# **STREAM RESTORATION PLAN**

## RICHLAND CREEK, WAKE COUNTY, NC



**Prepared** for

# NC Ecosystem Enhancement Program

Final - June 13, 2007



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### TABLE OF CONTENTS

### Stream Restoration Plan for Richland Creek Town of Wake Forest, Wake County, NC

#### 1. Introduction

- 2. Goals and Objectives
- 3. Location Information
  - a. River basin
  - b. USGS 8-digit catalog number
  - c. County
  - d. Nearest town
  - e. Stream name and classification
  - f. USGS quad sheet
  - g. Location map
- 4. General Watershed Information
  - a. Drainage area
  - b. Dominant land use
  - c. Relative distribution of land use
  - d. Estimation of future land use change
- 5. Description of Existing Conditions
  - a. Existing hydrological features
  - b. Soils
  - c. Existing plant communities
  - d. Threatened/endangered species
  - e. Stream geometry and substrate
    i. Level II classification
    ii. Pavement/subpavement analysis
- 6. Stream Reference Studies
  - a. Classification of reference stream(s)
  - b. Reference dimension, pattern, and profile
  - c. Reference stream morphological table
  - d. Reference stream vegetative community
- 7. Stream Restoration Plan
  - a. Stream classification of restored site
  - b. Morphological table
  - c. Scaled plans
  - d. Longitudinal profile

### Table of Contents - Stream Restoration Plan for Richland Creek

- e. Sediment transport analysis
- f. Special features
- 8. Typicals
  - a. Cross-sections
  - b. Structures
- 9. Riparian Planting Plan
  - a. Electrical transmission corridor restrictions
  - b. Neuse River buffer requirements
  - c. Planting plan outline
- 10. Stream Monitoring Plan
  - a. Photo reference sites
  - b. Plant survival
  - c. Channel stability
  - d. Biological indicators
- 11. Stream Success Criteria

### **Stream Restoration Plan for Richland Creek**

### Town of Wake Forest, Wake County, NC

### 1. Introduction:

The North Carolina Ecosystem Enhancement Program seeks to restore 2800 linear feet of Richland Creek, located in the Neuse River watershed in Wake County, North Carolina. Richland Creek is located in the Neuse River Basin. This document summarizes the project's purpose, existing site conditions, assessment methodologies, and proposed restoration design. Supporting information is included in the attached appendices.

### 2. Goals and Objectives:

- 1. Establish stable channel dimension, pattern, and profile;
- 2. Restore a functioning floodplain;
- 3. Enhance aquatic and terrestrial habitat in the stream corridor;
- 4. Provide a riparian management zone that is compatible with the surrounding uses (golf course and electrical transmission corridor) and yet retains the ecological function of the riparian zone; and
- 5. Improve water quality by reducing the sediment load generated by failing banks and by restoring a riparian buffer.

### **3.** Location Information:

**a. River basin:** Neuse River. Richland Creek joins the Neuse River just below Falls Lake. The project reach is about five miles upstream from this confluence.

- **b.** USGS 8-digit catalog number: 03020201 in subbasin 03-04-02
- **c. County**: Wake County
- **d.** Nearest Town: Wake Forest, NC. The reach is within Paschal Golf Course on the western edge of town.
- e. Stream name and classification: Richland Creek (F4)
- f. USGS quad sheet: Wake Forest quadrangle (See Map 3f)
- **g.** Location map: See Map 3g

### 4. General Watershed Information:

- a. Drainage area: Approximately 7.8 square miles.
- **b.** Dominant land use: The restoration reach bisects a golf course; otherwise the watershed is urbanized to the east and rural/ residential to the west.

### c. Relative distribution of land use:

The majority of the watershed, extending from Wake Forest, NC to northwest of Youngsville in Franklin County is rural. The upper watershed in Franklin County is comprised of farms including a small percentage of row crops (mainly corn and soybeans), with the predominant land use being pasture, hayfields and woodlands. The upper portion is about 45 percent forest, 45 percent agriculture and 10 percent residential/commercial. The lower portion of the watershed in Wake County is approximately 50 percent rural and 50 percent residential/ urban. The rural portion is split almost evenly between forest and active farmland. The farmland areas contain edge woodlots and forests, some of which are adjacent to grazing fields and are accessed by cattle and horses. The forested portions of the landscape are on steeper slopes, rocky soil areas and along stream corridors.

The Richland Creek watershed contains a high voltage electrical transmission corridor that parallels the creek along its entire length and crosses it several times. One of the crossings occurs in the upper 400 +/- feet of the proposed restoration reach.

### d. Estimation of future land use change:

Recent development relating to the urban sprawl of Wake County has intensified the conversion of farmland in the Richland Creek watershed into residential and related commercial uses. At the time of our watershed survey, there were about five new housing developments being built on recently converted farmland within sight of the main channel of Richland Creek, upstream of the restoration reach. There are many other developments that have been or are being built, or are planned within the watershed. Additionally, several large farms are for sale and forestland is being timbered, with the strong potential to be converted to non-farm uses.

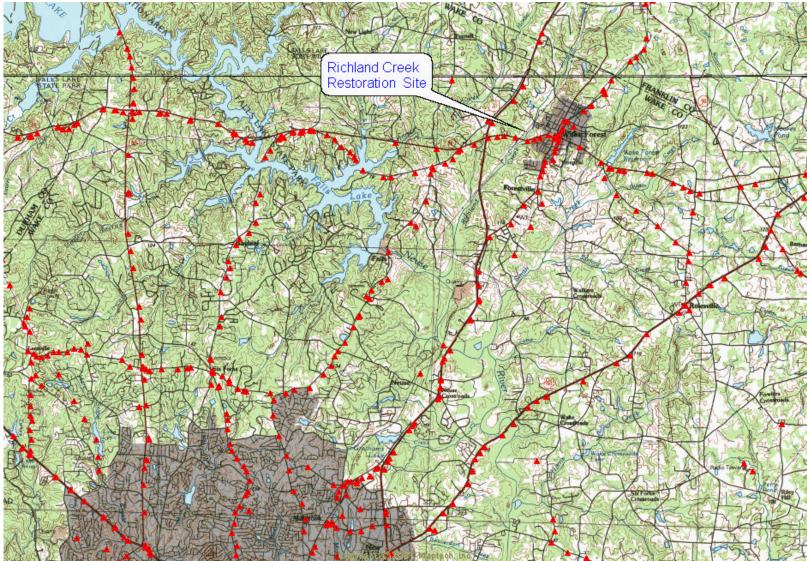
Given the recent history of land use in the Triangle area, it can be expected that land uses in this watershed will become increasingly converted to residential, commercial and other urban uses. This will likely result in increased levels of impervious surfaces, increased stormwater runoff, and declining water quality and impaired aquatic and riparian habitat throughout the watershed.

### 5. Description of Existing Conditions

### a. Existing hydrological features (See Aerial photo (1999)):

The existing stream reach is a highly modified channel with a long history of impact. The reach runs the length of Paschal Golf Course, which was first constructed in 1917. Development and management of the golf course involved straightening the creek channel and draining adjacent floodplains with ditches and buried tiles. Several ponds were also constructed on the floodplain over the years; the remnants of one still remains in the restoration corridor.

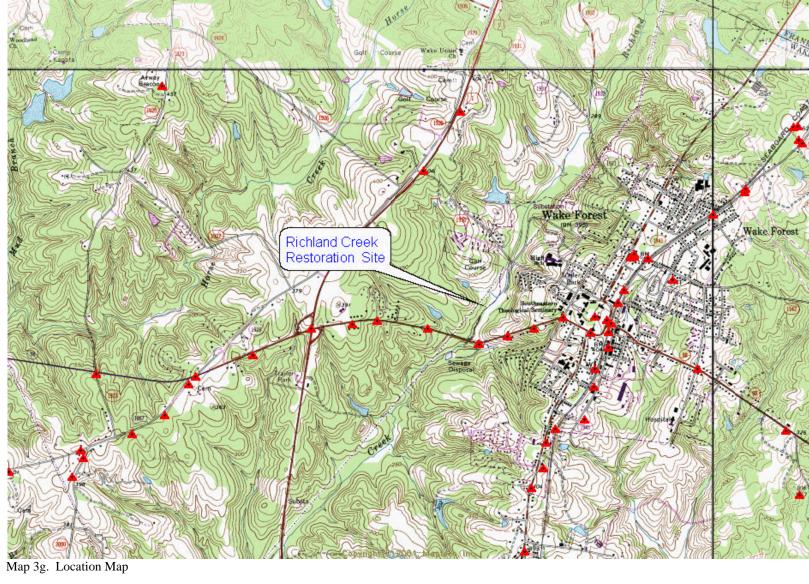
There are two small creeks that enter the restoration reach from the west. One of these creeks drains a small pond on the western edge of the golf course. This creek enters the



Map 3f General Location (from USGS Quadrangle "Wake Forest, NC")

December 3, 2004

EcoLogic Associates, P.C.



### Richland Creek Paschal Golf Course Wake Forest, NC







4321 A S. Elm-Eugene St. Greensboro, NC 27406 336-335-1108 336-335-3141 reach just inside the forested lower reach. The other creek enters from the west side at the lower end of the project near the Durham Road box culverts. Both of these creeks drain areas of 50 to 100 acres and can be easily integrated into the restoration plan.

There are several storm drains that enter the channel within the restoration reach. One of the storm drains enters the restoration reach after collecting stormwater from the studenthousing complex east of the floodplain. Other storm drains collect stormwater from the golf course parking lot and the access road.

The lower reach is dramatically impacted by large trees that have fallen in the channel and/or large logs lodged in the channel causing local deposition and scour.

### a. Soils (See Figure 5b and Table 5b):

The soils along the restoration corridor are relatively uniform throughout the reach based on the Soil Survey of Wake County. Richland Creek soils are predominately Chewacla Soils (Cm) which occur on 0 to 2 percent slopes. Chewacla soils have a surface layer of brown to dark grayish-brown sandy loam to silt loam 4 to 12 inches thick. Soil colors below the surface layer range from brown to dark grayish-brown, and the texture ranges from sandy loam or silt loam to clay. The total thickness of the series is from 34 inches to more than 72 inches. Infiltration is good and runoff is slow. Flooding hazard is high and the hazard of wetness is very severe.

Within the Richland Creek floodplain, two other soil classifications occur, Altavista and Madison.

Altavista (Afa) soils occur on 0 to 4 percent slopes. The soils are comprised of fine sandy loam located on low stream terraces. The surface layer is brownish-gray and light gray-brown fine sandy loam 3 to 15 inches thick. The subsoil is yellowish-brown to reddish-yellow and is 12 to 29 inches thick. Infiltration is good and runoff is slow to medium. Most of this soil type coincides with golf course fairways.

Madison (MdD2) occurs on 10 to 15 percent slopes. This series of Madison soils are an eroded sandy loam located on narrow side slopes bordering upland drainage ways. The surface layer is 3 to 7 inches thick of dark-brown to brown sandy loam, and in most cases it is comprised of a mixture of original surface soil and subsoils. The subsoil is a friable clay loam to clay, red to dark red that is 10 to 35 inches thick. Infiltration is fair and surface runoff is very rapid.

A shallow geotechnical exploration was conducted throughout the restoration corridor. The soils were found to generally match the mapped types (soil classification tests are available if needed). Analyses of samples collected along the corridor indicate the upper 2 feet is mostly loose to medium dense silty sand of either residual or alluvial derivation. Below this level to a depth of 3.5 to 5 feet, the soils are mostly residual, of medium density, and vary from silty sand to silty clay.

In some locations below the alluvial soils, dense saprolite of either clay or sand composition occurs. In several locations throughout the reach, bedrock or hard clay saprolite in the channel bottom functions as a grade control. Undisturbed residual soils are anticipated to have sufficient strength to form competent banks at slopes of 2(H) to 1(V) or steeper, but because the shallower soils are often alluvial and less dense, floodplain banks should be laid back to 3(H) to 1(V) where room allows.

In the central portion of the floodplain, the subsoil was saturated at a depth of approximately 3.5 feet, indicating the approximate surface of the water table.

### **b.** Existing plant communities (See Figure 5c):

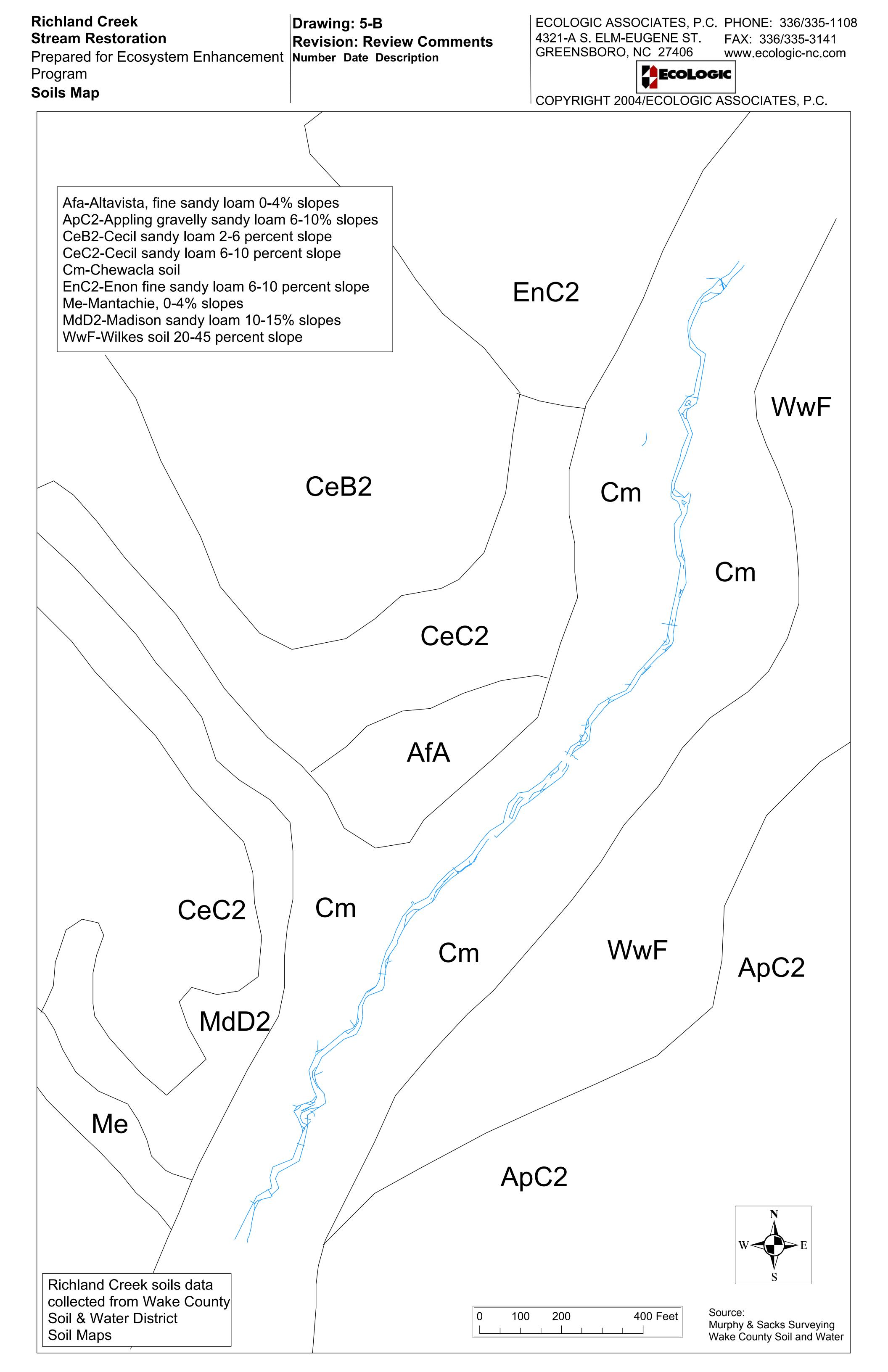
The existing plant communities throughout the reach are comprised of three different types. The three types are the result of different management practices applied to various areas of the restoration corridor.

