2011

Comprehensive Application Report for 6600167.11A Enviva Pellets Northampton, LLC - Gaston (6600167)

Northampton County

Location deposited: Calculated Issue Due Initial amount: Date received: Amount Due: Add. Amt Rcv'd: Date Rcv'd: Location rec'd: Clock Start Application Dates Fee Information Completeness Due 10/25/2011 Deposit Slip #: 08/29/2011 08/26/2011 Received Fund type: \$13488.00 2331 Permit/Latest Revision: 10203/ Application is COMPLETE Raleigh Regional Office Kevin Godwin/RCO Charles McEachern Greenfield Facility In progress Unknown Engineer/Rev. location: Facility classification: General Information: Regional Contact: Application type: Facility location: Permit code: Clock is ON Status is:

(757) 274-8377 (301) 657-5567 Telephone Bethesda, MD 20814 Bethesda, MD 20814 City State ZIP 7200 Wisconsin Avenue 7200 Wisconsin Avenue Address Norb Hintz, Vice President Engineering Glenn Gray, Plant Manager Contact Information Name Technical/Permit Authorized

Appropriate number of apps submitted Acceptance Criteria Description Source recycling/reduction form Authorized signature Zoning Addressed Application fee PE Seal Acceptance Criteria Received? Yes Yes Yes Yes

Complete Item Description Completeness Criteria Received?

WEW SCUOODS WAY

Staff Comments Complete Due Start Regulations Pertaining to this Permit Application Events Event

Regulation Description Audit Information Pertaining to this Application

Reference Rule

10203 821 (Charles McEachern) New Value PSD (PSD)

Old Value GRNTV (TV-Greenfield)

Column Name Date Changed perm_Code 08/29/2011 08/29/2011 reg_Cont

Charles McEachern

Mark Cuilla

<u>Editor</u> Mark Cuilla

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North Carolina Department of Environment and Natural Resources **Division of Air Quality**

Beverly Eaves Perdue Governor

Sheila C. Holman Director

Dee Freeman Secretary

August 29, 2011

Mr. Norb Hintz Vice President Engineering Enviva Pellets Northampton, LLC 7200 Wisconsin Avenue **Suite 1100** Bethesda, MD 20814

SUBJECT: Receipt of Permit Application

Greenfield Facility

Application No. 6600167.11A Enviva Pellets Northampton, LLC

Facility ID: 6600167, Gaston, Northampton County

Dear Mr. Hintz:

Your air permit application (6600167.11A) for Enviva Pellets Northampton, LLC, located in Northampton County, North Carolina was received by this Division on August 26, 2011.

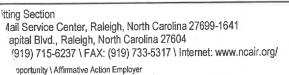
This application submittal did contain all the required elements as indicated and has been accepted for processing. Your application will be considered complete as of August 26, 2011, unless informed otherwise by this office within 60 days.

Should you have any questions concerning this matter, please contact Kevin Godwin at (919) 715-6255.

Sincerely,

Mary Cut.
Donald van der Vaart, Ph.D., P.E., J.D.

cc: Raleigh Regional Office Files





One Copley Parkway | Suite 310 | Morthy le, NC 27566 | P.(919) 462-9693 | F.(919) 462-9694
trinityconsultants.com

6600/67

Trinity

Consultants

November 18, 2011

Mr. John Evans North Carolina Division of Air Quality (NC DAQ) 217 West Jones Street Raleigh, NC 27603

RE: Permit Application Addendum Enviva Pellets Northampton, LLC Keceived

NOV 1 2 2011 Air Permits Section

Dear Mr. Name:

Dear Mr. Evans:

Enviva Pellets Northampton, LLC (Enviva) submitted a construction and operating permit application on August 21, 2011. This letter provides revised toxic air pollutant (TAP) emission rate calculations for the wood dryer and corresponding air dispersion modeling, as well as an update to greenhouse gas (GHG) calculations for the wood dryer.

REVISED EMISSIONS ESTIMATES

Originally, TAP and HAP emissions estimates for the direct-fired wood chip dryer were estimated using AP-42 emission factors for wood dryers that ostensibly should have included combustion by-products because the factors were identified as being applicable to direct contact, wood fired dryers. However during recent review of the calculations, we noticed that a number of TAPs and HAPs included in Section 1.6 of AP-42 (wood combustion) were not present in EPA's emission factors for wood dryers. Since it is reasonable to assume that these additional compounds would be present in the dryer exhaust, we have updated the emissions calculations for the dryer accordingly.

During a recent review of the calculation spreadsheets for the project, we discovered that a late change in dryer heat input to 207 MM Btu/hr was not updated in the GHG emissions calculations for the wood dryer.

Revised emission estimates are provided in Attachment 1. It should be noted that facility-wide emissions remain well below the HAP major source thresholds.

AIR DISPERSION MODELING

As presented in the updated emissions estimates in Attachment 1, the following addition for the dryer and result in facility-wide emissions that

Enviva Pellets Northampton, LLC - Page 2 11/18/2011

exceed the TPERs: arsenic, benzo(a)pyrene, cadmium, chlorine, hexachlorodibenzo-p-dioxin, hydrogen chloride, mercury, nickel, and vinyl chloride.

AERMOD air dispersion modeling for TAPs exceeding the TPERs were conducted in accordance with NCDAQ modeling guidelines. Please note that air dispersion modeling for TAPs provided in the initial permit application remain unchanged.

All TAPs were modeled using each source's respective emission rate.

