (ft) A	Bankfull Height (ft) B	A/B	5.3	Moderate				Very Low	Low	Moderate	High	Very High	Extreme
						Bank Height/	Value	1.0 - 1.1	1111-1119	12-1.5	1.6 - 2.0	21-28	8'2<
7.0	5.0	1.4				Bankfull Height	Index	1.0 - 1.9	20.39	4.0 - 5.9	67:09	80.90	10
Root Depth/Bank Height	k Height				əld	Root Depth/	Value	6'0 + 9'1	50-680	0.49 - 0.3	0.29 - 0.15	0.14 - 0.05	<0.05
Description of					she	Bank Height	Index	1.6 - 1.9	20.39	4.0-5.9	6.0 - 7.9	8.0 - 9.0	10
Moot Depm	C/A				ΛÁ	Weighted	Value	100 - 80	79 - 55	54-30	29 - 15	14.50	0°50
2 (0/2)			10.0	Extreme	illic	Root Density	Index	1.0 - 1.9	20-3.9	4.0 - 5.9	6.0 - 7.9	8.0 - 9.0	10
40.0	0.00				libo	Book Amelia	Value	0.20	21-60	01 - 8ti	81 - 90	91 - 119	>119
0.25	40.0				ыЭ	Dank Angre	Index	1.0-1.9	20-39	4.0 - 5.9	6.0 - 7.9	8.09.0	10
Weighted Root Density	Pensity					C of Description	Value	08 - 001	79 - 55	54-30	29:15	14 - 10	< 10
		F				Surface Protection	Index	1.0 < 1.9	2.0-3.9	4.0 - 5.9	67:09	8.0 - 9.0	10
(%) D	D*(C/A)	1	10.0	Extreme	Bank	Bank Materials	d an also						
0.3	0.01				Boulde	Bedrock (Bedrock banks have very low bank erosion potential) Boulders (Banks composed of boulders have low bank erosion potential)	e very low bank f boulders have	erosion potent low bank erosi	ial) on potential)	=			
Bank Angle					Cobble	Cobble (Subtract 10 points. If sand/gravel matrix greater than 50% of bank material, then do not adjust)	f sand/gravel m	atrix greater th	ran 50% of b	ank material, th	hen do not ad	(lnst)	
Bank Angle (degrees)			5.9	Moderate	Grave Sand (Silt/Cl	Gravel (Add 5-10 points depending on percentage of bank material that is composed of sand) Sand (Add 10 points if sand is exposed to erosional processes) Sit/Clay (+ 0, no adjustment)	ending on perce s exposed to ero	ntage of bank a	material that ces)	s composed o	f sand)		
80.0		(S			Stratif	Stratification							
Surface Protection					Add 5	Add 5-10 points depending on position of unstable layers in relation to bankfull stage.	n position of un	stable layers in	relation to b	ankfull stage.			
Surface													
(%)			52	High	Total Score	Score							
25.0				0		Very Low Low	Moderate	High	Very High	Extreme			
Materials:			10.0			5-9.5 10-19.5	30-29.5	30-39,5	40 - 45	46 - 50			
Stratification:			0.0										
TOTAL SCORE:	ORE:		56.7	Extreme									

CHANNEL STABILITY (PFANKUCH) EVALUATION

AND STREAM CLASSIFICATION SUMMARY Dye Branch Reach 3 Reach Location 3/14/2005 LT, MA Observers Date EXCELLENT CATEGORY UPPER 1 Landform Slope Bank Slope Gradient <30% No evidence of past or future mass wasting. BANKS Mass Wasting Essentially absent from immediate channel area. 2 Debris Jam Potential 90%+ plant density. Vigor and variety suggest a deep dense soil binding root mass Vegetative Bank Protection Ample for present plus some increases. Peak flows contained. W/D ratio <7. LOWER Channel Capacity 65%+ with large angular boulders. 12"+ common. BANKS Bank Rock Content Rocks and logs firmly imbedded. Flow pattern without cutting or deposition. Stable bed. Obstructions to Flow 4 Little or none. Infreq. raw banks less than 6". Cutting Deposition ittle or no enclargement of channel or pt. bars. 10 Rock Angularity Sharp edges and corners. Plane surfaces rough. BOTTOM Surfaces dull, dark or stained. 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Reach Condition Table for Stream Type GOOD FAIR POOR

Reach Condition

Remarks:

DATA FORM ROUTINE WETLAND DETERMINATION (1987 COE Wetlands Delineation Manual)

	on reverse)	Yes	s No	Date: County: State: Community Transect ID: Plot ID:		Wetland WA
Dominant Plant Sp		m <u>Indicator</u>	Dominar	nt Plant Species	Stratum	Indicator
1. Festuca spp.	<u>herb</u>	FACU	9.		····	
2. Juncus effusus	<u>herb</u>	FACW+	10			
3. <u>Lonicera japonio</u>	ica herb	FAC-				
4. Sambucus canad	densis shrub	FACW-				
5. <u>Salix nigra</u>	tree	OBL				
6.						
	Species that are OBL, FACW mature trees. Mostly domin	-	AC-).	60%		
HYDROLOGY	7					
Recorded Data (I	Describe in Remarks) cam, Lake, or tide Gauge ial Photographs er		Wetland Hydrology Indicators: Primary Indicators: Inundated x Saturated in Upper 12 Inches Water Marks Drift Lines			
Field Observations:				Sediment Deposits Drainage Patterns in		
Depth of Surface V	Water:(in.))		ary Indicators (2 or mor Oxidized Root Chann Water-Stained Leaves	nels in Upper	
Depth to Free Wate				Local Soil Survey Da FAC-Neutral Test Other (Explain in Rei	ıta	
Remarks:	2-41			-		

SOILS

Map Unit (Series and		Colfax sandy loa	m	Drainage Class: <u>Som</u> Field Observations	ewhat Poorly Drained
Taxonomy (S	ubgroup) <i>Fine-lo</i>	amy, mixed, subactive, th	ermic Aquic Fragiudui		e? Yes No
Profile Descri Depth (inches)	ption: <u>Horizon</u>	Matrix Color (Munsell Moist)	Mottle Colors (Munsell Moist)	Mottle Abundance/Contrast	Texture, Concretions, Structure, etc.
0 to 3	A	10YR 4/3	7.5YR 4/6	common/distinct	silt loam
3 to 8	<i>B</i>	2.5YR 4/6	7.5YR 4/1	many/prominent	loam
8 to 12+	Bt	7.5YR 4/1	2.5YR 4/6	many/prominent	loam
					
Hi: Su Aq Re	dicators: stosol stic Epipedon lfidic Odor quic Moisture Reg ducing Condition eyed or Low-Chro	s		Concretions High Organic Content Organic Streaking in S x Listed on Local Hydri Listed on National Hy Other (Explain in Res	c Soils List dric Soils List
WETLAN	ND DETERM	MINATION			
	Vegetation Presen ology Present? Present?	Yes	do I.	s this Sampling Point Within a Wetla	and? <u>Yes</u> No
Remarks: Sau	mpling point was	approximatley 8 ft. down	slope from WA2.		



The EDR Radius Map with GeoCheck®

Dye Branch Glenwood Memorial Park MOORESVILLE, NC 28115

Inquiry Number: 01415917.1r

May 06, 2005

The Standard in Environmental Risk Management Information

440 Wheelers Farms Road Milford, Connecticut 06460

Nationwide Customer Service

Telephone: 1-800-352-0050 Fax: 1-800-231-6802 Internet: www.edrnet.com

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Thank you for your business. Please contact EDR at 1-800-352-0050 with any questions or comments.

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EXECUTIVE SUMMARY

A search of available environmental records was conducted by Environmental Data Resources, Inc. (EDR). The report meets the government records search requirements of ASTM Standard Practice for Environmental Site Assessments, E 1527-00. Search distances are per ASTM standard or custom distances requested by the user.

TARGET PROPERTY INFORMATION

ADDRESS

GLENWOOD MEMORIAL PARK MOORESVILLE, NC 28115

COORDINATES

Latitude (North):

35.576200 - 35" 34' 34.3"

Longitude (West):

80.812500 - 80* 48' 45.0"

Universal Tranverse Mercator: Zone 17 UTM X (Meters): UTM Y (Meters):

516989.3 3936761.5

Elevation:

834 ft. above sea level

USGS TOPOGRAPHIC MAP ASSOCIATED WITH TARGET PROPERTY

Target Property:

35080-E7 MOORESVILLE, NC

Source:

USGS 7.5 min quad index

TARGET PROPERTY SEARCH RESULTS

The target property was not listed in any of the databases searched by EDR.

DATABASES WITH NO MAPPED SITES

No mapped sites were found in EDR's search of available ("reasonably ascertainable ") government records either on the target property or within the ASTM E 1527-00 search radius around the target property for the following databases:

FEDERAL ASTM STANDARD

NPL..... National Priority List

Proposed NPL Proposed National Priority List Sites

System

CERC-NFRAP...... CERCLIS No Further Remedial Action Planned

CORRACTS..... Corrective Action Report

RCRA-TSDF...... Resource Conservation and Recovery Act Information RCRA-LQG Resource Conservation and Recovery Act Information RCRA-SQG....... Resource Conservation and Recovery Act Information

ERNS Emergency Response Notification System

STATE ASTM STANDARD

SHWS..... Inactive Hazardous Sites Inventory

EXECUTIVE SUMMARY

SWF/LF.....List of Solid Waste Facilities

UST...... Petroleum Underground Storage Tank Database

OLI...... Old Landfill Inventory

VCP....... Responsible Party Voluntary Action Sites

INDIAN LUST. Leaking Underground Storage Tanks on Indian Land

INDIAN UST...... Underground Storage Tanks on Indian Land

FEDERAL ASTM SUPPLEMENTAL

CONSENT Superfund (CERCLA) Consent Decrees

ROD...... Records Of Decision

Delisted NPL...... National Priority List Deletions

FINDS...... Facility Index System/Facility Identification Initiative Program Summary Report

HMIRS...... Hazardous Materials Information Reporting System

MLTS..... Material Licensing Tracking System

MINES..... Mines Master Index File NPL Liens...... Federal Superfund Liens PCB Activity Database System US ENG CONTROLS..... Engineering Controls Sites List ODI Open Dump Inventory UMTRA...... Uranium Mill Tailings Sites FUDS. Formerly Used Defense Sites INDIAN RESERV. Indian Reservations

DOD...... Department of Defense Sites

RAATS......RCRA Administrative Action Tracking System TRIS...... Toxic Chemical Release Inventory System

TSCA..... Toxic Substances Control Act SSTS..... Section 7 Tracking Systems

STATE OR LOCAL ASTM SUPPLEMENTAL

NC HSDS...... Hazardous Substance Disposal Site

AST...... AST Database DRYCLEANERS Drycleaning Sites

EDR PROPRIETARY HISTORICAL DATABASES

Coal Gas Former Manufactured Gas (Coal Gas) Sites

BROWNFIELDS DATABASES

US BROWNFIELDS..... A Listing of Brownfields Sites US INST CONTROL..... Sites with Institutional Controls Brownfields Brownfields Projects Inventory

VCP...... Responsible Party Voluntary Action Sites

SURROUNDING SITES: SEARCH RESULTS

Surrounding sites were identified.

EXECUTIVE SUMMARY

Elevations have been determined from the USGS Digital Elevation Model and should be evaluated on a relative (not an absolute) basis. Relative elevation information between sites of close proximity should be field verified. Sites with an elevation equal to or higher than the target property have been differentiated below from sites with an elevation lower than the target property. Page numbers and map identification numbers refer to the EDR Radius Map report where detailed data on individual sites can be reviewed.

Sites listed in bold italics are in multiple databases.

Unmappable (orphan) sites are not considered in the foregoing analysis.

STATE ASTM STANDARD

LUST: The Leaking Underground Storage Tank Incidents Management Database contains an inventory of reported leaking underground storage tank incidents. The data come from the Department of Environment, & Natural Resources' Incidents by Address.

A review of the LUST list, as provided by EDR, and dated 03/04/2005 has revealed that there are 7 LUST sites within approximately 0.5 miles of the target property.

Equal/Higher Elevation Address Dist / Dir Map ID	
MOORESVILLE TOWN LIBRARY 121 EAST CATAWBA AVE 1/4 - 1/2NW 1	6
BURLINGTON MILLS 476 SOUTH MAIN STREET 1/4 - 1/2 WNW A3	9
BILLS EXXON(MOORESVILLE QUICKL 204 S. MAIN ST, MOORESV 1/4 - 1/2 NNW 4	11
GLASPY'S AUTO SERVICE 152 SOUTH MAIN STREET 1/4 - 1/2N B5	13
SHEPHERD'S 126 EAST CENTER AVENUE 1/4 - 1/2N 6	18
MOORESVILLE AMOCO SERVICE 151 S BROAD ST 1/4 - 1/2N B7	25
J.T. ALEXANDER HWY 115 N 1/4 - 1/2 NNW 9	34

STATE OR LOCAL ASTM SUPPLEMENTAL

LUST TRUST: This database contains information about claims against the State Trust Funds for reimbursements for expenses incurred while remediating Leaking USTs.

A review of the LUST TRUST list, as provided by EDR, and dated 03/11/2005 has revealed that there is 1 LUST TRUST site within approximately 0.5 miles of the target property.

Equal/Higher Elevation	Address	Dist / Dir	Map ID	Page
CARPET DEPOT	239 WEST CENTER STREET	1/4 - 1/2N	10	36

IMD: Incident Management Database.

A review of the IMD list, as provided by EDR, and dated 06/15/2004 has revealed that there are 9 IMD sites within approximately 0.5 miles of the target property.

Equal/Higher Elevation	Address	Dist / Dir	Map ID	Page
MOORESVILLE TOWN LIBRARY	121 EAST CATAWBA AVE	1/4 - 1/2 NW	1	6
BURLINGTON INDUSTRIES	476 SOUTH MAIN STREET	1/4 - 1/2 WNW	A2	8
BURLINGTON MILLS	476 SOUTH MAIN STREET	1/4 - 1/2 WNW	/ A3	9

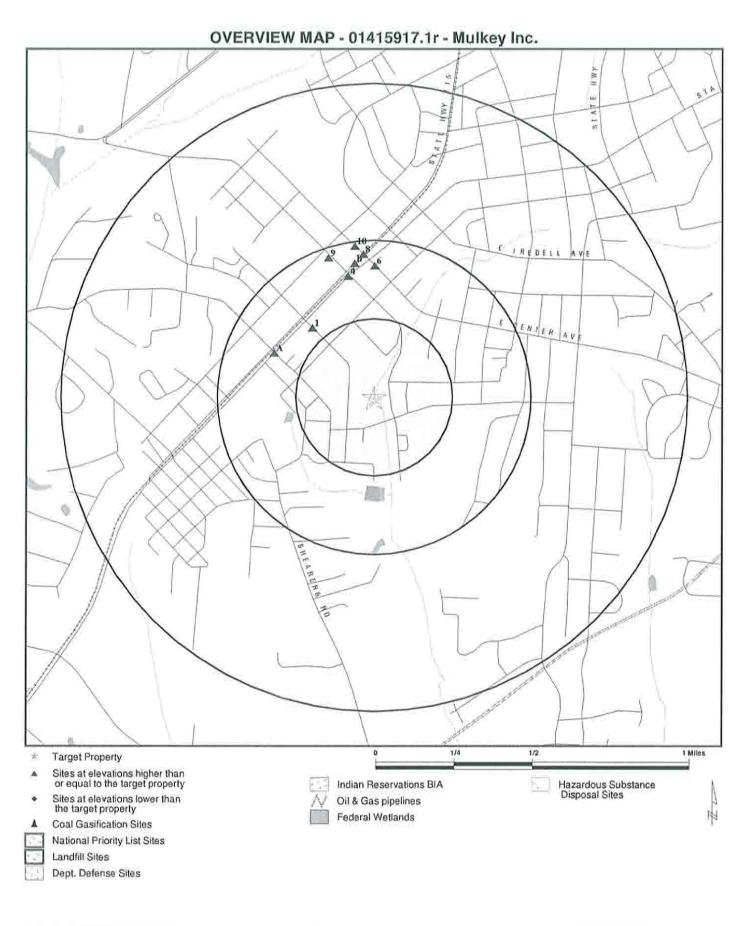
EXECUTIVE SUMMARY

Equal/Higher Elevation	Address	Dist / Dir	Map ID	Page
BILLS EXXON(MOORESVILLE QUICKL	204 S. MAIN ST, MOORESV	1/4 - 1/2 NNW	4	11
GLASPY'S AUTO SERVICE	152 SOUTH MAIN STREET	1/4 - 1/2 N	B5	13
SHEPHERD'S	126 EAST CENTER AVENUE	1/4 - 1/2 N	6	18
MOORESVILLE AMOCO SERVICE	151 S BROAD ST	1/4 - 1/2 N	B7	25
SERVICE AUTO SUPPLY	101 SOUTH BROAD STREET	1/4 - 1/2 N	8	33
J.T. ALEXANDER	HWY 115 N	1/4 - 1/2 NNW	9	34

EXECUTIVE SUMMARY

Due to poor or inadequate address information, the following sites were not mapped:

Site Name	Database(s)
OLD MOORE PLACE	IMD, LUST
IREDELL MILK TRANSPORTATION #2	IMD, LUST
SUPERBA PRINT WORKS	RCRA-SQG, IMD, LUST
COUNTRY CORNER MARINA	IMD, LUST
FRIENDLY FARE GROCERY (CAPPI'S)	LUST
CURT'S KWICK STOP	LUST
RUN IN STORE HWY 21	LUST
CASHION FAMILY FARM, FORMER	IMD, LUST
KEENER - GOODSON PROPERTY	IMD, LUST
CARISBROOK IND.	IMD, LUST
SUPERBA PRINT WORKS	LUST TRUST
WILCO SERVICE STATION HIGHWAY 150	LUST TRUST
PHIFER J JOHNSON BULLDOZING I	UST
M B OVERCASH	UST
REAL CHICKEN INC	UST
COOK'S AUTOMOTIVE	UST
CLYLE II	UST
J.T. SMITH STORE	UST
CATAWBA TIMBER CO. MOORESVILL	UST
GENERAL STORE	UST
SOUTHERN CONV 185-23623	UST
BRAWLEY CONST. CO.	UST
FRIENDLY FARE GROCERY	UST
RUN-IN HIGHWAY 21 (HILLTOP 66	UST
WILLIAM C. WALLER	UST
KEN F. SMITH'S GROCERY	UST
MRS. R.E. BUMGARDNER	UST
SHINN'S STORE	UST
TRADING POST	UST
LARRY HUDSON / TRADING POST	UST
SLOAN C. BROTHERTON	UST
SUPERBA PRINT WORKS	RCRA-SQG, FINDS
PHIL WILL ENTERPRISES	RCRA-SQG, FINDS
MOTORSPORTS FABRICATION	RCRA-SQG, FINDS
BEN HESS MOTOR SPORTS LTD	RCRA-SQG, FINDS IMD
FLAGSHIP AIRLINES MAINT FACILI	IMD
AEROQUIP CORP	IMD
E.F. BELK & SONS	IMD
MELCHOR PROPERTY	IMD
PARKER HANNIFIN #2	IMD
PARKER HANNIFIN FRIENDLY FARE GROCERY (NO FILE	IMD
MOORESVILLE DUMP	OLI
MOUNESVILLE DOMF	OL!



TARGET PROPERTY: Dye Branch
ADDRESS: Glenwood Memorial Park
CITY/STATE/ZIP: MOORESVILLE NC 28115
LAT/LONG: 35.5762 / 80.8125

CUSTOMER: Mulkey Inc.
CONTACT: Layna Thrush
INQUIRY #: 01415917.1r
DATE: May 06, 2005 1:29 pm

DETAIL MAP - 01415917.1r - Mulkey Inc. CENTERAVE E CENTER AVE SHARPE ST SHARPE ST E MICLELLAND AVE E CATAWBA, AVE 13 34416 CABARRUS AVE CADARRUS AVE FRE E LUIA INAEMMASIGEDAY CARE IICME CARARRUS AVE CABARRUS AVE CABARRUS AVE AVE BILLEF RD E WILSON AVE E CATAWBA AVE EGE ST WATER ST WATERS WATER ST AVE ON 1/16 1/8 1/4 Miles Target Property Sites at elevations higher than or equal to the target property Hazardous Substance Disposal Sites Indian Reservations BIA Sites at elevations lower than Oil & Gas pipelines the target property Federal Wetlands Coal Gasification Sites Sensitive Receptors National Priority List Sites Landfill Sites Dept. Defense Sites TARGET PROPERTY: ADDRESS: Dye Branch Glenwood Memorial Park MOORESVILLE NC 28115 CUSTOMER:

CITY/STATE/ZIP: LAT/LONG:

35.5762 / 80.8125

CONTACT: INQUIRY #: DATE:

Mulkey Inc. Layna Thrush 01415917.1r

May 06, 2005 1:29 pm

MAP FINDINGS SUMMARY

Database	Target Property	Search Distance (Miles)	< 1/8	1/8 - 1/4	1/4 - 1/2	1/2 - 1	<u>> 1</u>	Total Plotted
FEDERAL ASTM STANDAR	RD							
NPL Proposed NPL CERCLIS CERC-NFRAP CORRACTS RCRA TSD RCRA Lg. Quan. Gen. RCRA Sm. Quan. Gen. ERNS		1.000 1.000 0.500 0.250 1.000 0.500 0.250 0.250 TP	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 R 0 0 R R R R	O O O R NR O R NR NR NR NR	NR N	0 0 0 0 0 0 0 0 0 0 0 0
STATE ASTM STANDARD								
State Haz. Waste State Landfill LUST UST OLI VCP INDIAN LUST INDIAN UST		1.000 0.500 0.500 0.250 0.500 0.500 0.500 0.250	0 0 0 0 0 0	0 0 0 0 0	0 0 7 NR 0 0 0 NR	22222222222222222222222222222222222222	NR NR NR NR NR NR NR NR	0 7 0 0 0
FEDERAL ASTM SUPPLEM	IENTAL							
CONSENT ROD Delisted NPL FINDS HMIRS MLTS MINES NPL Liens PADS US ENG CONTROLS ODI UMTRA FUDS INDIAN RESERV DOD RAATS TRIS TSCA SSTS FTTS		1.000 1.000 1.000 TP TP TP 0.250 TP 0.500 0.500 0.500 1.000 1.000 TP TP TP	22222000000222222 222222000002222222	ZZZZZ000000ZZZ0ZZZ000	ZZZZZZ00000ZZZZZZZZZZZ	222222222222222222222222222222222222222	ZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZZ	000000000000000000000000000000000000000
STATE OR LOCAL ASTM S	UPPLEMENTA	=						
NC HSDS		1.000	O	0	0	0	NR	0

MAP FINDINGS SUMMARY

	Farget Property	Search Distance (Miles)	< 1/8	1/8 - 1/4	1/4 - 1/2	1/2 - 1	> 1	Total Plotted
AST		TP	NR	NR	NR	NR	NR	0
LUST TRUST		0.500	0	0	1	NR	NR	
DRYCLEANERS		0.250	0	0	NR	NR	NR	0
IMD		0.500	0	0	9	NR	NR	9
EDR PROPRIETARY HISTORIC	AL DATAB	ASES						
Coal Gas		1.000	0	0	0	0	NR	0
BROWNFIELDS DATABASES								
US BROWNFIELDS		0.500	0	0	0	NR	NR	0
US INST CONTROL		0.500	0	0	O	NR	NR	0 0 0
Brownfields		0.500	0	0	0	NR	NR	0
INST CONTROL		0.500	O	0	O	NR	NR	0
VCP		0.500	O	0	0	NR	NR	0

NOTES:

AQUIFLOW - see EDR Physical Setting Source Addendum

TP = Target Property

NR = Not Requested at this Search Distance

Sites may be listed in more than one database

Map ID
Direction
Distance
Distance (ft.)
Elevation Site

45 Day Report:

Close-out Report: Not reported

Not reported

Database(s)

EDR ID Number EPA ID Number

Coal Gas Site Search: No site was found in a search of Real Property Scan's ENVIROHAZ database.

MOORESVILLE TOWN LIBRARY IMD S105764931 NW 121 EAST CATAWBA AVE LUST N/A 1/4-1/2 MOORESVILLE, NC 28115 1565 ft. LUST: Relative: Incident Number: 27382 Date Occurred: 1/9/2003 Higher 5 Min Quad: Lat/Long: 353446 / 804857 Not reported Actual: Source Type: Leak-underground Region: Mooresville 911 ft. GPS Confirmed: Facility ID: Not reported No UST Number: MO-6647 Testlat: Not reported Product Type: Petroleum Date Reported: 1/9/2003 Responsible Party: Company: TOWN OF MOORESVILLE Contact Person: ERSKINE SMITH 413 N MAIN STREET Address: City/Stat/Zip: MOORESVILLE, NC 28115 County: Not reported Comm / Non-comm UST Site: Non commercial Tank Regulated Status: Non Regulated Regional Officer Project Mgr: ARL Risk Classification: Risk Classification Based On Review: Corrective Action Plan Type: Not reported Level Of Soil Cleanup Achieved: soil to GW levels Closure Request Date: Not reported Close Out: 5/22/2003 Contamination Type: NORR Issued Date: Not reported NOV Issued Date: Not reported Phase Of LSA Reg: Not reported Site Risk Reason: Not reported Land Use: Residential MTBE: # Of Supply Wells: 0 0 7046633800 Telephone: Flag: Error Flag: LUR Filed: Not reported 0 Error Code: Not reported LUR Filed: Not reported Valid: No Total Tanks: MTBE1: Unknown Flag1: No Cleanup: 1/9/2003 Current Status: File Located in House RBCA GW: Not reported PETOPT: 4 CD Num: Reel Num: 0 RPOW: RPOP: No Yes RPL: Yes Not reported Type: Ownership: Private Location: Residence Owner/Operator: Not reported Operation Type: Residential Site Priority: Not reported Priority Update: Not reported Wells Affected: Wells Affected #: Not reported Samples Taken: Yes Samples Include: Error Type: 5minguad: Not reported Not reported Incident Description: SOIL CONTAMINATION WAS DISCOVERED ADJACENT TO A HOME HEATING OIL UST. Last Modified: 5/22/2003 Incident Phase: Closed Out NORR Issued: NOV Issued: Not reported Not reported

SOC Sighned:

RS Designation:

Not reported

Not reported

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number **EPA ID Number**

S105764931

MOORESVILLE TOWN LIBRARY (Continued)

Public Meeting Held: Not reported Corrective Action Planned: Not reported Reclassification Report: Not reported Closure Request Date: Not reported

Comments: Not reported

IMD:

Incident Number: 27382 MOR Region: Date Occurred: 01/09/03 01/09/03 Submit Date: GW Contam: No Soil Contam: Yes

ERSKINE SMITH Operator:

413 N MAIN STREET

MOORESVILLE, NC 28115

Contact Phone: 7046633800 Priority Code: Not reported

Priority Update:

Site Priority: Not reported ARL Dem Contact: Wells Affected: No Num Affected:

Sampled By: Samples Include: 7.5 Min Quad: Not reported 5 Min Quad: Not reported

SOIL CONTAMINATION WAS DISCOVERED ADJACENT TO A HOME HEATING OIL UST. Incident Desc:

Agency:

Last Modified

Ownership: Private Operation: Residential Not reported Material: Qty Lost: Not reported Not reported Qty Recovered: Source: Leak-underground Gasoline/diesel Type: Location: Residence Setting: Not reported Wells Contam: Not reported

Sampled By: Samples Include: S

Owner Company: TOWN OF MOORESVILLE 353446 / 804857

Lat/Long:

Risk Site

Lat/Long Decimal: 35.57944 / 80.81583 Lat/Long Number 353446 / 804857

EST Incident Phase: Closed Out

NOV Issued: SOC Sighned: 45 Day Report:

Public Meeting Held: Corrective Action Planned: / /

Reclassification Report:

RS Designation: 11 Close-out Report: / / Closure Request Date:

Not reported

05/22/03

11

Map ID Direction Distance Distance (ft.)