The upper 400 feet of the reach lies within an electrical transmission corridor. The management of vegetation under the power lines includes seasonal cutting and mowing to maintain vegetation less than 12 feet tall. This results in a thick growth of tree resprouts, shrubs dominated by blackberry canes and aggressive vines like honeysuckle.

The middle section of the restoration reach (from Stations 400 to 1900 feet) is dominated by the developed golf course and is managed accordingly. With the exception of a few large specimen trees scattered along the creek corridor, the majority of woody vegetation has been removed from the stream banks and suppressed by herbicides and regular mowing. In most areas, turf grass exists right up to the tops of banks. Some areas have no vegetation as a result of bank failure creating vertical or undercut banks with exposed soils, or a thick mulch of grass clippings dumped on the banks from mowers used to maintain the course.

The lower section of the restoration reach (about 900 feet) has a forested bank on the right (west) side and a managed golf course link on the left (east) side. The forested side has many large and mature trees, subcanopy trees and shrubs along with thick vines and riparian herbs. The forested area is thickly invaded with invasive exotic species typical of creeks in urban areas of the Piedmont. The east bank is managed with mowed turf grass to the top of banks with few remaining woody plants.

The majority of vegetation in the Richland Creek riparian zone, as it flows through Paschal Golf Course, is mowed grass to the stream bank edge. Portions of the riparian buffer support multi-layered vegetation with canopy hardwoods, mostly in areas where the golf course is not maintained. Canopy and subcanopy trees include specimen loblolly pine (*Pinus taeda*), river birch (*Betula nigra*), boxelder (*Acer negundo*), and flowering dogwood (*Cornus florida*). Other trees noted include black willow (*Salix nigra*), sycamore (*Platanus occidentalis*), American ash (*Fraxinus americana*), water oak (*Quercus nigra*), sweet gum (*Liquidamber styraciflua*), red maple (*Acer rubrum*), black walnut (*Juglans nigra*), willow oak (*Quercus phellos*), redbud (*Cercis canadensis*), and swamp red oak (*Quercus shumardii*).



### Table 5b-1

### SOIL BORING LOG

### Richland Creek Town of Wake Forest, Wake County, NC

| Boring No. | Description   |
|------------|---|
| 1          | Stiff Clayey Silt (Residual) Augered into Rt. bank @ mid-height   |
| 2          | Med. Dense Sandy Silt (Residual) Augered into Rt. bank @ mid-height   |
| 3          | Hard Clay (Saprolite) Augered into stream bottom  |
| 4          | 0'-4' Firm Silty Sand (Alluvial or Residual) Augered on Rt. floodplain<br>Wet @ 3.5', Water at 4.0'   |
| 5          | Dense Silty Coarse-Med. Sand (Residual) Augered into Lt. bank toe   |
| 6          | 0'-2' Firm Silty Sand (Alluvial or Residual) Augered on Rt. floodplain<br>2'-4' Med. Dense Silty Sand with Gravel (Residual)<br>Wet @ 3.0', Saturated at 4.0' |
| 7          | 0'-2.5' Firm Silty Sand (Alluv. or Residual) Augered on Rt. floodplain<br>2.5'-4' Firm Clayey Sandy Silt (Residual)<br>Wet @ 3.5'                             |
| 8          | 0'-4' Firm Sandy Silty Clay (Residual) Augered on Rt. floodplain  |

NOTES: 1. Field exploration done on August 20, 2004

2. Golf course superintendent shared knowledge of past bedrock and/or boulder encounters on the east side of the stream, but none historically on the west side.

### Table 5b-2 SUMMARY OF LABORATORY TEST DATA\*

### Richland Creek (Ecologic)

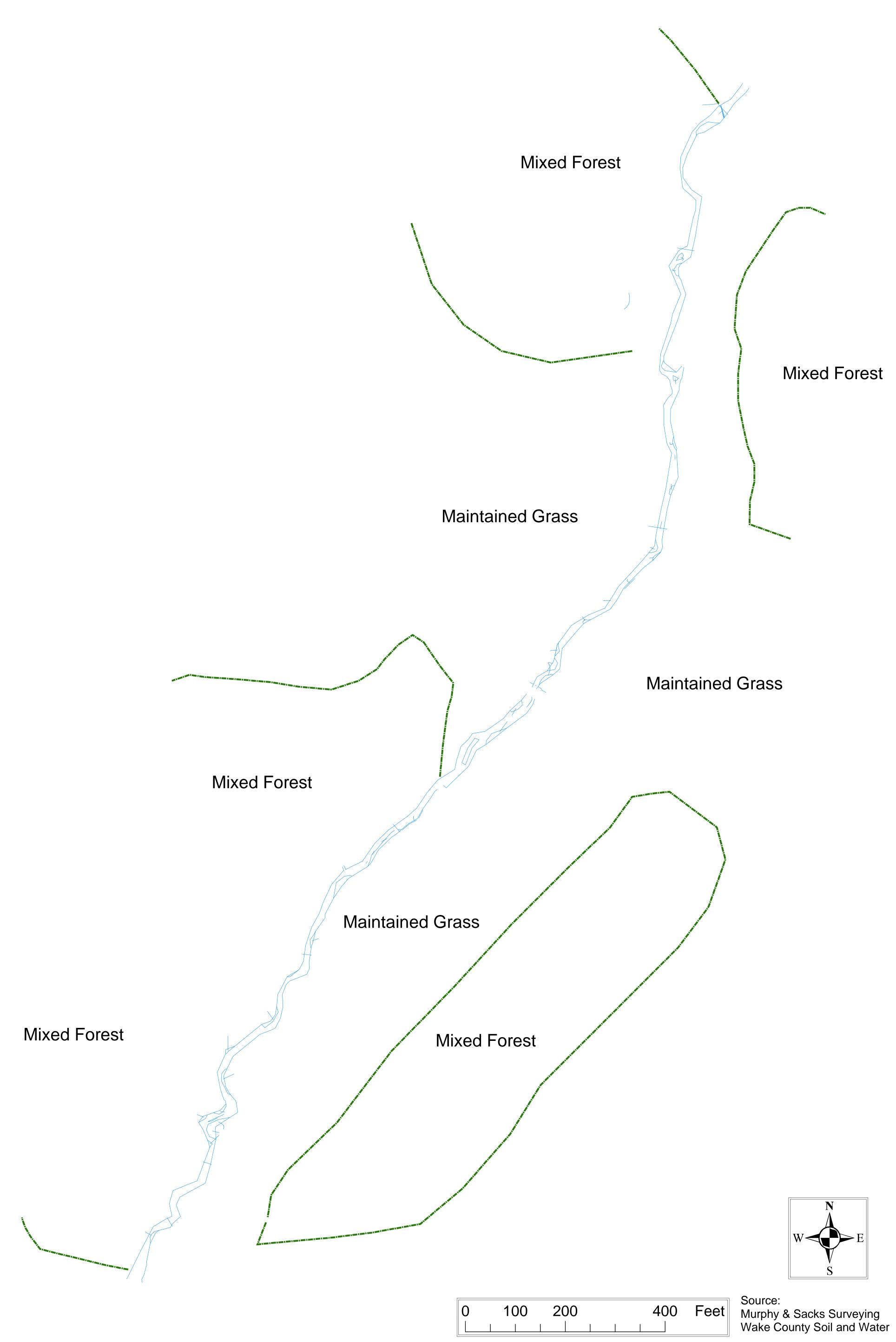
|                  | Sample          |                  |                        | Natural               | At  | erberg Lin | nits | Max. Dry         | Optimum<br>Moisture |     | led Unit<br>nt (psf) |                  | Internal Fri<br>(deg | ction Angle<br>rees) |                    |
|------------------|-----------------|------------------|------------------------|-----------------------|-----|------------|------|------------------|---------------------|-----|----------------------|------------------|----------------------|----------------------|--------------------|
| Boring<br>Number | Depth<br>(feet) | Sample<br>Type** | USCS<br>Classification | Moisture<br>Content % | L.L | P.L.       | P.I. | Density<br>(pcf) | Content<br>(%)      | Dry | Wet                  | Bearing<br>Ratio | Total                | Eff.                 | % Finer<br>No. 200 |
| 2                | 0-2             | Bulk             |                        |                       |     |            |      |                  |                     |     |                      |                  |                      |                      | 38                 |
| 3                | 0-0             | Bulk             | CL                     |                       | 36  | 16         | 20   |                  |                     |     |                      |                  |                      |                      | 62                 |
| 4                | 0-3             | Bulk             | SC                     |                       | 26  | 18         | 8    |                  |                     |     |                      |                  |                      |                      | 37                 |
| 6                | 2-4             | Bulk             | SM                     |                       | 11  | NP         | NP   |                  |                     |     |                      |                  |                      |                      | 16                 |
| 7B               | 2.5-4           | Bulk             |                        |                       |     |            |      |                  |                     |     |                      |                  |                      |                      | 27                 |
| 8                | 0-4             | Bulk             | CL                     |                       | 46  | 24         | 22.  |                  |                     |     |                      |                  |                      |                      | 83                 |
|                  |                 |                  |                        |                       |     |            |      |                  |                     |     |                      |                  |                      |                      |                    |
|                  |                 |                  |                        |                       |     |            |      |                  |                     |     |                      |                  |                      |                      |                    |
|                  |                 |                  |                        |                       |     |            |      |                  |                     |     |                      |                  |                      |                      |                    |
|                  |                 |                  |                        |                       |     |            |      |                  |                     |     |                      |                  |                      |                      |                    |

\* Graphic Presentations of Results of Triaxial, Consolidation, CBR, Proctor, Grain Size and other tests follow this summary.

### GEOSCIENCE GROUP, INC. GREENSBORO, NORTH CAROLINA

\*\* SS=Split Spoon Sample (ASTM D-1586) UD=Undisturbed Sample (ASTM D-1587) Job Number: \_\_\_\_\_ Page\_\_ of \_\_\_





The gravel bars in the channel support numerous saplings of sycamore (*Platanus occidentalis*), and black willow (*Salix nigra*). Native riparian shrubs that occur on the site include silky dogwood (*Cornus amomum*), tag alder (*Alnus serrulata*), elderberry (*Sambucus canadensis*), and hazelnut (*Corylus americana*). A few non-native, invasive shrubs that were noted include privet (*Ligustrum sinensis*), multiflora rose (*Rosa multiflora*), and silverberry (*Eleagnus umbellate*).

The herb and vine layer includes a mix of native and non-native species. Aggressive spreading non-native species noted include Japanese grass (*Microstegium vimineum*), chickweed (*Stellaria media*), Japanese honeysuckle (*Lonicera japonica*), fescue (*Festuca* sp), and bittersweet (*Cardamine* sp.). Native wetland species noted in the riparian buffer include needle rush (*Juncus effusus* and other spp.), sedges (*Carex lurida, C. criniata*), wing stem (*Verbesina occidentalis*), grapes (*Vitis* spp), cat-tails (*Typha latifolia*), jewelweed (*Impatiens capensis*), sensitive fern (*Onoclea sensibilis*), and jumpseed (*Tovara virginiana*).

### a. Threatened/endangered species

The North Carolina Natural Heritage Program lists three animal species, two vascular plants, two natural communities and one special habitat as significant in the Wake Forest quadrangle. Only one of these species is federally listed as a Federal Species of Concern and that is the Southeastern Myotis (a bat), which is only historically known and has not been observed in this area since 1979. Likewise, the Neuse River Waterdog is only known as a historic occurrence. The only currently known listed animal species is the Four-toed salamander (NC Special Concern) which lives in wetlands of a type that do not occur within the restoration reach corridor.

The two plant species listed for Wake Forest quadrangle also include one currently known species and one historic reference. The historic reference is to the Glade Milkvine, which occurs on mafic or calcareous soil types that do not occur within the Richland Creek restoration reach. Likewise, the Swamp Saxifrage, while known to occur in the area, requires wetland habitats that do not occur on the land surrounding the restoration reach.

The two listed natural community types include the Piedmont/Mountain Levee Forest and the Floodplain Pool, and the listed special habitat includes the Wading Bird Rookery, none of which occur in the area of the restoration reach.

### b. Stream geometry and substrate

### i. Level II classification

The stream channel within the restoration reach is a composite of two stream types. The upper reach is a C4 stream with more belt width and significantly larger point bars and deeper pools than most of the reach. The majority of the remaining reach is a F4 stream with little meander geometry, an entrenchment ratio of 1.4, a width-to-depth ratio of 11.6,

and a sinuosity of 1.22. The bankfull width of the existing stream varies between 22 and 35 feet, with a corresponding depth range of 1.4 to 2.8 feet at bankfull.

This reach of Richland Creek was first identified as a candidate for stream restoration by Wake County NRCS District Conservationist Tom Hill. In April 2001, Tom and his staff installed bank pins in several sections of the creek in order to document the rate of bank failure. The failure and movement of the banks was evident in the morphology of increasing meander in several areas, and substantiated by the long-term observations of Mr. Bobby Kinton, Paschal Golf Course Superintendent.

The results of bank pin measurements indicated at least 70 tons/100 feet of soil loss into Richland Creek in the area where the bank pins were placed. Mr. Hill measured over 800 feet of severely eroded banks similar to the area with the bank pins. For the remainder of the reach, he estimated at least 15 tons/100 feet of soil loss over an additional 2000 feet. The measurements were taken from April to December 2001. The calculated total sediment loss over this period from the entire reach is 860 tons. This equates to an annual rate of soil loss of 1290 tons/ year for the project reach.

Our survey found two of the bank pins at one location still in place, which were measured. Compared to an earlier photo of the site from Tom Hill, we estimate the bank has receded an additional 18 inches at that location over 26 months. In other locations of bank pins, the pins are gone, presumably due to the bank having moved roughly 3 to 6 feet during the same period. BEHI analysis rates the overall reach as having a High erodibility hazard rating, with an estimate of soil loss in the reach exceeding 9000 cubic feet/year, or approximately 540 tons/year.

### ii. Pavement/subpavement analysis

The existing condition of the stream reach through Paschal Golf Course, which exhibits a significant amount of bed and bank instability, limits the formation of well developed and stable riffle and bar features. Two riffles and two bars were sampled for particle size. The pavement and subpavement analysis indicates the  $D_{50}$  of the pavement is about 22 mm, while the  $D_{50}$  of the subpavement is 2.5 mm in a riffle in the well-defined C4 section. Near the low end of the reach in the F4 section, the riffle particles are smaller, with the  $D_{50}$  being 12 mm for pavement and 2.7 mm for subpavement. The largest particle from the pavement included a 61 mm, 339-gram rock, while the subpavement had a largest particle of 44 mm, 114 grams.

Given the proportion of riffle and subpavement  $D_{50}$ 's, the entrainment calculation indicates an aggrading channel bed. The Shields Diagram indicates the stream is competent to move the largest particles found in the system.