Modeling results indicate ambient concentrations well below the AALs. Since all concentrations fall below 50 percent of the AAL, only a single year (1992) of meteorological data was used. A summary of modeling parameters, a summary of modeling results, and a completed copy of the air dispersion modeling checklist are provided in Attachment 2.

CLOSING

Enviva would greatly appreciate prompt processing of this application. Feel free to contact me at 919-462-9693 or Glenn Gray of Enviva at 804-412-0227 with any questions or comments.

Sincerely,

TRINITY CONSULTANTS

Joe Sullivan, PE, CM Managing Consultant

cc: Glenn Gray (Enviva)

Goe W. Sullivan

Attachments

ATTACHMENT 1 Updated Emissions Calculations

TABLE 3-1
PSD APPLICABILITY SUMMARY
ENVIVA PELLETS NORTHAMPTON, LLC

Source Description	Unit ID	CO (tpy)	NOx (tpy)	TSP (tpy)	PM-10 (tpy)	PM-2.5 (tpy)	SO2 (tpy)	VOC (tpy)	CO _{2e} (tpy)
Dryer System	ES-DRYER	275.50	187.63	36.79	36.79	36.79	22.67	356.25	187,561.92
Emergency Generator	ES-EG	0.50	0.58	0.03	0.03	0.03	0.00	0.00	93.04
Fire Water Pump	ES-FWP	0,43	0.49	0.05	0,02	0.02	00.00	00.0	79.75
Hammermills	ES-HM-1, -2, -3, -4	1	1	15.02	15.02	15.02	,	,	ı
Hammermills Area Filter	ES-HMA	•	1	7.04	7.04	7.04	t	1	1
Pellet Mill Feed Silo	ES-PMFS	1		0.47	0.47	0.47	,	•	•
Pellet Coolers	ES-CLR	•	,	61.95	61.95	61.95		ı	•
Log Debarking/Chipping	ES-CHIP-1	1	t	,	1	ı	1	1.25	ı
Diesel Storage Tanks	TK1 & TK2	ı	ı	1	1	•	-	3.79E-03	1
Total Pro	Total Project Emission Increases	276.44	188.69	121.31	121.31	121.31	22.67	357.51	187,734.71
PSD Sign	PSD Significant Emission Rates	100	40	25	10	15	40	40	100,000
	PSD Review Required?	Yes	Yes	Yes	Yes	Yes	No	Yes	Yes

TABLE 3-2 FACILITYWIDE HAP EMISSIONS SUMMARY ENVIYA PELLETS NORTHAMPTON, JLC

Description	ES-DRYER	ES-EG	ES-FWP	ES-CHIP-1	Total
	(tpy)	(tpy)	(tpy)	(tpy)	(tby)
1,3-Buladiene	٠	2,39E-05	2,05E-05		4,45E-05
Acetaldeh 'de	2.60E+00	4,70E-04	4.03E-04	M	2.60
Acetophenone	2.90E-06		,	1	00'0
Acrolein	7.97E-01	5,67E-05	4.86E-05	•	0.80
Antimony & Compounds	5,19E-04	5	1	,	0.00
Arsenic & Compounds	L45E-03			,	00.0
Вепдепе	2.6313-01	5,71E-04	4.90E-04	1	0.26
Beryllium metal (un-reacted) (Also include in BEC)	7.23E-05	1			00'0
Cadmium Metal (elemental un-reacted) -(Add w/CDC)	2.70E-04		١		0.00
Carbon tetrachloride	4.08E-02	ı	'	3	0.04
Chlorine			1	14	0.72
Chlorobenzene	2,99E-02				0.03
Chromium-Other compds (add w/ehrom acid to get CRC)	1.15E-03	:			00'0
Cobalt compounds	4.27E-04	1	10		00'0
Chloroform	3.47E-03		00		3,47E-03
Cumene	6.93E-02		3	1	70.07
Dinitrophenol, 3,4-	1.63E-04	7/4	æ		0.00
Di(2-ethy/hexyl)/hthalate (DEHP)	4.26E-05			1	00'0
Ethyl benzene	2.81E-02		i i		0.03
Ethylene dichloride (1,2-dichloroethane)	2.63E-02	à	# (· ·		0.03
Formaldely de	4.85E+00	7,23E-04	6.20E-04	Z.	4.85
Hydrogen chloride (hydrochloric acid)	1.72E+00	4			1,72
Lead and Lead compounds	3.16E-03			-	0.00
m-,1-Xylene	1.66E-01	1.75E-04	1.50E-04	1	0.17
Manganese & compounds	1,05E-01	1			0,11
Mercury, valor (Include in Mercury&Compds)	3,17E-03			ı	000
Methanol	3.81E+00	1	1	0,24	3.81
Methyl bromide (bromomethane)	1.36E-02			00	0.01
Methyl chloride (chloromethane)	2.09E-02	1	ı	,	0.05
Methyl chloroform (1,1,1 trichloroethane)	2.81E-02		4		0.03
Methyl isobutyl ketone	2.39E-01				0.24
Methylene chloride	6.24E-02		•	,	90.0
Nickel metal (Component of Nickel & Compounds)	2.99E-02		1	х	0.03
o-Xylene	1.56E-02	٠	•		0.02
Pentachlorophenol	4.62E-05		ŭ.	1	00.0
Perchloroethylene (tetrachloroethylene)	3.45E-02	3			0.03
Phenol	9.71E-01	100			0.97
Phosphorus Metal, Yellow or White	2.4513-02		9	٠	0.02
Polychlorinated biphenyls	7.39E-06		3		00'0
Propionaldehyde	4,51E-01	-	141	. 4	0.45
Protivlene dichloride (1,2 dichloropropane)	2,99E-02		1		0.03
Selenium compounds	2.54E-03			,	0.00
Styrene	1.25E-02	-	ŀ		0.01
Toluene	4.51E-01	2.51E-04	2.15E-04	,	0.45
Total PAH (POM)	1.13E-01	1.03E-04	8.82E-05	ia	1.14B-01
Trichloroethylene	2.72E-02	(4)			0.03
Trichtorophenol. 2.4,6-	1,99E-05	1	,	A .	0.00
Vinyl chloride	1.63E-02	(*)		,	0.02
TOTAL HAP	17,74	2,37E-03	2.03E-03	0.24	17.75
		With 1 mm 11 to		1 80 1 11	11000