Close-out Report: / /

Closure Request Date:

11

EDR ID Number **EPA ID Number**

Elevation Database(s) A2 BURLINGTON INDUSTRIES IMD S105425771 WNW **476 SOUTH MAIN STREET** N/A 1/4-1/2 MOORESVILLE, NC 1839 ft. Site 1 of 2 in cluster A Relative: IMD: Higher Incident Number: 86089 Actual: Region: MOR 923 ft. Date Occurred: 11/13/01 Submit Date: 02/01/02 GW Contam: Yes Soil Contam: Not reported Operator: 702 OBERLIN ROAD, SUITE 150 RALEIGH Contact Phone: Not reported Priority Code: Priority Update: 11 Site Priority: Dem Contact: DWM Wells Affected: No Num Affected: Sampled By: Samples Include: 7.5 Min Quad: Not reported Not reported 5 Min Quad: Incident Desc: MINOR SOLVENT CONTAMINATION. ALSO MINOR PCBS. WORKING THROUGH BROWNFIELDS PROGRAM. Ownership: Not Reported Operation: Not Reported Material: Not reported Qty Lost: Not reported Qty Recovered: Not reported Source: Unknown Other inorganics Type: Location: Not reported Setting: Not reported Wells Contam: Not reported Sampled By: Not reported Samples Include: Not reported Owner Company: CHEROKEE INVESTMENT PARTNERS Lat/Long: Not reported Risk Site Not reported Lat/Long Decimal:0 / 0 Lat/Long Number 0 / 0 DWQ GPS: Agency: Incident Phase: NOD Last Modified 02/01/02 NOV Issued: 45 Day Report: SOC Sighned: Public Meeting Held: Corrective Action Planned: / / Reclassification Report:

RS Designation:

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number **EPA ID Number**

A3 WNW 1/4-1/2 1839 ft. **BURLINGTON MILLS** 476 SOUTH MAIN STREET MOORESVILLE, NC

Site 2 of 2 in cluster A

IMD LUST

S105764533 N/A

Relative: Higher

Actual:

923 ft.

LUST:

Incident Number: 8171 5 Min Quad: Not reported Source Type: Leak-underground Facility ID: Not reported UST Number: MO-3239 Product Type:

Petroleum

Responsible Party:

Company: **BURLINGTON INDUSTRIES**

Contact Person: Not reported PO BOX 540 Address:

MOORESVILLE, NC 28115 City/Stat/Zip:

County:

IREDELL Comm / Non-comm UST Site: Commercial Regulated Tank Regulated Status: Regional Officer Project Mgr: ARL Risk Classification: Risk Classification Based On Review:

Corrective Action Plan Type: Level Of Soil Cleanup Achieved: 3/26/2002 Closure Request Date:

Close Out:

Contamination Type: NORR Issued Date:

NOV Issued Date: Not reported Site Risk Reason: Not reported

MTBE: Not reported Telephone: Not reported

Error Flag: Error Code:

Not reported Valid: No MTBE1: No

6/9/1989 Cleanup: RBCA GW: Not reported CD Num: 115

RPOW: No RPL: No Pirf Type:

Ownership: Private Owner/Operator: Not reported Site Priority:

Wells Affected: Not reported

Not reported Samples Taken: Not reported 5minguad:

Last Modified: 4/2/2002 Incident Phase: Closed Out

Not reported NOV Issued: Not reported 45 Day Report: Close-out Report: 3/28/2002

Public Meeting Held: Corrective Action Planned: Reclassification Report:

Not reported Not reported

Not reported

Not reported Not reported Mooresville

GPS Confirmed: Not reported Not reported Date Reported: 6/9/1989

Not reported soil to GW levels

3/28/2002 GW

Not reported

Phase Of LSA Reg:1

Date Occurred:

Lat/Long:

Region:

Testlat:

Land Use: Industrial/commercial

Of Supply Wells: 0 Flag:

LUR Filed: Not reported Not reported LUR Filed:

Total Tanks: Flag1: No

Current Status: File Located in Archives

PETOPT: 0 Reel Num: RPOP: No

Location: Facility Operation Type: Industrial Priority Update: 2/15/1998

Wells Affected #: Samples Include:

Not reported Error Type: Not reported

Incident Description: SOIL SAMPLES TAKEN AT SITE DETECTED CONTAMINATION.

NORR Issued: Not reported SOC Sighned: Not reported RS Designation: Not reported

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number EPA ID Number

S105764533

BURLINGTON MILLS (Continued) Closure Request Date:

Not reported

Comments:

Not reported

IMD:

Incident Number: 8171 Region: MOR Date Occurred: Submit Date: 06/11/92 GW Contam: Yes Soil Contam: No

Operator: Not reported PO BOX 540

MOORESVILLE, NC 28115

IREDE County

Contact Phone: Not reported

Priority Code: Priority Update: 02/15/98 Site Priority: Dem Contact: ARL Wells Affected: Not reported Num Affected: Sampled By: Samples Include:

7.5 Min Quad: Not reported 5 Min Quad: Not reported

SOIL SAMPLES TAKEN AT SITE DETECTED CONTAMINATION. Incident Desc:

Ownership: Private Operation: Industrial GASOLINE Material: Qty Lost: Not reported Qty Recovered: UNK

Source: Leak-underground Type: Gasoline/diesel Location: Facility Setting: Urban Wells Contam: Not reported Sampled By: Not reported Samples Include: Not reported

Owner Company: BURLINGTON INDUSTRIES

Lat/Long: Not reported

Risk Site Lat/Long Decimal: 0 / 0 Lat/Long Number 0 / 0 GPS: NOD

DWM Agency: Incident Phase: Closed Out Last Modified 04/02/02 NOV Issued: 45 Day Report: SOC Sighned: 11

Public Meeting Held: Corrective Action Planned: / / Reclassification Report:

Close-out Report: 03/28/02 RS Designation:

Closure Request Date:

Map ID Direction Distance Distance (ft.) Elevation

Database(s)

EDR ID Number EPA ID Number

WNN 1/4-1/2 2086 ft. BILLS EXXON(MOORESVILLE QUICKL 204 S. MAIN ST, MOORESVILLE

IMD

S102868669 LUST N/A

Relative: Higher

Actual:

919 ft.

LUST:

MOORESVILLE, NC

Facility ID:

Incident Number: 18099 5 Min Quad: N65e Source Type:

Leak-underground 0-002016

UST Number: MO-5240 Product Type: Petroleum

Responsible Party:

MOORESVILLE OIL COMPANY Company:

Contact Person: BOBBY GRAHAM P.O. BOX 28 Address:

City/Stat/Zip: MOORESVILLE, NC 28115

IREDELL County:

Comm / Non-comm UST Site: Commercial Tank Regulated Status: Regulated KWC Regional Officer Project Mgr: Risk Classification:

Risk Classification Based On Review: Corrective Action Plan Type:

Not reported Not reported Level Of Soil Cleanup Achieved: Closure Request Date: Not reported Close Out: Not reported GW

Contamination Type:

NORR Issued Date: Not reported

NOV Issued Date: Not reported Site Risk Reason: Not reported Land Use: Not reported MTBE: Not reported

Not reported

Not reported Not reported

Not reported

Telephone: Not reported Error Flag:

Error Code: Not reported Valid: No

Unknown MTBE1: Cleanup: 2/1/1994 RBCA GW: Not reported

CD Num: RPOW: No

RPL: No Type: Pirf Ownership: Private

Owner/Operator: BOBBY GRAHAM Site Priority:

Wells Affected: Not reported

Samples Taken:

Not reported 5minguad: Incident Description: GW CONTAM, FOUND AS PART OF CLOSURE OF 3 USTS.

Last Modified: Not reported Incident Phase: RE

NOV Issued: Not reported 45 Day Report: Not reported Close-out Report: Not reported

Public Meeting Held: Corrective Action Planned: Reclassification Report: Closure Request Date:

Date Occurred: 2/1/1994 35 / 80 Lat/Long: Region: Mooresville GPS Confirmed: Not reported

Testlat: Not reported Date Reported: 8/11/1997

Phase Of LSA Reg: Not reported

Of Supply Wells: 0 Flag:

LUR Filed: Not reported LUR Filed: Not reported

Total Tanks: Flag1: No

Current Status: File Located in House PETOPT: Not reported

Reel Num: RPOP: No

Location: Facility Operation Type:

Commercial Priority Update: 5/30/1998 Wells Affected #:

Samples Include: Error Type:

Not reported

NORR Issued: Not reported SOC Sighned: Not reported RS Designation: Not reported Map ID Direction Distance Distance (ft.)

Elevation

MAP FINDINGS

Database(s)

EDR ID Number **EPA ID Number**

BILLS EXXON(MOORESVILLE QUICKL (Continued)

Comments: Not reported

IMD:

Incident Number: 18099 MOR Region: Date Occurred: 02/01/94 Submit Date: 12/22/97 GW Contam: Yes

Soil Contam: No

BOBBY GRAHAM Operator:

P.O. BOX 28

MOORESVILLE, NC 28115

IREDE County

Contact Phone: Not reported

Priority Code: 05/30/98 Priority Update: Site Priority: E Dem Contact: KWC Wells Affected: Not reported

Num Affected:

Samples Include: Sampled By: 7.5 Min Quad: Not reported 5 Min Quad:

Incident Desc:

GW CONTAM. FOUND AS PART OF CLOSURE OF 3 USTS.

Ownership: Private Operation: Commercial Material: GASOLINE Qty Lost: Not reported Qty Recovered: Not reported Source: Leak-underground Gasoline/diesel Type:

Location: Facility Setting: Urban Wells Contam: Not reported Sampled By: Responsible Parties Samples Include: Groundwater Samples

Owner Company: MOORESVILLE OIL COMPANY

Lat/Long: 35 / 80 Risk Site

Lat/Long Decimal: 35.57278 / 80.82417

Lat/Long Number 353422 / 804927 GPS: NOD RE

NOV Issued: 11 45 Day Report:

Incident Phase:

Public Meeting Held: Corrective Action Planned: / /

Reclassification Report:

Close-out Report: / / RS Designation: Closure Request Date: 11

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DWM

11

Agency:

Last Modified

SOC Sighned:

S102868669

Map ID Direction Distance Distance (ft.) Site Elevation

Database(s)

EDR ID Number **EPA ID Number**

U003698170

N/A

B5 North 1/4-1/2 2195 ft.

GLASPY'S AUTO SERVICE 152 SOUTH MAIN STREET MOORESVILLE, NC 28115

IMD LUST UST

Site 1 of 2 in cluster B

Relative: Higher Actual:

926 ft.

LUST:

Incident Number: 19930 5 Min Quad: N65D

Source Type: Leak-underground 0-035894 Facility ID: UST Number: MO-5641 Product Type: Petroleum

Responsible Party:

TEXACO Company:

Contact Person: JUDSON POLIKOFF 1111 BAGBY STREET Address: City/Stat/Zip: HOUSTON, TX 77002

HARRIS County:

Comm / Non-comm UST Site: Commercial Regulated Tank Regulated Status: Regional Officer Project Mgr: CBC Risk Classification: Risk Classification Based On Review:

Not reported Corrective Action Plan Type: Level Of Soil Cleanup Achieved: Not reported Closure Request Date: Not reported Not reported Close Out: GW Contamination Type: 4/14/1999 NORR Issued Date:

NOV Issued Date: Not reported Site Risk Reason: Free product

Not reported MTBE: Telephone: 713-752-6872

Error Flag: Error Code: Not reported

Valid: No MTBE1: Yes Cleanup: 12/1/1998 RBCA GW: Not reported

CD Num: RPOW: Yes RPL: No PIRF Type:

Ownership: Private JUDSON C. POLIKE Owner/Operator: Site Priority: Not reported

Not reported Wells Affected: Samples Taken: 5minguad: Not reported

Incident Description: REMOVED 3 USTS, SOILCONTAM, AT 4,590 PPM. Not reported Last Modified:

Incident Phase: NOV Issued: Not reported Not reported 45 Day Report: Close-out Report: Not reported

Public Meeting Held: Corrective Action Planned: Reclassification Report:

Not reported Not reported Not reported

12/1/1998 Date Occurred: Lat/Long: Region: Mooresville GPS Confirmed:

Testlat: Date Reported:

353453 / 804853 Not reported Not reported 1/4/1999

Phase Of LSA Req:1

Land Use: Not reported # Of Supply Wells: 0

Flag: LUR Filed:

Not reported LUR Filed: Not reported Total Tanks:

No Flag1:

Current Status: File Located in House PETOPT:

0 Reel Num: RPOP: No

Facility Location: Commercial Operation Type:

Priority Update: 5/17/1999 Wells Affected #: Not reported Samples Include:

Error Type: Not reported

Not reported NORR Issued: SOC Sighned: Not reported RS Designation: Not reported

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number **EPA ID Number**

U003698170

GLASPY'S AUTO SERVICE (Continued)

Closure Request Date: Not reported

Comments: Removal of three gasoline USTs on 12/1/98. Closure samples indicate a

release. LSA required. Abandonment in place of one 550-gallon waste oil UST in December 1998. Subsequent soil samples completed closure. LSA

investigation revealed 2.5+ feet o

f free product in MW-4 and GCL exceedances in MW-3.

IMD:

Incident Number: 19930 MOR Region: Date Occurred: 12/01/98 05/17/99 Submit Date: GW Contam: Yes Soil Contam:

JUDSON POLIKOFF Operator:

1111 BAGBY STREET HOUSTON, TX 77002

HARRI County

713-752-6872 Contact Phone: Not reported Priority Code: Priority Update: 05/17/99 Site Priority: Not reported Dem Contact: CBC Wells Affected: Not reported

Num Affected:

Sampled By: Samples Include: 7.5 Min Quad: Not reported

5 Min Quad: N65D

REMOVED 3 USTS, SOILCONTAM. AT 4,590 PPM. Incident Desc:

Ownership: Private Operation: Commercial Material: GASOLINE Qty Lost: Not reported Qty Recovered: Not reported Source: Leak-underground Gasoline/diesel Type: Location: Facility

Setting: Urban Wells Contam: Not reported Sampled By: Responsible Parties Samples Include: Soil Samples Owner Company: TEXACO 353453 / 804853 Lat/Long: Risk Site

Lat/Long Decimal: 35.58139 / 80.81472 Lat/Long Number 353453 / 804853

DWM GPS: NOD Agency: Incident Phase: Last Modified RE 11

SOC Sighned:

11

NOV Issued: 11 45 Day Report:

Public Meeting Held:

Corrective Action Planned: / / Reclassification Report:

Close-out Report: / / RS Designation:

Closure Request Date:

UST:

Facility ID: 0-035894

Map ID Direction Distance Distance (ft.) Elevation

Database(s)

EDR ID Number EPA ID Number

U003698170

GLASPY'S AUTO SERVICE (Continued)

Telephone: Owner name : (713) 752-6673 TEXACO

Owner Address:

1111 BAGBY STREET

HOUSTON, TX 77002

Owner Phone:

(713) 752-6872

Tank capacity:

3000 Not reported

Comment: Tank product:

Tank material: Interior Protection: Gasoline, Gasoline Mixture Unknown

Exterior Protection: Piping material:

Unknown Unknown Unknown

Certify Type: Leak Detection Type: Leak Detection Type 2;

Not reported Not reported Not reported Leak Detection Piping 1: Not reported

Corrosn Protec Tank: Corrosn Protec Pipe: Spill and Overfill:

Not reported Not reported Not reported Not reported

Financial Responsibility: Region:

03

Tank ID:

Date installed: Date removed: 12/31/1975 1/12/1998

Status:

Permanent Closed

Compartment Tank: Main Tank:

No No

Product Type:

NIU Piping System Type Code: Piping System Type Description:

Corrosion Protection Tank1: Corrosion Protection Tank Date:

Corrosion Piping: Corrosion Protection Piping Date: Not reported Not reported Not reported Not reported

Not reported

Not reported

Not reported

Overfill: Spill Overfill Date:

Not reported Financial Responsibility Code: Not reported Financial Responsibility Description: Not reported Not reported

Surface Water: Water Supply Well: Tank Last Used Date: Tank Certified Number: Date Last Certified: Begin Certified Number:

Not reported 12/31/1975 Not reported Not reported Not reported Not reported

End Certified Number: Lat/Long:

35.58182 / 80.81370 35 34 54.5 / 80 48 49.3

Lat/Long 1: GPS String Confirmed: Initials of Individual Confirming GPS:

Yes TNB

Tank ID Number: Last Update:

Not reported 12/14/1998

Facility ID: Telephone: 0-035894 (713) 752-6673

Owner name: Owner Address: **TEXACO** 1111 BAGBY STREET

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number **EPA ID Number**

GLASPY'S AUTO SERVICE (Continued)

U003698170

HOUSTON, TX 77002

Owner Phone: (713) 752-6872

3000 Tank capacity:

Comment: Not reported

Tank product : Gasoline, Gasoline Mixture

Tank material: Unknown Interior Protection: Unknown Exterior Protection: Unknown Piping material: Unknown Certify Type : Not reported Leak Detection Type: Not reported Leak Detection Type 2: Not reported Leak Detection Piping 1: Not reported Corrosn Protec Tank: Not reported Corrosn Protec Pipe: Not reported Spill and Overfill: Not reported Financial Responsibility: Not reported

Region: 03 Tank ID:

Date installed: 12/31/1975 Date removed: 1/12/1998 Status: Permanent Closed

Compartment Tank: No Main Tank: No Product Type: NIU Piping System Type Code:

Date Last Certified:

Not reported Piping System Type Description: Not reported Not reported Corrosion Protection Tank1: Corrosion Protection Tank Date: Not reported Corrosion Piping: Not reported Corrosion Protection Piping Date:

Overfill: Not reported Spill Overfill Date: Not reported Financial Responsibility Code: Not reported Financial Responsibility Description: Not reported Surface Water: Not reported Water Supply Well: Not reported Tank Last Used Date: 12/31/1975 Tank Certified Number: Not reported

Not reported Begin Certified Number: Not reported End Certified Number: Not reported Lat/Long: 35.58182 / 80.81370 Lat/Long 1: 35 34 54.5 / 80 48 49.3

Not reported

GPS String Confirmed: Yes Initials of Individual Confirming GPS: TNB Tank ID Number: Not reported Last Update: 12/14/1998

Facility ID: 0-035894 Telephone: (713) 752-6673 Owner name: **TEXACO**

Owner Address: 1111 BAGBY STREET

HOUSTON, TX 77002

Owner Phone: (713) 752-6872

Map ID Direction Distance Distance (ft.) Site Elevation

Database(s)

EDR ID Number EPA ID Number

U003698170

GLASPY'S AUTO SERVICE (Continued)

Tank capacity:

4000

Comment:

Not reported

Tank product:

Gasoline, Gasoline Mixture

Tank material: Interior Protection: Unknown Unknown

Exterior Protection: Piping material:

Unknown Unknown

Certify Type: Leak Detection Type: Leak Detection Type 2:

Not reported Not reported Not reported Leak Detection Piping 1: Not reported

Corrosn Protec Tank: Corrosn Protec Pipe: Spill and Overfill

Not reported Not reported Financial Responsibility: Not reported

Not reported

Region:

03 3

Tank ID: Date installed: Date removed:

12/31/1975 1/12/1998

Status:

Permanent Closed

Compartment Tank: Main Tank:

No No NIU

Product Type: Piping System Type Code:

Piping System Type Description: Corrosion Protection Tank1:

Corrosion Protection Tank Date: Corrosion Piping:

Corrosion Protection Piping Date: Overfill: Spill Overfill Date:

Financial Responsibility Code: Financial Responsibility Description:

Surface Water: Water Supply Well: Tank Last Used Date: Tank Certified Number: Date Last Certified: Begin Certified Number: End Certified Number:

Lat/Long : Lat/Long 1:

GPS String Confirmed: Initials of Individual Confirming GPS:

Tank ID Number: Last Update:

Yes TNB

Not reported 12/14/1998

Not reported

Not reported

Not reported Not reported

Not reported

Not reported

Not reported Not reported

Not reported

Not reported Not reported

Not reported

12/31/1975

Not reported Not reported

Not reported Not reported

35.58182 / 80.81370 35 34 54.5 / 80 48 49.3

Facility ID: Telephone: 0-035894 (713) 752-6673

Owner name:

TEXACO

Owner Address:

1111 BAGBY STREET

HOUSTON, TX 77002

Owner Phone: Tank capacity: (713) 752-6872 550

Comment:

Not reported

Tank product :

Oil, New/Used/Mixture

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number EPA ID Number

U003698170

GLASPY'S AUTO SERVICE (Continued)

Tank material: Unknown Interior Protection: Unknown Exterior Protection: Unknown Piping material: Unknown Certify Type: Not reported Leak Detection Type: Not reported Leak Detection Type 2: Not reported Leak Detection Piping 1: Not reported Corrosn Protec Tank: Not reported Corrosn Protec Pipe: Not reported Spill and Overfill: Not reported Financial Responsibility: Not reported

Region:

03

Tank ID:

Date installed:

12/31/1974 Not reported

Date removed: Status:

Temporary Closed

Compartment Tank:

No

Main Tank:

No NIU

Product Type: Piping System Type Code: Piping System Type Description:

Not reported Not reported

Corrosion Protection Tank1: Corrosion Protection Tank Date:

Not reported Not reported

Not reported

Corrosion Piping:

Not reported Not reported

Corrosion Protection Piping Date: Overfill:

Not reported

Spill Overfill Date: Financial Responsibility Code:

Not reported Not reported

Financial Responsibility Description: Surface Water:

Not reported Not reported 12/21/1998 Not reported

Water Supply Well: Tank Last Used Date: Tank Certified Number: Date Last Certified:

Not reported Not reported Not reported

Begin Certified Number: End Certified Number:

35.58182 / 80.81370 35 34 54.5 / 80 48 49.3

Lat/Long: Lat/Long 1:

Yes

GPS String Confirmed:

TNB

Initials of Individual Confirming GPS: Tank ID Number:

Not reported 12/14/1998

Last Update:

SHEPHERD'S

IMD

U001436122 N/A

North 1/4-1/2 2217 ft. 126 EAST CENTER AVENUE MOORESVILLE, NC 28115

LUST UST

Relative:

LUST:

Higher

Incident Number: 27225

Date Occurred: Lat/Long:

1/5/1993 Not reported

Actual: 935 ft.

5 Min Quad: Not reported Source Type:

Leak-underground Not reported

Region: GPS Confirmed:

Mooresville No

Facility ID: UST Number:

MO-2091 Petroleum Testlat: Date Reported: Not reported 2/4/1993

Product Type:

Responsible Party: Company: Not reported Contact Person: Not reported

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number EPA ID Number

U001436122

SHEPHERD'S (Continued)

Address: Not reported
City/Stat/Zip: Not reported
County: Not reported

Comm / Non-comm UST Site: Commercial Tank Regulated Status: Regulated Regional Officer Project Mgr: RBK Risk Classification: Not reported Risk Classification Based On Review: Not reported

Corrective Action Plan Type: Not reported Level Of Soil Cleanup Achieved: Not reported Closure Request Date: Not reported 2/14/1994

Contamination Type:

NORR Issued Date: Not reported

NOV Issued Date: Not reported
Site Risk Reason; Not reported
MTBE:
Not reported
H Of Supply Wells: 0

Telephone: Not reported Flag: 0
Error Flag: 0 LUR Filed: Not reported
Error Code: Not reported LUR Filed: Not reported

Valid: No Total Tanks: 1

MTBE1: Unknown Flag1: No

Cleanup: 1/5/1993 Current Status: File Located in Archives

SL

 Cleanup:
 1/5/1993
 Current Status:
 File

 RBCA GW:
 Not reported
 PETOPT:
 3

 CD Num:
 33
 Reel Num:
 0

 CD Num:
 33
 Reel Num:
 0

 RPOW:
 No
 RPOP:
 No

 RPL:
 No

 Type:
 Not reported

Ownership: P Location: Facility
Owner/Operator: Not reported Operation Type: Commercial
Site Priority: Not reported Priority Update: Not reported
Wells Affected: No Wells Affected #: Not reported

Samples Taken: Yes Samples Include: Not reported 5minquad: Not reported Error Type: Not reported

Incident Description: 2 PPM; SITE IS CLOSED; JT ALEXANDER PO 88 MOORESVILLE NC 28115 COMM/REG Last Modified: 2/14/1994

Incident Phase: Closed Out

NOV Issued: Not reported

45 Day Report: Not reported

Close-out Report: Not reported

RS Designation: Not reported

Close-out Report: Not reported RS De:
Public Meeting Held: Not reported
Corrective Action Planned: Not reported
Reclassification Report: Not reported
Closure Request Date: Not reported

Comments: Not reported

IMD:

Incident Number: 27225
Region: MOR
Date Occurred: 01/05/93
Submit Date: 02/04/93
GW Contam: No
Soil Contam: Yes

Operator: Not reported

Not reported Not reported

Contact Phone: Not reported Priority Code: Not reported

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number **EPA ID Number**

U001436122

SHEPHERD'S (Continued)

Priority Update: Site Priority: Not reported **Dem Contact:** RBK

Wells Affected: No Num Affected:

Sampled By: Samples Include: 7.5 Min Quad: Not reported 5 Min Quad: Not reported

Incident Desc: 2 PPM; SITE IS CLOSED; JT ALEXANDER PO 88 MOORESVILLE NC 28115

COMM/REG

Ownership:

Operation: Commercial Material: GASOLINE **Qty Lost:** UNKNOWN Qty Recovered: NONE

Source: Leak-underground Type: Gasoline/diesel Location: Facility Setting: Not reported Wells Contam: Not reported

Sampled By:

Samples Include: Not reported Owner Company: Not reported Lat/Long: Not reported Risk Site Not reported Lat/Long Decimal: 0 / 0 Lat/Long Number 0 / 0

GPS: EST Incident Phase: Closed Out

Agency: DWM Last Modified 02/14/94

SOC Sighned:

11

NOV Issued: 45 Day Report: Public Meeting Held: Corrective Action Planned: / /

Reclassification Report:

Close-out Report: / /

Closure Request Date: 11

RS Designation:

UST:

Facility ID: Telephone: 0-010721 (704) 664-1566

Owner name: Owner Address: J.T. ALEXANDER & SON INC P.O. BOX 88 / STATESVILLE HWY.

MOORESVILLE, NC 28115

Owner Phone:

(704) 664-1566

Tank capacity: Comment :

4000

Not reported

Tank product:

Gasoline, Gasoline Mixture Steel

Tank material: Interior Protection: Exterior Protection:

None Paint

Piping material: Steel Certify Type: Not reported Not reported Leak Detection Type: Leak Detection Type 2: Not reported Leak Detection Piping 1: Not reported

Corrosn Protec Tank: Corrosn Protec Pipe:

Not reported Not reported

Not reported

Not reported

Not reported Not reported

Not reported

Not reported

Not reported Not reported

Not reported

Not reported Not reported

Not reported

Not reported

Not reported

11/3/1989

No Not reported

00000.1.00000

1/31/1990 Not reported

Map ID Direction Distance Distance (ft.) Site Elevation

Database(s)

EDR ID Number EPA ID Number

SHEPHERD'S (Continued)

Spill and Overfill: Financial Responsibility: Not reported

Not reported

Region: Tank ID:

Date installed: Date removed:

12/29/1992

Status:

Compartment Tank: Main Tank:

No

Product Type:

NON

Piping System Type Code: Piping System Type Description: Corrosion Protection Tank1:

Not reported Not reported Not reported

Corrosion Protection Piping Date:

Spill Overfill Date:

Financial Responsibility Description:

Surface Water: Water Supply Well: Tank Last Used Date: Tank Certified Number: Date Last Certified: Begin Certified Number:

Lat/Long

Initials of Individual Confirming GPS:

Last Update:

0-010721

(704) 664-1566

Telephone: Owner name:

J.T. ALEXANDER & SON INC P.O. BOX 88 / STATESVILLE HWY.

Owner Address:

MOORESVILLE, NC 28115

Owner Phone:

(704) 664-1566

Tank capacity:

4000

Comment:

Not reported

Tank product : Tank material: Gasoline, Gasoline Mixture

Interior Protection:

Steel None Paint

Exterior Protection: Piping material:

Certify Type :

Steel Not reported Not reported

Leak Detection Type: Leak Detection Type 2: Leak Detection Piping 1: Not reported

Not reported

Corrosn Protec Tank: Corrosn Protec Pipe:

Not reported Not reported

Spill and Overfill: Financial Responsibility: Not reported

Not reported

03

Region:

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U001436122

03

11/5/1964

Permanent Closed

No

Corrosion Protection Tank Date: Corrosion Piping:

Overfill:

Financial Responsibility Code:

End Certified Number:

Lat/Long 1: GPS String Confirmed:

Tank ID Number:

Facility ID:

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number **EPA ID Number**

U001436122

SHEPHERD'S (Continued)

Tank ID:

Date installed: Date removed: 11/5/1964 12/29/1992

Status:

Compartment Tank:

Permanent Closed

Main Tank:

No No

NON

Product Type:

Piping System Type Code:

Not reported Not reported

Piping System Type Description: Corrosion Protection Tank1:

Not reported

Corrosion Protection Tank Date:

Not reported

Corrosion Piping:

Not reported

Corrosion Protection Piping Date:

Not reported

Overfill:

Not reported

Spill Overfill Date:

Not reported

Financial Responsibility Code:

Not reported

Financial Responsibility Description:

Not reported

Surface Water:

Not reported

Water Supply Well:

Not reported

Tank Last Used Date: Tank Certified Number: 1/31/1990 Not reported

Date Last Certified:

Not reported Not reported

Begin Certified Number: End Certified Number:

Not reported

Lat/Long:

00000, \ 00000.

Lat/Long 1:

Not reported

GPS String Confirmed:

No

Initials of Individual Confirming GPS:

Not reported

Tank ID Number:

Not reported

Last Update:

11/3/1989

Facility ID:

0-010721

Telephone:

(704) 664-1566

Owner name:

J.T. ALEXANDER & SON INC

Owner Address:

P.O. BOX 88 / STATESVILLE HWY.