### 6. Stream Reference Studies

### a. Classification of reference stream(s)

Two reference reaches were investigated for use in this restoration. An extended search was made to locate a reference reach close to the restoration reach, or at least in the eastern Piedmont. After discussions with colleagues who frequently work in the Raleigh area, we surveyed an unnamed tributary to Lake Wheeler, which classified as a C4 stream of reference quality. We deemed this reference suitable for use for project design. In addition, we consulted with KCI Associates, who is conducting stream restoration work just upstream from our project. KCI identified some short sections of Richland Creek near the Wake County line, which are of reference quality, and shared the data with us. The data is shown on the Morphological Data Table (Table 7b).

### b. Reference dimension, pattern, and profile

The reference reaches represent drainage areas of 0.28 to 4.8 square miles. The bankfull cross-sectional areas of the reference reaches are 13.5 to 70 square feet. The bankfull depths are 1.0 to 2.3 feet. Bankfull widths are 12 to 32 feet. These data fall just above the Piedmont Rural Regional Curve published by the NCSU Steam Restoration Institute. The pattern data also has a wide range of values that result from the differences in drainage areas and differences in valley type and adjacent land use. Meander lengths are 50 to 200 feet, radii of curvature are 18 to 70 feet, and belt widths are 50 to 300 feet. Valley slopes are .0045 to .006, with average water surface slopes of 0.004 to 0.005.

### c. Reference stream morphological table

The reference reach morphological table is attached as Table 7b. Reference reach data is included in the morphological table with existing and proposed channel geometry data.

### d. Reference stream vegetative community

The reference reaches both occur in forested portions of their watersheds. The vegetative communities are successional forest communities typical of the disturbed landscape of Piedmont NC. These alluvial forests occur along main channels and smaller tributaries. The canopy is patchy as a result of past agricultural and modern development activity, and is composed of river birch, Betula nigra, sweet gum, Liquidambar styraciflua, tulip tree, Liriodendron tulipifera, sycamore, Platanus occidentalis, red maple, Acer rubrum and box elder, Acer negundo. The understory contains ironwood, Carpinus caroliniana, flowering dogwood, Cornus florida, American beech, Fagus grandifolia, tree-of-heaven, Ailanthus altissima, red oak, Quercus rubra and black cherry, Prunus serotina. Occasional areas of shrubs contain strawberry bush, Euonymus americanus, yellowroot, Xanthorhiza simplicissima, Chinese privet, Ligustrum sinense, multiflora rose, Rosa multiflora, elderberry, Sambucus canadensis, and tag alder, Alnus serrulata. A mixture of herbs inhabit the various habitats along these alluvial valleys including native impatiens, Impatiens capensis, false nettle, Boehmeria cylindrica, knotweed, Polygonum punctatum, sedges, Carex spp, soft rush, Juncus effusus, may apple, Podophyllum peltatum, Japanese grass, Microstegium vimineum, tearthumb, Polygonum sagittatum, and asters, Aster spp.

### 7. Stream Restoration Plan

### a. Stream classification of restored site

We propose to create a restored stream with stable banks, improved bed morphology and enhanced aquatic habitat. The primary goal is to produce a stable dimension, pattern and profile that conveys channel-forming (bankfull) and lesser discharges efficiently, dissipates energy and moves sediment without significant degradation or aggradation, provides a floodplain (bankfull) bench to help contain flood flows, and minimizes impacts to the golf course and adjacent utility corridors, with a protected buffer that allows for revegetation of currently bare and failing banks and reforestation for long-term habitat and water quality improvements.

We propose to construct a C4 channel with increased meander geometry, consistent bankfull width, increased pool depth, steeper riffles, flatter pools and native riparian vegetation on the banks.

The most significant constraint on the site is the sanitary sewer line that parallels the entire length of the restoration reach along the eastern side. In some cases the current channel is less than 20 feet from the sewer centerline. This sewer line corridor, and its associated utility easement, is a significant constraint on the east side of the restoration corridor and will limit the meander geometry of the restored channel (belt width, etc.).

### b. Morphological table:

The attached Table 7b shows existing conditions, proposed conditions and reference conditions.

**Note on gage conditions:** Despite an intensive search, we were unable to locate a gage station in the Wake County area that had both a long history of record and identifiable and usable bankfull indicators. When we inquired with the NC Ecosystem Enhancement Program and the NCSU Stream Restoration Institute, they acknowledged the problem and recommended some possible gages that later proved to be unsuitable or in a different ecoregion of the state.

The two methods used to verify bankfull stage at Richland Creek were: 1) regional hydraulic geometry relationships (regional curves), and 2) stage/discharge data from KCI for Richland Creek.

KCI was also unable to find a suitable gage in the area, but they installed a staff gage, flow meter and pressure transducer in Richland Creek to allow them to determine the stage/discharge relationships of the creek directly.

Monitoring of surface water fluctuations was undertaken to understand the hydrologic response of the watershed and to verify the proposed design discharges. Two (2) surface water-monitoring gauges, one (1) barometric logger (required for gauge calibration), and one (1) rain gauge were used to perform this monitoring. Three months of continuous

|  |                     | Reference           | Reference        |             |
|--|---------------------|---------------------|------------------|-------------|
|  |                     | Upper               | Relefence        |             |
|  | Existing            | Richland            | UT to Lake       | Proposed    |
| CLASSIFICATION DATA  | Channel             | Creek               | Wheeler          | Channel     |
| Rosgen Stream Type   | F4/1<br>7.8         | C4<br>4.8           | C4<br>0.28       | C4/1<br>7.8 |
| Drainage Area (sq mi)<br>Bankfull Width (W <sub>bkf</sub> ) (ft) | 22-35               | 28-32               | 9.2-13.5         | 33          |
|  |                     |                     |                  |             |
| Bankfull Mean Depth (d <sub>bkf</sub> ) (ft)                     | 1.4-2.8             | 2.3-2.4             | .9-1.1           | 2.6         |
| Bankfull Cross Sectional Area (A <sub>bkf</sub> ) (sf)           | 48-72               | 67-75               | 6.5-13.8         | 85.0        |
| Width/Depth ratio (W <sub>bkf</sub> /d <sub>bkf</sub> )          | 12-13.8             | 12.2-13.3           | 10.5-12.3        | 12.1        |
| Maximum depth (d <sub>mbkf</sub> ) (ft)                          | 3.4-3.8             | 3.75                | .9-1.6           | 3.4         |
| Width of flood prone area $(W_{fpa})$ (ft)                       | 28-60               | >100                | 35-55+           | 100         |
| Entrenchment ratio (ER)  | 1.7-1.9             | 3.1-3.6             | 3.8-4.1          | 3.0         |
| Water surface slope (S) (ft/ft)                                  | 0.0028              | 0.004               | 0.0045           | 0.0028      |
| Sinuosity (stream length/valley length) (K)<br>DIMENSION DATA    | 1.22                | 1.1                 | 1.15-1.2         | 1.2         |
| Pool Depth (ft)  | 3.1                 | 2.9                 | 1.1-1.4          | 3.4         |
| Riffle Depth (ft)  | 1.4-2.8             | 2.3-2.4             | .9-1.6           | 2.6         |
| Pool Width (ft)  | 49.6                | 26-35               | 9.0-11.1         | 36          |
| Riffle Width (ft)  | 22-35               | 28-32               | 10-13.1          | 33          |
| Pool XS Area (sf)  | 56.0                | 70-75               | 11.1-14.1        | 120.0       |
| Riffle XS area (sf)  | 60.9                | 67-75               | 8.8-21.6         | 86.0        |
| Pool depth/mean riffle depth<br>Pool width/riffle width          | 1.5<br>1.7          | <u> </u>            | .9-1.3<br>.7-1.6 | 1.3<br>1.1  |
| Pool area/riffle area  |                     |                     |                  |             |
| Max pool depth/d <sub>bkf</sub>                                  | 0.9                 | .9-1.1<br>1.9-2.0   | 1.1<br>2.0-2.5   | 1.3<br>2.1  |
| Low bankheight/max bankfull depth                                | 1.2                 | 2-Jan               | 1-1.2            | 1           |
| Mean bankfull velocity (V) (fps)                                 | 3.1-7.0             | 3.6-5.0             | 2.5-3.5          | 5.0         |
| Bankfull discharge (Q) (cfs)                                     | 305-400             | 260-280             | 16-48            | 425         |
| PATTERN DATA   | 000 100             | 200 200             | 10 10            | .20         |
| Meander length (L <sub>m</sub> ) (ft)                            | 110-300             | 110-200             | 38-58            | 220-330     |
| Radius of curvature (Rc) (ft)                                    | 32-98               | 37-70               | 16-32            | 80-100      |
| Belt width (W <sub>blt</sub> ) (ft)                              | 22-71               | 100-300             | 30-60            | 60-300      |
| Meander width ratio (W <sub>blt</sub> /W <sub>bkf</sub> )        | 1.59                | 9.3-10.7            | 1.2-4.4          | 9.0         |
| Radius of curvature/bankfull width                               | 1.34                | 1.1-2.1             | 2.5-3.5          | 2.4         |
| Meander length/bankfull width                                    | 3.4-4.0             | 3.9-6.3             | 16-48            | 6.0-9.0     |
| PROFILE DATA   |                     |                     |                  |             |
| Valley slope   | 0.003               | 0.0045              | 0.005            | 0.003       |
| Average water surface slope                                      | 0.0028              | 0.004               | 0.005            | 0.0028      |
| Riffle slope   | 0.02037             | .005009             | .00703           | 0.0056      |
| Pool slope<br>Pool to pool spacing                               | .00090022<br>38-258 | .000-0.025<br>25-90 | 0000022          | 0.00056     |
| Pool length  | 23-96               | 25-90<br>25-May     | 8-22.0           | 41          |
| Riffle slope/avg water surface slope                             | 4.0                 | 1.3-2.3             | 1.4-6.0          | 1.5-2.0     |
| Pool slope/avg water surface slope                               | 0.6                 | 0.0-0.6             | 00.044           | 0.5         |
| Pool length/bankfull width                                       | 1.1                 | .29                 | .49-1.6          | 1.20        |
| Pool to pool spacing/bankfull width                              | 3.5                 | .8-3.0              | 1.4-5.9          | 4.5         |
| CHANNEL MATERIALS  |                     |                     | 0.70             | 1           |
| D16<br>D35   | 1.5                 |                     | 0.76             |             |
| D35<br>D50 riffle  | 7.3<br>12           |                     | 1.5<br>5.4       | >10         |
| D84  | 35                  |                     | 21.8             | >10         |
| D95  | 49                  |                     | 36               |             |
| PAVEMENT   |                     |                     | Bar              |             |
| D16  | 12                  |                     | 1.4              |             |
| D35  | 14                  |                     | 2-Jan            |             |
| D50  | 22.5                |                     | 7                |             |
| D84  | 54                  |                     | 29               |             |
| D95<br>Largest #1  | 61<br>61            |                     | 55<br>61/13oz    |             |
| Largest #2   | 56                  |                     | 44/6oz           |             |
| SUBPAVEMENT  |                     |                     | . 1/ 002         |             |
| D16  | 1.2                 |                     |                  |             |
| D35  | 1.7                 |                     |                  |             |
| D50  | 2.5                 |                     |                  |             |
| D84  | 14                  |                     |                  |             |
| D95  | 27                  |                     |                  |             |
|  |                     |                     | 1                | 1           |
| Largest #1<br>Largest #2   | 58<br>38            |                     |                  |             |

### Table 7b Morphological Data Richland Creek, Wake County, NC

recordings (June through September) were utilized in this study. In-situ gauging with a Doppler velocity meter was used to calibrate the discharge estimates from these instruments.

Stream stage data (water levels) were collected in the stream immediately up stream of the start of our restoration reach. Data was collected for three months (June through September) and water levels were correlated to an estimated discharge using a rating curve generated for the gauged section. Three significant flow events occurred during the monitoring period. On August 30<sup>th</sup>, Richland Creek in the vicinity of the gauge was discharging approximately 309 ft<sup>3</sup>/s. August 13<sup>th</sup> and June 8<sup>th</sup> experienced flows exceeding 185 and 155 ft<sup>3</sup>/s, respectively. The stage data collected during this period is useful in supporting/validating the bankfull identification from field indicators.

After these storm events a significant trend was apparent in the hydrograph and a stage/discharge relationship could be determined. This relationship was then plotted so that the discharge of known bankfull indicator elevations could be determined. These stage/discharge relationships were then adjusted for watershed area. This produced a sequence of bankfull discharges related to the watershed areas: 5.6 square miles = 320 cfs, 7.2 square miles = 400 cfs and 7.8 square miles = 425 cfs. Since the EEP restoration reach has the largest of these areas, we are using a design discharge of 425 cfs at bankfull. As expected, this level falls between the NC Rural Piedmont Regional Curve value of 390 cfs and the NC Urban Piedmont Regional Curve value of 770 cfs.

Figure 7b shows the stage/discharge relationship for Richland Creek from KCI.

### c. Scaled plans (See Drawings 7C-1 and 7C-2)

### d. Longitudinal profile (See Table 7d and Figure 7d)

The design longitudinal profile is attached in both table and chart form.

### e. Sediment transport analysis (Tables 7e)

Entrainment calculations for the existing and proposed channels are attached. The riffle pebble count  $D_{50}$  for both is 12 mm, and the bar/subpavement  $D_{50}$  for both is 2.5 mm. In addition, the largest particle from the bar/subpavement for both analyses is 58 mm. The only difference is the bankfull mean depth, which is deeper in the proposed channel. The entrainment calculations show the existing channel to be aggrading and the proposed channel to be stable.

# **f.** Special features (Rock ramp fishway) (See Drawing 7F and Tables 7f) (By Alan Schlindwein, PE, KCI Associates)

Rock ramps are essentially an analog of natural rock outcroppings. Within some watersheds, there are bedrock outcroppings that create steep and rough flow conditions in stream channels. Upstream and downstream of this natural feature, there may be normal

alluvial stream channels. These outcropping features are so common, that they are habitat for some species and are used for spawning by fish like the Sturgeon. The difficultly in analog design is to create a stable channel bed and predictable flow system.

Because these rock ramp channels are so steep (the proposed gradient on Richland Creek is only 10% as steep as the proposed rock ramp) they must be built with boulders. These boulders will not be replaced by natural means, so they must be immobile. To complicate matters, the modeling of shallow flow on boulders is not well defined in the literature and the length of rock ramps are such that the flow must be broken by a pattern of exposed rock for migratory fish to pass. This pattern of exposed rocks is called, a boulder garden, and it creates flow conditions of refuge, turbulence and chutes. The created chute flow intensifies the stress on the channel bed well above the average flow of the rock ramp.

To model the resistance of the rock surface at shallow depths, Mussetter's relationship (1989) for the Darcey-Wiesbach friction factor is used. A Manning's "n" is derived and used in the flow equation to generate average flow conditions. The concentration of flow and shear around the boulders is taken from Shamloo et al (2002) and used to determine the critical shear stresses that the channel must resist. The pattern of stone in the boulder garden is taken from Acharya et al (2000). The stone sizes are calculated using Andrews (1994) critical shear stress equation.

The exposed stone in the boulder garden pattern must be just high enough to affect the shallow flows and must be wide enough to create the chute & wake flow pattern. In between the chutes and the wake is a region of von Karman vortex flow streets. These turbulent vortex streets are where larger fish swim up the rock ramps (Liao et al, 2003). To cross the chute, the fish use a swimming burst to reach the wake of the upstream boulder. At the top of the structure, the fish burst into the slow moving water of the natural stream channel. Because rock ramps resemble natural geological features so well, they are two-way migration paths, both upstream and downstream.