TABLE 3-3 DETERMINATION OF POLLUTANTS SUBJECT TO AIR TOXICS PERMITTING ENVIVA PELLETS NORTHAMPTON, LLC

TAP Emissions

Description			Dryer		Eme	Emericacy Generator	itor	<u> </u>	Fire Water Pump	dt		Total	
Pollutant	CAS Number	(lb/hr)	(lb/day)	(lb/yr)	(3b/hr)	(Ib/day)	(lb/yr)	(Ib/hr)	(Ib/day)	(Ib/yr)	(lb/hr)	(Ib/day)	(Ib/kr)
1,3-Butadiene	106-99-0			0.00E+00			4,7915-02			4,11E-02			S.90E-02
Acetaldehyde	0-70-52	4.61E+00			1.88E-03			1,615-03			4.62E+00		
Acrolein	107-02-8	1.41E+00			2,27E-04			1,945-04			1,4115+00		
Arsenic				2.89E+00									2,89E+00
Benzene	71-43-2			5.27E+02			1.14E+00			9,80E-01			5.298+02
Benzo(a) wrene	50-32-8			4,71E+00			2,30E-04			1.97E-04			4,728+00
Beryllium				1,45E-01									1.45E-01
Cadmium				5.39E-01									5,398-01
Carbon Tetrachloride				8.16E+01									8,16E+01
Chlorine		1,64E-01	3.92E+00								1.64E-03	3.926+00	
Chlorobenzene			1.64E-01									1.64E-01	
Chloroform	67-66-3			6.93E+00									6.93E+00
Chromic acid (Chromium VI)	7738-94-5	5.25E-05	1,26E-03	4.60E-01								1,268-03	
Di(2-ethylhexyl)phthalate (DEHP)			2.33E-04									2.338-04	
Ethylene dichloride (1,2-dichloroethane)				5,26E+01									5,26[3:01
Formaldehyde	20-00-0	8.61E+00			2.89E-03			2,48E-03			8.62E+0H)		
Hexachlorodibenzo-p-dioxin 1,2,3,6,7,8				2,90E+00									2,900€+00
Hydrogen chloride (hydrochloric acid)		3,93E-01									3.93E-01		
Manganese & compounds			5.76E-01									5.76E-01	
Mercury, varior (Include in Mercury&Compds)			1,74E-02									1,748-02	
Methyl chloroform (1,1,1 trichloroethane)		6,42E-03	1.54E-01								6,42E-03	1.54E-01	
Methyl ethyl ketone		1,12E-03	2.68E-02								1.12E-03	2.68E-02	
Xylene	1330-30-7	3.23E-01	7.75E+00		6.98E-04	1.68E-02		5.99E-04	1,448-02		3.246-01	7,78E+00	
Methyl isobutyl ketone	108-10-1	4.24E-01	1.02E+01								4,24E-01	1,02E+01	
Methylene chloride	75-00-2	1.11E-01		1.25E+02							1.1115-01		1.258+02
Nickel metal (Component of Nickel & Compounds)			1,64E-01									1.64E-01	
Pentachlorophenol		1.06E-05	2.53E-04								1.06E-05	2.53E-04	
Perchloroethylene (tetrachloroethylene)				6.89E+01									6.895+01
Phenol	108-95-2	1.72E+00									1,72E+00		
Polychlorinated biphenyls				1,48E-02									1,4815-02
Styrene	100-42-5	2,21E-02									20-31127		
Tetrachlorodibenzo-p-dioxin, 2,3,7,8-				1.56E-05									1.5615-05
Toluene	108-88-3		1.92E+01			2.40E-02			2.06E-02			1.92E+01	
Trichloroethylene				5.44E+01									5,44E+01
Trichlorofluoromethane (CFC 111)		8.49E-03									8.49E-03		
Vinyl chloride				3.26E+01									3.26E+01