MOORESVILLE, NC 28115

Owner Phone:

(704) 664-1566

Tank capacity:

Comment:

3000

Tank product :

Not reported Gasoline, Gasoline Mixture

Tank material:

Steel None

Interior Protection: Exterior Protection:

Paint

Piping material:

Certify Type:

Steel

Leak Detection Type:

Not reported

Leak Detection Type 2:

Not reported

Leak Detection Piping 1: Not reported Corrosn Protec Tank:

Not reported

Corrosn Protec Pipe: Spill and Overfill:

Not reported Not reported

Financial Responsibility

Not reported : Not reported

Region: Tank ID: 03

Date installed:

11/5/1964

Date removed:

12/29/1992

Map ID
Direction
Distance
Distance (ft.)
Elevation Site

Database(s)

EDR ID Number EPA ID Number

U001436122

SHEPHERD'S (Continued)

Status: Permanent Closed

Compartment Tank : No Main Tank : No Product Type: NON

Piping System Type Code:

Piping System Type Description:

Corrosion Protection Tank1:

Corrosion Protection Tank Date:

Corrosion Piping:

Not reported

Not reported

Not reported

Corrosion Protection Piping Date: Not reported Overfill: Not reported Spill Overfill Date: Not reported Financial Responsibility Code: Not reported

Financial Responsibility Description: Not reported Not reported Surface Water: Water Supply Well: Not reported 1/31/1990 Tank Last Used Date: Tank Certified Number: Not reported Not reported Date Last Certified: Not reported Begin Certified Number: Not reported End Certified Number:

 End Certified Number:
 Not reported

 Lat/Long :
 .00000 / .00000

 Lat/Long 1 :
 Not reported

GPS String Confirmed: No Initials of Individual Confirming GPS: Not reported

Tank ID Number: Not reported Last Update: 11/3/1989

Facility ID: 0-010721 Telephone: (704) 664-1566

Owner name : J.T. ALEXANDER & SON INC
Owner Address: P.O. BOX 88 / STATESVILLE HWY.

MOORESVILLE, NC 28115

Owner Phone: (704) 664-1566

Tank capacity: 3000 Comment: Not reported

Tank product : Kerosene, Kerosene Mixture Tank material : Steel

Interior Protection: None Exterior Protection: Paint Piping material: Steel Not reported Certify Type: Not reported Leak Detection Type: Leak Detection Type 2: Not reported Leak Detection Piping 1: Not reported Corrosn Protec Tank: Not reported Not reported Corrosn Protec Pipe: Spill and Overfill: Not reported

Financial Responsibility: Not reported
Region: 03
Tank ID: 4
Date installed: 11/5/1964
Date removed: 12/29/1992
Status: Permanent Closed

Compartment Tank : No Main Tank : No

Map ID Direction Distance Distance (ft.)

Site

Elevation

MAP FINDINGS

Not reported

Not reported

Not reported Not reported

Not reported

Not reported

Not reported

Not reported

Not reported

Not reported

Not reported

Not reported 1/8/1980

Not reported

Not reported

Not reported

Not reported .00000 / .00000

Not reported

Not reported

Not reported 11/3/1989

No

Database(s)

EDR ID Number EPA ID Number

SHEPHERD'S (Continued)

U001436122

Product Type: NON

Piping System Type Code: Piping System Type Description: Corrosion Protection Tank1:

Corrosion Protection Tank Date: Corrosion Piping:

Corrosion Protection Piping Date: Overfill:

Spill Overfill Date: Financial Responsibility Code: Financial Responsibility Description:

Surface Water:
Water Supply Well:
Tank Last Used Date:
Tank Certified Number:
Date Last Certified:
Begin Certified Number:
End Certified Number:

Lat/Long : Lat/Long 1 : GPS String Confirmed:

Initials of Individual Confirming GPS: Tank ID Number:

Last Update:

Facility ID:

Telephone:

Owner name : Owner Address:

wner Address: P.O. BOX 88 / STATESVILLE HWY.

0-010721

(704) 664-1566

J.T. ALEXANDER & SON INC

MOORESVILLE, NC 28115 Owner Phone : (704) 664-1566 Tank capacity : 550

Tank capacity : Comment :

omment: Not reported ank product: Kerosene, Kerosene Mixture

Tank product : K Tank material : U

Tank material : Unknown
Interior Protection: Unknown

Exterior Protection: Unknown Piping material: Unknown Certify Type: Not reported Leak Detection Type : Not reported Leak Detection Type 2: Not reported Leak Detection Piping 1: Not reported Corrosn Protec Tank: Not reported Corrosn Protec Pipe: Not reported Spill and Overfill: Not reported Financial Responsibility Not reported

03

11/5/1964

12/29/1992

Region: Tank ID:

Date installed:

Date installed: Date removed: Status:

Status: Permanent Closed
Compartment Tank: No
Main Tank: No

Main Tank : No Product Type: NON Piping System Type Code:

Piping System Type Code: Piping System Type Description: Not reported Not reported

Not reported 11/3/1989

Map ID
Direction
Distance
Distance (ft.)
Elevation Site

Database(s)

EDR ID Number EPA ID Number

U001436122

SHEPHERD'S (Continued)

Corrosion Protection Tank1: Not reported Corrosion Protection Tank Date: Not reported Corrosion Piping: Not reported Corrosion Protection Piping Date: Not reported Overfill: Not reported Spill Overfill Date: Not reported Financial Responsibility Code: Not reported Financial Responsibility Description: Not reported

Surface Water: Not reported Water Supply Well: Not reported 1/31/1990 Tank Last Used Date: Tank Certified Number: Not reported Date Last Certified: Not reported Begin Certified Number: Not reported End Certified Number: Not reported .00000 / .00000 Lat/Long

Lat/Long 1: Not reported
GPS String Confirmed: No
Initials of Individual Confirming GPS: Not reported

Tank ID Number: Last Update:

> IMD U001437258 LUST N/A

UST

B7 North 1/4-1/2 2282 ft. MOORESVILLE AMOCO SERVICE 151 S BROAD ST MOORESVILLE, NC 28115

Relative: Higher Site 2 of 2 in cluster B

Actual: 920 ft. Incident Number: 6722 5 Min Quad: N65D

Source Type: Leak-underground Facility ID: 0-017464 UST Number: MO-3079 Product Type: Petroleum

Responsible Party:

Company: Not reported
Contact Person: Michael Peebles
Address: 169 East Plaza Drive
City/Stat/Zip: Mooresville, NC 28115
County: IR

County: IR
Comm / Non-comm UST Site: Commercial
Tank Regulated Status: Regulated
Regional Officer Project Mgr: CBC
Risk Classification: L
Risk Classification Based On Review: U

Corrective Action Plan Type:
Level Of Soil Cleanup Achieved:
Closure Request Date:
Close Out:
Contamination Type:
SL

NORR Issued Date: Not reported
NOV Issued Date: Not reported

Site Risk Reason: Not reported MTBE: Not reported Telephone: 7046642928

Error Flag: 0 Error Code: Not reported

Valid: No

 Date Occurred:
 4/9/1990

 Lat/Long:
 353457 / 804848

 Region:
 Mooresville

 GPS Confirmed:
 Not reported

Testlat: Not reported Date Reported: 5/9/1990

Phase Of LSA Req:1

Land Use: Not reported

Of Supply Wells: 0 Flag: 0

LUR Filed: Not reported LUR Filed: Not reported

Total Tanks:

Map ID Direction Distance Distance (ft.) Site Elevation

Database(s)

EDR ID Number EPA ID Number

U001437258

MOORESVILLE AMOCO SERVICE (Continued)

Flag1: No

MTBE1: Unknown Cleanup: 5/18/2004 Not reported

Current Status:

File Located in House

RBCA GW: CD Num:

Type:

Ownership:

PETOPT: Reel Num: RPOP:

3 0

No

RPOW: Yes RPL: No

Pirf

Private Owner/Operator: MICHAEL PEEBLES

Location: Operation Type: Facility Commercial 5/30/1998

Site Priority: Wells Affected: No

Samples Taken:

Priority Update: Wells Affected #:

Samples Include:

Error Type: 5minguad: Not reported

Not reported

Incident Description: UPON REMOVAL OF USTS, SOIL SAMPLES CONFIRMED CONTAMINATION.

Last Modified: Not reported Incident Phase: Follow Up NOV Issued:

Not reported 45 Day Report: Not reported NORR Issued: SOC Sighned: RS Designation:

Not reported Not reported Not reported

Close-out Report: Not reported Public Meeting Held:

Not reported Not reported

Corrective Action Planned: Reclassification Report: Closure Request Date:

Not reported Not reported

Comments:

ANHR cbc 7/12/2004 - downtown Mooresville. Soil samples collected in 1990 indicated a release from the regulated USTs. Tanks were not properly

closed until May 2004. Two 2,000-gallon and two 5,000-gallon gasoline USTs

were removed and one 550-gal Ion waste oil tank was closed in place. Closure sampling indicates three

source areas - waste oil and three gasoline. No over-excavation was

undertaken. LSA required.

IMD:

Incident Number: 6722 MOR Region:

Date Occurred: Submit Date: GW Contam:

04/09/90 07/16/91 No

Yes

Soil Contam: Operator:

MICHAEL PEEBLES 151 South Broad St.

MOORESVILLE, NC 28115

IR County

Contact Phone: Not reported

Priority Code:

05/30/98

Priority Update: Site Priority: Dem Contact:

FAB Wells Affected: No Num Affected:

Sampled By: 7.5 Min Quad:

Samples Include: Not reported 5 Min Quad: Not reported

Incident Desc: Ownership:

UPON REMOVAL OF USTS, SOIL SAMPLES CONFIRMED CONTAMINATION. Private

Operation: Material:

Commercial GASOLINE Not reported

Qty Lost: Qty Recovered:

Map ID Direction Distance Distance (ft.) Elevation Site

Agency:

Last Modified

SOC Sighned:

RS Designation:

DWM

11

11

Database(s)

EDR ID Number **EPA ID Number**

MOORESVILLE AMOCO SERVICE (Continued)

Leak-underground Gasoline/diesel Type: Location: Facility Setting: Rural Wells Contam: Not reported Responsible Parties Sampled By:

Owner Company: MOORESVILLE AMOCO

Lat/Long:

Risk Site Lat/Long Decimal: 35,58250 / 80.81333 Lat/Long Number 353457 / 804848

GPS: Incident Phase: RE NOV Issued: 45 Day Report:

Reclassification Report:

UST:

(704) 664-2928 W D PEEBLES

Tank material:

151 S BROAD

Owner Phone :

Tank capacity:

Comment:

Kerosene, Kerosene Mixture Tank product :

None Interior Protection: Paint Exterior Protection: Steel Piping material: Certify Type: Leak Detection Type: Leak Detection Type 2: Not reported Leak Detection Piping 1: Corrosn Protec Tank: Corrosn Protec Pipe:

Not reported Spill and Overfill: Financial Responsibility: Not reported

Tank ID: Date installed: Date removed:

Region:

Not reported Currently In Use Status:

Compartment Tank: Main Tank: No Product Type: NON

Piping System Type Code: Piping System Type Description: Corrosion Protection Tank1:

Not reported Not reported Not reported

Not reported

Corrosion Piping:

Not reported

TC01415917.1r Page 27

U001437258

Source:

Samples Include: Soil Samples

353457 / 804848

NOD

Public Meeting Held: Corrective Action Planned: / /

Close-out Report: / /

Closure Request Date:

Facility ID:

0-017464 Telephone: Owner name :

Owner Address:

MOORESVILLE, NC 28115 (999) 999-9999

280

Not reported

Steel

Not reported Not reported

Not reported Not reported Not reported

03

3/25/1978

Corrosion Protection Tank Date:

Map ID
Direction
Distance
Distance (ft.)
Elevation Site

Database(s)

EDR ID Number EPA ID Number

MOORESVILLE AMOCO SERVICE (Continued)

U001437258

Corrosion Protection Piping Date: Not reported Overfill: Not reported Spill Overfill Date: Not reported Financial Responsibility Code: Not reported Financial Responsibility Description: Not reported Surface Water: Not reported Water Supply Well: Not reported Tank Last Used Date: Not reported Tank Certified Number: Not reported Date Last Certified: Not reported Begin Certified Number: Not reported End Certified Number: Not reported Lat/Long:

Lat/Long: 35.58229 / 80.81392 Lat/Long 1: 35.34.56.2 / 80.48.50.1 GPS String Confirmed: Yes

Initials of Individual Confirming GPS: TNB
Tank ID Number: Not reported
Last Update: 9/16/2004

Facility ID: 0-017464
Telephone: (704) 664-2928
Owner name: W D PEEBLES
Owner Address: 151 S BROAD

MOORESVILLE, NC 28115

Owner Phone : (999) 999-9999 Tank capacity : 5000

Tank capacity: 5000
Comment: Not reported

Tank product : Gasoline, Gasoline Mixture

Tank material: Steel Interior Protection: None Exterior Protection: Paint Piping material: Steel Certify Type : Not reported Leak Detection Type : Not reported Leak Detection Type 2: Not reported Leak Detection Piping 1: Not reported Corrosn Protec Tank: Not reported Corrosn Protec Pipe: Not reported Spill and Overfill: Not reported Financial Responsibility: Not reported

 Region:
 03

 Tank ID:
 2

 Date installed:
 3/25/1978

 Date removed:
 5/18/2004

 Status:
 Permanent Closed

Compartment Tank : No Main Tank : No Product Type: NIU

Piping System Type Code: Not reported Piping System Type Description: Not reported Corrosion Protection Tank1: Not reported Not reported Corrosion Protection Tank Date: Corrosion Piping: Not reported Corrosion Protection Piping Date: Not reported Overfill: Not reported Spill Overfill Date: Not reported Map ID Direction Distance Distance (ft.)

Elevation

Site

MAP FINDINGS

Database(s)

EDR ID Number **EPA ID Number**

U001437258

MOORESVILLE AMOCO SERVICE (Continued)

Financial Responsibility Code:

Financial Responsibility Description:

Surface Water:

Water Supply Well:

Tank Last Used Date:

Tank Certified Number:

Date Last Certified:

Begin Certified Number:

End Certified Number:

Lat/Long:

Lat/Long 1:

GPS String Confirmed:

Initials of Individual Confirming GPS:

Tank ID Number:

Last Update:

Facility ID:

Telephone:

Owner name:

Owner Address:

(704) 664-2928 W D PEEBLES

0-017464

151 S BROAD

MOORESVILLE, NC 28115

Owner Phone:

Tank capacity: Comment:

Tank product:

Tank material: Interior Protection:

Exterior Protection:

Piping material:

Certify Type : Leak Detection Type:

Leak Detection Type 2: Leak Detection Piping 1: Not reported

Corrosn Protec Tank:

Corrosn Protec Pipe:

Spill and Overfill:

Region:

Tank ID:

Date installed:

Date removed:

Status:

Compartment Tank:

Main Tank:

Product Type:

NON Piping System Type Code:

Piping System Type Description: Corrosion Protection Tank1:

Corrosion Protection Tank Date:

Corrosion Piping:

Corrosion Protection Piping Date:

Overfill:

Spill Overfill Date:

Financial Responsibility Code:

Financial Responsibility Description:

Surface Water:

Not reported

Not reported

Not reported Not reported

Not reported

Not reported

Not reported

Not reported Not reported

35.58229 / 80.81392

35 34 56.2 / 80 48 50.1

Yes

TNB

Not reported

9/16/2004

(999) 999-9999

5000

Not reported

Gasoline, Gasoline Mixture

Steel None

Paint Steel

Not reported Not reported

Not reported

Not reported Not reported

Not reported Financial Responsibility: Not reported

03

No

3/25/1978 5/18/2004

Permanent Closed

No

Not reported

Not reported Not reported

Not reported Not reported

Not reported

Not reported Not reported

Not reported Not reported

Not reported

Map ID
Direction
Distance
Distance (ft.)
Elevation Site

Database(s)

EDR ID Number EPA ID Number

MOORESVILLE AMOCO SERVICE (Continued)

U001437258

Water Supply Well:

Tank Last Used Date:
Not reported
Not reported
Date Last Certified:
Not reported
Not reported
Not reported
Not reported
Regin Certified Number:
Not reported
Not reported
Not reported
LavLong:
35.58229 / 80.81392

Lat/Long 1 : 35.36227 66.0132

Lat/Long 1 : 35.34 56.2 / 80 48 50.1

GPS String Confirmed: Yes
Initials of Individual Confirming GPS: TNB

Initials of Individual Confirming GPS: TNB
Tank ID Number: Not reported
Last Update: 9/16/2004

Facility ID: 0-017464
Telephone: (704) 664-2928
Owner name: W D PEEBLES
Owner Address: 151 S BROAD

MOORESVILLE, NC 28115

Owner Phone : (999) 999-9999
Tank capacity : 2000
Comment : Not reported

Tank product : Gasoline, Gasoline Mixture

Tank material: Steel Interior Protection: None Exterior Protection: Paint Piping material: Steel Certify Type : Not reported Leak Detection Type ! Not reported Leak Detection Type 2: Not reported Leak Detection Piping 1: Not reported Corrosn Protec Tank: Not reported Corrosn Protec Pipe: Not reported Spill and Overfill: Not reported Financial Responsibility Not reported

Region: 03
Tank ID: 4
Date installed: 3/25/1978
Date removed: 5/18/2004
Status: Permanent Closed

Compartment Tank : No Main Tank : No Product Type: NON

Piping System Type Code: Not reported Piping System Type Description: Not reported Corrosion Protection Tank1: Not reported Corrosion Protection Tank Date: Not reported Not reported Corrosion Piping: Corrosion Protection Piping Date: Not reported Overfill: Not reported Spill Overfill Date: Not reported Financial Responsibility Code: Not reported Financial Responsibility Description: Not reported Not reported Surface Water: Water Supply Well: Not reported Tank Last Used Date: Not reported Tank Certified Number: Not reported

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number EPA ID Number

U001437258

MOORESVILLE AMOCO SERVICE (Continued)

Date Last Certified: Begin Certified Number: End Certified Number:

Lat/Long: Lat/Long 1:

GPS String Confirmed:

Initials of Individual Confirming GPS:

Tank ID Number:

Last Update:

Facility ID:

Telephone: Owner name: Owner Address:

Owner Phone:

W D PEEBLES

0-017464 (704) 664-2928

Steel

Tank capacity:

Comment: Tank product :

Tank material: Interior Protection: Exterior Protection:

Piping material: Certify Type :

Leak Detection Type: Leak Detection Type 2: Leak Detection Piping 1: Not reported Corrosn Protec Tank:

Corrosn Protec Pipe: Spill and Overfill:

Financial Responsibility: Not reported 03

No

NON

Region: Tank ID:

Date installed:

Date removed: 5/18/2004 Status:

Compartment Tank :

Main Tank: Product Type:

Piping System Type Code: Piping System Type Description: Corrosion Protection Tank1:

Corrosion Protection Tank Date: Corrosion Piping:

Corrosion Protection Piping Date: Overfill:

Spill Overfill Date:

Financial Responsibility Code: Financial Responsibility Description:

Surface Water: Water Supply Well: Tank Last Used Date: Tank Certified Number: Date Last Certified: Begin Certified Number: End Certified Number:

Not reported Not reported Not reported

35.58229 / 80.81392 35 34 56.2 / 80 48 50.1 Yes

TNB Not reported 9/16/2004

151 S BROAD

MOORESVILLE, NC 28115

(999) 999-9999

550

Not reported

Oil, New/Used/Mixture

Steel None Paint

Not reported Not reported Not reported

Not reported Not reported Not reported

3/25/1978

Permanent Closed No

Not reported

Not reported Not reported Not reported

Not reported Not reported Not reported

Not reported Not reported

Not reported Not reported Not reported

Not reported Not reported Not reported Not reported Not reported

Yes

TNB

Not reported

9/16/2004

35.58229 / 80.81392

35 34 56.2 / 80 48 50.1

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number **EPA ID Number**

U001437258

MOORESVILLE AMOCO SERVICE (Continued)

Lat/Long:

Lat/Long 1:

GPS String Confirmed:

Tank ID Number:

Last Update:

Facility ID:

Initials of Individual Confirming GPS:

0-017464

Telephone: Owner name: Owner Address:

W D PEEBLES 151 S BROAD

(704) 664-2928

MOORESVILLE, NC 28115

Owner Phone:

(999) 999-9999 2000

Tank capacity: Comment:

Not reported

Tank product:

Gasoline, Gasoline Mixture

Tank material:

Unknown

Interior Protection: Exterior Protection:

Unknown 16

Piping material: Certify Type :

Not reported Leak Detection Type: Not reported Leak Detection Type 2: Not reported Leak Detection Piping 1: Not reported Corrosn Protec Tank: Not reported

Corrosn Protec Pipe: Spill and Overfill:

Not reported Not reported Financial Responsibility: Not reported

Region: Tank ID: 03 6

Date installed:

3/25/1978 5/18/2004

Date removed: Status:

Permanent Closed

Compartment Tank: No Main Tank: No Product Type: NON

Piping System Type Code: Piping System Type Description:

Corrosion Protection Tank1: Corrosion Protection Tank Date: Corrosion Piping:

Corrosion Protection Piping Date:

Overfill: Spill Overfill Date:

Financial Responsibility Code: Financial Responsibility Description:

Surface Water: Water Supply Well: Tank Last Used Date: Tank Certified Number: Date Last Certified: Begin Certified Number: End Certified Number:

Lat/Long: Lat/Long 1:

GPS String Confirmed:

Not reported

Not reported Not reported Not reported

Not reported Not reported

Not reported Not reported Not reported

Not reported Not reported Not reported Not reported Not reported

Not reported Not reported Not reported

35.58229 / 80.81392 35 34 56.2 / 80 48 50.1

Yes

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

IMD

EDR ID Number **EPA ID Number**

U001437258

S106349484

N/A

MOORESVILLE AMOCO SERVICE (Continued)

Initials of Individual Confirming GPS:

Tank ID Number:

Last Update:

TNB

Not reported 9/16/2004

North 1/4-1/2 SERVICE AUTO SUPPLY 101 SOUTH BROAD STREET

MOORESVILLE, NC

2416 ft.

Relative:

Higher Actual:

927 ft.

IMD:

Incident Number: 86921 MOR Region: 02/19/04 Date Occurred: 02/23/04 Submit Date: NOD GW Contam:

Soil Contam: Operator:

Not reported BROWN, FRED 341 TEETER RD MOORESVILLE, NC

Contact Phone: Not reported NOD Priority Code: Priority Update:

Not reported Site Priority: Dem Contact: ARL Wells Affected: No Num Affected:

Samples Include: Sampled By: Not reported 7.5 Min Quad:

Not reported 5 Min Quad:

LOW LEVELS OF OIL & GREASE TPH DETECTED IN SOIL SAMPLES TAKEN AT FORMER Incident Desc:

ENGINE PARTS WASHER. OPHSCA NOTICE SENT.

Federal Ownership: Operation:

Not reported Material: Not reported Qty Lost: Qty Recovered: Not reported Source: Spill-surface

Other petroleum product Type:

Not reported Location: Not reported Setting: Wells Contam: Not reported Sampled By: Not reported Samples Include: Not reported Owner Company: Not reported Lat/Long: Not reported Not reported Risk Site Lat/Long Decimal: 0 / 0

Lat/Long Number 10 / 0 GPS: NOD

Incident Phase: Discovery 02/20/04 NOV Issued:

Last Modified SOC Sighned: 45 Day Report:

Public Meeting Held: Corrective Action Planned: / / Reclassification Report:

Close-out Report: / / Closure Request Date:

Agency:

DWQ

11

02/23/04

RS Designation:

Map ID Direction Distance Distance (ft.) Elevation Site

Database(s)

EDR ID Number EPA ID Number

N/A

J.T. ALEXANDER 9 NNW **HWY 115 N** 1/4-1/2 MOORESVILLE, NC 2471 ft.

S101643149 IMD

LUST

Relative:

LUST:

Higher Actual:

930 ft.

Incident Number: 13431 5 Min Quad: M65Q

Source Type: Leak-underground Facility ID: 0-010713 **UST Number:** MO-4274 Petroleum Product Type:

Responsible Party:

J.T. ALEXANDER & SON Company:

Contact Person: Not reported P.O. BOX 88 Address:

City/Stat/Zip: MOORESVILLE, NC 28115

County:

Comm / Non-comm UST Site: Commercial Tank Regulated Status: Regulated Regional Officer Project Mgr: KWC Risk Classification: Risk Classification Based On Review:

Corrective Action Plan Type: natural attenuation (not an L-CAP)

Level Of Soil Cleanup Achieved: Residential levels Closure Request Date: 6/10/1999 6/10/1999 Close Out: Contamination Type: GW NORR Issued Date: Not reported

NOV Issued Date: 6/14/1995 Site Risk Reason: Not reported MTBE: Not reported

Telephone: Not reported Error Flag:

Error Code: Not reported Valid: No MTBE1: Unknown Cleanup:

1/26/1995 Not reported

RBCA GW: CD Num: 115 RPOW: No RPL: No Type:

Pirf Ownership: Private Owner/Operator: Not reported Site Priority: 065B Wells Affected: No Samples Taken:

5minguad: Not reported Incident Description: Not reported

6/22/1999 Last Modified: Incident Phase: Closed Out 9/24/1996 NOV Issued: 45 Day Report: Not reported

Close-out Report: 6/11/1999 Public Meeting Held: Not reported Corrective Action Planned: Not reported Reclassification Report: Not reported Closure Request Date: Not reported

1/26/1995 Date Occurred:

Lat/Long: 353625 / 804858 Region: Mooresville GPS Confirmed: No

Testlat: Not reported Date Reported: 2/9/1995

Phase Of LSA Req:Not reported

0

No

0

No

Not reported

Not reported

Not reported

File Located in Archives

Land Use:

LUR Filed:

LUR Filed:

Total Tanks:

Current Status:

Flag:

Flag1:

PETOPT:

Location:

Operation Type:

Priority Update:

Wells Affected #:

Samples Include:

Error Type:

NORR Issued:

SOC Sighned:

RS Designation:

RPOP:

Reel Num:

Of Supply Wells:

5/15/1998 0

Commercial

Not reported

Facility

Not reported Not reported Not reported

MAP FINDINGS

Map ID Direction Distance Distance (ft.) Site Elevation

Database(s)

EDR ID Number **EPA ID Number**

S101643149

J.T. ALEXANDER (Continued)

Comments: Not reported

IMD:

Incident Number: 13431 MOR Region: Date Occurred: 01/26/95 06/14/95 Submit Date: GW Contam: Yes Soil Contam: No

Operator: Not reported

P.O. BOX 88

MOORESVILLE, NC 28115

IR County Contact Phone: Not reported Priority Code: 05/15/98 Priority Update: Site Priority: 065B

KWC Dem Contact: Wells Affected: No Num Affected:

Sampled By: Samples Include: 7.5 Min Quad: Not reported M65Q 5 Min Quad: Incident Desc: Not reported Private Ownership: Commercial Operation: GASOLINE Material: Not reported Qty Lost: Qty Recovered: Not reported Leak-underground Source: Gasoline/diesel

Type: Location: Facility Urban Setting: Not reported Wells Contam: Sampled By: Responsible Parties Samples Include: Groundwater Samples Owner Company: J.T. ALEXANDER & SON

Lat/Long:

353625 / 804858

Risk Site

Lat/Long Decimal: 35.60694 / 80.81611 Lat/Long Number 353625 / 804858

GPS: EST Incident Phase: Closed Out 09/24/96 NOV Issued:

45 Day Report:

Public Meeting Held: Corrective Action Planned: / /

Reclassification Report: Close-out Report: 06/11/99

Closure Request Date:

06/22/99 Last Modified

Agency:

DWM

SOC Sighned: 11

RS Designation:

MAP FINDINGS

Map ID Direction Distance Distance (ft.)

Elevation Site

Database(s)

EDR ID Number **EPA ID Number**

10 CARPET DEPOT

239 WEST CENTER STREET

LUST TRUST S105922631 N/A

North 1/4-1/2

MOORESVILLE, NC

2568 ft.

LUST TRUST:

Relative: Higher

Facility ID: Site ID:

Not reported 24489 Not reported

Actual: 911 ft.

Site Note: Site Eligible?:

Yes 100% Non-Commercial

Commercial Find:

Priority Rank:

Not reported

3rd Party Deductable Amount:

0 0

Sum of 3rd Party Amounts Applied: Deductable Amount:

Click this hyperlink while viewing on your computer to access additional NC LUST TRUST detail in the EDR Site Report.

To maintain currency of the following federal and state databases, EDR contacts the appropriate governmental agency on a monthly or quarterly basis, as required.

Elapsed ASTM days: Provides confirmation that this EDR report meets or exceeds the 90-day updating requirement

of the ASTM standard.