The cross section of the fishway is "V" shaped, which concentrates low flows into a small channel. The boulder garden is spaced such that large boulders border this narrow, low flow every 9 feet along the profile. At higher flows the central boulders will be washed out hydraulically, so lateral boulders are needed in shallower water to create the necessary flow conditions for fish passage. The horizontal spacing is 6 feet for each row of three exposed boulders. By providing multiple pathways up the structure, debris or ice can only temporarily block an individual pathway. Higher flows will wash trees and ice off of the rock ramp; in this way they are self-cleaning and low maintenance. These rock ramps are so steep, that sediments will not settle on these features and they will remain flush and well aerated.

### h-Q Relationship

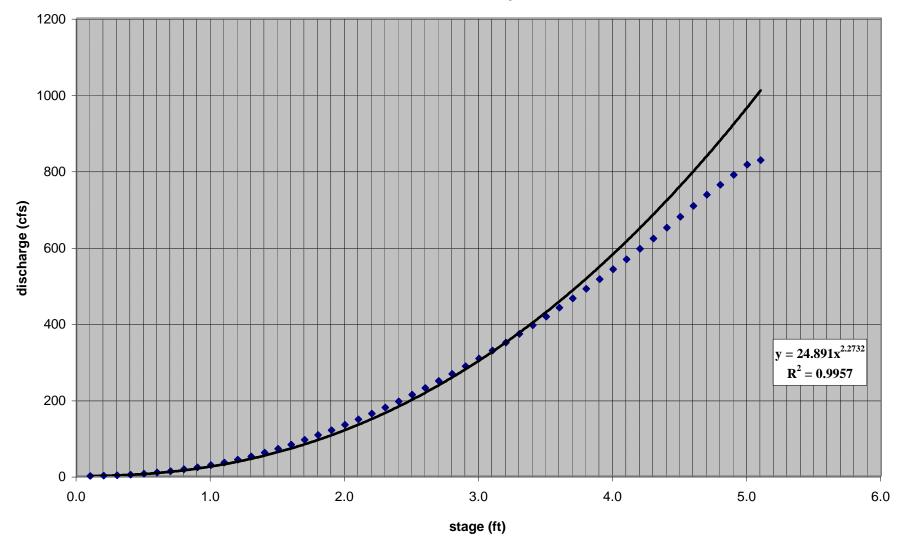
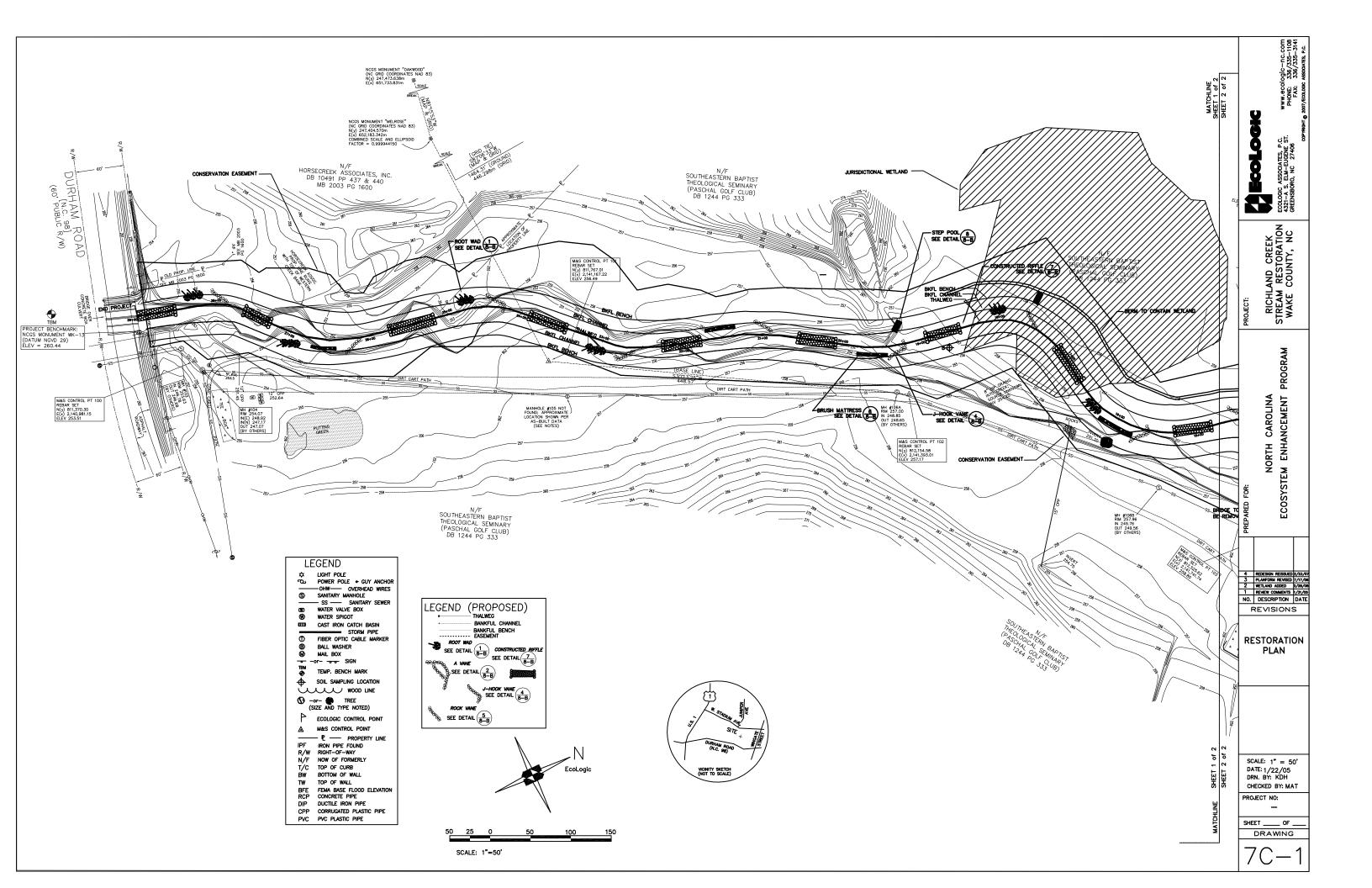
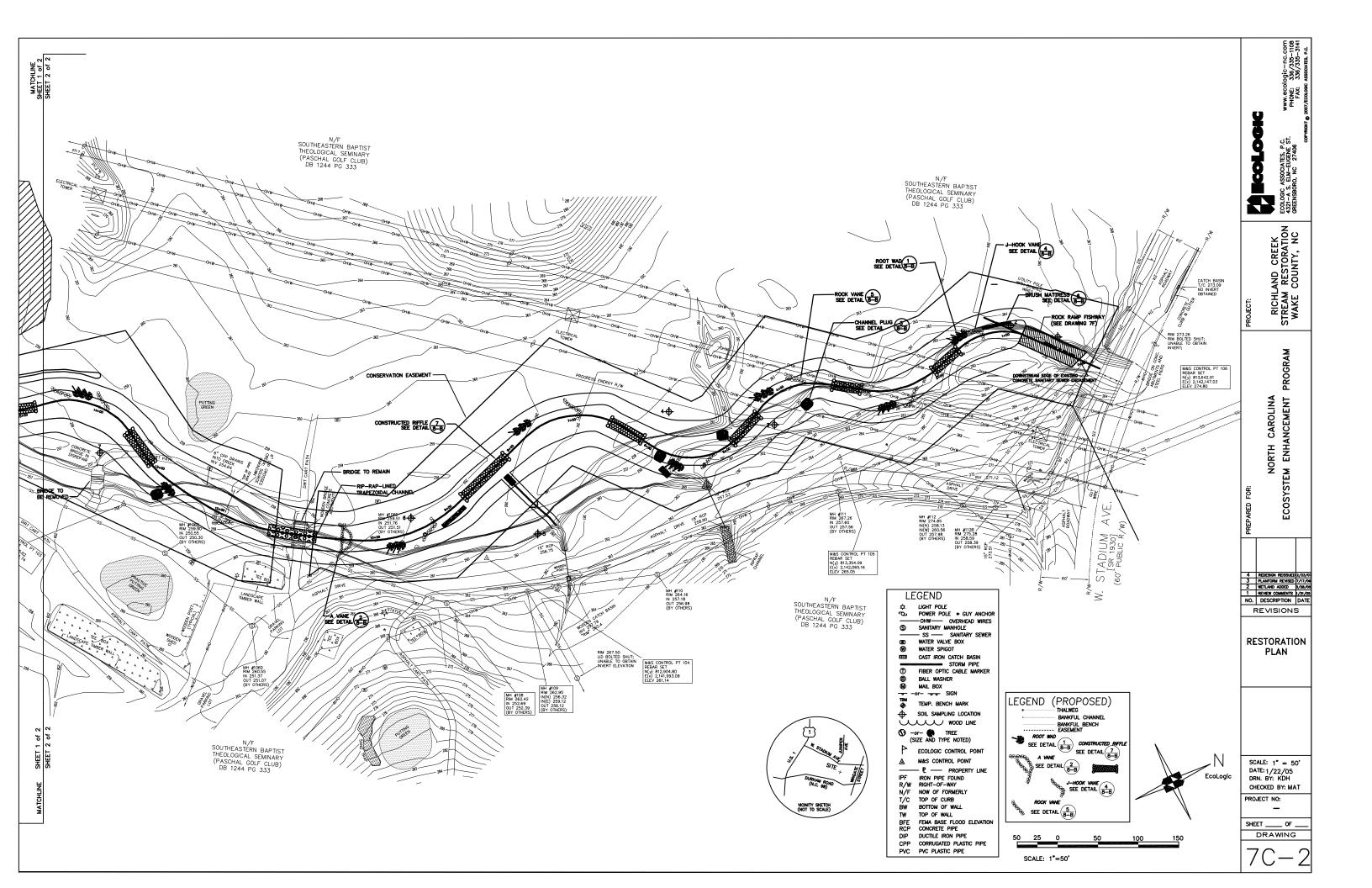


Figure 7b (from KCI Associates)