			Total			TPER (2Q .0711)	-	Modeling
Polintant	CAS Number	(Jb/hr)	(Ib/day)	(lb/yr)	(Jb/hr)	(lb/day)	(lb/yr)	Required?
1.3-Butadiene	106-99-0			8,90E-02			1,108+01	°Z
Acetaldehyde	75-07-0	4.62E+00			6.80E+00			°Z
Acrolein	107-02-8	1.41E+00			2.00E-02			Yes
Arsenic				2.89E+00			1.60E-02	y.es
Benzene	71-43-2			5.29E+02			8.10E+00	Yes
Benzo(a) pyrene	50-32-8			4,72E+00			2.20E+00	Yes
Beryllium				1.45E-01			2,80E-01	oN
Cadmium				5,30E-01			3.70E-01	y es
Carbon Tetrachloride				8.16E+01			4.60E+02	oN
Chlorine		1.6415-01	3,026+00		2,308-01	7,908-01		Yes
Chlorobenzene			1,64E-01			4.60E+01		oN
Chlorofarm	67-66-3			6.93E+00			2,908+02	οN
Chromic acid (Chromium VI)	7738-94-5		1.268-03			1,308-02		oN
Di(2-ethylhexyl)phthalate (DEHP)			2.336-04			6,30E-01		oN
Ethylene dichloride (1,2-dichloroethane)				5,26E+01			2,608+02	oN
Formaldehade	20-00-0	8.62E+00			4.00E-02			Yes
Hexachlorodibenzo-p-dioxin 1,2,3,6,7,8				2.908+00			5.10E-03	Yes
Hydrogen chloride (hydrochloric acid)		3.93E-01			1.80E-01			Yes
Manzanese & compounds			5.76E-01			6.30E-01		No
Mercury, vapor (Include in Mercury &Compds)			1,74E-02			1.30E-02		Yes
Methyl chloroform (1,1,1 trichloroethane)		6.42E-03	1.54E-01		6.40E+01	2.50E+02		No
Methyl ethyl ketone		1.12E-03	2.68E-02		2.24E+01	7,80E+01		Ν̈́ο
Xylene	1330-20-7	3.24E-01	7,78E+00		1.64E+01	5.70E+01		No
Methyl isobutyl ketone	108-10-1	4.24E-01	1.02E+01		7.60E+00	5,20E+01		No
Meth Jene chloride	75-09-3	1.11E-01		1.25E+02	3.90E-01		1.60E+03	No
Nickel metal (Component of Nickel & Compounds)			1.64E-01			1.30E-01		Yes
Pentachlorophenol		1.06E-05	2.53E-04		6.40E-03	6,30E-02		No
Perchloroeth Jene (tetrachloroeth Jene)				6.89E+01			1,30E+04	oN
Phenol	108-95-2	1.72E+00			2,40E-01			Yes
Polychlorinated biphenyls				1,48E-02			5.60E+00	No
Styrene	100-42-5	2,21E-02			2,70E+00			No
Tetrachlorodibenzo-p-dioxin, 2,3,7,8-				1.56E-05			2.00E-04	οN
Toluene	108-88-3		1.92E+01			9.80E+01		oN
Trichloroethylene				5.44E+01			4,00E+03	ν°ο
Trichlorofluoromethane (CFC 111)		8.49E-03			1.40E+02			oN.
Vinvl chloride				3.26E+01			2,60E+01	Yes

Rotary Dryer - Criteria Pollutant Emissions

Dryer Inputs

Dryer Throughput (@ Dryer Exit)	527,778 tons/year @ 10% moisture	
Annual Dried Wood Throughput of Dryer	475,000 ODT/year	
Max. Hourly Dried Wood Throughput of Dryer	61.50 ODT/hr	
Burner Heat Input	207.0 MMBtu/hr	
Percent Hardwood	90%	
Percent Softwood	10%	
Potential Operation	8,760 hr/yr	

Criteria Pollutant Calculations:

	Biomass		Emission	Total Po	otential
Pollutant	Emission Factor	Units	Factor Source	Emis	
	(lb/ODT)			(lb/hr)	(tpy)
СО	1.16	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	71.34	275.5
NO _x	0.79	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	48.59	187.6
PM/PM ₁₀ /PM _{2.5} Condensible Fraction	0.017	lb/MMBtu	AP-42, Section 1.6 ²	3.52	15.4
TSP (Filterable)	0.090	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	5.54	21.4
Total TSP (Filterable + Condensible)				9.05	36.8
PM ₁₀ (Filterable)	0.090	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	5.54	21.4
Total PM ₁₀ (Filterable + Condensible)				9.05	36.8
PM _{2.5} (Filterable)	0.090	lb/ODT	Calculated from Guaranteed WESP Specifications	5.54	21.4
Total PM _{2.5} (Filterable + Condensible)				9.05	36.8
SO ₂	0.025	lb/MMBtu	AP-42, Section 1.6 ³	5.18	22.7
VOC	1.50	lb/ODT	Calculated from Guaranteed WESP Specifications	92.25	356.3
Lead	0.00	N/A	N/A	0.00	0.0

Note:

 $^{^{1}}$ CO, NO_x, VOC, and filterable PM/PM₁₀ emission factors were provided by the dryer system vendor. The PM_{2.5} filterable emission factor is assumed to be the same as PM and PM₁₀.

² The vendor only provided the filterable fraction of particulate matter in the emission factors. The condensible fraction of particulate matter from a rotary dryer controlled by a WESP is not provided in AP-42, Section 10.6.2. Enviva has conservatively calculated the condensible fraction based upon the heat input of the dryer burners using an emission factor for wood combustion from AP-42, Section 1.6.

³ No emission factor is provided in AP-42, Section 10.6.2 for SO₂ for rotary dryers. Enviva has conservatively calculated SO₂ emissions based upon the heat input of the dryer burners using an emission factor for wood combustion from AP-42, Section 1.6.