FEDERAL ASTM STANDARD RECORDS

NPL: National Priority List

Source: EPA Telephone: N/A

National Priorities List (Superfund). The NPL is a subset of CERCLIS and identifies over 1,200 sites for priority cleanup under the Superfund Program. NPL sites may encompass relatively large areas. As such, EDR provides polygon coverage for over 1,000 NPL site boundaries produced by EPA's Environmental Photographic Interpretation Center (EPIC) and regional EPA offices.

Date of Government Version: 12/14/04 Date Made Active at EDR: 02/03/05 Database Release Frequency: Quarterly

Date of Data Arrival at EDR: 02/01/05 Elapsed ASTM days: 2 Date of Last EDR Contact: 02/01/05

NPL Site Boundaries

Sources:

EPA's Environmental Photographic Interpretation Center (EPIC)

Telephone: 202-564-7333

EPA Region 1

Telephone 617-918-1143

EPA Region 3

Telephone 215-814-5418

EPA Region 4

Telephone 404-562-8033

EPA Region 6

Telephone: 214-655-6659

EPA Region 8

Telephone: 303-312-6774

Proposed NPL: Proposed National Priority List Sites

Source: EPA Telephone: N/A

> Date of Government Version: 12/14/04 Date Made Active at EDR: 02/03/05

Database Release Frequency: Quarterly

Date of Data Arrival at EDR: 02/01/05

Elapsed ASTM days: 2

Date of Last EDR Contact: 02/01/05

CERCLIS: Comprehensive Environmental Response, Compensation, and Liability Information System

Source: EPA

Telephone: 703-413-0223

CERCLIS contains data on potentially hazardous waste sites that have been reported to the USEPA by states, municipalities, private companies and private persons, pursuant to Section 103 of the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA). CERCLIS contains sites which are either proposed to or on the National Priorities List (NPL) and sites which are in the screening and assessment phase for possible inclusion on the NPL.

Date of Government Version: 02/15/05 Date Made Active at EDR: 04/06/05 Database Release Frequency; Quarterly

Date of Data Arrival at EDR: 03/22/05 Elapsed ASTM days: 15 Date of Last EDR Contact: 03/22/05

CERCLIS-NFRAP: CERCLIS No Further Remedial Action Planned

Source: EPA

Telephone: 703-413-0223

As of February 1995, CERCLIS sites designated "No Further Remedial Action Planned" (NFRAP) have been removed from CERCLIS. NFRAP sites may be sites where, following an initial investigation, no contamination was found, contamination was removed quickly without the need for the site to be placed on the NPL, or the contamination was not serious enough to require Federal Superfund action or NPL consideration. EPA has removed approximately 25,000 NFRAP sites to lift the unintended barriers to the redevelopment of these properties and has archived them as historical records so EPA does not needlessly repeat the investigations in the future. This policy change is part of the EPA's Brownfields Redevelopment Program to help cities, states, private investors and affected citizens to promote economic redevelopment of unproductive urban sites.

Date of Government Version: 03/22/05 Date Made Active at EDR: 04/06/05 Database Release Frequency: Quarterly Date of Data Arrival at EDR: 04/01/05 Elapsed ASTM days: 5 Date of Last EDR Contact: 04/01/05

CORRACTS: Corrective Action Report

Source: EPA

Telephone: 800-424-9346

CORRACTS identifies hazardous waste handlers with RCRA corrective action activity.

Date of Government Version: 12/15/04 Date Made Active at EDR: 02/25/05 Database Release Frequency: Quarterly Date of Data Arrival at EDR: 01/07/05 Elapsed ASTM days: 49

Date of Last EDR Contact: 03/07/05

RCRA: Resource Conservation and Recovery Act Information

Source: EPA

Telephone: 800-424-9346

RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. RCRAInfo replaces the data recording and reporting abilities of the Resource Conservation and Recovery Information System (RCRIS). The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Conditionally exempt small quantity generators (CESQGs) generate less than 100 kg of hazardous waste, or less than 1 kg of acutely hazardous waste per month. Small quantity generators (SQGs) generate between 100 kg and 1,000 kg of hazardous waste per month. Large quantity generators (LQGs) generate over 1,000 kilograms (kg) of hazardous waste, or over 1 kg of acutely hazardous waste per month. Transporters are individuals or entities that move hazardous waste from the generator off-site to a facility that can recycle, treat, store, or dispose of the waste. TSDFs treat, store, or dispose of the waste.

Date of Government Version: 03/13/05 Date Made Active at EDR: 04/25/05 Database Release Frequency: Quarterly Date of Data Arrival at EDR: 03/23/05 Elapsed ASTM days: 33 Date of Last EDR Contact: 03/23/05

ERNS: Emergency Response Notification System

Source: National Response Center, United States Coast Guard

Telephone: 202-260-2342

Emergency Response Notification System. ERNS records and stores information on reported releases of oil and hazardous substances.

Date of Government Version: 12/31/04 Date Made Active at EDR: 03/24/05 Database Release Frequency: Annually Date of Data Arrival at EDR: 01/27/05 Elapsed ASTM days: 56 Date of Last EDR Contact: 04/25/05

FEDERAL ASTM SUPPLEMENTAL RECORDS

BRS: Biennial Reporting System

Source: EPA/NTIS Telephone: 800-424-9346

The Biennial Reporting System is a national system administered by the EPA that collects data on the generation and management of hazardous waste. BRS captures detailed data from two groups: Large Quantity Generators (LQG) and Treatment, Storage, and Disposal Facilities.

Date of Government Version: 12/01/01 Database Release Frequency: Biennially Date of Last EDR Contact: 04/15/05 Date of Next Scheduled EDR Contact: 06/13/05

CONSENT: Superfund (CERCLA) Consent Decrees

Source: Department of Justice, Consent Decree Library

Telephone: Varies

Major legal settlements that establish responsibility and standards for cleanup at NPL (Superfund) sites. Released periodically by United States District Courts after settlement by parties to litigation matters.

Date of Government Version: 12/14/04 Database Release Frequency: Varies Date of Last EDR Contact: 04/26/05

Date of Next Scheduled EDR Contact: 07/25/05

ROD: Records Of Decision

Source: EPA

Telephone: 703-416-0223

Record of Decision. ROD documents mandate a permanent remedy at an NPL (Superfund) site containing technical

and health information to aid in the cleanup.

Date of Government Version: 01/10/05 Database Release Frequency: Annually Date of Last EDR Contact: 04/04/05

Date of Next Scheduled EDR Contact: 07/04/05

DELISTED NPL: National Priority List Deletions

Source: EPA Telephone: N/A

The National Oil and Hazardous Substances Pollution Contingency Plan (NCP) establishes the criteria that the EPA uses to delete sites from the NPL. In accordance with 40 CFR 300.425.(e), sites may be deleted from the

NPL where no further response is appropriate.

Date of Government Version: 12/14/04 Database Rélease Frequency: Quarterly Date of Last EDR Contact: 02/01/05

Date of Next Scheduled EDR Contact: 05/02/05

FINDS: Facility Index System/Facility Identification Initiative Program Summary Report

Source: EPA Telephone: N/A

Facility Index System. FINDS contains both facility information and 'pointers' to other sources that contain more detail. EDR includes the following FINDS databases in this report: PCS (Permit Compliance System), AIRS (Aerometric Information Retrieval System), DOCKET (Enforcement Docket used to manage and track information on civil judicial enforcement cases for all environmental statutes), FURS (Federal Underground Injection Control), C-DOCKET (Criminal Docket System used to track criminal enforcement actions for all environmental statutes), FFIS (Federal Facilities Information System), STATE (State Environmental Laws and Statutes), and PADS (PCB Activity Data System).

Date of Government Version: 01/12/05 Database Release Frequency: Quarterly Date of Last EDR Contact: 04/04/05

Date of Next Scheduled EDR Contact: 07/04/05

HMIRS: Hazardous Materials Information Reporting System

Source: U.S. Department of Transportation

Telephone: 202-366-4555

Hazardous Materials Incident Report System, HMIRS contains hazardous material spill incidents reported to DOT.

Date of Government Version: 11/16/04 Database Release Frequency: Annually Date of Last EDR Contact: 04/19/05

Date of Next Scheduled EDR Contact: 07/18/05

MLTS: Material Licensing Tracking System Source: Nuclear Regulatory Commission

Telephone: 301-415-7169

MLTS is maintained by the Nuclear Regulatory Commission and contains a list of approximately 8,100 sites which possess or use radioactive materials and which are subject to NRC licensing requirements. To maintain currency,

EDR contacts the Agency on a quarterly basis.

Date of Government Version: 01/12/05 Database Release Frequency: Quarterly Date of Last EDR Contact: 04/04/05

Date of Next Scheduled EDR Contact: 07/04/05

MINES: Mines Master Index File

Source: Department of Labor, Mine Safety and Health Administration

Telephone: 303-231-5959

Contains all mine identification numbers issued for mines active or opened since 1971. The data also includes violation information.

Date of Government Version: 11/15/04 Database Release Frequency: Semi-Annually Date of Last EDR Contact: 03/30/05 Date of Next Scheduled EDR Contact: 06/27/05

NPL LIENS: Federal Superfund Liens

Source: EPA

Telephone: 202-564-4267

Federal Superfund Liens. Under the authority granted the USEPA by the Comprehensive Environmental Response, Compensation and Liability Act (CERCLA) of 1980, the USEPA has the authority to file liens against real property in order to recover remedial action expenditures or when the property owner receives notification of potential liability.

USEPA compiles a listing of filed notices of Superfund Liens.

Date of Government Version: 10/15/91

Database Release Frequency: No Update Planned

Date of Last EDR Contact: 02/22/05

Date of Next Scheduled EDR Contact: 05/23/05

PADS: PCB Activity Database System

Source: EPA

Telephone: 202-564-3887

PCB Activity Database. PADS Identifies generators, transporters, commercial storers and/or brokers and disposers

of PCB's who are required to notify the EPA of such activities.

Date of Government Version: 12/21/04 Database Release Frequency: Annually Date of Last EDR Contact: 02/23/05

Date of Next Scheduled EDR Contact: 05/09/05

DOD: Department of Defense Sites

Source: USGS

Telephone: 703-692-8801

This data set consists of federally owned or administered lands, administered by the Department of Defense, that have any area equal to or greater than 640 acres of the United States, Puerto Rico, and the U.S. Virgin Islands.

Date of Government Version: 10/01/03 Database Release Frequency: Semi-Annually Date of Last EDR Contact: 02/08/05

Date of Next Scheduled EDR Contact: 05/09/05

UMTRA: Uranium Mill Tallings Sites Source: Department of Energy Telephone: 505-845-0011

Uranium ore was mined by private companies for federal government use in national defense programs. When the mills shut down, large piles of the sand-like material (mill tailings) remain after uranium has been extracted from the ore. Levels of human exposure to radioactive materials from the piles are low; however, in some cases tailings were used as construction materials before the potential health hazards of the tailings were recognized. In 1978, 24 inactive uranium mill tailings sites in Oregon, Idaho, Wyoming, Utah, Colorado, New Mexico, Texas, North Dakota, South Dakota, Pennsylvania, and on Navajo and Hopi tribal lands, were targeted for cleanup by the Department of

Date of Government Version: 12/29/04 Database Release Frequency: Varies Date of Last EDR Contact: 03/22/05

Date of Next Scheduled EDR Contact: 06/20/05

ODI: Open Dump Inventory

Source: Environmental Protection Agency

Telephone: 800-424-9346

An open dump is defined as a disposal facility that does not comply with one or more of the Part 257 or Part 258

Subtitle D Criteria.

Date of Government Version: 06/30/85

Database Release Frequency: No Update Planned

Date of Last EDR Contact: 05/23/95
Date of Next Scheduled EDR Contact: N/A

FUDS: Formerly Used Defense Sites Source: U.S. Army Corps of Engineers

Telephone: 202-528-4285

The listing includes locations of Formerly Used Defense Sites properties where the US Army Corps of Engineers

is actively working or will take necessary cleanup actions.

Date of Government Version: 12/31/03 Database Release Frequency: Varies

Date of Last EDR Contact: 04/04/05

Date of Next Scheduled EDR Contact: 07/04/05

INDIAN RESERV: Indian Reservations

Source: USGS

Telephone: 202-208-3710

This map layer portrays Indian administered lands of the United States that have any area equal to or greater

than 640 acres.

Date of Government Version: 10/01/03 Database Release Frequency: Semi-Annually Date of Last EDR Contact: 02/08/05

Date of Next Scheduled EDR Contact: 05/09/05

US ENG CONTROLS: Engineering Controls Sites List

Source: Environmental Protection Agency

Telephone: 703-603-8867

A listing of sites with engineering controls in place. Engineering controls include various forms of caps, building foundations, liners, and treatment methods to create pathway elimination for regulated substances to enter environmental

media or effect human health.

Date of Government Version: 01/10/05

Database Release Frequency: Varies

Date of Last EDR Contact: 04/04/05

Date of Next Scheduled EDR Contact: 07/04/05

RAATS: RCRA Administrative Action Tracking System

Source: EPA

Telephone: 202-564-4104

RCRA Administration Action Tracking System, RAATS contains records based on enforcement actions issued under RCRA pertaining to major violators and includes administrative and civil actions brought by the EPA. For administration actions after September 30, 1995, data entry in the RAATS database was discontinued. EPA will retain a copy of the database for historical records, It was necessary to terminate RAATS because a decrease in agency resources made it impossible to continue to update the information contained in the database.

Date of Government Version: 04/17/95

Database Release Frequency: No Update Planned

Date of Last EDR Contact: 03/07/05

Date of Next Scheduled EDR Contact: 06/06/05

TRIS: Toxic Chemical Release Inventory System

Source: EPA

Telephone: 202-566-0250

Toxic Release Inventory System. TRIS identifies facilities which release toxic chemicals to the air, water and

land in reportable quantities under SARA Title III Section 313.

Date of Government Version: 12/31/02

Database Release Frequency: Annually

Date of Last EDR Contact: 03/22/05

Date of Next Scheduled EDR Contact: 06/20/05

TSCA: Toxic Substances Control Act

Source: EPA

Telephone: 202-260-5521

Toxic Substances Control Act. TSCA identifies manufacturers and importers of chemical substances included on the TSCA Chemical Substance Inventory list. It includes data on the production volume of these substances by plant

Date of Government Version: 01/01/05

Database Release Frequency: Every 4 Years

Date of Last EDR Contact: 04/05/05

Date of Next Scheduled EDR Contact: 06/06/05

FTTS INSP: FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide Act)/TSCA (Toxic Substances Control Act)

Source: EPA

Telephone: 202-566-1667

Date of Government Version: 04/13/04

Database Release Frequency: Quarterly

Date of Last EDR Contact: 03/21/05

Date of Next Scheduled EDR Contact: 06/20/05

SSTS: Section 7 Tracking Systems

Source: EPA

Telephone: 202-564-5008

Section 7 of the Federal Insecticide, Fungicide and Rodenticide Act, as amended (92 Stat. 829) requires all registered pesticide-producing establishments to submit a report to the Environmental Protection Agency by March 1st each year. Each establishment must report the types and amounts of pesticides, active ingredients and devices being produced, and those having been produced and sold or distributed in the past year.

Date of Government Version: 12/31/03 Database Release Frequency: Annually Date of Last EDR Contact: 04/19/05
Date of Next Scheduled EDR Contact: 07/18/05

FTTS: FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide Act)/TSCA (Toxic Substances Control Act)

Source: EPA/Office of Prevention, Pesticides and Toxic Substances

Telephone: 202-566-1667

FTTS tracks administrative cases and pesticide enforcement actions and compliance activities related to FIFRA, TSCA and EPCRA (Emergency Planning and Community Right-to-Know Act). To maintain currency, EDR contacts the Agency on a quarterly basis.

Date of Government Version: 09/13/04 Database Release Frequency: Quarterly Date of Last EDR Contact: 03/21/05 Date of Next Scheduled EDR Contact: 06/20/05

STATE OF NORTH CAROLINA ASTM STANDARD RECORDS

SHWS: Inactive Hazardous Sites Inventory

Source: Department of Environment, Health and Natural Resources

Telephone: 919-733-2801

State Hazardous Waste Sites. State hazardous waste site records are the states' equivalent to CERCLIS. These sites may or may not already be listed on the federal CERCLIS list. Priority sites planned for cleanup using state funds (state equivalent of Superfund) are identified along with sites where cleanup will be paid for by potentially responsible parties. Available information varies by state.

Date of Government Version: 04/12/05 Date Made Active at EDR: 04/25/05 Database Release Frequency: Quarterly Date of Data Arrival at EDR: 04/12/05 Elapsed ASTM days: 13 Date of Last EDR Contact: 04/11/05

SWF/LF: List of Solid Waste Facilities

Source: Department of Environment and Natural Resources

Telephone: 919-733-0692

Solid Waste Facilities/Landfill Sites. SWF/LF type records typically contain an inventory of solid waste disposal facilities or landfills in a particular state. Depending on the state, these may be active or inactive facilities or open dumps that failed to meet RCRA Subtitle D Section 4004 criteria for solid waste landfills or disposal sites.

Date of Government Version: 02/17/05 Date Made Active at EDR: 03/29/05 Database Release Frequency: Semi-Annually Date of Data Arrival at EDR: 02/17/05 Elapsed ASTM days: 40 Date of Last EDR Contact: 04/25/05

LUST: Regional UST Database

Source: Department of Environment and Natural Resources

Telephone: 919-733-1308

This database contains information obtained from the Regional Offices. It provides a more detailed explanation of current and historic activity for individual sites, as well as what was previously found in the Incident Management Database. Sites in this database with Incident Numbers are considered LUSTs.

Date of Government Version: 03/04/05 Date Made Active at EDR: 04/06/05 Database Release Frequency: Quarterly Date of Data Arrival at EDR: 03/08/05 Elapsed ASTM days: 29 Date of Last EDR Contact: 03/08/05

UST: Petroleum Underground Storage Tank Database

Source: Department of Environment and Natural Resources

Telephone: 919-733-1308

Registered Underground Storage Tanks. UST's are regulated under Subtitle I of the Resource Conservation and Recovery Act (RCRA) and must be registered with the state department responsible for administering the UST program. Available

information varies by state program.

Date of Government Version: 02/25/05 Date Made Active at EDR: 04/07/05

Database Release Frequency: Quarterly

Date of Data Arrival at EDR: 03/08/05

Elapsed ASTM days: 30

Date of Last EDR Contact: 03/08/05

OLI: Old Landfill Inventory

Source: Department of Environment & Natural Resources

Telephone: 919-733-4996

Old landfill inventory location information. (Does not include no further action sites and other agency lead

sites).

Date of Government Version: 01/06/05 Date Made Active at EDR: 03/16/05

Database Release Frequency: Varies

Date of Data Arrival at EDR: 01/28/05

Elapsed ASTM days: 47

Date of Last EDR Contact: 04/28/05

VCP: Responsible Party Voluntary Action Sites

Source: Department of Environment and Natural Resources

Telephone: 919-733-4996

Date of Government Version: 04/12/05 Date Made Active at EDR: 04/25/05

Database Release Frequency: Semi-Annually

Date of Data Arrival at EDR: 04/12/05

Elapsed ASTM days: 13

Date of Last EDR Contact: 04/11/05

INDIAN UST: Underground Storage Tanks on Indian Land

Source: EPA Region 4 Telephone: 404-562-9424

Date of Government Version: 03/03/05 Date Made Active at EDR: 04/19/05

Database Release Frequency: Varies

Date of Data Arrival at EDR: 03/18/05

Elapsed ASTM days: 32

Date of Last EDR Contact: 02/15/05

INDIAN LUST: Leaking Underground Storage Tanks on Indian Land

Source: EPA Region 4 Telephone: 404-562-8677

LUSTs on Indian land in Florida, Minnesota, Mississippi and North Carolina.

Date of Government Version: 03/01/05 Date Made Active at EDR: 04/19/05

Database Release Frequency: Varies

Date of Data Arrival at EDR: 03/18/05

Elapsed ASTM days: 32

Date of Last EDR Contact: 02/15/05

STATE OF NORTH CAROLINA ASTM SUPPLEMENTAL RECORDS

HSDS: Hazardous Substance Disposal Site

Source: North Carolina Center for Geographic Information and Analysis

Telephone: 919-733-2090

Locations of uncontrolled and unregulated hazardous waste sites. The file includes sites on the National Priority

List as well as those on the state priority list.

Date of Government Version: 06/21/95

Database Release Frequency: Biennially

Date of Last EDR Contact: 02/28/05

Date of Next Scheduled EDR Contact: 05/30/05

AST: AST Database

Source: Department of Environment and Natural Resources

Telephone: 919-715-6183

Facilities with aboveground storage tanks that have a capacity greater than 21,000 gallons.

Date of Government Version: 01/14/05 Database Release Frequency: Semi-Annually Date of Last EDR Contact: 04/18/05 Date of Next Scheduled EDR Contact: 07/18/05

LUST TRUST: State Trust Fund Database

Source: Department of Environment and Natural Resources

Telephone: 919-733-1315

This database contains information about claims against the State Trust Funds for reimbursements for expenses

incurred while remediating Leaking USTs.

Date of Government Version: 03/11/05

Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 02/08/05

Date of Next Scheduled EDR Contact: 05/09/05

DRYCLEANERS: Drycleaning Sites

Source: Department of Environment & Natural Resources

Telephone: 919-733-2801

Potential and known drycleaning sites, active and abandoned, that the Drycleaning Solvent Cleanup Program has

knowledge of and entered into this database.

Date of Government Version: 11/12/04

Database Release Frequency: Varies

Date of Last EDR Contact: 04/18/05

Date of Next Scheduled EDR Contact: 07/18/05

IMD: Incident Management Database

Source: Department of Environment and Natural Resources

Telephone: 919-733-3221

Groundwater and/or soil contamination incidents

Date of Government Version: 06/15/04

Date of Last EDR Contact: 04/27/05

Date of Next Scheduled EDR Contact: 07/25/05 Database Release Frequency: Quarterly

EDR PROPRIETARY HISTORICAL DATABASES

Former Manufactured Gas (Coal Gas) Sites: The existence and location of Coal Gas sites is provided exclusively to EDR by Real Property Scan, Inc. @Copyright 1993 Real Property Scan, Inc. For a technical description of the types of hazards which may be found at such sites, contact your EDR customer service representative.

Disclaimer Provided by Real Property Scan, Inc.

The information contained in this report has predominantly been obtained from publicly available sources produced by entitles other than Real Property Scan. While reasonable steps have been taken to insure the accuracy of this report, Real Property Scan does not guarantee the accuracy of this report. Any liability on the part of Real Property Scan is strictly limited to a refund of the amount paid. No claim is made for the actual existence of toxins at any site. This report does not constitute a legal opinion.

BROWNFIELDS DATABASES

Brownfields: Brownfields Projects Inventory

Source: Department of Environment and Natural Resources

Telephone: 919-733-4996

A brownfield site is an abandoned, idled, or underused property where the threat of environmental contamination has hindered its redevelopment. All of the sites in the inventory are working toward a brownfield agreement for cleanup and liabitly control.

Date of Government Version: 09/30/04 Database Release Frequency: Varies

Date of Last EDR Contact: 02/04/05 Date of Next Scheduled EDR Contact: 05/02/05

VCP: Responsible Party Voluntary Action Sites

Source: Department of Environment and Natural Resources

Telephone: 919-733-4996

Date of Government Version: 04/12/05 Database Release Frequency: Semi-Annually Date of Last EDR Contact: 04/11/05
Date of Next Scheduled EDR Contact: 07/11/05

INST CONTROL: No Further Action Sites With Land Use Restrictions Monitoring

Source: Department of Environment, Health and Natural Resources

Telephone: 919-733-2801

Date of Government Version: 04/12/05 Database Release Frequency: Quarterly Date of Last EDR Contact: 04/11/05

Date of Next Scheduled EDR Contact: 07/11/05

US BROWNFIELDS: A Listing of Brownfields Sites Source: Environmental Protection Agency

Telephone: 202-566-2777

Included in the listing are brownfields properties addresses by Cooperative Agreement Recipients and brownfields properties addressed by Targeted Brownfields Assessments. Targeted Brownfields Assessments-EPA's Targeted Brownfields Assessments (TBA) program is designed to help states, tribes, and municipalities—especially those without EPA Brownfields Assessment Demonstration Pilots—minimize the uncertainties of contamination often associated with brownfields. Under the TBA program, EPA provides funding and/or technical assistance for environmental assessments at brownfields sites throughout the country. Targeted Brownfields Assessments supplement and work with other efforts under EPA's Brownfields Initiative to promote cleanup and redevelopment of brownfields. Cooperative Agreement Recipients-States, political subdivisions, territories, and Indian tribes become Brownfields Cleanup Revolving Loan Fund (BCRLF) cooperative agreement recipients when they enter into BCRLF cooperative agreements with the U.S. EPA, EPA selects BCRLF cooperative agreement recipients based on a proposal and application process. BCRLF cooperative agreement recipients must use EPA funds provided through BCRLF cooperative agreement for specified brownfields-related cleanup activities.

Date of Government Version: 01/10/05 Database Release Frequency; Semi-Annually Date of Last EDR Contact: 03/14/05 Date of Next Scheduled EDR Contact: 06/13/05

US INST CONTROL: Sites with Institutional Controls

Source: Environmental Protection Agency

Telephone: 703-603-8867

A listing of sites with institutional controls in place. Institutional controls include administrative measures, such as groundwater use restrictions, construction restrictions, property use restrictions, and post remediation care requirements intended to prevent exposure to contaminants remaining on site. Deed restrictions are generally required as part of the institutional controls.

Date of Government Version: 01/10/05 Database Release Frequency: Varies Date of Last EDR Contact: 04/04/05

Date of Next Scheduled EDR Contact: 07/04/05

OTHER DATABASE(S)

Depending on the geographic area covered by this report, the data provided in these specially databases may or may not be complete. For example, the existence of wetlands information data in a specific report does not mean that all wetlands in the area covered by the report are included. Moreover, the absence of any reported wetlands information does not necessarily mean that wetlands do not exist in the area covered by the report.

Oil/Gas Pipelines: This data was obtained by EDR from the USGS in 1994. It is referred to by USGS as GeoData Digital Line Graphs from 1:100,000-Scale Maps. It was extracted from the transportation category including some oil, but primarily gas pipelines.

Electric Power Transmission Line Data

Source: PennWell Corporation Telephone: (800) 823-6277

This map includes information copyrighted by PennWell Corporation. This information is provided on a best effort basis and PennWell Corporation does not guarantee its accuracy nor warrant its fitness for any particular purpose. Such information has been reprinted with the permission of PennWell.

Sensitive Receptors: There are individuals deemed sensitive receptors due to their fragile immune systems and special sensitivity to environmental discharges. These sensitive receptors typically include the elderly, the sick, and children. While the location of all sensitive receptors cannot be determined, EDR indicates those buildings and facilities - schools, daycares, hospitals, medical centers, and nursing homes - where individuals who are sensitive receptors are likely to be located.

AHA Hospitals:

Source: American Hospital Association, Inc.

Telephone: 312-280-5991

The database includes a listing of hospitals based on the American Hospital Association's annual survey of hospitals.

Medical Centers: Provider of Services Listing

Source: Centers for Medicare & Medicaid Services

Telephone: 410-786-3000

A listing of hospitals with Medicare provider number, produced by Centers of Medicare & Medicaid Services,

a federal agency within the U.S. Department of Health and Human Services.

Nursing Homes

Source: National Institutes of Health

Telephone: 301-594-6248

Information on Medicare and Medicaid certified nursing homes in the United States.

Public Schools

Source: National Center for Education Statistics

Telephone: 202-502-7300

The National Center for Education Statistics' primary database on elementary

and secondary public education in the United States. It is a comprehensive, annual, national statistical database of all public elementary and secondary schools and school districts, which contains data that are comparable across all states.

Private Schools

Source: National Center for Education Statistics

Telephone: 202-502-7300

The National Center for Education Statistics' primary database on private school locations in the United States.

Daycare Centers: Child Care Facility List

Source: Department of Health & Human Services

Telephone: 919-662-4499

Flood Zone Data: This data, available in select counties across the country, was obtained by EDR in 1999 from the Federal Emergency Management Agency (FEMA). Data depicts 100-year and 500-year flood zones as defined by FEMA.

NWI: National Wetlands Inventory. This data, available in select counties across the country, was obtained by EDR in 2002 from the U.S. Fish and Wildlife Service.