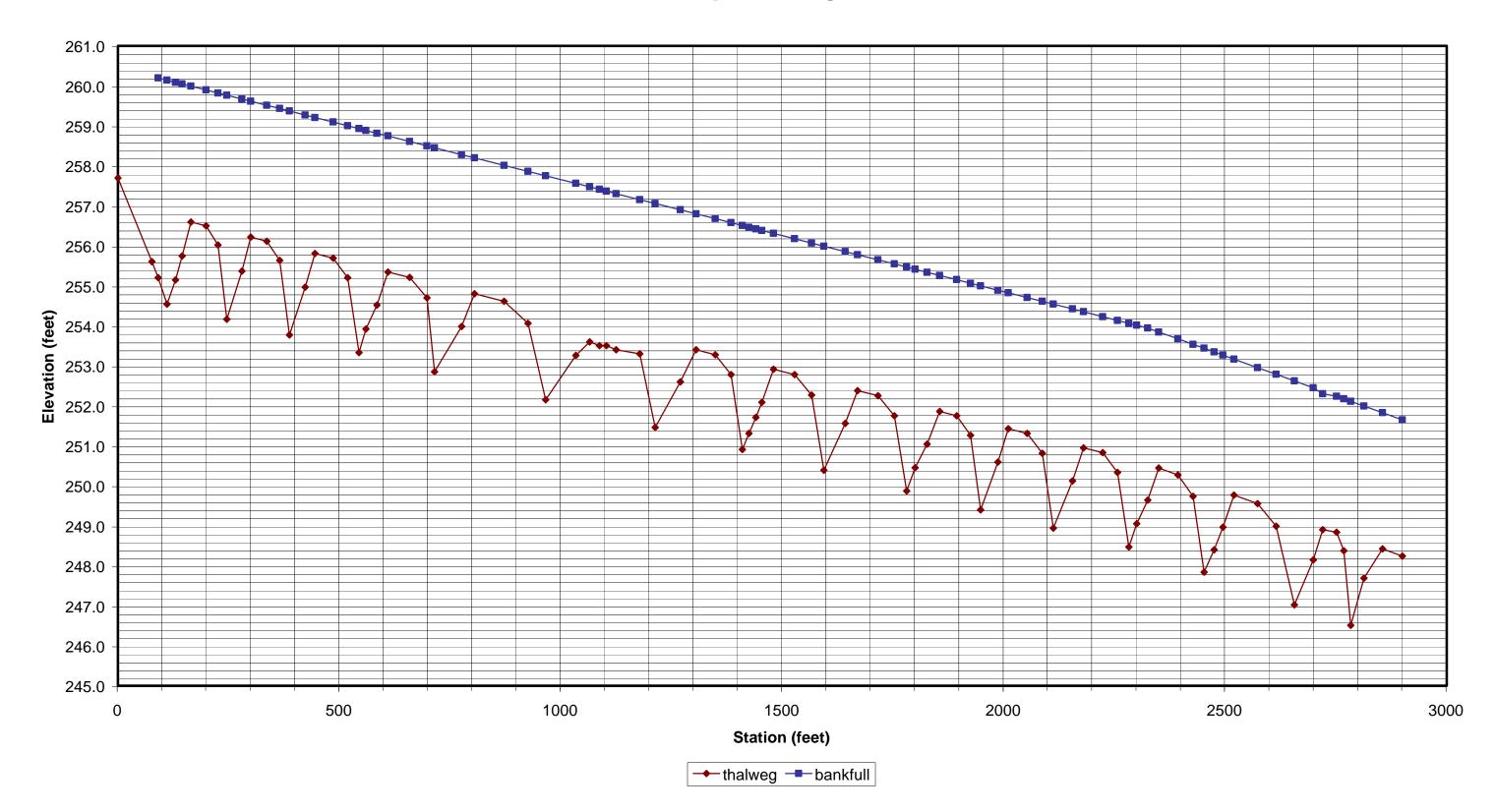
# Table 7dProposed Longitudinal Profile

| Richland Creek  |              |                        | ws slope =     | 0.0028         | d rif =              | 3.4 | ft |
|-----------------|--------------|------------------------|----------------|----------------|----------------------|-----|----|
| Stream Restorat | ion          | Last 600'              | ws slope =     | 0.0040         | d run =              | 3.8 | ft |
| Wake County, NO | C            |                        | ramp slope =   | 0.028          | d pool =             | 5.6 | ft |
| NC Ecosystem E  |              |                        |                |                | d glide =            | 4.3 | ft |
|                 |              | <u> </u>               |                |                | d bkf =              | 2.6 | ft |
|                 | Station      | Feature                | BKF EL         | TW Elev        | Structure            |     |    |
|                 | 0            | Fish Ramp              | NA             | 257.7          | Fish Ramp            |     |    |
|                 | 77           | Fish Ramp              | NA             | 255.6          | Fish Ramp            |     |    |
|                 | 91           | Transition             | 260.2          | 255.2          |                      |     |    |
|                 | 111          | Pool                   | 260.1          | 254.5          |                      |     |    |
|                 | 130          |                        | 260.1          | 255.1          | J-Hook Vane          |     |    |
|                 | 145          | Glide                  | 260.0          | 255.7          | Root Wads            |     |    |
|                 | 165          | RiffleTop              | 260.0          | 256.6          | Const. Riffle        |     |    |
|                 | 199          | RiffleBot              | 259.9          | 256.5          | Const. Riffle        |     |    |
|                 | 226          | Run                    | 259.8          | 256.0          | Rock Vane            |     |    |
|                 | 246          | Pool                   | 259.8          | 254.2          |                      |     |    |
|                 | 280          | Glide                  | 259.7          | 255.4          | Root Wads            |     |    |
|                 | 300          | RiffleTop              | 259.6          | 256.2          | Const. Riffle        |     |    |
|                 | 336          | RiffleBot              | 259.5          | 256.1          | Const. Riffle        |     |    |
|                 | 365          | Run                    | 259.4          | 255.6          | Rock Vane            |     |    |
|                 | 387          | Pool                   | 259.4          | 253.8          |                      |     |    |
|                 | 423          | Glide                  | 259.3          | 255.0          | Root Wads            |     |    |
|                 | 445          | RiffleTop              | 259.2          | 255.8          | Const. Riffle        |     |    |
|                 | 486          | RiffleBot              | 259.1          | 255.7          | Const. Riffle        |     |    |
|                 | 519          | Run                    | 259.0          | 255.2          | Rock Vane            |     |    |
|                 | 544          | Pool                   | 258.9          | 253.3          |                      |     |    |
|                 | 560          |                        | 258.9          | 253.9          | Root Wads            |     |    |
|                 | 585          | Glide                  | 258.8          | 254.5          |                      |     |    |
|                 | 610          | RiffleTop              | 258.7          | 255.3          | Const. Riffle        |     |    |
|                 | 659          | RiffleBot              | 258.6          | 255.2          | Const. Riffle        |     |    |
|                 | 698          | Run                    | 258.5          | 254.7          | J-Hook Vane          |     |    |
|                 | 715          | Pool                   | 258.5          | 252.9          |                      |     |    |
|                 | 776          | Glide                  | 258.3          | 254.0          | Root Wads            |     |    |
|                 | 805          | RiffleTop              | 258.2          | 254.8          | Const. Riffle        |     |    |
|                 | 872          | RiffleBot              | 258.0          | 254.6          | Const. Riffle        |     |    |
|                 | 926          | Run                    | 257.9          | 254.1          | J-Hook Vane          |     |    |
|                 | 966          | Pool                   | 257.8          | 252.2          | A \/c===             |     |    |
|                 | 1034         | Glide<br>Bridge B      | 257.6          | 253.3          | A Vane               |     |    |
|                 | 1065         | Bridge B               | 257.5          | 253.6          | Rip-Rap              |     |    |
|                 | 1087         | Bridge A               | 257.4          | 253.5          | Rip-Rap<br>Bip Bop   |     |    |
|                 | 1103         | Bridge A               | 257.4          | 253.5          | Rip-Rap<br>Bin Ban   |     |    |
|                 | 1125         | Bridge B               | 257.3          | 253.4<br>253.3 | Rip-Rap<br>Rock Vane |     |    |
|                 | 1178         | Run                    | 257.2          |                | NUCK VALLE           |     |    |
|                 | 1213<br>1270 | Pool<br>Glide          | 257.1          | 251.5<br>252.6 | Root Wads            |     |    |
|                 |              |                        | 256.9<br>256.8 | 252.6          | Const. Riffle        |     |    |
|                 | 1305         | RiffleTop<br>BiffleBot | 256.8          |                |                      |     |    |
|                 | 1349         | RiffleBot              | 256.7<br>256.6 | 253.3          | Const. Riffle        |     |    |
|                 | 1384<br>1410 | Run<br>Pool            | 256.6<br>256.5 | 252.8<br>250.9 | Rock Vane            |     |    |

# Table 7dProposed Longitudinal Profile

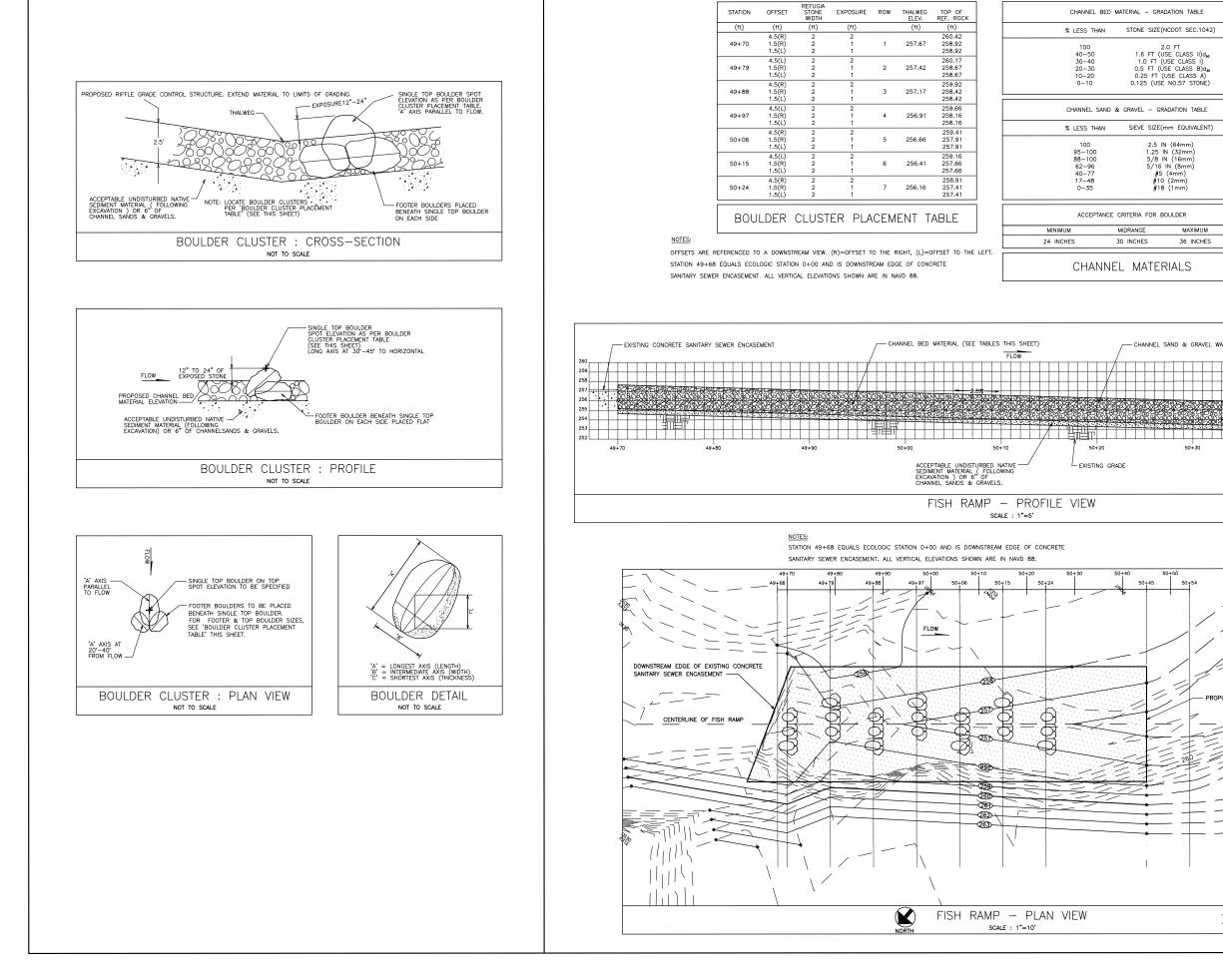
| 4.405 | 1 1       |       | 0.5.4.0 |               |
|-------|-----------|-------|---------|---------------|
| 1425  |           | 256.5 | 251.3   | Root Wads     |
| 1440  |           | 256.4 | 251.7   | Rock Vane     |
| 1454  | Glide     | 256.4 | 252.1   | _             |
| 1480  | RiffleTop | 256.3 | 252.9   | Const. Riffle |
| 1528  | RiffleBot | 256.2 | 252.8   | Const. Riffle |
| 1566  | Run       | 256.1 | 252.3   | J-Hook Vane   |
| 1594  | Pool      | 256.0 | 250.4   |               |
| 1642  | Glide     | 255.9 | 251.6   | Root Wads     |
| 1670  | RiffleTop | 255.8 | 252.4   | Const. Riffle |
| 1716  | RiffleBot | 255.7 | 252.3   | Const. Riffle |
| 1753  | Run       | 255.5 | 251.7   | Rock Vane     |
| 1781  | Pool      | 255.5 | 249.9   |               |
| 1800  |           | 255.4 | 250.5   | Root Wads     |
| 1827  | Glide     | 255.3 | 251.0   |               |
| 1855  | RiffleTop | 255.3 | 251.9   | Const. Riffle |
| 1894  | RiffleBot | 255.2 | 251.8   | Const. Riffle |
| 1925  | Run       | 255.1 | 251.3   | J-Hook Vane   |
| 1948  | Pool      | 255.0 | 249.4   |               |
| 1987  | Glide     | 254.9 | 250.6   |               |
| 2010  | RiffleTop | 254.8 | 251.4   | Const. Riffle |
| 2053  | RiffleBot | 254.7 | 251.3   | Const. Riffle |
| 2087  | Run       | 254.6 | 250.8   | Rock Vane     |
| 2112  | Pool      | 254.5 | 248.9   |               |
| 2155  | Glide     | 254.4 | 250.1   |               |
| 2180  | RiffleTop | 254.4 | 251.0   | Const. Riffle |
| 2223  | RiffleBot | 254.2 | 250.8   | Const. Riffle |
| 2257  | Run       | 254.1 | 250.3   | Rock Vane     |
| 2282  | Pool      | 254.1 | 248.5   |               |
| 2300  |           | 254.0 | 249.1   | Root Wads     |
| 2325  | Glide     | 253.9 | 249.6   |               |
| 2350  | RiffleTop | 253.8 | 250.4   | Const. Riffle |
| 2393  | RiffleBot | 253.7 | 250.3   | Const. Riffle |
| 2427  | Run       | 253.5 | 249.7   | J-Hook Vane   |
| 2452  | Pool      | 253.4 | 247.8   |               |
| 2475  |           | 253.3 | 248.4   | Root Wads     |
| 2495  | Glide     | 253.3 | 249.0   |               |
| 2520  | RiffleTop | 253.2 | 249.8   | Const. Riffle |
| 2573  | RiffleBot | 253.0 | 249.6   | Const. Riffle |
| 2615  | Run       | 252.8 | 249.0   | Rock Vane     |
| 2656  | Pool      | 252.6 | 247.0   |               |
| 2699  | Glide     | 252.4 | 248.1   | Root Wads     |
| 2730  | RiffleTop | 252.3 | 248.9   | Const. Riffle |
| 2761  | RiffleBot | 252.2 | 248.8   | Const. Riffle |
| 2786  | Run       | 252.1 | 248.3   | Rock Vane     |
| 2805  | Pool      | 252.0 | 246.4   |               |
| 2836  | Glide     | 251.9 | 247.6   | Root Wads     |
| 2855  | RiffleTop | 251.8 | 248.4   | Const. Riffle |
| 2900  | RiffleBot | 251.6 | 248.2   | Const. Riffle |

# **Richland Creek Proposed Longitudinal Profile**

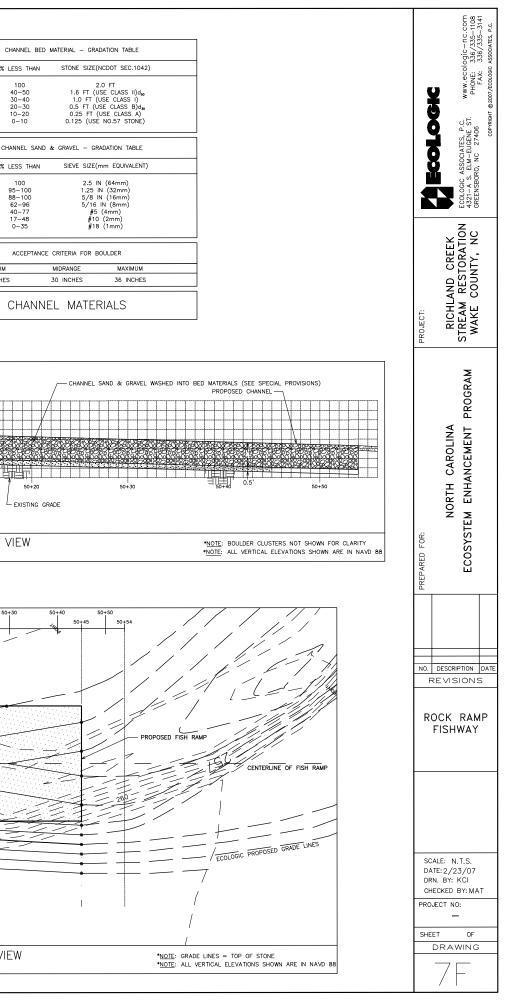


|           |   | ENTRAINMENT CA  |                             | N FORM   |  |   |  |  |  |  |
|-----------|---|---|-----------------------------|--|--|---|--|--|--|--|
| Stream:   | Rich  | land Creek, Existing                                    | Reach:                      | Pa   | schal Golf Cou                                   | rse   |  |  |  |  |
| Team:     |   | Ken, Kyle, Moni Date: 5/10/2004                         |                             |  |  |   |  |  |  |  |
|           |   | Informatio  | n Input Area                |  |  |   |  |  |  |  |
| 12        | D <sub>50</sub>   | Riffle bed material D50 (mr                             | n)                          |  |  |   |  |  |  |  |
| 2.5       | D <sup>^</sup> <sub>50</sub>  | Bar sample D50 (mm)                                     |                             | -  |  |   |  |  |  |  |
| 58.0      | Di  | Largest particle from bar sa                            | ample (mm)                  | 0.19   | (feet)   | 304.8 mm/foot                                     |  |  |  |  |
| 0.003     | S <sub>e</sub>  | Existing bankfull water surfa                           | ace slope (ft/ft)           |  |  |   |  |  |  |  |
| 2.1       | d <sub>e</sub>  | Existing bankfull mean dept                             | h (ft)                      |  |  |   |  |  |  |  |
| 2         | R   | Hydraulic Radius of Riffle C                            | ross Section (ft            | )  |  |   |  |  |  |  |
| 1.65      | g₅  | Submerged specific weight                               | of sediment                 |  |  |   |  |  |  |  |
|           |   | Calculation of Critical Di                              | mensionless S               | hear Stress                                    |  |   |  |  |  |  |
| 4.80      | D <sub>50</sub> /D <sup>^</sup> <sub>50</sub>   | If value is between 3-7                                 |                             |  | <sub>ci</sub> = 0.0834(D <sub>50</sub> /         |   |  |  |  |  |
| 4.83      | D <sub>i</sub> /D <sub>50</sub>   | If value is between 1.3-3.0                             | Equation 2 w                | ill be used: t <sup>*</sup>                    | <sub>ci</sub> = 0.0384(D <sub>i</sub> /D         | 0 <sub>50</sub> ) <sup>-0.887</sup>               |  |  |  |  |
| 0.0212    | t <sup>*</sup> <sub>ci</sub>  | Critical Dimensionless Shea                             | r Stress                    | E  | quation used:                                    | 1   |  |  |  |  |
| Calcul    | ation of Bank   | full Mean Depth Required for                            | or Entrainment              | t of Largest Pa                                | article in Bar S                                 | ample   |  |  |  |  |
| 2.38      | d <sub>r</sub>  | Required bankfull mear                                  | n depth (ft)                |  | $d_{r} = \frac{t_{ci}^{*} g_{s} D_{i}}{S_{e}}$   |   |  |  |  |  |
| 0.88      | d <sub>e</sub> /d <sub>r</sub>  | <u>Existing mean bankf</u><br>Required mean bankf       |                             | Stable<br>(d <sub>e</sub> /d <sub>r</sub> = 1) | Aggrading<br>(d <sub>e</sub> /d <sub>r</sub> <1) | Degrading<br>(d <sub>e</sub> /d <sub>r</sub> >1)  |  |  |  |  |
| aggrading | Vertical Sta  | ability of Stream                                       |                             |  |  |   |  |  |  |  |
| Calculat  | ion of BKF Wa   | ater Surface Slope Required                             | d for Entrainme             | ent of Largest                                 | Particle in Ba                                   | r Sample  |  |  |  |  |
| 0.0032    | Sr  | Required bankfull water su                              |                             |  | $S_r = \frac{t_{ci}^* g_s D_i}{d_e}$             |   |  |  |  |  |
| 0.88      | S <sub>e</sub> /S <sub>r</sub>  | <u>Existing water surface</u><br>Required water surface |                             | Stable $(S_e/S_r = 1)$                         | Aggrading $(S_e/S_r < 1)$                        | Degrading<br>(S <sub>e</sub> /S <sub>r</sub> > 1) |  |  |  |  |
| aggrading | Vertical Sta  | ability of Stream                                       |                             |  |  |   |  |  |  |  |
|           |   | Sediment Tran   | sport Validatio             | n n  |  |   |  |  |  |  |
| 0.35      | Bankfull Shea   |   | •                           |  | v of water = 62                                  | 4 lbs/ft <sup>3</sup>                             |  |  |  |  |
| 20-80     | Bankfull Shear Stress $t_c = gRS$ (lb/ft2) $g = Density of water = 62.4 lbs/ft^3$ Moveable particle size (mm) at bankfull shear stress (predicted by the Shields Diagram: Blue field<br>book:p238, Red field book:p190) |   |                             |  |  |   |  |  |  |  |
| .3090     |   | ar stress required to initate m<br>ed field book:p190)  | ovement of D <sub>i</sub> ( | (mm) (see Shie                                 | elds Diagram: B                                  | lue field   |  |  |  |  |