Rotary Dryer - Federal Hazardous Air Pollutant (HAP) and North Carolina Toxic Air Pollutant (TAP) Emissions

Calculation Inputs:

Dryer Throughput (Ton/yr)	527,778
ODT/vr	475,000
ОДТИЛ	61.50
Hardwood Composition	%06
Softwood Composition	%01

HAP & TAP Emission Calculations:

			•	Direct v	Direct wood-fired, hardwood	rdwood	Green, D moisture e	Green, Direct wood-fired (inlet moisture content >50%, dry basis), softwood 1	red (inlet dry basis),		
HAP/TAP Pollutant	CAS Number	HAP	NC TAP	Emission Factor ²	Emissions ³	ions ³	Emission Factor	Emis	Emissions ³	MAXIMUR	MAXIMUM TOTAL EMISSIONS
		(Yes/No)	(Yes/No)	(Ib/ODT)	(Ib/hr)	(tpy)	(Ib/ODT)	(lb/hr)	(tpy)	(lb/hr)	(tpy)
Acetaldehyde	75-07-0	Yes	Yes	3.83E-03	2,36E-01	8.19E-01	7.50E-02	4.61E+00	1.78E+00	4.61E+00	2.60E+00
Acrolein	107-02-8	Yes	Yes	1.17E-03	7.22E-02	2.51E-01	2.30E-02	1.41E+00	5.46E-01	1.41E+00	7.97E-01
Benzene	71-43-2	Yes	Yes	3.88E-04	2.39E-02	8.30E-02	7.60E-03	4.67E-01	1.81E-01	4.67E-01	2.63E-01
Chloroform	67-66-3	Yes	Yes	5.11E-06	3.14E-04	1.09E-03	1.00E-04	6.15E-03	2.38E-03	6.15E-03	3.47E-03
Chromic Acid (Chromium VI)	7738-94-5	Yes	Yes								
Cumene	98-82-8	Yes	No	1.02E-04	6.28E-03	2.18E-02	2.00E-03	1.23E-01	4.75E-02	1.23E-01	6.93E-02
Formaldehyde	20-00-0	Yes	Yes	7.15E-03	4.40E-01	1.53E+00	1.40E-01	8.61E+00	3.33E+00	8.61E+00	4.85E+00
m-,p-X lene	1330-20-7	Yes	Yes	2.45E-04	1.51E-02	5.24E-02	4.80E-03	2.95E-01	1.14E-01	2.95E-01	1.66E-01
Methanol	67-56-1	Yes	No	5.62E-03	3.45E-01	1.20E+00	1.10E-01	6.77E+00	2.61E+00	6.77E+00	3.81E+00
Methyl isobutyl ketone	108-10-1	Yes	Yes	3.52E-04	2.17E-02	7.53E-02	6.90E-03	4.24E-01	1.64E-01	4,24E-01	2.39E-01
Methylene chloride	75-09-2	Yes	Yes	9.19E-05	5.65E-03	1.96E-02	1.80E-03	1,11E-01	4.28E-02	1.11E-01	6.24E-02
o-Xylene	95-47-6	Yes	°Ž	2,30E-05	1.41E-03	4.91E-03	4.50E-04	2.77E-02	1.07E-02	2.77E-02	1.56E-02
Phenol	108-95-2	Yes	Yes	1.43E-03	8.79E-02	3.06E-01	2.80E-02	1.72E+00	6.65E-01	1.72E+00	9,71E-01
Propionaldehyde	123-38-6	Yes	°N	6.64E-04	4.08E-02	1.42E-01	1.30E-02	8.00E-01	3.09E-01	8.00E-01	4.51E-01
Styrene	100-42-5	Yes	Yes	1.84E-05	1.13E-03	3.93E-03	3.60E-04	2.21E-02	8.55E-03	2.21E-02	1.25E-02
Toluene	108-88-3	Yes	Yes	6.64E-04	4.08E-02	1.42E-01	1.30E-02	8.00E-01	3.09E-01	8.00E-01	4.51E-01
									Total HAP	2.62E+01	1.48E+01

Note:

HAP & TAP emission factors for "green, direct wood-fired (inlet moisture content >50%, dry basis" softwood were obtained from AP-42, Section 10.6.2, Table 10.6.2-3.

² To account for hardwood HAP & TAP emissions, factors were conservatively calculated by taking the AP-42 HAP factors for 100% softwood (green) and multiplying by the ratio of the total listed VOC emission factors for hardwood and softwood (0.24 / 4.7).

³ Short-term HAP & TAP emissions were calculated based upon a worst-case scenario of 100% hardwood or softwood firing (in which case, softwood is always the overall worst case).

207.00 8.760 1,813,320 92,75% Heat Input (MMBtu/hr)
Operating Schedule (hrs/yr)
Heat Input (MMBtu/yr) WESP Metal HAP Control Efficiency2 HCI Control Efficiency

HAP & TAP Emission Calculations:

		Cluiss	CHIESTON PARTONS					entheenthen .	SHILLS			
	Pollutant	-	Bionuss		Biomass	113.55	Maxim	Maximum Uncontrolled Total (per boiler)	d Total	Mavin	Maximum Controlled Total (per boiler)	[ota]
Pollutant		B/mmBln	lb/mmBtu	Ref.	lb/hr	:1 = .	lb/hr	lb/yr	λd)	ll/hr	lb/vr	łpy
		Uncontrolled	Controlled		Uncontrolled	Controlled						
Acetophenone	HAP	3.20E-09	3.20E-09	-	6.62E-07	6.62E-07	6,62E-07	5.8015-03	00'0	6,628-07	5.80E-03	0.00
Antimony & Compounds	IIAP	7.90E-06	5,73E-07	<u></u>	1.648-03	1.19E-04	1,64E-03	1,43/E+01	10,0	1,19E-04	1,04E+n0	U'U
Arsenic & Compounds	TAP/HAP	2.2015-05	1.60E-06	7.7	4.55E-03	1,30E-04	4,55 E-03	3,99E+01	50,0	3,306-04	2,80E+00	0,00
Benzo(a)pyrene	TAP/HAP	2.60E-06	2.60E-06		5.38E-04	5.38E-04	5,38E-04	4.718+00	0,00	5.38E-04	4,71E+00	0,00
Beryllium metal (un-reacted) (Also include in BEC)	TAPHAP	1,10E-06	7,98E-08	1. 2	2.28E-04	1,6515-05	2,28 E-04	1,995-00	0,00	30-313971	1,45E-01	(1,0)
Cadmium Metal (elemental un-reacted)(Add w/CDC)	TAPHAP	4,10E-06	2.97E-07	2.	8,49E-04	6.15E-05	8,49E-04	7,43E+00	0.00	6.15E-05	S,39E-01	0.00
Carbon tetrachloride	TAP/HAP	4.50E-05	4.50E-05	-	9,32E-03	9.32E-03	9,32E-03	8,16E+01	D.04	9,32E-03	8,16E+01	0,04
Chlorine	TAP/HAP	7.90E-04	7,90E-04	-	1.64E-01	1.64E-01	1.64E-01	1.43E+03	0,72	1.64E-01	1,43E+03	0.72
Chlorobenzene	TAP/HAP	3,30E-05	3.30E-05	-	6.83E-03	6.83E-03	6.83E-03	5.98E+01	0.03	6.83E-03	5.98E+01	0.03
Chromic acid (Chromium VI)	TAP	3.50E-D6	2,546-07	1.2	7,25E-04	5.25E-05	7.25E-04	6.35E+00	00.00	5,25E-05	4.60E-01	0,00
Chromium-Other compds (add w/chrom acid to get CRC)	HAP	1.75E-05	1,27E-06	<u></u>	3.62E-03	2.63E-04	3.62E-03	3,17E±01	0,02	2.63E-04	2,30E+00	00.0
Cohali compounds	HAP	6.50E-06	4.71E-07	1, 2	1,35E-03	9.75E-05	1,35E-03	1.18E+01	0,01	9,75E-05	8,55E-01	00'0
Dinitraphenol. 2.4-	HAP	1.80E-07	1.80E-07	-	3.73E-05	3,73E-05	3.73E-05	3,26E-01	00.00	3,73E-05	3,26E-01	00'0
Di(2-ethylbexyl)phthalate (DEHP)	TAP/HAP	4,70E-08	4,70E-08	-	9,73E-06	9.73E-06	9,73,8-06	8.5218-02	00'0	9.7315-06	8,52E-02	00.00
Ethyl benzene	HAP	3.10E-05	3,10E-05	-	6,42E-03	6.4215-03	6.42E-03	5,62E+01	0,03	6,4215-03	5,62E+01	£0.0
Ethylene dichloride (1,2-dichloroethane)	TAP/HAP	2,90E-05	2.90E-05	-	6,00E-03	6,000-03	6,00E-03	5,26B+01	0.03	6.00E+03	5,26E+01	0,03
Hexachlorodibenzo-p-dioxin 1.2.3.6.7.8	TAP	1.60E-06	1.60E-06	-	3,316-04	3,31E-04	3.31E-04	2,40E+00	0.00	3,318-04	2.90E+00	00'0
Hydrogen chloride (hydrochloric acid)	TAP/HAP	1,90E-02	1.90E-03	۲.,	3.93E+00	3.93E-01	3,93E+00	3,45E+04	17.23	3,93E-01	3,45E+03	1.72
Lead and Lead compounds	HAP	4.80E-05	3,48E-06	1,2	9,948-03	7,20E-04	9,94E-03	8,70E+01	0.04	7,20E-04	6,31,5400	0.00