STREET AND ADDRESS INFORMATION

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GEOCHECK ®- PHYSICAL SETTING SOURCE ADDENDUM

TARGET PROPERTY ADDRESS

DYE BRANCH GLENWOOD MEMORIAL PARK MOORESVILLE, NC 28115

TARGET PROPERTY COORDINATES

Latitude (North): 35.576199 - 35° 34′ 34.3″ Longitude (West): 80.812500 - 80° 48′ 45.0″

Universal Tranverse Mercator: Zone 17 UTM X (Meters): 516989.3 UTM Y (Meters): 3936761.5

Elevation: 834 ft. above sea level

EDR's GeoCheck Physical Setting Source Addendum has been developed to assist the environmental professional with the collection of physical setting source information in accordance with ASTM 1527-00, Section 7.2.3. Section 7.2.3 requires that a current USGS 7.5 Minute Topographic Map (or equivalent, such as the USGS Digital Elevation Model) be reviewed. It also requires that one or more additional physical setting sources be sought when (1) conditions have been identified in which hazardous substances or petroleum products are likely to migrate to or from the property, and (2) more information than is provided in the current USGS 7.5 Minute Topographic Map (or equivalent) is generally obtained, pursuant to local good commercial or customary practice, to assess the impact of migration of recognized environmental conditions in connection with the property. Such additional physical setting sources generally include information about the topographic, hydrologic, hydrogeologic, and geologic characteristics of a site, and wells in the area.

Assessment of the impact of contaminant migration generally has two principle investigative components:

- 1. Groundwater flow direction, and
- 2. Groundwater flow velocity.

Groundwater flow direction may be impacted by surface topography, hydrology, hydrogeology, characteristics of the soil, and nearby wells. Groundwater flow velocity is generally impacted by the nature of the geologic strata. EDR's GeoCheck Physical Setting Source Addendum is provided to assist the environmental professional in forming an opinion about the impact of potential contaminant migration.

GROUNDWATER FLOW DIRECTION INFORMATION

Groundwater flow direction for a particular site is best determined by a qualified environmental professional using site-specific well data. If such data is not reasonably ascertainable, it may be necessary to rely on other sources of information, such as surface topographic information, hydrologic information, hydrogeologic data collected on nearby properties, and regional groundwater flow information (from deep aquifers).

TOPOGRAPHIC INFORMATION

Surface topography may be indicative of the direction of surficial groundwater flow. This information can be used to assist the environmental professional in forming an opinion about the impact of nearby contaminated properties or, should contamination exist on the target property, what downgradient sites might be impacted.

TARGET PROPERTY TOPOGRAPHY

USGS Topographic Map:

35080-E7 MOORESVILLE, NC

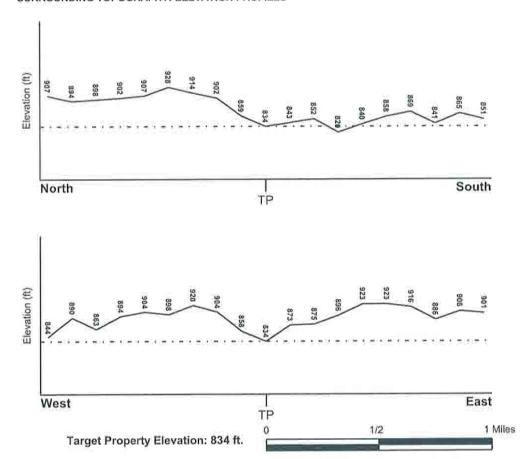
General Topographic Gradient:

General SSE

Source:

USGS 7.5 min quad index

SURROUNDING TOPOGRAPHY: ELEVATION PROFILES



Source: Topography has been determined from the USGS 7.5' Digital Elevation Model and should be evaluated on a relative (not an absolute) basis. Relative elevation information between sites of close proximity should be field verified.

HYDROLOGIC INFORMATION

Surface water can act as a hydrologic barrier to groundwater flow. Such hydrologic information can be used to assist the environmental professional in forming an opinion about the impact of nearby contaminated properties or, should contamination exist on the target property, what downgradient sites might be impacted.

Refer to the Physical Setting Source Map following this summary for hydrologic information (major waterways and bodies of water).

FEMA FLOOD ZONE

FEMA Flood

Target Property County IREDELL, NC

Electronic Data

Not Available

Flood Plain Panel at Target Property:

Not Reported

Additional Panels in search area:

Not Reported

NATIONAL WETLAND INVENTORY

NWI Electronic

NWI Quad at Target Property

Data Coverage

MOORESVILLE

YES - refer to the Overview Map and Detail Map

HYDROGEOLOGIC INFORMATION

Hydrogeologic information obtained by installation of wells on a specific site can often be an indicator of groundwater flow direction in the immediate area. Such hydrogeologic information can be used to assist the environmental professional in forming an opinion about the impact of nearby contaminated properties or, should contamination exist on the target property, what downgradient sites might be impacted.

AQUIFLOW®

Search Radius: 1.000 Mile.

EDR has developed the AQUIFLOW Information System to provide data on the general direction of groundwater flow at specific points. EDR has reviewed reports submitted by environmental professionals to regulatory authorities at select sites and has extracted the date of the report, groundwater flow direction as determined hydrogeologically, and the depth to water table.

> MAP ID Not Reported

LOCATION FROM TP GENERAL DIRECTION GROUNDWATER FLOW

GROUNDWATER FLOW VELOCITY INFORMATION

Groundwater flow velocity information for a particular site is best determined by a qualified environmental professional using site specific geologic and soil strata data. If such data are not reasonably ascertainable, it may be necessary to rely on other sources of information, including geologic age identification, rock stratigraphic unit and soil characteristics data collected on nearby properties and regional soil information. In general, contaminant plumes move more quickly through sandy-gravelly types of soils than silty-clayey types of soils.

GEOLOGIC INFORMATION IN GENERAL AREA OF TARGET PROPERTY

Geologic information can be used by the environmental professional in forming an opinion about the relative speed at which contaminant migration may be occurring.

ROCK STRATIGRAPHIC UNIT

GEOLOGIC AGE IDENTIFICATION

Era:

Paleozoic

Category: Plutonic and Intrusive Rocks

System: Series:

Ordovian

Code:

Lower Paleozoic granitic rocks Pzq1 (decoded above as Era, System & Series)

Geologic Age and Rock Stratigraphic Unit Source: P.G. Schruben, R.E. Arndt and W.J. Bawiec, Geology of the Conterminous U.S. at 1:2,500,000 Scale - a digital representation of the 1974 P.B. King and H.M. Beikman Map, USGS Digital Data Series DDS - 11 (1994).

DOMINANT SOIL COMPOSITION IN GENERAL AREA OF TARGET PROPERTY

The U.S. Department of Agriculture's (USDA) Soil Conservation Service (SCS) leads the National Cooperative Soil Survey (NCSS) and is responsible for collecting, storing, maintaining and distributing soil survey information for privately owned lands in the United States. A soil map in a soil survey is a representation of soil patterns in a landscape. Soil maps for STATSGO are compiled by generalizing more detailed (SSURGO) soil survey maps. The following information is based on Soil Conservation Service STATSGO data.

Soil Component Name:

CECIL

Soil Surface Texture:

sandy clay loam

Hydrologic Group:

Class B - Moderate infiltration rates. Deep and moderately deep, moderately well and well drained soils with moderately coarse

textures.

Soil Drainage Class:

Well drained. Soils have intermediate water holding capacity. Depth to

water table is more than 6 feet.

Hydric Status: Soil does not meet the requirements for a hydric soil.

Corrosion Potential - Uncoated Steel: HIGH

Depth to Bedrock Min:

> 60 inches

Depth to Bedrock Max:

> 60 inches

			Soil Layer	Information			
	Bou	ındary		Classi	fication		
Layer	Upper	Lower	Soil Texture Class	AASHTO Group	Unified Soil	Permeability Rate (in/hr)	Soil Reaction (pH)
1	0 inches	7 inches	sandy clay loam	Silt-Clay Materials (more than 35 pct. passing No. 200), Silty Solls.	COARSE-GRAINED SOILS, Sands, Sands with fines, Silty Sand.	Max: 2.00 Min: 0.60	Max: 6.50 Min: 4.50
2	7 inches	11 inches	sandy clay loam	Silt-Clay Materials (more than 35 pct. passing No. 200), Silty Soils.	COARSE-GRAINED SOILS, Sands, Sands with fines, Silty Sand.	Max: 2.00 Min: 0.60	Max: 5.50 Min: 4.50
3	11 inches	50 inches	clay	Silt-Clay Materials (more than 35 pct. passing No. 200), Clayey Soils.	FINE-GRAINED SOILS, Silts and Clays (liquid limit 50% or more), Elastic silt.	Max: 2.00 Min: 0.60	Max: 5.50 Min: 4.50
4	50 inches	75 Inches	variable	Not reported	Not reported	Max: 0.00 Min: 0.00	Max: 0.00 Min: 0.00

OTHER SOIL TYPES IN AREA

Based on Soil Conservation Service STATSGO data, the following additional subordinant soil types may appear within the general area of target property.

Soil Surface Textures: sandy loam

loam clay loam silt loam

very channery - silt loam gravelly - sandy loam

Surficial Soil Types: sandy loam

loam clay loam silt loam

very channery - silt loam gravelly - sandy loam

Shallow Soil Types: silt loam

sandy clay clay silty clay loam

very channery - silt loam

loam

Deeper Soil Types: weathered bedrock

fine sandy loam silty clay loam unweathered bedrock sandy clay loam

ADDITIONAL ENVIRONMENTAL RECORD SOURCES

According to ASTM E 1527-00, Section 7.2.2, "one or more additional state or local sources of environmental records may be checked, in the discretion of the environmental professional, to enhance and supplement federal and state sources... Factors to consider in determining which local or additional state records, if any, should be checked include (1) whether they are reasonably ascertainable, (2) whether they are sufficiently useful, accurate, and complete in light of the objective of the records review (see 7.1.1), and (3) whether they are obtained, pursuant to local, good commercial or customary practice." One of the record sources listed in Section 7.2.2 is water well information. Water well information can be used to assist the environmental professional in assessing sources that may impact groundwater flow direction, and in forming an opinion about the impact of contaminant migration on nearby drinking water wells.

WELL SEARCH DISTANCE INFORMATION

DATABASE

SEARCH DISTANCE (miles)

Federal USGS

1.000

Federal FRDS PWS

Nearest PWS within 1 mile

State Database

1.000

FEDERAL USGS WELL INFORMATION

FROM TP
1/2 - 1 Mile North
1/2 - 1 Mile NNE
1/2 - 1 Mile NNE
1/2 - 1 Mile NNW

FEDERAL FRDS PUBLIC WATER SUPPLY SYSTEM INFORMATION

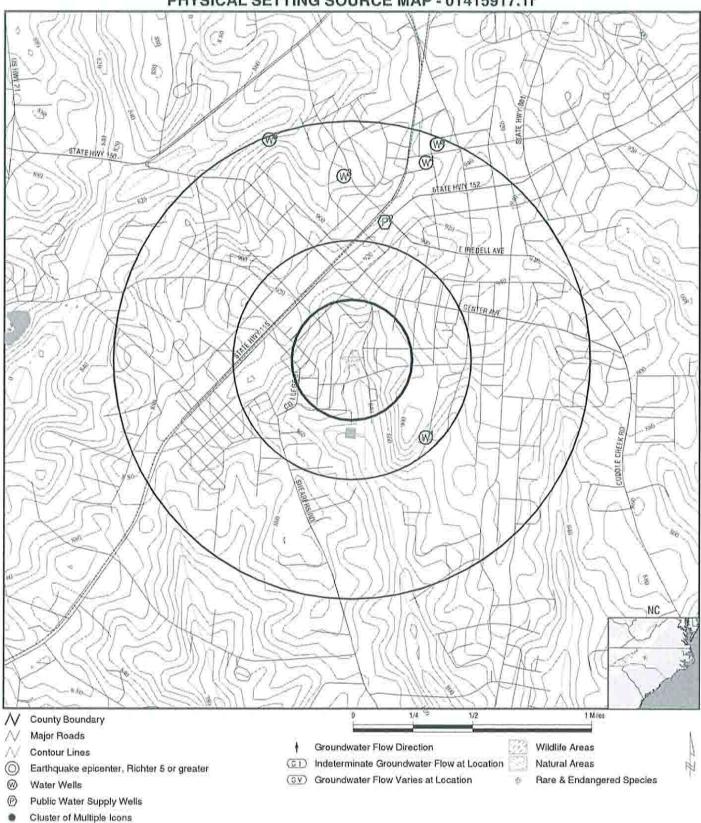
MAP ID	WELL ID	LOCATION FROM TP
2	NC0149414	1/2 - 1 Mile NNE

Note: PWS System location is not always the same as well location.

STATE DATABASE WELL INFORMATION

		LOCATION
MAP ID	WELL ID	FROM TP
1	NCWS002110	1/4 - 1/2 Mile SE

PHYSICAL SETTING SOURCE MAP - 01415917.1r



TARGET PROPERTY: ADDRESS: CITY/STATE/ZIP:

LAT/LONG:

Dye Branch Glenwood Memorial Park MOORESVILLE NC 28115 35.5762 / 80.8125 CUSTOMER: CONTACT: INQUIRY #: DATE: Mulkey Inc. Layna Thrush 01415917.1r May 06, 2005 1:29 pm

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Map ID Direction Distance Elevation

Database

NC WELLS NCWS002110

EDR ID Number

NC0149414

1/4 - 1/2 Mile Higher

Site Name:

WELL #1 0149600 MOORESVILLE

Source code:

S01

PWS ID: City: County:

redell

Longitude:

804825.169

FRDS PWS

Latitude: Availability: 353417.387 Permanent Ground

JOHN MURRAY

Depth:

0

2 NNE

PWS ID:

1/2 - 1 Mile Higher

Type:

Owner:

NC0149414

PWS Status: Active

Date Deactivated Not Reported

Date Initiated: PWS Name:

AMITY LUTH CH

MOORESVILLE, NC 28115

Addressee / Facility:

System Owner/Responsible Party

AMITY LUTH CH

RT 5

7706

MOORESVILLE, NC 28115

Addressee / Facility:

System Owner/Responsible Party

AMITY LUTH CH

RT 5

MOORESVILLE, NC 28115

Facility Latitude: Facility Latitude:

35 35 04 35 44 15 MOORESVILLE Facility Longitude080 48 37 Facility Longitude080 46 15

City Served: Treatment Class:

Untreated

Population:

00000050

PWS currently has or had major violation(s) or enforcement:

Violations information not reported.

ENFORCEMENT INFORMATION:

System Name:

AMITY LUTHERAN CHURCH

Violation Type:

Monitoring, Regular

Contaminant: Compliance Period: NITRATE 2002-01-01 - 2002-12-31

Analytical Value: Enforcement ID:

Violation ID:

0318039

0316019

Enforcement Date:

2003-02-18

Enf. Action:

State Formal NOV Issued

System Name:

Violation ID:

AMITY LUTHERAN CHURCH

Violation Type:

Monitoring, Regular

Contaminant:

NITRATE

Compliance Period:

2002-01-01 - 2002-12-31

0318039

Enforcement ID:

0316018

Enforcement Date:

2003-02-18

Enf. Action:

Analytical Value:

State Public Notif Requested

ENFORCEMENT INFORMATION:

System Name: AMITY LUTHERAN CHURCH

Violation Type: Monitoring, Regular

Contaminant: NITRATE

Compliance Period: 2002-01-01 - 2002-12-31 Analytical Value: Violation ID: 0318039 Enforcement ID:

Violation ID: 0318039 Enforcement ID: 0316020
Enforcement Date: 2003-03-03 Enf. Action: State Compliance Achieved

System Name: AMITY LUTHERAN CHURCH Violation Type: Monitoring, Routine Major (TCR)

Contaminant: COLIFORM (TCR)
Compliance Period: 2000-04-01 - 2000-06-30

 Compliance Period:
 2000-04-01 - 2000-06-30
 Analytical Value:
 0

 Violation ID:
 0100397
 Enforcement ID:
 0013593

 Enforcement Date:
 2000-08-11
 Enf. Action:
 State Formal NOV Issued

System Name: AMITY LUTHERAN CHURCH Violation Type: Monitoring, Routine Major (TCR)

Contaminant: COLIFORM (TCR)
Compliance Period: 2000-07-01 - 2000-09-30 Analytical Value: 0

Violation ID: 0318039 Enforcement ID: 0102540 Enforcement Date: 2000-11-08 Enf. Action: State Formal NOV Issued

System Name: AMITY LUTHERAN CHURCH Violation Type: Monitoring, Routine Major (TCR)

 Contaminant:
 COLIFORM (TCR)

 Compliance Period:
 2002-08-01 - 2002-08-31
 Analytical Value:
 0

 Violation ID:
 0318039
 Enforcement ID:
 0305040

Enforcement Date: 2002-10-01 Enf. Action: State Formal NOV Issued

System Name: AMITY LUTHERAN CHURCH
Violation Type: Monitoring, Routine Major (TCR)
Contaminant: COLIFORM (TCR)

 Contaminant;
 COLIFORM (TCR)

 Compliance Period;
 2000-04-01 - 2000-06-30
 Analytical Value;
 0

 Violation ID:
 0300056
 Enforcement ID;
 0013592

Enforcement Date: 2000-08-11 Enf, Action: State Public Notif Requested

System Name: AMITY LUTHERAN CHURCH
Violation Type: Monitoring, Routine Major (TCR)

 Contaminant:
 COLIFORM (TCR)

 Compliance Period:
 2000-07-01 - 2000-09-30
 Analytical Value;
 0

 Violation ID:
 0318039
 Enforcement ID:
 0102539

Enforcement Date: 2000-11-08 Enf. Action: State Public Notif Requested

System Name: AMITY LUTHERAN CHURCH Violation Type: Monitoring, Routine Major (TCR)

Contaminant: COLIFORM (TCR)
Compliance Period: 2002-08-01 - 2002-08-31 Analytical Value: 0

Violation ID: 0318039 Enforcement ID: 0305039 Enforcement Date; 2002-10-01 Enf. Action: State Public Notif Requested

System Name: AMITY LUTHERAN CHURCH

Violation Type: Monitoring, Routine Major (TCR)
Contaminant: COLIFORM (TCR)
Compliance Period: 2002-08-01 - 2002-08-31 Analytical Value: 0

Violation ID: 0318039 Enforcement ID: 0305041
Enforcement Date: 2002-10-18 Enf. Action: State Public

Enforcement Date: 2002-10-18 Enf. Action: State Public Notif Received

System Name: AMITY LUTHERAN CHURCH

Violation Type: Monitoring, Routine Major (TCR)
Contaminant: COLIFORM (TCR)

 Compliance Period:
 2000-04-01 - 2000-06-30
 Analytical Value:
 0

 Violation ID:
 0006503
 Enforcement ID:
 0300031

Enforcement Date: 2003-03-31 Enf. Action: State Compliance Achieved

ENFORCEMENT INFORMATION:

System Name: Violation Type:

AMITY LUTHERAN CHURCH Monitoring, Routine Major (TCR)

Contaminant: Compliance Period: COLIFORM (TCR) 2000-07-01 - 2000-09-30

Violation ID: Enforcement Date: 0318039 2003-03-31

System Name: Violation Type: AMITY LUTHERAN CHURCH Monitoring, Routine Major (TCR)

Contaminant: Compliance Period: COLIFORM (TCR) 2002-08-01 - 2002-08-31

Violation ID: Enforcement Date: 0318039 2003-03-31

System Name:

AMITY LUTHERAN CHURCH

Violation Type: Contaminant: Compliance Period: Monitoring, Routine Major (TCR) COLIFORM (TCR)

1999-04-01 - 1999-06-30 0000371

Violation ID: Enforcement Date:

1999-08-12

System Name: Violation Type: Contaminant:

AMITY LUTHERAN CHURCH Monitoring, Routine Major (TCR) COLIFORM (TCR)

Compliance Period: Violation ID:

1999-10-01 - 1999-12-31

Enforcement Date:

0000371 2000-02-04

System Name: Violation Type: Contaminant:

AMITY LUTHERAN CHURCH Monitoring, Routine Major (TCR) COLIFORM (TCR)

Compliance Period: Violation ID:

1999-10-01 - 1999-12-31 0003413

Enforcement Date:

2000-02-04 AMITY LUTHERAN CHURCH

System Name: Violation Type: Contaminant:

Monitoring, Routine Major (TCR) COLIFORM (TCR)

Compliance Period: Violation ID:

1999-10-01 - 1999-12-31

Enforcement Date:

0003413 2000-02-15

System Name: Violation Type: AMITY LUTHERAN CHURCH

Contaminant: Compliance Period: Monitoring, Routine Major (TCR) COLIFORM (TCR)

Violation ID:

1999-10-01 - 1999-12-31

Enforcement Date:

System Name:

0003413 2000-02-15

Violation Type: Contaminant:

AMITY LUTHERAN CHURCH Monitoring, Routine Major (TCR)

Compliance Period: Violation ID: 9909608

COLIFORM (TCR) 1999-04-01 - 1999-06-30

Enforcement Date: System Name:

1999-08-12 AMITY LUTHERAN CHURCH

Violation Type: Contaminant: Compliance Period:

Monitoring, Routine Major (TCR) COLIFORM (TCR)

1999-04-01 - 1999-06-30 Violation ID: 9909608 Enforcement Date:

1999-08-12

Analytical Value:

Enforcement ID:

Enf. Action:

0300031

State Compliance Achieved

Analytical Value:

Enforcement ID: 0300031

Enf. Action:

State Compliance Achieved

Analytical Value:

00000000.000000000

Enforcement ID: 9906278

Enf. Action:

State Public Notif Requested

Analytical Value:

00000000.000000000

Enforcement ID: 0006223

Enf. Action:

State Formal NOV Issued

Analytical Value: 0000000.000000000

Enforcement ID: 0006224

Enf. Action: State Public Notif Requested

Analytical Value: 0000000.000000000 Enforcement ID: 0009904

Enf. Action:

State Admin Penalty Assessed

Analytical Value: Enforcement ID:

00000000.000000000

Enf. Action:

0009905

State AO (w/penalty) Issued

0000000.000000000 Analytical Value:

Enforcement ID: 9906277 Enf. Action:

State Formal NOV Issued

Analytical Value:

0000000.000000000

Enforcement ID: 9906278

Enf. Action:

State Public Notif Requested

ENFORCEMENT INFORMATION:

System Name: Violation Type: AMITY LUTHERAN CHURCH Monitoring, Routine Major (TCR)

Contaminant:

COLIFORM (TCR)

Compliance Period: Violation ID:

1999-04-01 - 1999-06-30 9912229

Enforcement Date: 1999-08-12 Analytical Value:

0000000.000000000

Enforcement ID:

9906277

Enf. Action:

State Formal NOV Issued

North 1/2 - 1 Mile Higher

Agency cd:

Coor accr:

State:

Country:

Altitude:

Aquifer Type:

Aquifer:

Well depth:

USGS

IR-113

Site no:

353514080484801

Site name: Latitude: Longitude: Dec Ion:

Dec lallong datum:

353514 0804848 -80.81312796 S

> NAD83 37

US

Location map: Not Reported Not Reported Altitude accuracy: Not Reported Not Reported

Hydrologic: Topographic: Hillside (slope) Site type:

Date inventoried: Local standard time flag: Ground-water other than Spring Not Reported

Not Reported Not Reported

Source of depth data: Real time data flag: Daily flow data end date: 148.0 reporting agency (generally USGS)roject number:

0000-00-00 0000-00-00 Peak flow data begin date:

Peak flow data count: Water quality data end date:0000-00-00

Ground water data begin date: 1954-00-00

Ground water data count:

FED USGS

USGS2259828

Dec lat: Coor meth: Latlong datum: District:

County: Land net: Map scale: Altitude method: Altitude datum:

Date construction:

35.58735962 NAD27 37 097 Not Reported

Not Reported Not Reported Not Reported

Not Reported EST

Mean greenwich time offset: Single well, other than collector or Ranney type Type of ground water site:

Not Reported Hole depth: 453709900

Daily flow data begin date: 0000-00-00 Daily flow data count: 0000-00-00

Peak flow data end date: Water quality data begin date: 0000-00-00 Water quality data count:

Ground water data end date: 1954-00-00

Ground-water levels, Number of Measurements: 1

Feet below Date Surface

Feet to Sealevel

1954 25

NNE 1/2 - 1 Mile Higher

FED USGS

USGS2259832

USGS Site no: 353517080482601 Agency cd: Site name: IR-115 Latitude: 353517 35.58819307 0804826 Dec lat: Longitude: -80.8070167 Coor meth: Dec Ion: NAD27 Latlong datum: Coor accr: Dec latlong datum: NAD83 District: 37 097 County: State: 37 Not Reported Country: US Land net: Not Reported Not Reported Map scale: Location map: Not Reported Not Reported Altitude method: Altitude: Not Reported Altitude accuracy: Not Reported Altitude datum: Not Reported Hydrologic; Topographic: Hillside (slope) Ground-water other than Spring Not Reported Date construction: Site type: Mean greenwich time offset: Date inventoried: Not Reported EST Type of ground water site: Single well, other than collector or Ranney type Local standard time flag: Aquifer Type: Not Reported Aquifer: Not Reported Hole depth: Not Reported Well depth: 400.0 453709900 reporting agency (generally USGS) roject number: Source of depth data: Daily flow data begin date: 0000-00-00 Real time data flag: Daily flow data end date: 0000-00-00 Daily flow data count: 0000-00-00 Peak flow data begin date: 0000-00-00 Peak flow data end date: Water quality data begin date: 0000-00-00 Peak flow data count: Water quality data end date:0000-00-00 Water quality data count: Ground water data end date: 1954-00-00 Ground water data begin date: 1954-00-00 Ground water data count:

Ground-water levels, Number of Measurements: 1

Feet below

Feet to

Date

Surface

Sealevel

1954

25

NNE 1/2 - 1 Mile Higher

FED USGS

USGS2259834

353521080482301 USGS Site no: Agency cd: Site name: IR-114 353521 Latitude: 35.5893042 Longitude: 0804823 Dec lat: -80.80618334 Coor meth: Dec lon: Latlong datum: NAD27 Coor accr: NAD83 District: 37 Dec latlong datum: 097 County: State: 37 Not Reported Country: US Land net: Map scale: Not Reported Not Reported Location map: Not Reported Altitude: Not Reported Altitude method: Not Reported Not Reported Altitude datum: Altitude accuracy: Not Reported Hydrologic:

Topographic: Hillside (slope)

Site type: Ground-water other than Spring

Date inventoried: Not Reported

Aquifer Type: Not Reported

Local standard time flag:

Aquifer: Not Reported

Well depth: 270.0

Source of depth data:

Real time data flag: Daily flow data end date: 00-00-00 Peak flow data begin date: 0000-00-00

Hole depth: reporting agency (generally USGS) roject number:

Date construction:

Daily flow data begin date: Daily flow data count: Peak flow data end date:

Mean greenwich time offset:

Type of ground water site:

Not Reported

Single well, other than collector or Ranney type

Not Reported 453709900

0000-00-00 0000-00-00

TC01415917.1r Page A-12

Site no:

Peak flow data count:

Water quality data end date:0000-00-00

Ground water data begin date: 1954-00-00

Ground water data count:

Ground-water levels, Number of Measurements: 1

Feet below

Feet to

Date

Surface

Sealevel

1954

25

USGS2259836

WNN 1/2 - 1 Mile

Agency cd:

Site name:

Latitude:

Longitude:

Dec Ion: Coor accr.

Dec latlong datum:

State: Country:

Location map: Altitude:

Altitude accuracy:

Hydrologic:

Topographic:

Site type:

Date inventoried:

Local standard time flag:

Aquifer Type: Aquifer:

Well depth:

Source of depth data:

Real time data flag:

Daily flow data end date:

Peak flow data begin date: Peak flow data count:

Ground water data begin date: Not Reported

USGS

IR-112 353522

0804908 -80.81868363

NAD83 37

US Not Reported Not Reported Not Reported

Not Reported Hillside (slope)

Ground-water other than Spring

Not Reported

Not Reported

Not Reported 150.0

reporting agency (generally USGS) roject number: Not Reported

Not Reported Not Reported

Not Reported

Water quality data end date: Not Reported

Ground water data count: Not Reported

FED USGS

353522080490801

35.58958176 Dec lat: Coor meth: Latlong datum: NAD27 District: 37

Water quality data begin date: 0000-00-00

Ground water data end date: 1954-00-00

Water quality data count:

County: 097 Not Reported Land net: Not Reported Map scale: Not Reported Altitude method:

Attitude datum: Not Reported

Not Reported

Mean greenwich time offset: Type of ground water site:

Date construction:

Single well, other than collector or Ranney type

Hole depth: Not Reported

453709900 Not Reported Daily flow data begin date: Not Reported Daily flow data count: Not Reported Peak flow data end date: Water quality data begin date: Not Reported

Water quality data count: Not Reported Ground water data end date: Not Reported

Ground-water levels, Number of Measurements: 0

AREA RADON INFORMATION

State Database: NC Radon

Radon Test Results

County	Result Type	Total Sites	Avg pCi/L	Range pCi/L
ACCOMMON W	Hay Kee It IV		0 102	0.00.0.50
IREDELL	Statistical	52	1.83 2.27	-0.80-9.50 0.00-9.50
IREDELL	Non-Statistical	84	2.21	0.00-0.00

Federal EPA Radon Zone for IREDELL County: 2

Note: Zone 1 indoor average level > 4 pCl/L.

: Zone 2 Indoor average level >= 2 pCi/L and <= 4 pCi/L.