|          |  | ENTRAINMENT CA   | ALCULATIO                    | N FORM   |   |   |  |  |  |
|----------|--|--|------------------------------|--|---|---|--|--|--|
| Stream:  | Richla   | and Creek, Proposed                                    | Reach:                       | Pa   | aschal Golf Cou                                       | rse   |  |  |  |
| Team:    | Ken, Kyle Date: 9/29/2004  |  |                              |  |   |   |  |  |  |
|          |  | Informatio   | n Input Area                 |  |   |   |  |  |  |
| 12       | D <sub>50</sub>  | Riffle bed material D50 (m                             | m)                           |  |   |   |  |  |  |
| 2.5      | D <sup>^</sup> <sub>50</sub>   | Bar sample D50 (mm)                                    |                              |  |   |   |  |  |  |
| 58.0     | Di   | Largest particle from bar sa                           | ample (mm)                   | 0.19   | (feet)  | 304.8 mm/foot                                     |  |  |  |
| 0.003    | S <sub>e</sub>   | Proposed bankfull water su                             | irface slope (ft/f           | t)   |   |   |  |  |  |
| 2.5      | d <sub>e</sub>   | Proposed bankfull mean de                              | epth (ft)                    |  |   |   |  |  |  |
| 2.3      | R  | Hydraulic Radius of Riffle C                           | Cross Section (ft            | )  |   |   |  |  |  |
| 1.65     | g₅   | Submerged specific weight                              | of sediment                  |  |   |   |  |  |  |
|          |  | Calculation of Critical Di                             | mensionless S                | Shear Stress                                   |   |   |  |  |  |
| 4.80     | D <sub>50</sub> /D <sup>^</sup> <sub>50</sub>  | If value is between 3-7                                | Equation 1 w                 | ill be used: t                                 | <sup>*</sup> <sub>ci</sub> = 0.0834(D <sub>50</sub> / | /D <sup>^</sup> <sub>50</sub> ) <sup>-0.872</sup> |  |  |  |
| 4.83     | D <sub>i</sub> /D <sub>50</sub>  | If value is between 1.3-3.0                            | Equation 2 w                 | ill be used: t                                 | * <sub>ci</sub> = 0.0384(D <sub>i</sub> /D            | 0 <sub>50</sub> ) <sup>-0.887</sup>               |  |  |  |
| 0.0212   | t <sup>*</sup> <sub>ci</sub>   | Critical Dimensionless Shea                            | r Stress                     | E  | quation used:   | 1   |  |  |  |
| Calcu    | lation of Bank   | full Mean Depth Required f                             | or Entrainmen                | t of Largest P                                 | article in Bar S                                      | ample   |  |  |  |
| 2.38     | d <sub>r</sub>   | Required bankfull mean                                 | n depth (ft)                 |  | $d_r = \frac{t_{ci}^* g_s D_i}{S_e}$                  |   |  |  |  |
| 1.05     | d <sub>e</sub> /d <sub>r</sub>   | _Existing mean banki<br>Required mean banki            |                              | Stable $(d_e/d_r = 1)$                         | Aggrading<br>(d <sub>e</sub> /d <sub>r</sub> <1)      | Degrading<br>(d <sub>e</sub> /d <sub>r</sub> >1)  |  |  |  |
| stable   | Vertical Sta   | ability of Stream                                      | •                            |  |   |   |  |  |  |
| Calculat | ion of BKF Wa  | ter Surface Slope Require                              | d for Entrainm               | ent of Largest                                 | Particle in Ba  | r Sample  |  |  |  |
| 0.0027   | S <sub>r</sub>   | Required bankfull water su                             |                              |  | $S_{r} = \frac{t_{ci}^{*} g_{s} D_{i}}{d_{e}}$        |   |  |  |  |
| 1.05     | S <sub>e</sub> /S <sub>r</sub>   | <u>Existing water surfa</u><br>Required water surfa    |                              | Stable<br>(S <sub>e</sub> /S <sub>r</sub> = 1) | Aggrading $(S_e/S_r < 1)$                             | Degrading<br>(S <sub>e</sub> /S <sub>r</sub> > 1) |  |  |  |
| stable   | Vertical Sta   | ability of Stream                                      |                              |  |   |   |  |  |  |
|          |  | Sediment Tran  | sport Validatio              | on   |   |   |  |  |  |
| 0.40     | Bankfull Shea  |  | -                            |  | y of water = 62.                                      | 4 lbs/ft <sup>3</sup>                             |  |  |  |
| 20-90    | Moveable particle size (mm) at bankfull shear stress (predicted by the Shields Diagram: Blue field book:p238, Red field book:p190) |  |                              |  |   |   |  |  |  |
| .39      |  | ar stress required to initate m<br>ed field book:p190) | novement of D <sub>i</sub> ( | (mm) (see Shie                                 | elds Diagram: B                                       | lue field   |  |  |  |



STATION OFFSET



### Table 7f-1

### Richland Creek Wake Forest, NC

### Rock Ramp Fishway Cross-Sections

| Station | 49+70     | Station | 50+00     | Station | 50+30     | Station | 50+45     |
|---------|-----------|---------|-----------|---------|-----------|---------|-----------|
|         |           |         |           |         |           |         |           |
| Off Set | Elevation |
| (ft)    | (ft)      | (ft)    | (ft)      | (ft)    | (ft)      | (ft)    | (ft)      |
|         |           |         |           |         |           |         |           |
| -12     | 258.00    | -12     | 258.83    | -12     | 258.00    | -12     | 257.58    |
| -8      | 257.89    | -7      | 258.00    | -6      | 257.00    | -8.5    | 257.00    |
| -4      | 257.78    | -1      | 257.00    |         |           | -2.5    | 256.00    |
| 0       | 257.67    | 0       | 256.83    | 0       | 256.00    | 0       | 255.58    |
| 4       | 257.78    | 1       | 257.00    |         |           | 2.5     | 256.00    |
| 8       | 257.89    | 7       | 258.00    | 6       | 257.00    | 8.5     | 257.00    |
| 12      | 258.00    | 12      | 258.83    | 12      | 258.00    | 12      | 257.58    |

### Table 7f-2

### Richland Creek Wake Forest, NC

### Refugia Boulders - Boulder Garden Pattern

| Station | Offset | Refugia Ste    | one Size |     | Thalweg   | Top of   |
|---------|--------|----------------|----------|-----|-----------|----------|
|         |        | Width Exposure |          | Row | Elevation | Ref Rock |
| (ft)    | (ft)   | (ft)           | (ft)     |     | (ft)      | (ft)     |
| 4970    | 4.5    | 2              | 2        |     |           | 260.42   |
| 4970    | 1.5    | 2              | 1        | 1   | 257.67    | 258.92   |
| 4970    | -1.5   | 2              | 1        |     |           | 258.92   |
| 4979    | -4.5   | 2              | 2        |     |           | 260.17   |
| 4979    | -1.5   | 2              | 1        | 2   | 257.42    | 258.67   |
| 4979    | 1.5    | 2              | 1        |     |           | 258.67   |
| 4988    | 4.5    | 2              | 2        |     |           | 259.92   |
| 4988    | 1.5    | 2              | 1        | 3   | 257.17    | 258.42   |
| 4988    | -1.5   | 2              | 1        |     |           | 258.42   |
| 4997    | -4.5   | 2              | 2        |     |           | 259.66   |
| 4997    | -1.5   | 2              | 1        | 4   | 256.91    | 258.16   |
| 4997    | 1.5    | 2              | 1        |     |           | 258.16   |
| 5006    | 4.5    | 2              | 2        |     |           | 259.41   |
| 5006    | 1.5    | 2              | 1        | 5   | 256.66    | 257.91   |
| 5006    | -1.5   | 2              | 1        |     |           | 257.91   |
| 5015    | -4.5   | 2              | 2        |     |           | 259.16   |
| 5015    | -1.5   | 2              | 1        | 6   | 256.41    | 257.66   |
| 5015    | 1.5    | 2              | 1        |     |           | 257.66   |
| 5024    | 4.5    | 2              | 2        |     |           | 258.91   |
| 5024    | 1.5    | 2              | 1        | 7   | 256.16    | 257.41   |
| 5024    | -1.5   | 2              | 1        |     |           | 257.41   |

### Table 7f-3

### Richland Creek Wake Forest, NC

### **Rock Ramp Hydraulics**

|          |            |          |          |          |       | R    | lock Ram | Hydraulics    |          | Boulder Ga | rden Patter | n        |             |      |            |           |        |          |           |          |            |          |             |
|----------|------------|----------|----------|----------|-------|------|----------|---------------|----------|------------|-------------|----------|-------------|------|------------|-----------|--------|----------|-----------|----------|------------|----------|-------------|
|          |            |          |          |          |       |      |          | 5 Tryuraulics |          | Douider Oa |             |          |             |      |            |           |        |          |           |          |            |          |             |
|          | side slope | 6        |          |          | 0.028 | 1.2  | 1.7      | class 2 ripra | a        |            |             |          |             | 0.   | 1          |           | 0.71   |          |           |          |            |          |             |
|          |            |          |          |          | 0.020 |      |          | Mussetter     |          |            | max         |          | Englsh Unit |      |            | max       |        |          | Andrews 9 | 5        |            |          |             |
| d        | q          | А        | Wp       | Rh       | So    | D50  | D84      | n             | V        | Q          | shear       | V        | Q           | d    | CrestElev. | shear     | D05    | tau*c50  | tau*c5    | tau5     | tau5/shear | tau50    | tau50/shear |
| (m)      | m/s2       | (m2)     | (m)      | (m)      | (m/m) | (m)  | (m)      |               | (m/s)    | (m3/s)     | (N/m2)      | (fps)    | (ft3/s)     | (ft) | ft         | (lbs/ft2) | (m)    |          |           |          |            |          |             |
|          |            | · · · ·  |          |          | × /   |      |          |               |          | . ,        | ,           | 0        | 0           | 0    | 258.7      | 0         |        |          |           |          |            |          |             |
| 0.030488 | 9.81       | 0.005577 | 0.3709   | 0.015036 | 0.028 | 0.96 | 1.36     | 0.303386      | 0.033695 | 0.000188   | 0.008374    | 0.110519 | 0.006631    | 0.1  | 258.8      | 0.17472   | 0.568  | 0.0375   | 0.059263  | 0.544855 | 65.06      | 0.582714 | 69.58       |
| 0.060976 | 9.81       | 0.022308 | 0.7418   | 0.030073 | 0.028 | 0.96 | 1.36     | 0.247573      | 0.065515 | 0.001462   | 0.016749    | 0.21489  | 0.051573    | 0.2  | 258.9      | 0.34944   |        |          |           |          | 32.53      |          | 34.79       |
| 0.091463 | 9.81       | 0.050193 | 1.1127   | 0.045109 | 0.028 | 0.96 | 1.36     | 0.219814      | 0.096664 | 0.004852   | 0.025123    | 0.317059 | 0.171212    | 0.3  | 259        | 0.52416   |        |          |           |          | 21.69      |          | 23.19       |
| 0.121951 | 9.81       | 0.089233 | 1.483601 | 0.060146 | 0.028 | 0.96 | 1.36     | 0.202028      | 0.127385 | 0.011367   | 0.033498    | 0.417824 | 0.401111    | 0.4  | 259.1      | 0.69888   |        |          |           |          | 16.27      |          | 17.40       |
| 0.152439 | 9.81       | 0.139426 | 1.854501 | 0.075182 | 0.028 | 0.96 | 1.36     | 0.189229      | 0.157792 | 0.022      | 0.041872    | 0.517559 | 0.776337    | 0.5  | 259.2      | 0.8736    |        |          |           |          | 13.01      |          | 13.92       |
| 0.182927 | 9.81       | 0.200773 | 2.225401 | 0.090219 | 0.028 | 0.96 | 1.36     | 0.179375      | 0.187951 | 0.037736   | 0.050246    | 0.616479 | 1.331592    | 0.6  | 259.3      | 1.04832   |        |          |           |          | 10.84      |          | 11.60       |
| 0.213415 | 9.81       | 0.273275 | 2.596301 | 0.105255 | 0.028 | 0.96 | 1.36     | 0.171446      | 0.217905 | 0.059548   | 0.058621    | 0.714727 | 2.101294    | 0.7  | 259.4      | 1.22304   |        |          |           |          | 9.29       |          | 9.94        |
| 0.243902 | 9.81       | 0.35693  | 2.967201 | 0.120292 | 0.028 | 0.96 | 1.36     | 0.164861      | 0.247684 | 0.088406   | 0.066995    | 0.812404 | 3.119625    | 0.8  | 259.5      | 1.39776   |        |          |           |          | 8.13       |          | 8.70        |
| 0.27439  | 9.81       | 0.45174  | 3.338101 | 0.135328 | 0.028 | 0.96 | 1.36     | 0.159263      | 0.277312 | 0.125273   | 0.07537     | 0.909583 | 4.420568    | 0.9  | 259.6      | 1.57248   |        |          |           |          | 7.23       |          | 7.73        |
| 0.304878 | 9.81       | 0.557704 | 3.709002 | 0.150365 | 0.028 | 0.96 | 1.36     | 0.154417      | 0.306806 | 0.171107   | 0.083744    | 1.006323 | 6.037932    | 1    | 259.7      | 1.7472    |        |          |           |          | 6.51       |          | 6.96        |
| 0.335366 | 9.81       | 0.674822 | 4.079902 | 0.165401 | 0.028 | 0.96 | 1.36     | 0.15016       | 0.33618  | 0.226861   | 0.092118    | 1.10267  | 8.005373    | 1.1  | 259.8      | 1.92192   | *** DE | SIGN DEP | PTH ***   |          | 5.91       |          | 6.33        |
| 0.365854 | 9.81       | 0.803093 | 4.450802 | 0.180438 | 0.028 | 0.96 | 1.36     | 0.146376      | 0.365445 | 0.293487   | 0.100493    | 1.19866  | 10.35641    | 1.2  | 259.9      | 2.09664   |        |          |           |          | 5.42       |          | 5.80        |
| 0.396341 | 9.81       | 0.942519 | 4.821702 | 0.195474 | 0.028 | 0.96 | 1.36     | 0.14298       | 0.394611 | 0.371929   | 0.108867    | 1.294325 | 13.12444    | 1.3  | 260        | 2.27136   |        |          |           |          | 5.00       |          | 5.35        |
| 0.426829 | 9.81       | 1.093099 | 5.192602 | 0.210511 | 0.028 | 0.96 | 1.36     | 0.139906      | 0.423686 | 0.463131   | 0.117241    | 1.389691 | 16.34274    | 1.4  | 260.1      | 2.44608   |        |          |           |          | 4.65       |          | 4.97        |
| 0.457317 | 9.81       | 1.254833 | 5.563502 | 0.225547 | 0.028 | 0.96 | 1.36     | 0.137103      | 0.452677 | 0.568034   | 0.125616    | 1.484779 | 20.04449    | 1.5  | 260.2      | 2.6208    |        |          |           |          | 4.34       |          | 4.64        |
| 0.487805 | 9.81       | 1.427722 | 5.934402 | 0.240584 | 0.028 | 0.96 | 1.36     | 0.134532      | 0.481588 | 0.687574   | 0.13399     | 1.57961  | 24.26278    | 1.6  | 260.3      | 2.79552   |        |          |           |          | 4.07       |          | 4.35        |
| 0.518293 | 9.81       |          | 6.305303 |          | 0.028 | 0.96 | 1.36     | 0.132161      | 0.510427 | 0.822687   | 0.142365    | -        | 29.03058    | 1.7  | 260.4      | 2.97024   |        |          |           |          | 3.83       |          | 4.09        |
| 0.54878  | 9.81       | 1.80696  | 6.676203 | 0.270657 | 0.028 | 0.96 | 1.36     | 0.129964      | 0.539196 | 0.974306   | 0.150739    | 1.768563 | 34.38081    | 1.8  | 260.5      | 3.14496   |        |          |           |          | 3.61       |          | 3.87        |
| 0.579268 | 9.81       | 2.013311 | 7.047103 | 0.285693 | 0.028 | 0.96 | 1.36     | 0.127919      | 0.5679   | 1.14336    | 0.159113    | 1.862713 | 40.3463     | 1.9  | 260.6      | 3.31968   |        |          |           |          | 3.42       |          | 3.66        |
| 0.609756 | 9.81       | 2.230815 | 7.418003 | 0.30073  | 0.028 | 0.96 | 1.36     | 0.126009      | 0.596543 | 1.330777   | 0.167488    | 1.956661 | 46.95981    | 2    | 260.7      | 3.4944    |        |          |           |          | 3.25       |          | 3.48        |
| 0.640244 | 9.81       | 2.459474 | 7.788903 | 0.315766 | 0.028 | 0.96 | 1.36     | 0.124219      | 0.625128 | 1.537485   | 0.175862    | 2.050419 | 54.254      | 2.1  | 260.8      | 3.66912   |        |          |           |          | 3.10       |          | 3.31        |
| 0.670732 | 9.81       | 2.699286 | 8.159803 | 0.330803 | 0.028 | 0.96 | 1.36     | 0.122536      | 0.653657 | 1.764407   | 0.184237    | 2.143995 | 62.26151    | 2.2  | 260.9      | 3.84384   |        |          |           |          | 2.96       |          | 3.16        |
| 0.70122  | 9.81       | 2.950253 | 8.530704 | 0.345839 | 0.028 | 0.96 | 1.36     | 0.120948      | 0.682133 | 2.012466   | 0.192611    | 2.237397 | 71.01489    | 2.3  | 261        | 4.01856   |        |          |           |          | 2.83       |          | 3.03        |
| 0.731707 | 9.81       |          |          | 0.360876 | 0.028 | 0.96 | 1.36     | 0.119448      | 0.710559 | 2.282582   |             | 2.330635 | 80.54663    | 2.4  | 261.1      | 4.19328   |        |          |           |          | 2.71       |          | 2.90        |
| 0.762195 | 9.81       | 3.485648 | 9.272504 | 0.375912 | 0.028 | 0.96 | 1.36     | 0.118026      | 0.738937 | 2.575676   | 0.20936     | 2.423715 | 90.88916    | 2.5  | 261.2      | 4.368     |        |          |           |          | 2.60       |          | 2.78        |
| 0        | 9.81       | 0        | 0        | #DIV/0!  | 0.028 | 0.96 |          |               |          |            |             |          |             |      |            |           |        |          |           |          |            |          |             |
| 0        | 9.81       | 0        | 0        | #DIV/0!  | 0.028 | 0.96 |          |               |          |            |             |          |             |      |            |           |        |          |           |          |            |          |             |
| 0        | 9.81       | 0        | 0        | #DIV/0!  | 0.028 | 0.96 |          |               |          |            |             |          |             |      |            |           |        |          |           |          |            |          |             |