Manganese & compounds	TAP/HAP	1.60E-03	1.16E-04	<u>.;</u>	3,31E-01	2.40E-02	3,31E-01	2,90E+03	1.45	2,40E-02	2,10E+02	0.13
Mercury, vapor (Include in Mercury & Compds)	TAP/HAP	3,50E-06	2.54E-07	1.7	7.25E-04	5.25E-05	7,256-04	6.35E+00	00.0	7,25E-04	6,35E+00	0.00
Methyl bromide (bromomethane)	HAP	1.50E-05	1,50E-05	-	3,11E-03	3,11E-03	3,11E-03	2,72E+01	0.01	3.11E-03	2,7215+01	0.0
Methyl chloride (chloromothane)	HAP	2,306-05	2.30E-05	-	4,7615-03	4,76E-03	4,7615-03	4,17E+01	0.02	4.76E-03	4,175 +01	000
Methyl chloroform (1,1,1 trichloroethane)	TAP/HAP	3.10E-05	3,10E-05	-	6.42E-03	6.42E-03	6,42E-03	5.62E+01	0.03	6,4215-03	5.62E+01	0.03
Methyl ethyl ketone	TAP/HAP	5.40E-06	5.40E-06	-	1,12E-03	1.12E-03	1,12E-03	9,79E+00	00'0	1,126-03	9,70E+00	0.00
Naplithalene	HAP	9.70E-05	9.70E-05	-	2.01E-02	2.01E-02	2.01E-02	1.76E+02	0.09	2,01E-02	1.76E+02	0.09
Nickel metal (Component of Nickel & Compounds)	TAP/HAP	3.30E-05	2,39E-06		6.83E-03	4.95E-04	6.83E-03	5.98E+01	0.03	6,83E-03	5.98E+01	0.03
Nirrophenol, 4-	HAP	1,10E-07	1.10E-07		2,28E-05	2,28E-05	2,28E-05	1,99E-01	0.00	2,28E-05	1.99E-01	0,00
Pentachlorophenol	TAP/HAP	5.10E-08	5.10E-08	-	1.06E-05	1.06E-05	1.06E-05	9,25E-02	0.00	1.06E-05	9,25E-02	0.00
Perchloroethylene (tetrachloroethylene)	TAP/HAP	3.80E-05	3.80E-05	-	7.87E-03	7.87E-03	7.87E-03	6.89E+01	0.03	7.87E-03	6.89E+01	0.03
Phosphorus Metal, Yellow or White	HAP	2.70E-05	1,96E-06	1,2	5,59E-03	4.05E-04	5.59E-03	4.90E+01	0,02	5.59E-03	4.90E+01	0,02
Polychlorinated biphenyls	TAP/HAP	8.15E-09	8.15E-09	-	1.69E-06	1.69E-06	1.69E-06	1,48E-02	0.00	1,69E-06	1,48E-02	00.0
Polycyclic Organic Matter	HAP	1,25E-04	1,25E-04	-	2.59E-02	2.59E-02	2.59E-02	2.27E+02	0.11	2,596-02	2,27E+02	- C
Propylene dichloride (1,2 dichloropropane)	HAP	3,30E-05	3,30E-05	-	6.83E-03	6.83E-03	6.83E-03	5.98E+01	0.03	6.83E-03	S.98E+01	0,03
Selenium connounds	HAP	2.80E-06	2,03E-07	1, 2	5.80E-04	4,20E-05	5.80E-04	5.08E+00	00'0	5,80E-04	SOREHD	00'0
Tetrachlorodibenzo-p-dioxin, 2.3.7.8-	TAP/HAP	8.60E-12	8.60E-12	-	1.78E-09	1.78E-09	1.78E-09	1.56E-05	00'0	1,78E-09	1,56E-05	0.00
Trichloroethylene	TAP/HAP	3.00E-05	3.00E-05	-	6,21E-03	6.21E-03	6,21E-03	5,44E+01	0.03	6.21 E-03	5,446+01	0.03
Trichlorofluoromethane (CFC 111)	TAP	4,10E-05	4,10E-05		8,496-03	8.49E-03	8,49E-03	7,43E+01	0.04	8,49E-03	7,43(5+01	10.0
Trichlorophenol, 2,4,6-	HAP	2.20E-08	2,20E-08	-	4.55E-06	4,55E-06	4.55E-06	3,99E-02	0.00	4.55B-06	3.99E-02	0.00
Minut addressed	TAD/HAD	1.80E-05	1.80E-05	-	3.73E-03	3,73E-03	3,73E-03	3.26E+01	0.02	3.73E-03	3,26E+01	0.02