: Zone 3 indoor average level < 2 pCi/L:

Federal Area Radon Information for Zip Code: 28115

Number of sites tested: 11

Area	Average Activity	% <4 pCi/L	% 4-20 pCi/L	% >20 pCi/L
Living Area - 1st Floor Living Area - 2nd Floor	1.255 pCi/L Not Reported	100% Not Reported	0% Not Reported	0% Not Reported
Basement	4.267 pCI/L	67%	33%	0%

PHYSICAL SETTING SOURCE RECORDS SEARCHED

TOPOGRAPHIC INFORMATION

USGS 7.5' Digital Elevation Model (DEM)

Source: United States Geologic Survey

EDR acquired the USGS 7.5' Digital Elevation Model in 2002, 7.5-Minute DEMs correspond to the USGS 1:24,000- and 1:25,000-scale topographic quadrangle maps.

HYDROLOGIC INFORMATION

Flood Zone Data: This data, available in select counties across the country, was obtained by EDR in 1999 from the Federal Emergency Management Agency (FEMA). Data depicts 100-year and 500-year flood zones as defined by FEMA.

NWI: National Wetlands Inventory. This data, available in select counties across the country, was obtained by EDR in 2002 from the U.S. Fish and Wildlife Service.

HYDROGEOLOGIC INFORMATION

AQUIFLOWR Information System

Source: EDR proprietary database of groundwater flow information

EDR has developed the AQUIFLOW Information System (AIS) to provide data on the general direction of groundwater flow at specific points. EDR has reviewed reports submitted to regulatory authorities at select sites and has extracted the date of the report, hydrogeologically determined groundwater flow direction and depth to water table information.

GEOLOGIC INFORMATION

Geologic Age and Rock Stratigraphic Unit

Source: P.G. Schruben, R.E. Arndt and W.J. Bawiec, Geology of the Conterminous U.S. at 1:2,500,000 Scale - A digital representation of the 1974 P.B. King and H.M. Beikman Map, USGS Digital Data Series DDS - 11 (1994).

STATSGO: State Soil Geographic Database

Source: Department of Agriculture, Natural Resources Conservation Services

The U.S. Department of Agriculture's (USDA) Natural Resources Conservation Service (NRCS) leads the national Conservation Soil Survey (NCSS) and is responsible for collecting, storing, maintaining and distributing soil survey information for privately owned lands in the United States. A soil map in a soil survey is a representation of soil patterns in a landscape. Soil maps for STATSGO are compiled by generalizing more detailed (SSURGO) soil survey maps.

ADDITIONAL ENVIRONMENTAL RECORD SOURCES

FEDERAL WATER WELLS

PWS: Public Water Systems

Source: EPA/Office of Drinking Water

Telephone: 202-564-3750

Public Water System data from the Federal Reporting Data System. A PWS is any water system which provides water to at least 25 people for at least 60 days annually. PWSs provide water from wells, rivers and other sources.

PWS ENF: Public Water Systems Violation and Enforcement Data

Source: EPA/Office of Drinking Water

Telephone: 202-564-3750

Violation and Enforcement data for Public Water Systems from the Safe Drinking Water Information System (SDWIS) after August 1995. Prior to August 1995, the data came from the Federal Reporting Data System (FRDS).

USGS Water Wells: USGS National Water Inventory System (NWIS)

This database contains descriptive information on sites where the USGS collects or has collected data on surface water and/or groundwater. The groundwater data includes information on wells, springs, and other sources of groundwater.

PHYSICAL SETTING SOURCE RECORDS SEARCHED

STATE RECORDS

NC Natural Areas: Significant Natural Heritage Areas

Source: Center for Geographic Information and Analysis

Telephone: 919-733-2090

A polygon converage identifying sites (terrestrial or aquatic that have particular biodiversity significance.

A site's significance may be due to the presenceof rare species, rare or hight quality natural communities, or other important ecological features.

NC Game Lands: Wildlife Resources Commission Game Lands

Source: Center for Geographic Information and Analysis

Telephone: 919-733-2090

All publicly owned game lands managed by the North Carolina Wildlife Resources Commission and as listed in Hunting and Fishing Maps.

NC Natural Heritage Sites: Natural Heritage Element Occurrence Sites

Source: Center for Geographic Information and Analysis

Telephone: 919-733-2090

A point coverage identifying locations of rare and endangered species, occurrences of exemplary or unique natural ecosystems (terrestrial or aquatic), and special animal habitats (e.g., colonial waterbird nesting sites).

North Carolina Public Water Supply Wells

Source: Department of Environmental Health

Telephone: 919-715-3243

RADON

State Database: NC Radon

Source: Department of Environment & Natural Resources

Telephone: 919-733-4984

Radon Statistical and Non Statiscal Data

Area Radon Information

Source: USGS

Telephone: 703-356-4020

The National Radon Database has been developed by the U.S. Environmental Protection Agency (USEPA) and is a compilation of the EPA/State Residential Radon Survey and the National Residential Radon Survey. The study covers the years 1986 - 1992. Where necessary data has been supplemented by information collected at private sources such as universities and research institutions.

EPA Radon Zones

Source: EPA

Telephone: 703-356-4020

Sections 307 & 309 of IRAA directed EPA to list and identify areas of U.S. with the potential for elevated indoor

OTHER

Airport Landing Facilities: Private and public use landing facilities

Source: Federal Aviation Administration, 800-457-6656

Epicenters: World earthquake epicenters, Richter 5 or greater

Source: Department of Commerce, National Oceanic and Atmospheric Administration

Dye Branch Stream Restoration Cemetery Branch 5/26/2005 Project: Stream:

Date:

Location:

Mooresville, NC

Reach: Observers: Trib (Existing) Mulkey

					nsionless Shear Stres	ss:	
Malue	I Describe				834(di/d50)^-0.872		
Value	Variable			V	Definition		
6	di mm	D50 from	Riffle	or	Pavement*		*Choose
2	d50 mm	D50 from	Bar Sample	or	Sub Pavement*		One
0.0320	Tci	Critical Dime	nsionless Shear S	Stress			
				largest p	oth Required for Entra particle in Bar Sample 1.65 = submerged	4	eight of sedimer
88.9	mm	Largest Bar	Sample Particle in	nmm			
0.29	Di ft	Largest Bar	Sample Particle in	ı ft			
0.0190	Se ft/ft	Bankfull Wat	er Surface Slope				
0.81	dr ft	Bankfulli Mea	an Depth Require	d			
0.97	de ft	The same of the sa	n Depth (From Ri		s Section)		
de/dr=	1.20	if = 1		<	1		>1
Choose one	e:	Stable		argest p	ding Slope Required for E article in Bar Sample	ntrainme	
Choose one		Stable	of I	Surface largest p	ding Slope Required for E article in Bar Sample	ntrainme	nt
Choose one	Di ft	Largest Bar S	of I Sr = (Tci*1.6 Sample Particle	Surface largest p 65*Di)/de	ding Slope Required for Earticle in Bar Sample 1.65 = submerged	ntrainme	nt
0.29 0.97	Dift de ft	Largest Bar S Bankfull Mea	of I Sr = (Tcl*1.6 Sample Particle n Depth (<i>From Ri</i>	Surface largest p 65*Di)/de	ding Slope Required for Earticle in Bar Sample 1.65 = submerged	ntrainme	nt
0.29 0.97 0.0159	Dift de ft Sr ft/ft	Largest Bar S Bankfull Mea Bankfull Wat	of I Sr = (Tci*1.6 Sample Particle	Surface largest p 65*Di)/de ifffle Cros Required	ding Slope Required for Earticle in Bar Sample 1.65 = submerged SS Section)	ntrainme	nt
0.29 0.97 0.0159 Se/Sr=	Dift de ft Sr ft/ft	Largest Bar S Bankfull Mea Bankfull Wat if = 1	of I Sr = (Tcl*1.6 Sample Particle n Depth (<i>From Ri</i>	r Surface largest p 65*Di)/de ifffle Cros Required	ding Slope Required for Earticle in Bar Sample 1.65 = submerged SS Section)	ntrainme	nt eight of sediment
0.29 0.97 0.0159 Se/Sr=	Dift de ft Sr ft/ft	Largest Bar S Bankfull Mea Bankfull Wat	of I Sr = (Tci*1.6 Sample Particle n Depth (From Ri er Surface Slope	r Surface largest p 65*DI)/de ifffle Cros Required < aggra	ding Slope Required for E article in Bar Sample 1.65 = submerged SS Section) I I ding	intrainme : specific we	nt eight of sediment >1 Degrading
0.29 0.97	Dift de ft Sr ft/ft	Largest Bar S Bankfull Mea Bankfull Wat if = 1	of I Sr = (Tci*1.6 Sample Particle n Depth (From Ri er Surface Slope	r Surface largest p 65*DI)/de ifffle Cros Required < aggra	ding Slope Required for Earticle in Bar Sample 1.65 = submerged SS Section)	intrainme : specific we	nt eight of sediment >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one	Dift de ft Sr ft/ft 1.20 e:	Largest Bar S Bankfull Mea Bankfull Wat if = 1	of I Sr = (Tci*1.6 Sample Particle n Depth (From Ri er Surface Slope	r Surface largest p 65*DI)/de ifffle Cros Required < aggra	ding Slope Required for E article in Bar Sample 1.65 = submerged SS Section) I I ding	intrainme : specific we	nt eight of sediment >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one	Dift de ft Sr ft/ft 1.20 e:	Largest Bar S Bankfull Mea Bankfull Wat if = 1	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri In Surface Slope Sediment Trans	r Surface largest p 65*DI)/de ifffle Cros Required < aggra	ding Slope Required for Estricle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull St	intrainme : specific we	nt eight of sediment >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one	Dift de ft Sr ft/ft 1.20 e: y lbs/cu ft R=A/Wp	Largest Bar S Bankfull Mea Bankfull Wat if = 1 Stable Density of wa	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri In Surface Slope Sediment Transiter	r Surface largest p 65*Di)/de ifffle Cros Required aggra	ding Slope Required for Estricle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull St	intrainme : specific we	nt eight of sediment >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one 62.4 0.76 6.76	Dift de ft Sr ft/ft 1.20 e: y lbs/cu ft R=A/Wp A sq ft	Largest Bar S Bankfull Mea Bankfull Wat if = 1 Stable Density of wa	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri In Surface Slope Sediment Trans	r Surface largest p 65*Di)/de ifffle Cros Required aggra	ding Slope Required for Estricle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull St	intrainme : specific we	nt eight of sedimer >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one 62.4 0.76 6.76 8.92	Dift de ft Sr ft/ft 1.20 e: y lbs/cu ft R=A/Wp A sq ft Wp	Largest Bar S Bankfull Mea Bankfull Wat if = 1 Stable Density of wa Bankfull Cros Wetted parar	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri In Ser Surface Slope I Sediment Transiter In Sectional Area In Sectional Area	r Surface largest p 65*Di)/de ifffle Cros Required aggra	ding Slope Required for Estricle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull St	intrainme : specific we	nt eight of sedimer >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one 62.4 0.76 6.76 8.92 0.0190	Di ft de ft Sr ft/ft 1.20 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft	Largest Bar S Bankfull Mea Bankfull Wat if = 1 Stable Density of wa Bankfull Cros Wetted parar	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri In Ser Surface Slope I Sediment Transter Iter In Sectional Area	r Surface largest p 65*Di)/de ifffle Cros Required aggra	ding Slope Required for Estricle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull St	intrainme : specific we	nt eight of sediment >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one 62.4 0.76 6.76 8.92 0.0190	Dift de ft Sr ft/ft 1.20 e: y lbs/cu ft R=A/Wp A sq ft Wp	Largest Bar S Bankfull Mea Bankfull Wat if = 1 Stable Density of wa Bankfull Cros Wetted parar Bankfull Wat Tc = yRS	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri er Surface Slope Sediment Tran Itter Is-Sectional Area Ineter Ineter Surface Slope	r Surface argest p 65*DI)/de ifffle Cros Required aggra asport V	ding Slope Required for Estricle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull St	intrainme : specific we	nt eight of sedimer >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one 62.4 0.76 6.76 8.92 0.0190 0.898504	Di ft de ft Sr ft/ft 1.20 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft	Largest Bar S Bankfull Mea Bankfull Wat if = 1 Stable Density of wa Bankfull Cros Wetted parar Bankfull Wat Tc = yRS Largest Bar S	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri er Surface Slope Sediment Tran Iter Is-Sectional Area Ineter Is Surface Slope Sample Particle (In	r Surface largest p 65*DI)/de ifffle Cros Required aggra nsport V	ding Slope Required for Earticle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull Si Tc = yRS	intrainme : specific we	nt eight of sedimer >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one 62.4 0.76 6.76 8.92 0.0190 0.898504	Di ft de ft Sr ft/ft 1.20 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft	Largest Bar S Bankfull Mea Bankfull Wat if = 1 Stable Density of wa Bankfull Cros Wetted parar Bankfull Wat Tc = yRS Largest Bar S	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri er Surface Slope Sediment Tran Itter Is-Sectional Area Ineter Ineter Surface Slope	r Surface largest p 65*DI)/de ifffle Cros Required aggra nsport V	ding Slope Required for Earticle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull Si Tc = yRS	intrainme : specific we	nt eight of sedimer >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one 62.4 0.76 6.76 8.92 0.0190 0.898504	Dift de ft Sr ft/ft 1.20 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft Di mm	Largest Bar S Bankfull Mea Bankfull Wat if = 1 Stable Density of wa Bankfull Cros Wetted parar Bankfull Wat Tc = yRS Largest Bar S Moveable Pa	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri er Surface Slope Sediment Tran Iter Iter Iter Iter Iter Iter Iter Iter	r Surface largest p 65*Di)/de ifffle Cros Required aggra asport V	ding Slope Required for Earticle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull Si Tc = yRS	near Stres	nt eight of sedimer >1 Degrading
0.29 0.97 0.0159 Se/Sr= Choose one 62.4 0.76 6.76 8.92 0.0190 0.898504 88.9	Dift de ft Sr ft/ft 1.20 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft Di mm	Largest Bar S Bankfull Mea Bankfull Wat if = 1 Stable Density of wa Bankfull Cros Wetted parar Bankfull Wat Tc = yRS Largest Bar S Moveable Pa	of I Sr = (Tci*1.6 Sample Particle In Depth (From Ri er Surface Slope Sediment Tran Iter Iter Iter Iter Iter Iter Iter Iter	r Surface largest p 65*Di)/de ifffle Cros Required aggra asport V	ding Slope Required for Bearticle in Bar Sample 1.65 = submerged SS Section) I I ding alidation - Bankfull Si Tc = yRS I Shear Stress I field book: p.190; Blu	near Stres	nt eight of sedimer >1 Degrading

Project: Dye Branch Stream Restoration Stream:

Cemetery Branch

Date: 5/26/2005 Location:

Mooresville, NC

Reach:

Proposed UT

Observers:

			Critic		ensionless Shear Stress: 0834(di/d50)^-0.872	
Value	Variable				Definition	
6	di mm	D50 from	Riffle	or	Pavement*	*Choose
1.8	d50 mm	D50 from	Bar Sample	or	Sub Pavement*	One
0.0292	Tci	Critical Dime	ensionless Shear	Stress		
			of dr = (Tci*1.	largest 65*DI)/S	epth Required for Entrain particle in Bar Sample: ie 1.65 = submerged spo	
88.9	mm	Largest Bar	Sample Particle is	n mm		
0.29	Di ft	Largest Bar	Sample Particle in	ı ft		
0.0190	Se ft/ft	Bankfull Wa	ter Surface Slope	\		
0.74	dr ft	Bankfulli Me	an Depth Require	d		
0.70	de ft	Bankfull Me	an Depth (From F	ifffle Cro	oss Section)	
de/dr=	0.95	if = 1			<1	>1
Choose on		Stable		aggr	ading	Degrading
0.29	Di ft		Sr = (Tci*1. Sample Particle			ecific weight of sedimen
120000000000000000000000000000000000000	de ft		an Depth (From F	ittle Cr	nes Cootion\	
0.0201			iter Surface Slope			
Se/Sr=	0.95				<1	>1
Choose on	Newson	Stable		aggr	ading	Degrading
			Sediment Tra	nsport	Validation - Bankfull Shea Tc = yRS	ar Stress
	y lbs/cu ft	Density of w	vater			
0.61	R=A/Wp					
	A sq ft	to his his William Address to the single form the	oss-Sectional Area			
11.4		Wetted peri				
0.0190			iter Surface Slope	6		
	Tc lb/sqr ft	Tc = yRS				
88.9	Di mm		Sample Particle (
Gestella Meninson			'article size (mm) a			THE EASTER
OF 4FO	mm*	predicted	by the Sheilds dia	gram, R	ed field book: p.190; Blue:	p.238
35-150	1		hear Stress Requ			

^{*}Modified Shields Curve data from Rosgen 2001

 Project:
 Dye Branch Stream Restoration
 Location:
 Mooresville, NC

 Stream:
 Dye Branch
 Reach:
 Reach 3 (Existing)

 Date:
 5/26/2005
 Observers:
 Mulkey

				al Dimensionless Shear Stree Tci = 0.0834(di/d50)^-0.872	ss:
Value	Variable			Definition	
2.6	di mm	D50 from	Riffle	or Pavement*	*Choose
2.8	d50 mm	D50 from	Bar Sample	or Sub Pavement*	One
0.0890	Tci	Critical Dime	ensionless Shear	Stress	
			of	lean Depth Required for Entra largest particle in Bar Sample 55*Di)/Se 1.65 = submerged	•
45.7		The second secon	Sample Particle in	- USS A CHIEF	
0.15	Di ft	Largest Bar	Sample Particle in	ı ft	
0.0110	Se ft/ft	Bankfull Wa	ter Surface Slope		
2.00	dr ft	Bankfulli Me	an Depth Require	d	
1.18	de ft	Bankfull Me	an Depth (From F	lifffle Cross Section)	
de/dr=	0.59	if = 1		<1	>1
Choose one		Stable		aggrading	Degrading
0.15	Di ft	Largest Bar	Sr = (Tcl*1.6 Sample Particle	largest particle in Bar Sample 65*Di)/de 1.65 = submerged	specific weight of sedimen
	de ft			ifffle Cross Section)	
1.18					
0.0187		Bankfull Wa	ter ourrace Stope	Required	
		Bankfull Wa if = 1	ter ourrace Stope	required <1	>1
0.0187	Sr ft/ft 0.59		ter surface slope		>1 Degrading
0.0187 Se/Sr=	Sr ft/ft 0.59	if = 1		<1	Degrading
0.0187 Se/Sr= Choose one	Sr ft/ft 0.59 e: y lbs/cu ft	if = 1	Sediment Trai	<1 aggrading asport Validation - Bankfull S	Degrading
0.0187 Se/Sr= Choose one	Sr ft/ft 0.59	if = 1 Stable	Sediment Trai	<1 aggrading asport Validation - Bankfull S	Degrading
0.0187 Se/Sr= Choose one 62.4 1.02 17.4	Sr ft/ft 0.59 e; y lbs/cu ft R=A/Wp A sq ft	if = 1 Stable Density of w	Sediment Trai	<1 aggrading nsport Validation - Bankfull S Tc = yRS	Degrading
0.0187 Se/Sr= Choose one 62.4 1.02 17.4	Sr ft/ft 0.59 e: y lbs/cu ft R=A/Wp A sq ft Wp	if = 1 Stable Density of w Bankfull Crowetted para	Sediment Trainater ass-Sectional Area	aggrading asport Validation - Bankfull S Tc = yRS	Degrading
0.0187 Se/Sr= Choose one 62.4 1.02 17.4 17.11 0.0110	Sr ft/ft 0.59 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft	if = 1 Stable Density of w Bankfull Cro Wetted para Bankfull Wa	Sediment Trai	aggrading asport Validation - Bankfull S Tc = yRS	Degrading
0.0187 Se/Sr= Choose one 62.4 1.02 17.4 17.11 0.0110 0.698034	sr ft/ft 0.59 e; y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft	if = 1 Stable Density of w Bankfull Cro Wetted para Bankfull Wa Tc = yRS	Sediment Trainater Ses-Sectional Area Timeter Iter Surface Slope	aggrading nsport Validation - Bankfull S Tc = yRS	Degrading
0.0187 Se/Sr= Choose one 62.4 1.02 17.4 17.11 0.0110 0.698034	Sr ft/ft 0.59 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft	if = 1 Stable Density of w Bankfull Cro Wetted para Bankfull Wa Tc = yRS Largest Bar	Sediment Trainstance Sectional Areastmeter Sectional Slope Sample Particle (aggrading nsport Validation - Bankfull S Tc = yRS	Degrading
0.0187 Se/Sr= Choose one 62.4 1.02 17.4 17.11 0.0110 0.698034 45.7	y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft Di mm	if = 1 Stable Density of w Bankfull Cro Wetted para Bankfull Wa Tc = yRS Largest Bar Moveable P	Sediment Trainstance Sectional Area	aggrading nsport Validation - Bankfull S Tc = yRS mm) at Bankfull Shear Stress	Degrading hear Stress
0.0187 Se/Sr= Choose one 62.4 1.02 17.4 17.11 0.0110 0.698034	y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft Di mm	if = 1 Stable Density of w Bankfull Cro Wetted para Bankfull Wa Tc = yRS Largest Bar Moveable P predicted	Sediment Trainstance Sectional Area Section	aggrading nsport Validation - Bankfull S Tc = yRS	Degrading hear Stress

^{*}Modified Shields Curve data from Rosgen 2001

Project: Dye Branch Stream Restoration

Location: Reach: Mooresville, NC

Stream: I

Dye Branch 5/26/2005

Reach: Observers: Proposed Reach 3

				al Dimensionless Shear Str Tci = 0.0834(di/d50)^-0.872	ess:
Value	Variable	T		Definition	
2.6	di mm	D50 from	Riffle	or Pavement*	*Choose
2.8	d50 mm	D50 from	Bar Sample	or Sub Pavement*	One
0.0890	Tci	Critical Dime	ensionless Shear	Stress	
			of	lean Depth Required for Ent largest particle in Bar Samp 55*DI)/Se 1,65 = submerge	le:
45.7	mm	Largest Bar	Sample Particle in	n mm	
0.15	Di ft	Largest Bar	Sample Particle in	n ft	
0.0102	Se ft/ft	Bankfull Wa	ter Surface Slope		
2.16	dr ft	Bankfulli Me	an Depth Require	d	
1.90	de ft			lifffle Cross Section)	
de/dr=	0.88	3 if = 1	***	<1	>1
Choose on	e:	Stable		aggrading	Degrading
0.15	Di ft	Largest Bar	Sr = (Tci*1.6 Sample Particle	55*Di)/de 1,65 = submerge	d specific weight of sedimen
	de ft			ifffle Cross Section)	
0.0116			ter Surface Slope		
Se/Sr=	0.88			<1	>1
Choose on	e:	Stable		aggrading	Degrading
			Sediment Tra	nsport Validation - Bankfull Tc = yRS	Shear Stress
	y lbs/cu ft	Density of w	ater		
1.07	R=A/Wp				
	A sq ft		ss-Sectional Area	<u> </u>	
17.6		Wetted peri			
0.0102			ter Surface Slope		
	To lb/sqr ft	Tc ≃ yRS			
45.7	Di mm		Sample Particle (
		Moveable P	article size (mm) a	at Bankfull Shear Stress	
				market and the second	21 000
35-120	mm*	predicted		gram, Red field book: p.190; I red to move Di (lb/ft2)	3lue: p.238

^{*}Modified Shields Curve data from Rosgen 2001

Project:

Dye Branch Stream Restoration

Mooresville, NC

Stream: Date: Dye Branch 5/26/2005 Location: Reach:

Reach 2 (Existing)

Observers:

Mulkey

				al Dimensionle Tci = 0.0834(di/	d50)^-0.872	ss:
Value	Variable			Definition	on	
9	di mm	D50 from	Riffle	or Pav	ement*	*Choose
2.8	d50 mm	D50 from	Bar Sample	or Sub Pa	vement*	One
0.0301	Tci	Critical Dime	ensionless Shear	Stress		
			of	lean Depth Req largest particle 55*Di)/Se 1.65	in Bar Sample	
	mm		Sample Particle in			
0.08	Di ft	Largest Bar	Sample Particle in	n ft		
0.0080	Se ft/ft	Bankfull Wa	ter Surface Slope			
0.49	dr ft	Bankfulll Me	an Depth Require	d		
1.63	de ft	Bankfull Me	an Depth (<i>From F</i>	ifffle Cross Secti	ion)	
de/dr=	3.33	if = 1		<1		>1
Choose on	e:	Stable		aggrading		Degrading
			Sr = (Tci*1.6	largest particle 55*Di)/de 1.65	in Bar Sample = submerged s	: specific weight of sedimen
	Dift		Sample Particle	iiii - Caaaa Caal	re-x	
0.0024	de ft		an Depth (<i>From F</i> ter Surface Slope		ion)	
Se/Sr=	3.33		ter Suriace Slope	<1		>1
Choose on	1004-730	Stable		aggrading		Degrading
				nsport Validatio		
	y lbs/cu ft	Density of w	ater			
	R=A/Wp	D-216 0-2				
18.13	A sq ft	Wetted para	ss-Sectional Area			
0.0080			ter Surface Slope			
	Tc lb/sqr ft	Tc = yRS	ter ourrace orope	,		
	Di mm		Sample Particle (mm)		
	ALL STANLING		article size (mm)		Stress	
38	mm*	predicted	by the Sheilds dia	gram, Red field t	oook: p.190; Blu	ue: p.238
0.44	lb/ft2*		near Stress Requi by the Sheilds dia			ie: n 238

^{*}Modified Shields Curve data from Rosgen 2001

Project: Dye Branch Stream Restoration
Stream: Dye Branch

tream Restoration Location: Reach:

cation: Mooresville, NC ach: Proposed Reach 2

Date: 6/7/2005

Observers: LT

			10000000	cal Dimensionless Shear Stres Tci = 0.0834(di/d50)^-0.872	ss:
Value	Variable	_		Definition	
9	di mm	D50 from	Riffle	or Pavement*	*Choose
	d50 mm	D50 from	Bar Sample	or Sub Pavement*	One
0.0301	TANKA LAVI COMPOSITO	Critical Dime	ensionless Shear	Stress	
				Mean Depth Required for Entra largest particle in Bar Sample 55*Di)/Se 1.65 = submerged	
45.7		Largest Bar	Sample Particle i	n mm	
0.15	Di ft	Largest Bar	Sample Particle is	n ft	
0.0094	Se ft/ft	Bankfull Wa	ter Surface Slope	i e	
0.79	dr ft	Bankfulll Me	an Depth Require	ed	
	de ft			Rifffle Cross Section)	
de/dr=	1.5	7 if = 1		<1	>1
Choose on		Stable		aggrading	Degrading
			of	r Surface Slope Required for largest particle in Bar Sample	:
0.45	Inca	Daniel Bar	of Sr = (Tci*1.	largest particle in Bar Sample	:
	Di ft	Largest Bar	of Sr = (Tci*1. Sample Particle	largest particle in Bar Sample 65*Di)/de 1.65 = submerged	:
1.24	de ft	Bankfull Me	of Sr = (Tci*1. Sample Particle an Depth (<i>From F</i>	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section)	:
1.24 0.0060	de ft Sr ft/ft	Bankfull Me Bankfull Wa	of Sr = (Tci*1. Sample Particle	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section)	:
1.24	de ft Sr ft/ft 1.5	Bankfull Me Bankfull Wa	of Sr = (Tci*1. Sample Particle an Depth (<i>From F</i>	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section)	t: specific weight of sedimer
1.24 0.0060 Se/Sr= Choose on	de ft Sr ft/ft 1.5 e:	Bankfull Me Bankfull Wa 7 if = 1 Stable	of Sr = (Tci*1. Sample Particle an Depth (From F ter Surface Slope Sediment Tra	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section) a Required	specific weight of sedimer
1.24 0.0060 Se/Sr= Choose on	de ft Sr ft/ft 1.5 e: y lbs/cu ft	Bankfull Me Bankfull Wa 7 if = 1	of Sr = (Tci*1. Sample Particle an Depth (From F ter Surface Slope Sediment Tra	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section) a Required <1 aggrading nsport Validation - Bankfull S	specific weight of sedimers >1 Degrading
1.24 0.0060 Se/Sr= Choose on 62.4 1.08	de ft Sr ft/ft 1.5 e; y lbs/cu ft R=A/Wp	Bankfull Me Bankfull Wa 7 if = 1 Stable Density of w	of Sr = (Tci*1. Sample Particle an Depth (From F ter Surface Slope Sediment Tra	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section) a Required	specific weight of sedimers >1 Degrading
1.24 0.0060 Se/Sr= Choose on 62.4 1.08	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft	Bankfull Me Bankfull Wa if = 1 Stable Density of w	of Sr = (Tci*1. Sample Particle an Depth (From F ter Surface Slope Sediment Tra rater pss-Sectional Area	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section) a Required	specific weight of sedimers >1 Degrading
1.24 0.0060 Se/Sr= Choose on 62.4 1.08 20 18.58	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft Wp	Bankfull Me Bankfull Wa if = 1 Stable Density of w Bankfull Cro Wetted perio	of Sr = (Tci*1. Sample Particle an Depth (From F ter Surface Slope Sediment Tra vater pass-Sectional Area meter	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section) a Required	specific weight of sedimers >1 Degrading
1.24 0.0060 Se/Sr= Choose on 62.4 1.08 20 18.58 0.0094	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft	Bankfull Me Bankfull Wa if = 1 Stable Density of w Bankfull Cro Wetted perii Bankfull Wa	of Sr = (Tci*1. Sample Particle an Depth (From F ter Surface Slope Sediment Tra rater pss-Sectional Area	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section) a Required	specific weight of sedimers >1 Degrading
1.24 0.0060 Se/Sr= Choose on 62.4 1.08 20 18.58 0.0094 0.633404	de ft Sr ft/ft 1.5 e; y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft	Bankfull Me Bankfull Wa if = 1 Stable Density of w Bankfull Cro Wetted perii Bankfull Wa Tc = yRS	of Sr = (Tci*1. Sample Particle an Depth (From F ter Surface Slope Sediment Tra rater pass-Sectional Area meter ter Surface Slope	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS	specific weight of sedimers >1 Degrading
1.24 0.0060 Se/Sr= Choose on 62.4 1.08 20 18.58 0.0094	de ft Sr ft/ft 1.5 e; y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft	Bankfull Me Bankfull Wa if = 1 Stable Density of w Bankfull Cro Wetted peri Bankfull Wa Tc = yRS Largest Bar	of Sr = (Tci*1. Sample Particle an Depth (From F ter Surface Slope Sediment Tra vater pass-Sectional Area meter ter Surface Slope Sample Particle	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS a (mm)	specific weight of sedimers >1 Degrading
1.24 0.0060 Se/Sr= Choose on 62.4 1.08 20 18.58 0.0094 0.633404	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft Di mm	Bankfull Me Bankfull Wa if = 1 Stable Density of w Bankfull Cro Wetted peri Bankfull Wa Tc = yRS Largest Bar Moveable P	of Sr = (Tci*1. Sample Particle an Depth (From F ter Surface Slope Sediment Tra rater pss-Sectional Area meter ater Surface Slope Sample Particle (article size (mm))	largest particle in Bar Sample 65*DI)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS	specific weight of sedimers >1 Degrading hear Stress