### <u>References</u>

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### 8. Typicals (Drawings 8-A and 8-B)

- a. Cross-sections See Drawing 8-A
- **b. Structures** See Drawing 8-B

### 9. Stream Riparian Planting Plan

### a. Electrical transmission corridor restrictions:

Progress Energy requirements for planting beneath the three-phase, high voltage power lines are that plants not exceed 12 feet in height (personal communication: Mark Smith, Progress Energy Forester). At the time of correspondence, Mr. Smith stated no other requirements, but noted he would advise if he found any. As of this writing, no additional requirements have been provided.

A low-growing plant species list will be specified for use under the power lines. This includes species with height at maturity under the height limit and aggressive enough to compete with invasive vegetation to establish bank protection and riparian corridor wildlife habitat.

### b. Neuse River buffer requirements:

The restoration reach is in the upper watershed of the Neuse River basin. As a result the restoration project is subject to buffer requirements that apply to streams in this basin. The regulations stipulate that the buffer shall have two zones: (1) an undisturbed forest zone beginning at the centerline of intermittent and perennial streams and extending

landward a distance of 30 feet on all sides of the waterbody, and (2) a vegetated zone beginning at the outer edge of Zone1 and extending an additional 20 feet. The combined width of Zones 1 and 2 shall be 50 feet.

### c. Planting plan outline

The following sections outline the planting plan specifications:

### 1. Site Preparation

The planting plan includes the preservation of suitable existing vegetation, the reuse (transplanting) of suitable woody and herbaceous plants that must be disturbed, and the addition of new, native plant material. Site preparation will consist of preparing the planting areas, including the removal of undesirable vegetation, such as weedy, invasive or otherwise pest plants, and other plants that must be cleared to construct the restoration.

A serious effort shall be made to retain and protect existing native vegetation that is well rooted, healthy and appropriately sited alongside the impacted channel. In those areas, plants suitable for reuse shall be flagged by a representative of the Planting Plan Designer who is familiar with native riparian flora, then carefully extracted and stored by the Contractor for subsequent transplanting. Transplanting during channel shaping is preferred to limit the time the transplant is in transition.

Those areas of the site that become or have previously been compacted by construction equipment, trucks, etc. shall be ripped with a subsoiler, raked, and left in a rough, loose condition. Subsoil ripping should also occur on exposed banks and other denuded areas where trees are to be planted. The surface should be left rough for tree planting, with the orientation of any furrows being parallel to the stream and to the slope contours. Following this step, the surface shall be prepared for seeding using rubber-tired equipment or by hand to avoid re-compaction.

### 2. Soil Tests and Amendments

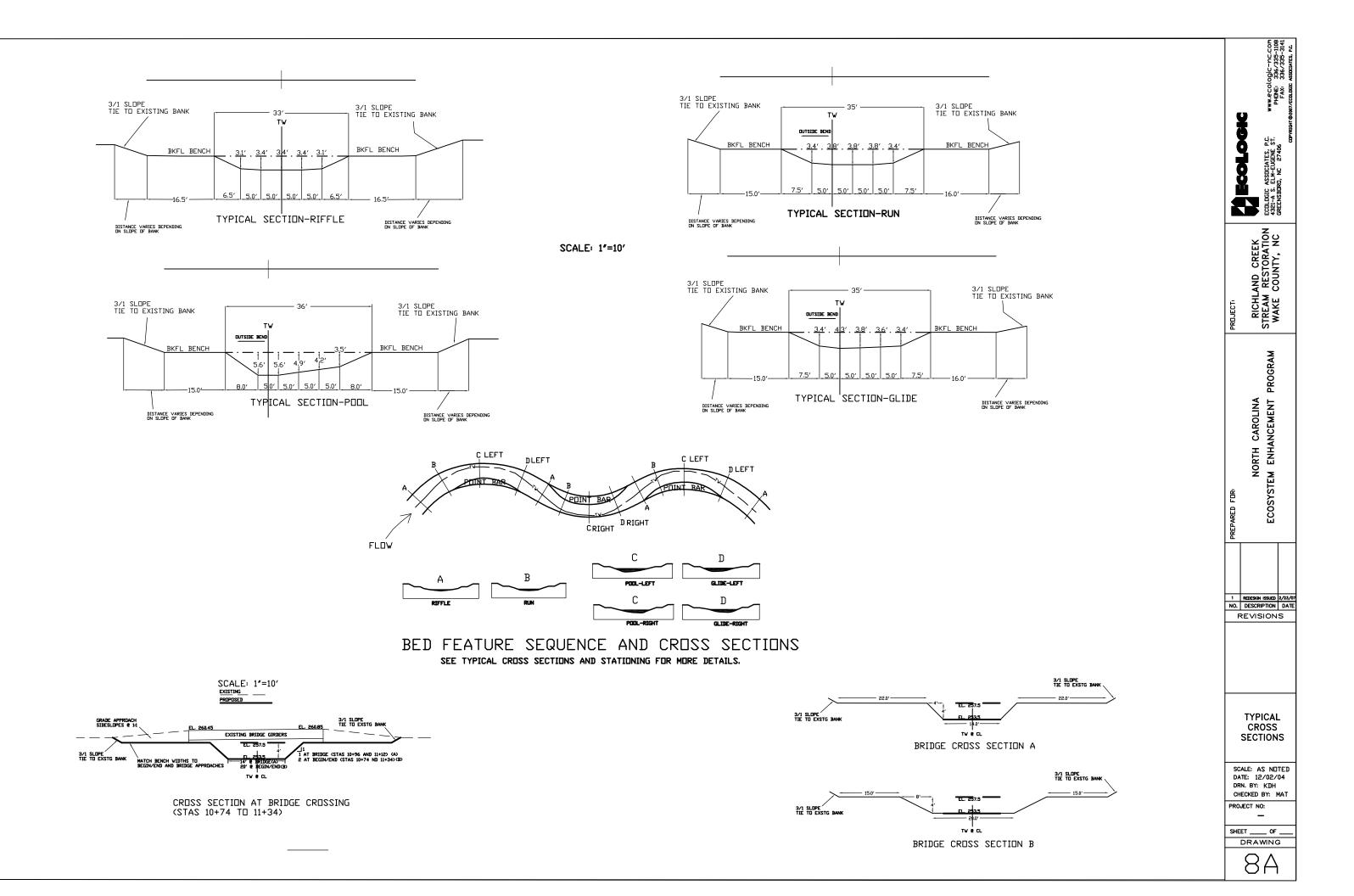
Soil in all planting areas shall be amended in accordance with test recommendations, and the rate of fertilization and lime application shall be in accordance with the test results. Soil sampling shall be performed utilizing sample methods recommended by the North Carolina Department of Agriculture and Consumer Services (NCDA&CS). The Planting Plan Designer is responsible for the soil sampling and adjusting the soil amendments according to the test results.

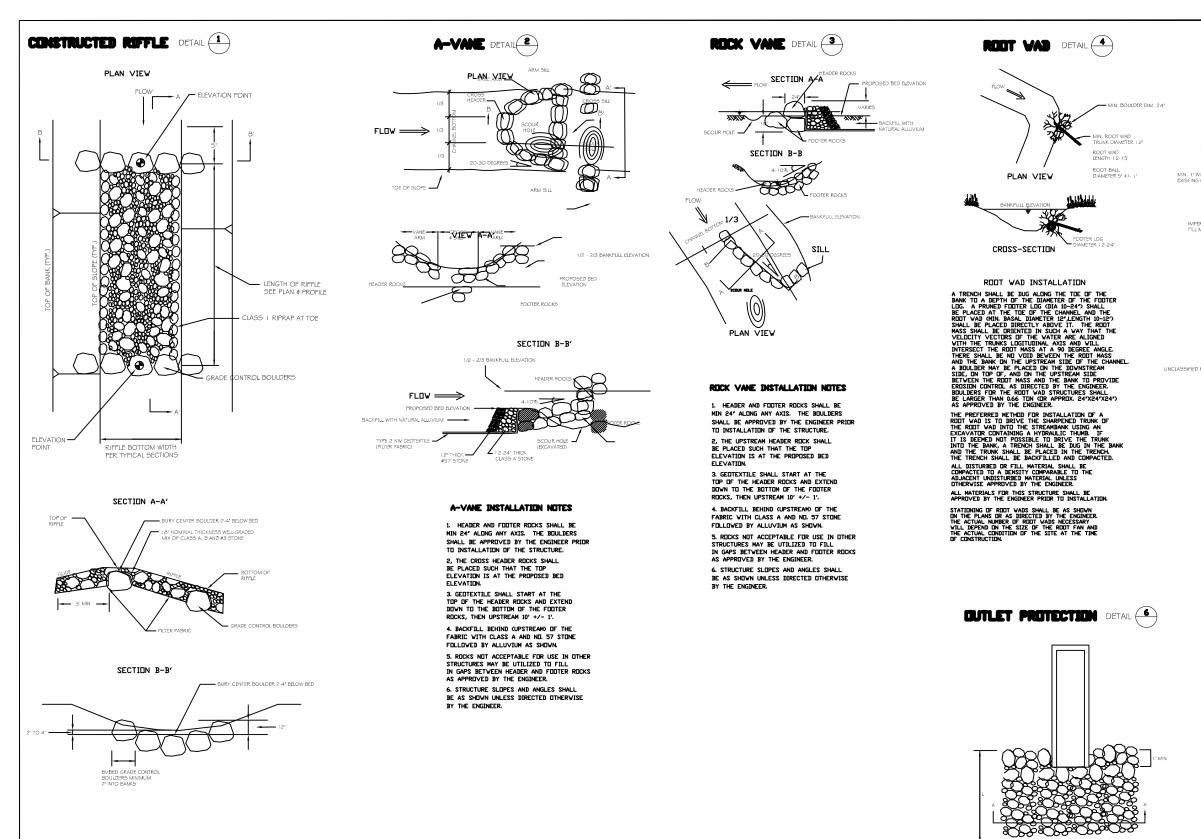
Soil amendment recommendations for native plant establishment:

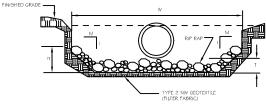
| Lime                 | 50-100 lbs./1000 sq. ft. | (1-2 tons/acre)     |
|----------------------|--------------------------|---------------------|
| Fertilizer (4-24-24) | 4-6 lbs./1000 sq. ft.    | (200-250 lbs./acre) |

Recommendations for grass establishment (also used on other areas disturbed during construction and planted with something other than native grasses)

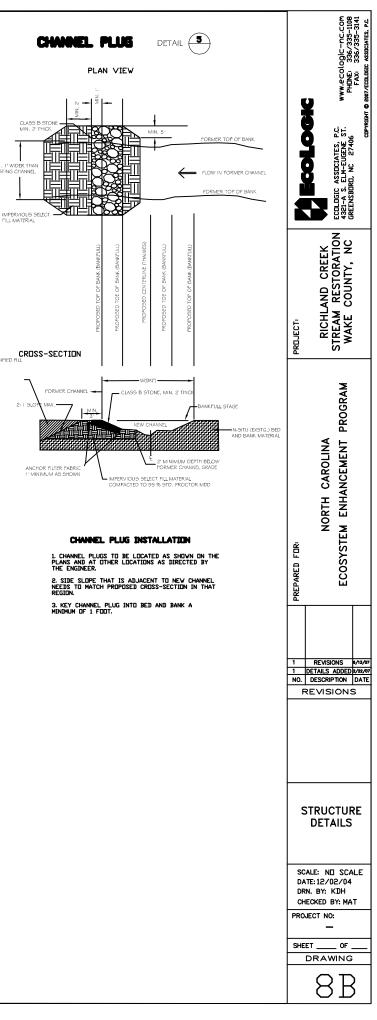
| Lime                  | 50-100 lbs./1000 sq. ft. | (1-2 tons/acre)     |
|-----------------------|--------------------------|---------------------|
| Fertilizer (10-10-10) | 8-12 lbs./1000 sq. ft.   | (400-500 lbs./acre) |







SECTION A-A'



### 3. Temporary Seeding

Temporary seeding shall be required on all disturbed areas that are: a) associated with temporary erosion or sediment control measures or other temporary features (e.g., haul roads, diversions, sediment traps, stockpiles) that will not be removed within 7 calendar days, b) planned to receive permanent seeding but will remain exposed for more than 15 working days; or c) planned to receive permanent seeding that is out of season for the construction period. In all cases, the temporary ground cover must be established within 15 working days following completion of any phase of grading.

### 4. Permanent Seeding

Permanent ground cover shall be provided in all designated areas within 15 working days or 90 calendar days (30 calendar days on exposed slopes), whichever is shorter, following completion of construction of any portion of the work.

Use permanent seeding on channel banks that will receive channel lining, on the bankfull bench, on terrace side slopes, and upslope of the channel in the riparian buffer. A mixture of native grasses and herbs shall be used. Competing, sod-forming grasses like fescue and bluegrass should be removed by either mechanical or chemical methods before planting native mixes. Seeding shall occur before coir fiber mats or other channel linings are placed on the subgrade.

### a. Seed Mixtures

The permanent seed mixture for the riparian corridor shall be approximately as follows:

| Oat Grain, Avena sativa or Rye Grain, Secale Cereale | 25% |
|--|-----|
| Virginia Wild Ryegrass, Elymus virginicus            | 25% |
| Switchgrass, Panicum virgatum var. Carthage          | 25% |
| Showy native wildflower mix (Ernst Seed)             | 25% |

### 5. Woody Plant Installation (Trees and Shrubs)

New woody plant material shall be installed in the restoration corridor as shown on the plans to enhance biodiversity, which improves both ecological function and aesthetics. This also allows the introduction of species that would not establish on their own and provides for site selection to enhance plant performance and restoration success. Planting stock may include containerized, bare root, or balled and burlaped trees and shrubs. Bare root seedlings shall be planted using a spade. Rooted plants shall be planted in holes sized to match the existing container or root ball.

The storage, handling, and planting of bare-root seedlings will follow the procedures outlined in the NC Division of Forest Resources' (NCFS) *Pocket Guide to Seedling Care and Planting Standards*, 4<sup>th</sup> Edition, which can be obtained at all NCFS county offices. Planting will not take place on 'Severe Days' as defined by the *Pocket Guide To Seedling Care and Planting Standards*.

All planting stock shall be handled in such a manner as to promote the health and vigor of the plant material and reduce the stress of transplanting and reestablishment. This means that all woody planting shall occur in the plant's dormant season, normally from November 15 to March 31. Planting stock shall be stored in a cool and moist environment and protected from direct sun and drying winds. Roots of bare root stock shall be kept moist before and during planting operations. Containerized or potted stock shall be kept moist at all times. Live stakes shall be prevented from drying and kept in a dormant condition, which may require daily moisture addition and refrigeration (below 40° F) if the weather is dry and warm. Damaged roots or shoots should be pruned appropriately before or during installation.

### a. Species Selection

It is important to plant as much diversity as is available to enhance the wildlife value, aesthetics and resilience of the riparian corridor restoration. A minimum of six (6) tree and four (4) shrub species shall be selected to enhance the species diversity that occurs naturally at the site. The density, effectiveness and ecological function of the woody plantings will be enhanced by combining canopy trees, understory trees and shrubs in a mixture that approximates a natural riparian forest that would occur at an undisturbed site.

### i. Tree Species Suitable for Richland Creek Restoration

Black Willow (Salix nigra), Green Ash (Fraxinus pennsylvanica), Sugar Maple (Acer floridanum), Sycamore (Platanus occidentalis), American Chestnut (Castanea dentata), Hackberry (Celtis occidentalis), River Birch (Betula nigra), Bitternut (Carya cordiformis) or Pignut Hickory (Carya glabra), Persimmon (Diospyros virginiana), Black Walnut (Juglans nigra), Black Gum (Nyssa sylvatica), Sourwood (Oxydendrum arboreum), Black Cherry (Prunus serotina), Red Oak (Quercus rubra), Water Oak (Quercus nigra), Black Locust (Robinia psuedo-acacia), American Elm (Ulmus americana), Pawpaw (Asimina triloba) Dogwood (Cornus florida), Redbud (Cercis Canadensis), American Holly (Ilex opaca) and Fringetree (Chionanthus virginicus).

### ii. Shrub Species Suitable for Richland Creek Restoration

Buttonbush (*Cephalanthus occidentalis*), Hazelnut (*Corylus flavula*), Elderberry (*Sambucus Canadensis*), Red Chokeberry (*Aronia arbutifolia*), Silky Dogwood (*Cornus amomum*), Spicebush (*Lindera benzoin*), Serviceberry (*Amelanchier laevis*), Hawthorne (*Crategus punctata*), Highbush Blueberry (*Vaccinium constablaei*), Tag Alder (*Alnus serrulata*), Witch Hazel (*Hamamelis virginiana*), Sweet Shrub (*Calycanthus floridus*), Sweet Pepperbush (*Clethera acuminata*), Winterberry (*Ilex verticillata*), Mountain Laurel (*Kalmia latifolia*), Blackhaw (*Viburnum prunifolium*) and Yellowroot (*Xanthorhiza simplicissima*).

*iii. Live Stake Species Suitable for Richland Creek Restoration* Black Willow, Silky Willow, Silky Dogwood, Buttonbush (requires pilot hole), and Elderberry (requires pilot hole).

### iv. Recommended Species for Richland Creek Restoration

Based on observations of the natural riparian communities in the Wake County region, there are several plant species that are recommended. It can be assumed that Red Maple (*Acer rubrum*) and Tulip Tree (*Liriodendron tulipifera*) will establish themselves voluntarily in the restoration reach as they are well represented in the adjacent forests; thus, their use is discouraged.

The added woody plants may include Sycamore, Walnut, Red Oak, Hickory, Green Ash and Black Willow as eventual canopy species. Subcanopy species may include Dogwood, Redbud, American Holly, Fringetree and Sourwood. Shrub species may include Elderberry, Tag Alder, Highbush Blueberry, Silky Dogwood, Red Chokeberry, Buttonbush and Hawthorne.

This mixture will maximize the vertical diversity for wildlife, produce a wide range of fruit and seed types, and provide the human neighborhood with seasonal displays of flower, fruit and leaf color.

### b. Planting Density (including transplants)

| Trees       | Spacing = 8 feet | 680 plants/acre initial stock density  |
|-------------|------------------|--|
| Shrubs      | Spacing = 4 feet | 1360 plants/acre initial stock density |
| Live Stakes | Spacing = 3 feet | 4840 plants/acre initial stock density |

Target density of plantings at maturity: 320 trees/acre and 1200 shrubs/acre.

### c. Woody Plant Protection

The use of tree shelters, bark wrap, fencing or chemical deterrents may be necessary at Richland Creek to prevent damage by deer and beaver. The shelters can be used on the more valuable material and the most slow growing and hard to establish species. These shelters will also accelerate the growth of the woody plants so that they can withstand herbivore attack. Anti-browsing chemical deterrents may also be needed to train the animals to avoid the plantings until they become established.

### 6. Invasive/Exotic Species Control

a. Removal of Exotic Grasses and Ground Cover

The work involves removal of exotic grasses that are located in non-wooded areas included in the proposed stream buffer through application of herbicide. Designer will identify location of grasses to be removed.

Any commercially available herbicide designated and suitable for extermination of grasses is allowable as long as it is labeled for use in riparian and wetland areas. The company performing the work in this section must have a commercial license as required by the North Carolina Pesticide Board. The work in this section must comply with the North Carolina Pesticide Law of 1971 and applicable federal laws

including but not limited to purchase, transport, storage, application, and disposal of chemical herbicides.

### b. Removal of Exotic Trees and Shrubs

The work involves removal and extermination of individual trees and shrubs through application of herbicide and hand excavation as identified by the Designer. This work does not include those exotic trees and shrubs that are excavated and removed as part of clearing and grubbing for site preparation.

Any commercially available herbicide designated and suitable for extermination of trees and shrubs is allowable as long as it is labeled for use in riparian and wetland areas. The company performing the work in this section must have a commercial license as required by the North Carolina Pesticide Board. The work in this section must comply with the North Carolina Pesticide Law of 1971 and applicable federal laws including but not limited to purchase, transport, storage, application, and disposal of chemical herbicides.

### 10. Stream Monitoring Plan

Stream restoration in North Carolina requires physical and biological monitoring based on NC Division of Water Quality criteria (Monitoring Level 1). The monitoring period is five (5) years. This time is required to assess the stability of the restored channel and the survivability of the vegetation planted during the restoration. The monitoring should be done annually following the completion of construction. Reports should be sent to the USACE each year and NC DWQ on the first, third and fifth years.

The restoration of this creek involves changes to dimension, pattern and profile. Benchmarks for permanent cross sections, photo points and the top of the restoration reach profile will be installed during construction. These benchmarks will be referenced during all following data collection visits. Use of benchmarks will allow all monitoring data to be comparable.

### a. Photo reference sites

Longitudinal and lateral photos showing the banks and the channel with a scale included will document the restored reach and each permanent cross-section. Photographs may also be taken of in-stream structures, plant survival plots, and any other noteworthy features. A map of the location and direction of each photograph shall be developed during the as-built survey. The same points should be included in subsequent monitoring visits as a minimum.

### b. Plant survival

Plant survival will be monitored in accordance with EEP's most current version of vegetation monitoring guidance. Plots will be established during the as-built survey for monitoring riparian vegetation. Transplants and woody stems will be counted and assessed for survivability and attainment of the success criteria of 320 trees per acre after three years. Allowances for additional mortality with time provide a final criterion of

260 trees per acre through year five. Observations of vegetation loss or damage due to drought, disease or herbivore predation will also be noted.

### c. Channel stability

Permanent cross-sections shall be established to monitor the upper, middle and lower sections of the reach since the amount of channel relocation and in-situ vegetation differs across this range. These cross-sections will be located in such a way as to capture the range of cross-sectional geometry installed at this site. One section will be a riffle section in the middle of the project that will also be the site of monitoring pebble counts and channel geometry diagnostics like width-depth ratio, entrenchment ratio, bank height ratio and bankfull depth measurements. One additional riffle cross-section will be established and a third cross-section will be located in one of the curves to measure stability of a pool. The cross-section locations will be determined and permanently marked by the designer at the time of the as-built survey.

The bed materials will be documented by conducting a pebble count at each reference location. The  $d_{50}$  and  $d_{84}$  of the riffles will be calculated and reported. A classification pebble count based on the proportional percentage of riffles and pools will also be conducted and reported.

Observation of rock and log structures, root wads, erosion control matting, permanent erosion control measures, stream crossings, bridges and exclusion fencing will also be conducted to evaluate the stability and durability of these installations.

### d. Biological indicators

If required, benthic macroinvertebrates may be collected using standard methods outlined in the Benthic Macroinvertibrate Monitoring Protocols for Compensatory Stream Restoration Projects technical guide.

### 11. Stream Success Criteria

The success of the stream restoration will be determined by how it achieves the general criteria outlined in Appendix II of the multi-agency workgroup document titled "Stream Mitigation Guidelines, April 2003" (Figure 11). Also important is how well it satisfies the landowner's requirements for a stable, aesthetic creek channel.

Criteria for success include that the stream be vertically and horizontally stable, i.e., "minimal evidence of instability (down-cutting, deposition, bank erosion, increase in sands or finer substrate material)". Furthermore, a stable stream channel should neither aggrade nor degrade substantially over time. Channel adjustments over time are a normal aspect of a dynamic stream. This is especially true of watersheds like Richland Creek's, which are undergoing transformation from rural to increasingly urban land uses. Appendix II. General criteria used to evaluate the success or failure of activities at mitigation sites and required remedial actions to be 5.0 indicate failu . ..... 1.1 d' ch. 10.1 .

| Action   | ACUOI                        | When substantial aggradation,<br>degradation or bank erosion occurs,<br>remedial actions will be planned,<br>approved, and implemented. | Areas of less than 75% coverage<br>will be re-seeded and or fertilized,<br>live stakes and bare rooted trees will<br>be planted to achieve desired<br>densities.   | When Substantial evidence of<br>instability occurs, remedial actions<br>will be planned, approved, and<br>implemented.            | Reasons for failure will be evaluated<br>and remedial action plans<br>developed, approved, and<br>implemented.   |
|--|------------------------------|---|--|---|--|
| dicate failure of a component.                                 | Fallure →                    | Substantial aggradation,<br>degradation or bank erosion.  | < 75% coverage in photo plots<br>for herbaceous cover.<br>Survival of less than 320 trees<br>per acre through year 3 and<br>then less than the success<br>criteria for years 4 and 5.  | Substantial* evidence of instability.   | Population measurements and<br>species composition indicate a<br>negative trend.                                 |
| implemented should monitoring indicate failure of a component. | Success (requires no action) | No substantial* aggradation,<br>degradation or bank erosion.  | <ul> <li>▶ 75% Coverage in Photo Plots</li> <li>Survival and growth of at least 320</li> <li>trees/acre through year 3, then</li> <li>10% mortality allowed in year 4</li> <li>(288 trees/acre) and additional</li> <li>10% mortality in year 5 for 260</li> <li>trees/acre through year 5.</li> </ul> | Minimal evidence of instability<br>(down-cutting, deposition, bank<br>erosion, increase in sands or finer<br>substrate material). | Population measurements remain<br>the same or improve, and species<br>composition indicates a positive<br>trend. |
|  | Mitigation Component         | (1.) <u>Photo Reference Sites</u><br>Longitudinal photos<br>Lateral photos  | (2.) <u>Plant Survival</u><br>Survival plots<br>Stake counts<br>Tree counts  | (3.) <u>Channel Stability</u><br>Cross-sections<br>Longitudinal profiles<br>Pebble counts   | (4.) <u>Biological Indicators</u><br>Invertebrate populations<br>Fish populations                                |

\*Substantial or subjective determinations of success will be made by the mitigation sponsor and confirmed by COE and review agencies. Monitoring Level 1 will include items 1, 2, and 3, and may include item 4 based on the project review. Monitoring Level 2 will include items 1 and 2, and may include item 3 based on the project review. Monitoring Level 3 will include only item 1.

Figure 11