^{*}Modified Shields Curve data from Rosgen 2001

Dye Branch Stream Restoration Project: Stream:

Date:

Dye Branch 5/26/2005

Location:

Mooresville, NC

Reach:

Reach 1 (Existing) Mulkey

Observers:

				al Dimensionless Shear Stres Tci = 0.0834(di/d50)^-0.872	ss:
Value	Variable			Definition	
6	di mm	D50 from	Riffle	or Pavement*	*Choose
2.8	d50 mm	D50 from	Bar Sample	or Sub Pavement*	One
0.0429	Tci	Critical Dime	nsionless Shear	Stress	
			of i dr = (Tci*1.6	lean Depth Required for Entra largest particle in Bar Sample 55*Di)/Se 1.65 = submerged	*
	mm	Largest Bar Sample Particle in mm			
0.08	Di ft	Largest Bar Sample Particle in ft			
0.0056	Se ft/ft	Bankfull Water Surface Slope			
1.00	dr ft	Bankfulll Mean Depth Required			
1.58	de ft	Bankfull Mean Depth (From Riffle Cross Section)			
de/dr=	1.5	9 if = 1		<1	>1
Choose one	93	Stable		aggrading	Degrading
			of	r Surface Slope Required for largest particle in Bar Sample	Entrainment ::
0.08	Dift		of Sr = (Tci*1.6	r Surface Slope Required for	Entrainment ::
0.08	Di ft	Largest Bar	of Sr = (Tci*1.6 Sample Particle	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged	Entrainment :
	de ft	Largest Bar	of Sr = (Tci*1.6 Sample Particle	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged	Entrainment :
1.58	de ft	Largest Bar Bankfull Mea Bankfull Wa	of I Sr = (Tci*1.6 Sample Particle an Depth (<i>From R</i>	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged	Entrainment :
1.58 0.0035	de ft Sr ft/ft 1.5	Largest Bar Bankfull Mea Bankfull Wa	of I Sr = (Tci*1.6 Sample Particle an Depth (<i>From R</i>	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section)	Entrainment : specific weight of sedimen
1.58 0.0035 Se/Sr= Choose one	de ft Sr ft/ft 1.5 e:	Largest Bar Bankfull Mea Bankfull Wal 9 if = 1 Stable	of Sr = (Tci*1.6 Sample Particle an Depth (From Ri ter Surface Slope Sediment Trai	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section) Required <1	Entrainment specific weight of sedimen >1 Degrading
1.58 0.0035 Se/Sr= Choose one	de ft Sr ft/ft 1.5 e: y lbs/cu ft	Largest Bar Bankfull Mea Bankfull Wal	of Sr = (Tci*1.6 Sample Particle an Depth (From Ri ter Surface Slope Sediment Trai	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S	Entrainment specific weight of sedimen >1 Degrading
1.58 0.0035 Se/Sr= Choose one 62.4 1.05	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp	Largest Bar Bankfull Mea Bankfull War if = 1 Stable Density of w	of Sr = (Tci*1.6 Sample Particle an Depth (From R ter Surface Slope Sediment Trai	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS	Entrainment specific weight of sedimen >1 Degrading
1.58 0.0035 Se/Sr= Choose one 62.4 1.05 19.68	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft	Largest Bar Bankfull Mas Bankfull Was if = 1 Stable Density of w	of Sr = (Tci*1.6 Sample Particle an Depth (From Fi ter Surface Slope Sediment Trai ater ss-Sectional Area	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS	Entrainment specific weight of sediment >1 Degrading
1.58 0.0035 Se/Sr= Choose one 62.4 1.05 19.68 18.79	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft Wp	Largest Bar Bankfull Mag Bankfull War if = 1 Stable Density of w Bankfull Cro Wetted para	of Sr = (Tci*1.6 Sample Particle an Depth (From Filter Surface Slope Sediment Trainater ass-Sectional Area meter	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS	Entrainment specific weight of sediment >1 Degrading
1.58 0.0035 Se/Sr= Choose one 62.4 1.05 19.68 18.79 0.0056	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft	Largest Bar Bankfull Mas Bankfull Wal if = 1 Stable Density of wal Bankfull Cro Wetted para Bankfull Wal	of Sr = (Tci*1.6 Sample Particle an Depth (From Fi ter Surface Slope Sediment Trai ater ss-Sectional Area	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS	Entrainment specific weight of sediment >1 Degrading
1.58 0.0035 Se/Sr= Choose one 62.4 1.05 19.68 18.79 0.0056 0.365991	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft	Largest Bar Bankfull Mas Bankfull Wal if = 1 Stable Density of w Bankfull Cro Wetted para Bankfull Wal Tc = yRS	of Sr = (Tci*1.6 Sample Particle an Depth (From Filter Surface Slope Sediment Transter ater ss-Sectional Area meter ter Surface Slope	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS	Entrainment specific weight of sediment >1 Degrading
1.58 0.0035 Se/Sr= Choose one 62.4 1.05 19.68 18.79 0.0056	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft	Largest Bar Bankfull Mas Bankfull Wal if = 1 Stable Density of w Bankfull Cro Wetted para Bankfull Wal Tc = yRS Largest Bar	of Sr = (Tci*1.6 Sample Particle an Depth (From Filter Surface Slope Sediment Transtater as-Sectional Area meter ter Surface Slope Sample Particle (r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS	Entrainment specific weight of sediment >1 Degrading
1.58 0.0035 Se/Sr= Choose one 62.4 1.05 19.68 18.79 0.0056 0.365991	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft Di mm	Largest Bar Bankfull Mag Bankfull Wal if = 1 Stable Density of w Bankfull Cro Wetted para Bankfull Wa Tc = yRS Largest Bar Moveable Pa	of Sr = (Tci*1.6 Sample Particle an Depth (From Filter Surface Slope Sediment Trainater ass-Sectional Area meter ter Surface Slope Sample Particle (article size (mm) a	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Riffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS (mm) at Bankfull Shear Stress	Entrainment s: specific weight of sediment >1 Degrading hear Stress
1.58 0.0035 Se/Sr= Choose one 62.4 1.05 19.68 18.79 0.0056 0.365991	de ft Sr ft/ft 1.5 e: y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft Di mm	Largest Bar Bankfull Mea Bankfull Wal if = 1 Stable Density of w Bankfull Cro Wetted para Bankfull Wa Tc = yRS Largest Bar Moveable Pare	of Sr = (Tci*1.6 Sample Particle an Depth (From Filter Surface Slope Sediment Trainater ass-Sectional Area meter ter Surface Slope Sample Particle (article size (mm) a py the Sheilds dia	r Surface Slope Required for largest particle in Bar Sample 65*Di)/de 1.65 = submerged Rifffle Cross Section) Required <1 aggrading nsport Validation - Bankfull S Tc = yRS	Entrainment s: specific weight of sediment >1 Degrading hear Stress

^{*}Modified Shields Curve data from Rosgen 2001

Entrainment Calculation Form

Project: Dye Branch Stream Restoration

Location:

Mooresville, NC

Stream: Dye Branch Date: 6/7/2005 Reach: Observers: Proposed Reach 1

			ARCHAROL .	al Dimensionless Shear S Tci = 0.0834(di/d50)^-0.872	MINISTER .
Value	Variable	T		Definition	
6	di mm	D50 from	Riffle	or Pavement*	*Choose
2.8	d50 mm	D50 from	Bar Sample	or Sub Pavement*	One
0.0429	Tci	Critical Dime	ensionless Shear S	Stress	
			of I	lean Depth Required for E argest particle in Bar Sam 5*DI)/Se 1.65 = submerg	
	mm		Sample Particle in		
0.08	Di ft	Largest Bar	Sample Particle in	ft	
0.0052	Se ft/ft	Bankfull Wa	ter Surface Slope		
1.07	dr ft	Bankfulli Me	an Depth Require	d	
1.40	de ft	Bankfull Mea	an Depth (<i>From Ri</i>	ifffle Cross Section)	
de/dr=	1.31	if = 1		<1	>1
Choose on	e:	Stable		aggrading	Degrading
	Tour or	<u> </u>	Sr = (Tci*1.6	argest particle in Bar Sam i5*Di)/de 1.65 = submerg	ple: ed specific weight of sedimen
- Contract and Allerta	Di ft de ft		Sample Particle	ifffle Cross Section)	
0.0040			ter Surface Slope		
Se/Sr=	1,31		tor duritide diope	rioquirou	
00/01-				<1	×1
Choose on		Stable		<1 aggrading	>1 Degrading
	e:	Stable			Degrading
62.4	e: y lbs/cu ft			aggrading nsport Validation - Bankfu	Degrading
62.4 1.21	y lbs/cu ft R=A/Wp	Stable Density of w	rater	aggrading nsport Validation - Bankfu Tc = yRS	Degrading
62.4 1.21 24.1	y lbs/cu ft R=A/Wp A sq ft	Stable Density of w Bankfull Cro	rater ess-Sectional Area	aggrading nsport Validation - Bankfu Tc = yRS	Degrading
62.4 1,21 24.1 20	y lbs/cu ft R=A/Wp A sq ft	Stable Density of w Bankfull Cro	rater oss-Sectional Area meter	aggrading nsport Validation - Bankfu Tc = yRS	Degrading
62.4 1.21 24.1 20 0.0052	y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft	Stable Density of w Bankfull Cro Wetted perin Bankfull Wa	rater ess-Sectional Area	aggrading nsport Validation - Bankfu Tc = yRS	Degrading
62.4 1.21 24.1 20 0.0052 0.390998	y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft	Stable Density of w Bankfull Cro Wetted perir Bankfull Wa Tc = yRS	rater ess-Sectional Area meter iter Surface Slope	aggrading nsport Validation - Bankfu Tc = yRS	Degrading
62.4 1.21 24.1 20 0.0052 0.390998	y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft	Density of w Bankfull Cro Wetted perir Bankfull Wa Tc = yRS Largest Bar	rater pss-Sectional Area meter iter Surface Slope Sample Particle (r	aggrading nsport Validation - Bankfu Tc = yRS	Degrading
62.4 1.21 24.1 20 0.0052 0.390998	y lbs/cu ft R=A/Wp A sq ft Wp S ft/ft Tc lb/sqr ft Di mm	Density of w Bankfull Cro Wetted perin Bankfull Wa Tc = yRS Largest Bar Moveable P predicted	rater pss-Sectional Area meter iter Surface Slope Sample Particle (r article size (mm) a by the Sheilds diag	aggrading nsport Validation - Bankfu Tc = yRS mm)	Degrading II Shear Stress

^{*}Modified Shields Curve data from Rosgen 2001

Project: Stream:

Date:

Dye Branch Stream Restoration Dye Branch 5/26/2005

Location:

Reach:

Mooresville, NC Existing Reach 1

Observers:

Mulkey

Input Variables		Output Variables		
Bankfull X-Sec Area (A	Abkf)	19.68 sq ft	Bankfull Mean Depth (Dbkf)	1.58 ft
Bankfull Width (\	Nbkf)	12.47 ft	Wetted Parameter (WP)	15.63 ft
D84 (Riffle or pavemen	nt)	11 mm	D84 (mm/304.8)	0.04 ft
Bankfull Slope	(S)	0.0056 ft/ft	Hydraulic Radius (R)	1.26 ft
Gravitational Accleration	on (g)	32.2 ft/sq sec	Dbkf/D84 (use D84 in ft)	39.50 ft/ft
Bankfull Maximum Dej	oth	2.2 ft.	R/D84 (use D84 in ft)	31.48 ft/ft

Dbkf/D84, u/u*, Mannings n		
u/u*	(Using Dbkf/D84 Red Book: p188; Blue p233)	11.6 ft/s/ft/s
Mannings n	(Red Book: p189; Blue :p236)	0.025
Velocity (From	Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	5.19 ft/s

u/u*=2.83+5.7logR/D84		
u*	u* = (gRS)^.5	0.48 ft/s
Velocity:	$u = u^*(2.83+5.7log(R/D84))$	5.42 ft/s

Mannings n by StreamType		
Stream type	E4	
Mannings n	(Red Book: p187; Blue :p237)	0.032
Velocity (From Man	nings' equation: u=1,4865 * (R^2/3)(S^1/2)/n)	4.05 ft/s

	Continuity Equation	
	s) original curve or stream gage hydraulic geometry	63.75 cfs
Velocity	(u=Q/A) or from stream gage hydraulic geometry	3.24 ft/s

	Dr. Richard Hey Method	
Coefficient a	a = 11(R/dmax)^-0.314	13.22583012
Friction Factor - f	$1/f^{1/2} = 2.03 \log (aR/(D84*3.5))$	0.056340489
Velocity (From I	D'Arcy Weisbach equation: u=(8*g*R S/f)^1/2)	5.68 ft/s

Project: Stream:

Date:

Dye Branch Stream Restoration Dye Branch 6/7/2005

Location:

Mooresville, NC Proposed Reach 1

Reach: Mulkey Observers:

Input Variables		Output Variables	
Bankfull X-Sec Area (Abkf)	24.1 sq ft	Bankfull Mean Depth (Dbkf)	1.40 ft
Bankfull Width (Wbkf)	17.2 ft	Wetted Perimeter (WP)	20.00 ft
D84 (Riffle or pavement)	11 mm	D84 (mm/304.8)	0.04 ft
Bankfull Slope (S)	0.0052 ft/ft	Hydraulic Radius (R)	1.20 ft
Gravitational Accleration (g)	32.2 ft/sq sec	Dbkf/D84 (use D84 in ft)	35.03 ft/ft
Bankfull Maximum Depth	2.1 ft.	R/D84 (use D84 in ft)	30.12 ft/ft

Dbkf/D84, u/u*, Mannings n		
u/u*	(Using Dbkf/D84 Red Book: p188; Blue p233)	11.4 ft/s/ft/s
Mannings n	(Red Book: p189; Blue :p236)	0.026
Velocity (From	n Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	4.67 ft/s

	u/u*=2.83+5.7logR/D84	
u*	$u^* = (gRS)^*.5$	0.45 ft/s
Velocity:	$u = u^*(2.83+5.7log(R/D84))$	5.06 ft/s

	Mannings n by StreamType	
Stream type	C4	
Mannings n	(Red Book: p187; Blue :p237)	0.018
Velocity (From Man	nings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	6.74 ft/s

Continuity Equation		
Qbkf (cfs) original curve or stream gage hydraulic geometry	63.75 cfs	
Velocity (u=Q/A) or from stream gage hydraulic geometry	2.65 ft/s	

Dr. Richard Hey Method		
Coefficient a	a = 11(R/dmax)^-0.314	13.22
Friction Factor - f	$1/f^{1/2} = 2.03 \log (aR/(D84*3.5))$	0.06
Velocity (From D')	Arcy Weisbach equation: u=(8*g*R S/f)^1/2)	5.30 ft/s

Project: Stream:

Date:

Dye Branch Stream Restoration Dye Branch 5/26/2005

Location:

Reach: Observers: Mooresville, NC Existing Reach 2 Mulkey

Input Variables		Output Variables	
Bankfull X-Sec Area (Abkf)	18.13 sq ft	Bankfull Mean Depth (Dbkf)	1.63 ft
Bankfull Width (Wbkf)	11.15 ft	Wetted Parameter (WP)	14.40 ft
D84 (Riffle or pavement)	11 mm	D84 (mm/304.8)	0.04 ft
Bankfull Slope (S)	0.008 ft/ft	Hydraulic Radius (R)	1.26 ft
Gravitational Accleration (g)	32.2 ft/sq sec	Dbkf/D84 (use D84 in ft)	40.65 ft/ft
Bankfull Maximum Depth	2.81 ft.	R/D84 (use D84 in ft)	31.47 ft/ft

Dbkf/D84, u/u*, Mannings n		
u/u*	(Using Dbkf/D84 Red Book: p188; Blue p233)	11.8 ft/s/ft/s
Mannings n	(Red Book: p189; Blue :p236)	0.025
Velocity (Fron	Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	6.20 ft/s

	u/u*=2.83+5.7logR/D84	
u*	u* = (gRS)^.5	0.57 ft/s
Velocity:	$u = u^*(2.83+5.7log(R/D84))$	6.47 ft/s

Mannings n by StreamType		
Stream type	E4	
Mannings n (Red Book: p187; Blue :p237)		0.032
Velocity (From Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)		4.84 ft/s

Continuity Equation		
Qbkf (cfs) original curve or stream gage hydraulic geometry 63.75 c		63.75 cfs
Velocit	y (u=Q/A) or from stream gage hydraulic geometry	3.52 ft/s

	Dr. Richard Hey Method	
Coefficient a	a = 11(R/dmax)^-0.314	14.28317587
Friction Factor - f	$1/f^{1/2} = 2.03 \log (aR/(D84*3.5))$	0.054574553
Velocity (From D'A	Arcy Weisbach equation: u=(8*g*R S/f)^1/2)	6.89 ft/s

Project:

Stream:

Date:

Dye Branch Stream Restoration Dye Branch 6/7/2005

Location:

Mooresville, NC Proposed Reach 2 Mulkey

Reach:

Observers:

Input Variables		Output Variables	
Bankfull X-Sec Area (Abkf)	20 sq ft	Bankfull Mean Depth (Dbkf)	1.24 ft
Bankfull Width (Wbkf)	16.1 ft	Wetted Perimeter (WP)	18.58 ft
D84 (Riffle or pavement)	11 mm	D84 (mm/304.8)	0.04 ft
Bankfull Slope (S)	0.00943 ft/ft	Hydraulic Radius (R)	1.08 ft
Gravitational Accleration (g)	32.2 ft/sq sec	Dbkf/D84 (use D84 in ft)	31.06 ft/ft
Bankfull Maximum Depth	1.8 ft.	R/D84 (use D84 in ft)	26.90 ft/ft

Dbkf/D84, u/u*, Mannings n		
u/u*	(Using Dbkf/D84 Red Book: p188; Blue p233)	11 ft/s/ft/s
Mannings n	(Red Book: p189; Blue :p236)	0.026
Velocity (Fron	n Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	5.83 ft/s

u/u*=2.83+5.7logR/D84		
u*	$u^* = (gRS)^*.5$	0.57 ft/s
Velocity:	$u = u^{*}(2.83+5.7\log(R/D84))$	6.28 ft/s

Mannings n by StreamType		
Stream type C4		
Mannings n	(Red Book: p187; Blue :p237)	0.018
Velocity (From Mar	nings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	8.42 ft/s

Continuity Equation		
Qbkf	(cfs) original curve or stream gage hydraulic geometry	63.75 cfs
Velocity	(u=Q/A) or from stream gage hydraulic geometry	3.19 ft/s

	Dr. Richard Hey Method	
Coefficient a	a = 11(R/dmax)^-0.314	13.04572737
Friction Factor - f	1/f^1/2 = 2.03 log (aR/(D84*3.5))	0.060592412
Velocity (From D'/	Arcy Weisbach equation: u=(8*g*R S/f)^1/2)	6.57 ft/s

Project:

Date:

Dye Branch Stream Restoration Dye Branch 5/26/2005

Stream:

Location:

Reach:

Mooresville, NC Existing Reach 3

Observers:

Mulkey

Input Variables		Output Variables	
Bankfull X-Sec Area (Abkf)	17.4 sq ft	Bankfull Mean Depth (Dbkf)	1.18 ft
Bankfull Width (Wbkf)	14.75 ft	Wetted Parameter (WP)	17.11 ft
D84 (Riffle or pavement)	8.5 mm	D84 (mm/304.8)	0.03 ft
Bankfull Slope (S)	0.011 ft/ft	Hydraulic Radius (R)	1.02 ft
Gravitational Accleration (g)	32.2 ft/sq sec	Dbkf/D84 (use D84 in ft)	39.33 ft/ft
Bankfull Maximum Depth	1.71 ft.	R/D84 (use D84 in ft)	33.90 ft/ft

Dbkf/D84, u/u*, Mannings n		
u/u*	(Using Dbkf/D84 Red Book: p188; Blue p233)	11.6 ft/s/ft/s
Mannings n	(Red Book: p189; Blue :p236)	0.026
Velocity (Fro	om Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	6.06 ft/s

u/u*=2.83+5.7logR/D84		
u*	u* = (gRS)^.5	0.60 ft/s
Velocity:	$u = u^*(2.83+5.7\log(R/D84))$	6.93 ft/s

Mannings n by StreamType		
Stream type		G5
Mannings n	(Red Book: p187; Blue :p237)	0.038
Velocity (From Man	nings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	4.15 ft/s

	Continuity Equation		
Qbkf	(cfs) original curve or stream gage hydraulic geometry	63.67 cfs	
Velocit	y (u=Q/A) or from stream gage hydraulic geometry	3.66 ft/s	

	Dr. Richard Hey Method	
Coefficient a	a = 11(R/dmax)^-0.314	13.06747857
Friction Factor - f	1/f^1/2 = 2.03 log (aR/(D84*3.5))	0.05490575
Velocity (From D')	Arcy Weisbach equation: u=(8*g*R S/f)^1/2)	7.24 ft/s

Project:

Stream: Date:

Dye Branch Stream Restoration Dye Branch 5/26/2005

Location:

Reach:

Mooresville, NC Proposed Reach 3

Observers:

Mulkey

Input Variables		Output Variables	
Bankfull X-Sec Area (Abkf)	18.8 sq ft	Bankfull Mean Depth (Dbkf)	1.30 ft
Bankfull Width (Wbkf)	15 ft	Wetted Perimeter (WP)	17.60 ft
D84 (Riffle or pavement)	8.5 mm	D84 (mm/304.8)	0.03 ft
Bankfull Slope (S)	0.01017 ft/ft	Hydraulic Radius (R)	1.07 ft
Gravitational Accleration (g)	32.2 ft/sq sec	Dbkf/D84 (use D84 in ft)	43.33 ft/ft
Bankfull Maximum Depth	1.9 ft.	R/D84 (use D84 in ft)	35.61 ft/ft

Dbkf/D84, u/u*, Mannings n		
u/u*	(Using Dbkf/D84 Red Book: p188; Blue p233)	11.8 ft/s/ft/s
Mannings n	(Red Book: p189; Blue :p236)	0.026
Velocity (From	n Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	6.02 ft/s

u/u*=2.83+5.7logR/D84		
u*	$u^* = (gRS)^*.5$	0.59 ft/s
Velocity:	$u = u^*(2.83+5.7log(R/D84))$	6.90 ft/s

	Mannings n by StreamType	
Stream type		C4
Mannings n (Red Book: p187; Blue :p237)		0.018
Velocity (From Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)		8.70 ft/s

Continuity Equation		
Qbkf (cfs) original curve or stream gage hydraulic geometry		63.67 cfs
Velocit	y (u=Q/A) or from stream gage hydraulic geometry	3.39 ft/s

	Dr. Richard Hey Method	
Coefficient a	a = 11(R/dmax)^-0.314	13.30016481
Friction Factor - f	$1/f^1/2 = 2.03 \log (aR/(D84*3.5))$	0.053421182
Velocity (From D'/	Arcy Weisbach equation: u=(8*g*R S/f)^1/2)	7.24 ft/s

Project: Stream: Date:

Dye Branch Stream Restoration Cemetery Branch 5/26/2005

Location:

Reach:

Observers:

Mooresville, NC Existing Trib Mulkey

Input Variables		Output Variables	
Bankfull X-Sec Area (Abkf)	6.76 sq ft	Bankfull Mean Depth (Dbkf)	0.97 ft
Bankfull Width (Wbkf)	6.98 ft	Wetted Parameter (WP)	8.92 ft
D84 (Riffle or pavement)	10.5 mm	D84 (mm/304.8)	0.03 ft
Bankfull Slope (S)	0.019 ft/ft	Hydraulic Radius (R)	0.76 ft
Gravitational Accleration (g)	32.2 ft/sq sec	Dbkf/D84 (use D84 in ft)	32.33 ft/ft
Bankfull Maximum Depth	1.52 ft.	R/D84 (use D84 in ft)	25.26 ft/ft

Dbkf/D84, u/u*, Mannings n		
u/u*	(Using Dbkf/D84 Red Book: p188; Blue p233)	11.2 ft/s/ft/s
Mannings n	(Red Book: p189; Blue :p236)	0.026
Velocity (Fron	Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	6.55 ft/s

	u/u*=2.83+5.7logR/D84		
u*	$u^* = (gRS)^*.5$	0.68 ft/s	
Velocity:	$u = u^*(2.83+5.7log(R/D84))$	7.37 ft/s	

Mannings n by StreamType			
Stream type		G4	
Mannings n (Red Book: p187; Blue :p237)		0.038	
Velocity (From Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)		4.48 ft/s	

Continuity Equation		
Qbkf	(cfs) original curve or stream gage hydraulic geometry	52.13 cfs
Velocit	ty (u=Q/A) or from stream gage hydraulic geometry	7.71 ft/s

	Dr. Richard Hey Method	
Coefficient a	a = 11(R/dmax)^-0.314	13.81125574
Friction Factor - f	$1/f^{1/2} = 2.03 \log (aR/(D84^{3.5}))$	0.060749818
Velocity (From D'A	Arcy Weisbach equation: u=(8*g*R S/f)^1/2)	7.81 ft/s

Project: Stream:

Date:

Dye Branch Stream Restoration Cemetery Branch 5/26/2005

Location:

Mooresville, NC Proposed UT Mulkey

Reach:

Observers:

Input Variables		Output Variables	
Bankfull X-Sec Area (Abkf)	7 sq ft	Bankfull Mean Depth (Dbkf)	0.7 ft
Bankfull Width (Wbkf)	10 ft	Wetted Perimeter (WP)	11.4 ft
D84 (Riffle or pavement)	10.5 mm	D84 (mm/304.8)	0.03 ft
Bankfull Slope (S)	0.019 ft/ft	Hydraulic Radius (R)	0.61 ft
Gravitational Accleration (g)	32.2 ft/sq sec	Dbkf/D84 (use D84 in ft)	23.33 ft/ft
Bankfull Maximum Depth	1.1 ft.	R/D84 (use D84 in ft)	20.47 ft/ft

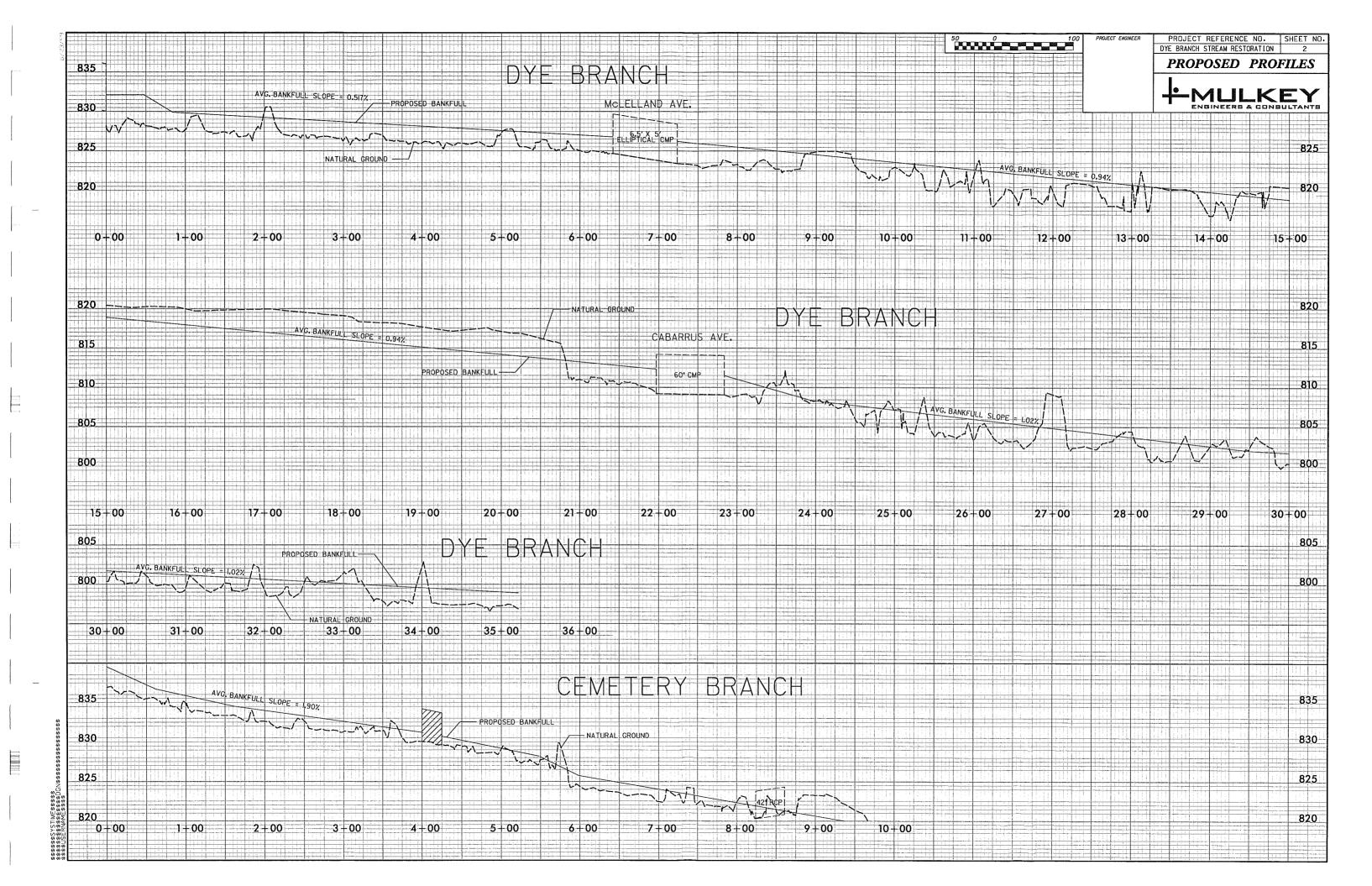
Dbkf/D84, u/u*, Mannings n		
u/u*	(Using Dbkf/D84 Red Book: p188; Blue p233)	10.5 ft/s/ft/s
Mannings n	(Red Book: p189; Blue :p236)	0.027
Velocity (Fro	om Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)	5,48 ft/s

u/u*=2.83+5.7logR/D84		
u*	$u^* = (gRS)^*.5$	0.61 ft/s
Velocity:	$u = u^*(2.83+5.7log(R/D84))$	6.31 ft/s

Mannings n by StreamType			
Stream type		C4	
Mannings n (Red Book: p187; Blue :p237)		0.018	
/elocity (From Mannings' equation: u=1.4865 * (R^2/3)(S^1/2)/n)		8.22 ft/s	

Continuity Equation		
Qbkf	(cfs) original curve or stream gage hydraulic geometry	52.13 cfs
Velocity	(u=Q/A) or from stream gage hydraulic geometry	7.45 ft/s

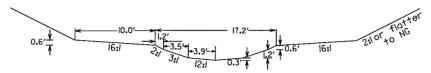
	Dr. Richard Hey Method	
Coefficient a	a = 11(R/dmax)^-0.314	13.32992238
Friction Factor - f	1/f^1/2 = 2.03 log (aR/(D84*3.5))	0.06780208
Velocity (From D'Arcy Weisbach equation: u=(8*g*R S/f)^1/2)		6.66 ft/s



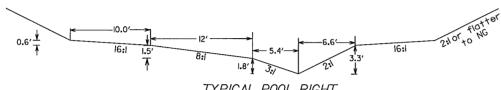
TYPICALS NOT TO SCALE

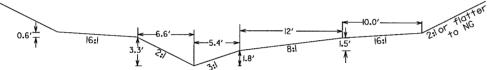


DYE BRANCH - UPPER REACH (0+00 to 9+25)



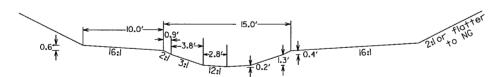
TYPICAL RIFFLE BANKFULL CROSS SECTIONAL AREA = 24,1 SQ.FT.



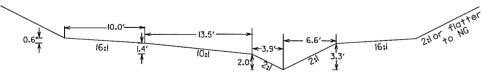


TYPICAL POOL LEFT
BANKFULL CROSS SECTIONAL AREA = 36.4 SQ.FT.

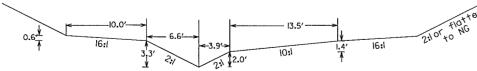
DYE BRANCH - LOWER REACH (26+85 to 37+70)



TYPICAL RIFFLE BANKFULL CROSS SECTIONAL AREA = 18.8 SQ.FT.

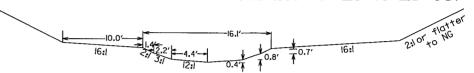


TYPICAL POOL RIGHT BANKFULL CROSS SECTIONAL AREA = 29.0 SQ.FT.



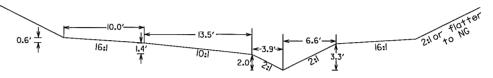
TYPICAL POOL LEFT BANKFULL CROSS SECTIONAL AREA = 29.0 SQ.FT.

DYE BRANCH - MIDDLE REACH (9+25 to 26+85)

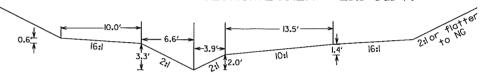


TYPICAL RIFFLE

BANKFULL CROSS SECTIONAL AREA = 20.0 SQ.FT.



TYPICAL POOL RIGHT BANKFULL CROSS SECTIONAL AREA = 29.0 SQ.FT.

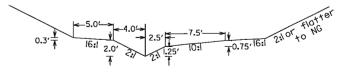


TYPICAL POOL LEFT BANKFULL CROSS SECTIONAL AREA = 29.0 SQ.FT.

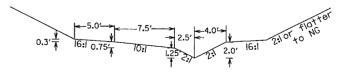
CEMETERY TRIBUTARY



TYPICAL RIFFLE BANKFULL CROSS SECTIONAL AREA = 7.0 SQ.FT.



TYPICAL POOL RIGHT BANKFULL CROSS SECTIONAL AREA = 10.3 SQ.FT.



TYPICAL POOL LEFT BANKFULL CROSS SECTIONAL AREA = 10.3 SQ.FT.

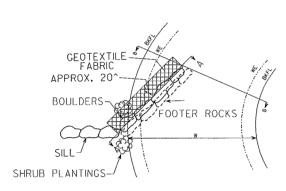
PROJECT REFERENCE NO. | SHEET NO. DYE BRANCH STREAM RESTORATION

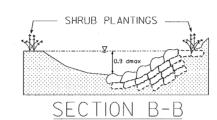
DETAILS

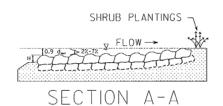
INCOMPLETE PLANS

PO BOX 33127 RALEIGH, N.C. 27636 (919) 851-1912 (919) 851-1918 (FAX) WWW.MULKEYING.COM

ROCK VANE DETAILS

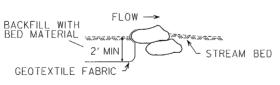






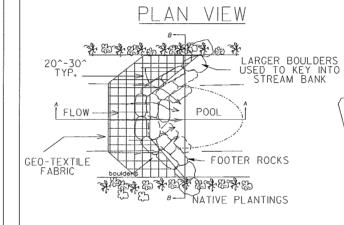
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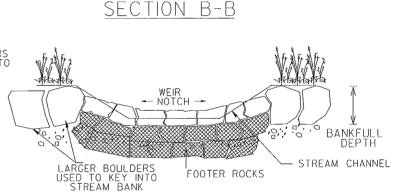
- I. BOULDERS SHOULD BE NATIVE QUARRIED ROCK OR LOCALLY SHOT ROCK, ANGULAR AND OBLONG WITH THE FOLLOWING DIMENSION:
- 2. AVERAGE SIZE IS 4'X3'X2' (APPROX. 3600 LB)
- 3. ROCKS SHOULD FIT TIGHTLY WITH MINIMAL SPACES.
- 4. FOOTER ROCKS SHOULD BE A MINIMUM OF 3 TIMES 'H' IN GRAVEL BED STREAMS.
- 5. GEOTEXTILE FABRIC SHOULD BE PLACED ON UPSTREAM SIDE OF BOULDERS, FABRIC SHOULD BE OVERLAIN ON EXPOSED BOULDERS AND BURIED TO A MINIMUM DEPTH OF 2 FT. OR AS DIRECTED BY ON SITE DESIGNER. FABRIC SHOULD EXTEND UPSTREAM A MINIMUM LENGTH OF OF 6 FT. OR AS DIRECTED BY ON SITE DESIGNER, FABRIC SHOULD BE BACKFILLED WITH 3" STONE.
- 6. H = MIN. OF 0.3'

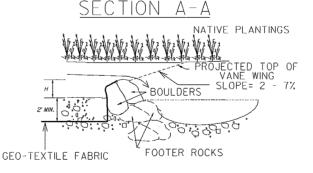


DETAIL OF GEOTEXTILE FABRIC

CROSS VANE DETAILS







- I. BOULDERS SHOULD BE NATIVE QUARRIED ROCK OR LOCALLY SHOT ROCK, ANGULAR AND OBLONG WITH THE FOLLOWING DIMENSION:
- 2. AVERAGE SIZE IS 4'X3'X2' (APPROX. 3600 LB)**
- 3. ROCKS SHOULD FIT TIGHTLY WITH MINIMAL SPACES.
- 4. FOOTER ROCKS SHOULD BE A MINIMUM OF 3 TIMES 'H' IN GRAVEL BED STREAMS.
- 5. GEOTEXTILE FABRIC SHOULD BE PLACED ON UPSTREAM SIDE OF BOULDERS, FABRIC SHOULD BE OVERLAIN ON EXPOSED BOULDERS AND BURIED TO A MINIMUM DEPTH OF 2 FT. OR AS DIRECTED BY ON SITE DESIGNER. FABRIC SHOULD EXTEND UPSTREAM A MINIMUM LENGTH OF OF 6 FT. OR AS DIRECTED BY ON SITE DESIGNER. FABRIC SHOULD BE BACKFILLED WITH 3" STONE.
- 6. H = MIN. OF 0.3'

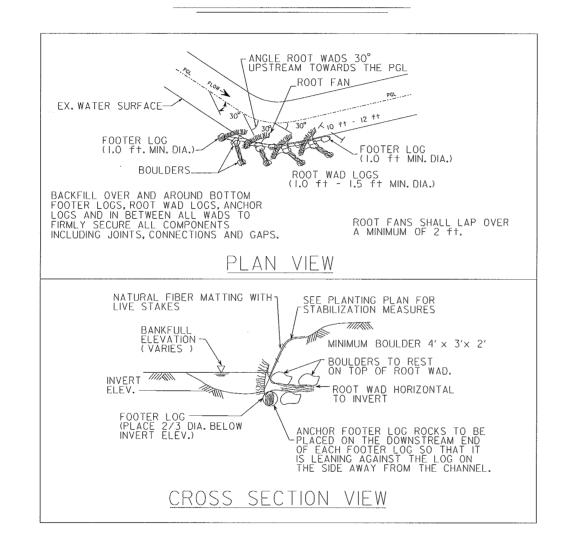
**DYE BRANCH MAIN CHANNEL. STRUCTURES ON CEMETERY BRANCH AVERAGE SIZE IS 2'X2'X1'

PROJECT REFERENCE NO. | SHEET NO. DYE BRANCH STREAM RESTORATION **DETAILS** INCOMPLETE PLANS

-MULKEY ENGINEERS & CONSUL

PO Box 33127 RALEIGH, N.C. 27636 (919) 851-1912 (919) 851-1918 (FAX) WWW.MULKEYING.COM

ROOTWAD DETAILS

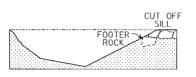


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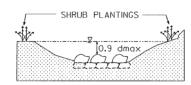
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- I. A TRENCH SHALL BE DUG ALONG THE TOE OF THE BANK TO A DEPTH OF TOE DIAMETER OF THE FOOTER LOG. A PRUNED FOOTER LOG (MIN. DIA. 12") SHALL BE PLACED AT THE TOE OF THE CHANNEL AND THE ROOTWAD (MIN. BASAL DIA. 12", LENGTH 10-12') SHALL BE PLACED DIRECTLY ABOVE IT. THE ROOT MASS SHALL BE ORIENTED IN SUCH A WAY THAT THE VELOCITY VECTORS OF THE WATER ARE ALIGNED WITH THE TRUNKS LONGITUDINAL AXIS AND WILL INTERSECT THE ROOT MASS AT A 90° ANGLE. THERE SHALL BE NO VOID BETWEEN THE ROOT MASS AND THE BANK ON THE UPSTREAM SIDE OF THE CHANNEL. A BOULDER MAY BE PLACED ON THE DOWNSTREAM SIDE, ON TOP OF, AND ON THE UPSTREAM SIDE BETWEEN THE ROOT MASS AND THE BANK TO PROVIDE EROSION CONTROL AS DIRECTED BY THE DESIGNER. BOULDERS FOR THE ROOTWAD STRUCTURES SHALL BE, 1.75 TONS (APPROX, 4' x 3' x 2') ON DYE BRANCH AS APPROVED BY THE DESIGNER.
- 2. THE PREFERRED METHOD FOR INSTALLATION OF A ROOTWAD IS TO DRIVE THE SHARPENED TRUNK OF THE ROOTWAD INTO THE STREAMBANK USING AN EXCAVATOR CONTAINING A HYDRAULIC THUMB. IF IT IS DEEMED NOT POSSIBLE TO DRIVE THE TRUNK INTO THE BANK, A TRENCH SHALL BE DUG IN THE BANK AND THE TRUNK SHALL BE PLACED IN THE TRENCH. THE TRENCH SHALL BE BACKFILLED AND COMPACTED.
- 3, ALL MATERIALS FOR THIS STRUCTURE SHALL BE APPROVED BY THE DESIGNER PRIOR TO INSTALLATION.
- 4. STATIONING OF ROOTWADS SHALL BE AS SHOWN ON THE PLANS OR AS DIRECTED BY THE DESIGNER. THE ACTUAL NUMBER OF ROOTWADS NECESSARY WILL DEPEND ON THE SIZE OF THE ROOT FAN AND THE ACTUAL CONDITION OF THE SITE AT THE TIME OF CONSTRUCTION.
- 5. ROOT WADS SHOULD BE FROM NATIVE HARDWOOD TREES WITH SPREADING ROOT SYSTEMS, NO TAP ROOTS.

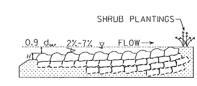
J-HOOK VANE DETAILS



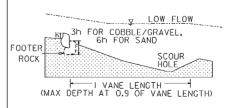
SECTION A-A



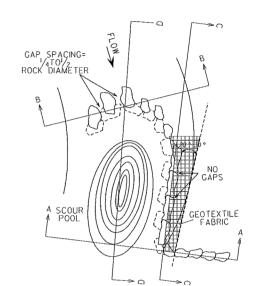
SECTION B-B

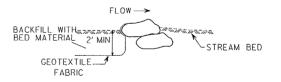


SECTION C-C



SECTION D-D





GEOTEXTILE FABRIC

- I. BOULDERS SHOULD BE NATIVE QUARRIED ROCK OR LOCALLY SHOT ROCK, ANGULAR AND OBLONG WITH THE FOLLOWING DIMENSION:
- 2. AVERAGE SIZE IS 4'X3'X2' (APPROX. 3600 LB)
- 3. ROCKS SHOULD FIT TIGHTLY WITH MINIMAL SPACES.
- 4. FOOTER ROCKS SHOULD BE A MINIMUM OF 3 TIMES 'H' IN GRAVEL BED STREAMS.
- 5. GEOTEXTILE FABRIC SHOULD BE PLACED ON UPSTREAM SIDE OF BOULDERS. FABRIC SHOULD BE OVERLAIN ON EXPOSED BOULDERS AND BURIED TO A MINIMUM DEPTH OF 2 FT. OR AS DIRECTED BY ON SITE DESIGNER. FABRIC SHOULD EXTEND UPSTREAM A MINIMUM LENGTH OF OF 6 FT. OR AS DIRECTED BY ON SITE DESIGNER. FABRIC SHOULD BE BACKFILLED WITH 3" STONE.

6. H = MIN. OF 0.3'

PROJECT ENGINEER PROJECT REFERENCE NO. SHEET NO.

DYE BRANCH STREAM RESTORATION 2H

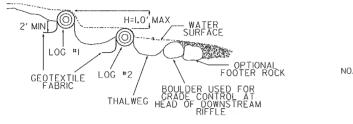
DETAILS

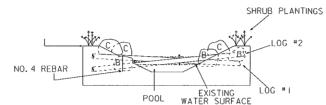
INCOMPLETE PLANS

LENGINEERS & CONSULTANTS

PO 80x 33127 Raleigh, N.C. 27636 (919) 851-1912 (919) 851-1918 (FAX) WWW.MULKEYINC.COM

DOUBLE LOG DROP STRUCTURE



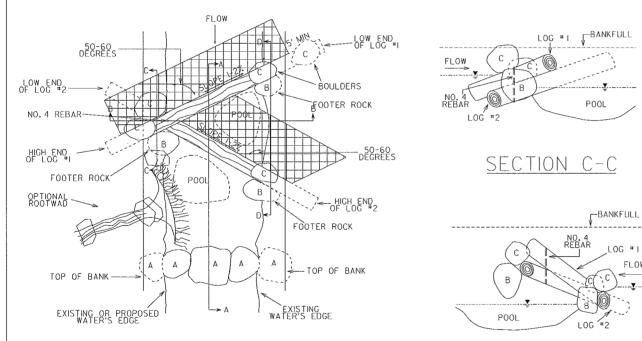


SECTION A-A

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<u>Plan view</u>

SECTION D-D

- I. LOGS MAY BE NOTCHED TO ALLOW FOR PROPER CONNECTION.
 THEY SHOULD BE ANCHORED TO ONE ANOTHER VIA NO. 4 REBAR BY DRILLING AND HAMMERING.
- 2. LOGS SHOULD BE OBTAINED FROM ON-SITE RESOURCES, WHEN APPROPRIATE. THEY SHOULD CONSIST OF NATIVE HARDWOOD MATERIAL, UNLESS DIRECTED OTHERWISE BY ON-SITE ENGINEER. MINIMUM DIAMETER OF LOGS IS 12 INCHES.
- 3. BOULDERS SHOULD BE NATIVE QUARRIED ROCK, OR LOCAL SHOT ROCK, ANGULAR OR OBLONG WITH THE FOLLOWING DIMENSIONS: 4' x 3' x 2'(1.75 TONS) OR LARGER.
- 4. GEOTEXTILE FABRIC SHOULD BE PLACED ON UPSTREAM SIDE OF LOGS. FABRIC SHOULD BE ATTACHED TO THE LOGS VIA I.O INCH LONG MINIMUM ROOFING NAILS WITH PLASTIC WASHERS SPACED NO GREATER THAN I6 INCHES APART. THE ATTACHMENT POINT SHOULD BE APPROXIMATELY ONE HALF THE HEIGHT OF THE LOG SO THAT IT REMAINS UNSEEN ONCE THE STRUCTURE IS COMPLETED. FABRIC SHOULD BE BURIED TO A MINIMUM DEPTH OF 2.O FEET, OR AS DIRECTED BY THE ON-SITE ENGINEER. FABRIC SHOULD EXTEND UPSTREAM A MINIMUM LENGTH OF 6.O FEET, OR AS DIRECTED BY THE ON-SITE ENGINEER. FABRIC SHOULD BE BACKFILLED WITH NATIVE STONE, OR THE APPROPRIATE STREAM BED COMPOSITION, AS DIRECTED BY ON-SITE ENGINEER.

5. H = MIN. OF 0.2", UNLESS DIRECTED OTHERWISE BY ON-SITE ENGINEER.

MAX OF 1.0'

NOTES:

* RIFFLE BED MATERIAL ONLY TO BE PROPOSED BANKFULL INSTALLED AS SHOWN ON PLANS LINE TOE OF BANK WITH OR AS DIRECTED BY ON-SITE ENGINEER 8"- IO" RIP RAP FLOM RIFFLE BED MATERIAL PROPOSED SHALL BE NATIVE RIPRAP / CHANNEL TOE QUARRIED STONE BED MATERIAL ROCK/LOG SILL (SEE DETAIL) -HEAD OF RIFFLE (See profiles for elevations) NATIVE BED MATERIAL PROPOSED BETWEEN LOGS7 - LOG / ROCK SILL STREAMBED 6ª MIN I" MIN GEOTEXTILE FABRIC RIFFLE LENGTH = 10' ON DYE BRANCH 5' ON CEMETERY BRANCH

NOTES:

CONSTRUCTED RIFFLE

FABRIC INSTALLATION

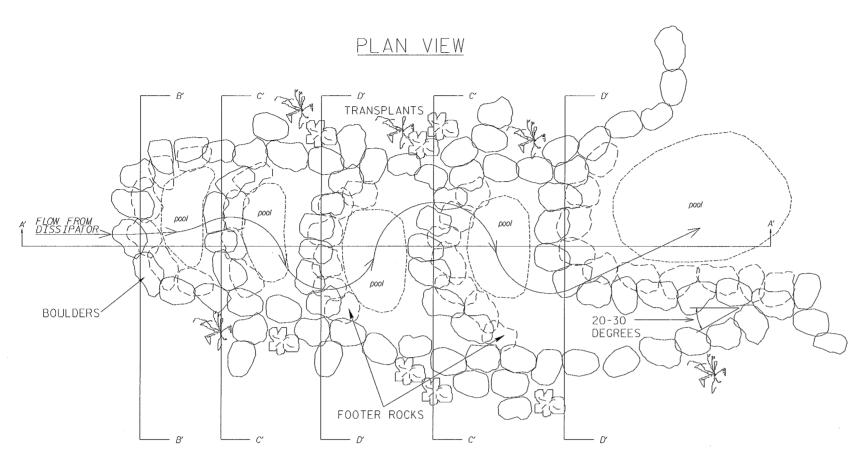
FABRIC TO LOOP TWICE AROUND LOG

I. RIFFLE BED MATERIAL SHALL BE A MINIMUM OF 6 INCHES IN DEPTH.

2. ROCK OR LOG SILL REQUIRED UP & DOWNSTREAM OF RIFFLE.

ATTACH FABRIC TO LOG WITH
PLASTIC CAP ROOFING NAILS

- I. SILL TO BE CONSTRUCTED OF BOULDERS 3'X 2'X I' (MIN. SIZE) OR LOGS WITH A DIAMETER OF 12' MINIMUM.
- 2. RIFFLE BED MATERIAL TO BE NATIVE BED RIP RAP/ QUARRIED STONE MATERIAL INSTALLED TO A MINIMUM OF 6" IN DEPTH.
- 3. GEOTEXTILE FABRIC TO USED ON ALL SILLS (ROCK & LOG). IF LOG SILLS ARE USED, FABRIC SHOULD WRAP AROUND LOG A MINIMUM OF 2 TIMES.
- 4. LOG SILLS SHALL BE ANCHORED AT TOE OF BANKS WITH BOULDERS TO PREVENT FLOATING OF LOG OR SCOUR.
- 5. TOE OF BANK TO BE LINED WITH 8"-10" RIP RAP.



SECTION A-A'

SLOPE= 2-7%

BOULDERS

FOOTER ROCKS

GEO-TEXTILE FABRIC

NATIVE PLANTINGS

- PROJECTED TOP OF VANE WING

GEOTEXTILE FABRIC (TYP.)

FOOTER ROCKS

NOTE: BOULDERS SHOULD BE NATIVE QUARRIED ROCK OR LOCALLY SHOT ROCK, ANGULAR AND OBLONG WITH APPROXIMATE MINIMUM DIMENSIONS OF 4' X 3' X 2' FOR DYE BRANCH.

ROCKS SHOULD FIT TIGHTLY WITH MINIMAL SPACES

FOOTER ROCKS SHOULD BE A MINIMUM OF 6 TIMES 'H' IN SAND BED STREAMS AND 3 TIMES 'H' FOR COBBLE/ GRAVEL BED STREAMS.

GEOTEXTILE FABRIC SHOULD BE PLACED ON UPSTREAM SIDE OF BOULDERS. FABRIC SHOULD BE OVERLAIN ON EXPOSED BOULDERS AND BURIED TO A MINIMUM DEPTH AS DIRECTED BY ON SITE DESIGNER. FABRIC SHOULD EXTEND UPSTREAM A MINIMUM LENGTH OF OF 6 FT. OR AS DIRECTED BY ON SITE DESIGNER. FABRIC SHOULD BE BACKFILLED WITH EXISTING BED MATERIAL.

H = 0.3'

MAXIMUM DROP PER STEP = 1.0'
BACKFILL BEHIND STEPS WITH 3" WASHED STONE

PROJECT ENGINEER

PROJECT REFERENCE NO. SHEET NO.

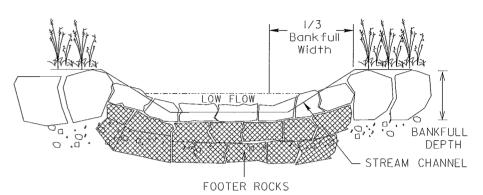
DYE BRANCH STREAM RESTORATION 2G

DETAILS

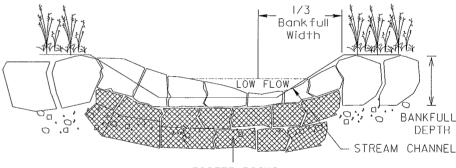
DETAILS

PO BOX 33127
RALEIGH, N.G. 27636
(919) 851-1912
(919) 851-1912
(919) 851-1918 (FAX)
WWW.MULKEYING.COM

SECTION B-B

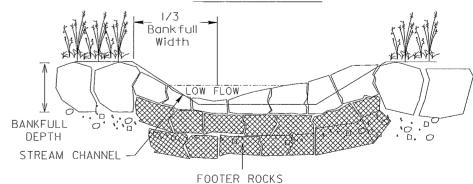


SECTION C-C



FOOTER ROCKS

SECTION D-D



STEP POOL DETAIL

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40.00



Debris in Dye Branch upper reach. Approximately 50 feet downstream of Center Ave.



Old pipe in Dye Branch upper reach. Approximately 80 feet upstream of Mclelland Street culvert.



Existing basketball courts along middle reach of Dye Branch. Proposed area for channel relocation.



Eroded banks along western side of basketball courts. Dye Branch middle reach.



Eroded banks along southern end of basketball courts. Dye Branch middle reach.



Concrete in steam on western side of basketball courts. Dye Branch middle reach looking downstream.





Eroded bank along last house before project ending boundary. Dye Branch lower reach.



Photo Point 1. View looking downstream from Center Avenue.



Photo Point 2. View looking upstream on Dye Branch from Mclelland Street.



Photo Point 2. View looking downstream on Dye Branch from McLelland Street.



Photo Point 3. View looking north toward the cemetery.



Photo Point 3. View looking south toward the bathrooms in Glenwood Memorial Park.



Photo Point 4. View looking upstream from Cabarrus Avenue.



Photo Point 4. View looking downstream from Cabarrus Avenue.



Photo Point 5. View looking at washout area approximately 50 ft. downstream of Cabarrus Avenue.



Photo Point 6. View looking upstream from lower end of existing Dye Branch.



Photo Point 7. View looking downstream on existing Cemetery Branch near confluence with Dye Branch.



Photo Point 7. View looking upstream on existing Cemetery Branch toward Church Street.



Photo Point 8. View looking southeast toward existing Cemetery Branch.



Photo Point 8. View looking southwest toward existing Cemetery Branch.