Uncontrolled and controlled emission factors (criteria and HAPTAP) for wood combustion in a stoker boiler from NCDAQ Wood waste Combustion Spreadsheet AP-42. Compilation of Air Pollutant Emission Factors Vol. 1 - Stationary Sources USEPA, 5th ed. Section 1.6, 9/03

The control efficiency of the wet electrostatic precipitator (WESP) for filterable particulate matter (88.9%) is applied to all metal bazardous and taxic pollutants.

The WESP employs a caustic solution in its operation in which hydrochloric acid will have high water solubility. This caustic solution will neutralize the acid and effectively control it by 90%, per conversation on 10.18/2011

with Steven A. Jansund, P.E. of Lundberg Associates, a manufacturer of WESPs.

Chromic acid is a subset of chrome compounds, which is accounted for seperately as a HAP. As such, chromic acid is only calculated as a TAP.

Emergency Generator Emissions (ES-EG)

Equipment and Fuel Characteristics

Engine Output	0.26	MW
Engine Power	350	hp (brake)
Hours of Operation	500	hr/yr ¹
Heating Value of Diesel	19,300	Btu/lb
Power Conversion	2,545	Btu/hr/hp

Criteria Pollutant Emissions

				Potential Em	issions
Pollutant	Category	Emission Factor	Units	lb/hr	tpy
TSP	PSD	4.41E-04	lb/kW-hr (2)	0.12	2.88E-02
PM ₁₀	PSD	4.41E-04	lb/kW-hr (2)	0.12	2.88E-02
PM _{2.5}	PSD	4.41E-04	lb/kW-hr (2)	0.12	2.88E-01
NO _x	PSD	8.82E-03	lb/kW-hr (5)	2.30	5.75E-0
SO_2	PSD	15	ppmw (3)	1.38E-03	3.46E-0
CO	PSD	7.72E-03	lb/kW-hr (2)	2.01	5.03E-0
VOC (NMHC)	PSD	2.51E-03	lb/MMBtu (4)	2.24E-03	5.59E-0
Acetaldehyde	HAP/TAP	5.37E-06	lb/hp-hr (4)	1.88E-03	4.70E-0
Acrolein	HAP/TAP	6.48E-07			4.70E-0
				2.275.01	5 67E 0
Benzene	НАР/ТАР		lb/hp-hr (4)	2.27E-04	5.67E-0
Benzene Benzo(a)pyrene ⁶	НАР/ТАР НАР/ТАР	6.53E-06	lb/hp-hr (4)	2.29E-03	5.71E-0
Benzo(a)pyrene ⁶	HAP/TAP	6.53E-06 1.32E-09	lb/hp-hr (4) lb/hp-hr (4)	2.29E-03 4.61E-07	5.71E-0 1.15E-0
	НАР/ТАР НАР/ТАР	6.53E-06 1.32E-09 2.74E-07	lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4)	2.29E-03 4.61E-07 9.58E-05	5:71E-0 1.15E-0 2.39E-0
Benzo(a)pyrene ⁶ 1,3-Butadiene	HAP/TAP	6.53E-06 1.32E-09 2.74E-07 8.26E-06	lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4)	2.29E-03 4.61E-07 9.58E-05 2.89E-03	5.71E-0 1.15E-0 2.39E-0 7.23E-0
Benzo(a)рутепе ⁶ 1,3-Butadiene Formaldehyde	НАР/ТАР НАР/ТАР НАР/ТАР НАР	6.53E-06 1.32E-09 2.74E-07 8.26E-06 1.18E-06	lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4)	2.29E-03 4.61E-07 9.58E-05 2.89E-03 4.12E-04	5.71E-0 1.15E-0 2.39E-0 7.23E-0 1.03E-0
Benzo(a)pyrene ⁶ 1,3-Butadiene Formaldehyde Total PAH (POM) Toluene	HAP/TAP HAP/TAP HAP/TAP	6.53E-06 1.32E-09 2.74E-07 8.26E-06 1.18E-06 2.86E-06	lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4) ib/hp-hr (4)	2.29E-03 4.61E-07 9.58E-05 2.89E-03 4.12E-04 1.00E-03	5.71E-0 1.15E-0 2.39E-0 7.23E-0 1.03E-0 2.51E-0
Benzo(a)pyrene ⁶ 1,3-Butadiene Formaldehyde Total PAH (POM)	НАР/ТАР НАР/ТАР НАР/ТАР НАР НАР/ТАР	6.53E-06 1.32E-09 2.74E-07 8.26E-06 1.18E-06	lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4) lb/hp-hr (4)	2.29E-03 4.61E-07 9.58E-05 2.89E-03 4.12E-04	5.71E-0 1.15E-0 2.39E-0 7.23E-0 1.03E-0

Note:

¹ NSPS allows for only 100 hrs/yr of non-emergency operation of these engines (not the 500 hours shown). The PTE for the emergency generator is based on 500 hr/yr, though, because the regs allow non-emergency operation and EPA guidance is 500 hr/yr for emergency generators.

² Emissions factors from NSPS Subpart IIII (or 40 CFR 89.112 where applicable) in compliance with post-2009 construction.

³ Sulfur content in accordance with Year 2010 standards of 40 CFR 80.510(a) as required by NSPS Subpart IIII.

⁴ Emission factor obtained from AP-42 Section 3.3, Tables 3.3-1 Table 3.3-2.

⁵ Emission factor for NOx is listed as NOx and NMHC (Non-Methane Hydrocarbons or VOC) in Table 4 of NSPS Subpart IIII. Conservatively assumed entire limit attributable to NOx.

⁶ Benzo(a)pyrene is included as a HAP in Total PAH.

Firewater Pump Emissions (ES-FWP)

Equipment and Fuel Characteristics

Engine Output	0.22	MW
Engine Power	300	hp
Hours of Operation	500	hr/yr ¹
Heating Value of Diesel	19,300	Btu/lb
Power Conversion	2,545	Btu/hr/hp

Criteria Pollutant Emissions

				Potential Em	nissions
Pollutant	Category	Emission Factor	Units	lb/hr	tpy
TSP	PSD	4.41E-04	lb/kW-hr (2)	0.10	2.47E-02
PM ₁₀	PSD	4.41E-04	lb/kW-hr (2)	0.10	2.47E-02
PM _{2.5}	PSD	4.41E-04	lb/kW-hr (2)	0.10	2.47E-02
NO _x	PSD	8.82E-03	lb/kW-hr (5)	1.97	4.93E-01
SO_2	PSD	15	ppmw (3)	1:19E-03	2.97E-04
CO	PSD	7.72E-03	lb/kW-hr (2)	1.73	4.32E-01
VOC (NMHC)	PSD	2.51E-03	lb/MMBtu (4)	1.92E-03	4.79E-04
Acetaldehyde			lb/hp-hr (4)		
Acetaldehyde	HAP/TAP	5.37E-06	lb/hp-hr (4)	1.61E-03	4.03E-04
Acrolein	HAP/TAP	6.48E-07	lb/hp-hr (4)	1.94E-04	4.86E-05
Benzene	HAP/TAP	6.53E-06	lb/hp-hr (4)	1.96E-03	4.90E-04
Benzo(a)pyrene ⁶	HAP/TAP	1.32E-09	lb/hp-hr (4)	3.95E-07	9.87E-08
1,3-Butadiene	НАР/ТАР	2.74E-07	lb/hp-hr (4)	8.21E-05	2.05E-05
Formaldehyde	HAP/TAP	8.26E-06	lb/hp-hr (4)	2.48E-03	6.20E-04
Total PAH (POM)	HAP	1.18E-06	lb/hp-hr (4)	3.53E-04	8.82E-05
Toluene	HAP/TAP	2.86E-06	lb/hp-hr (4)	8.59E-04	2.15E-04
Xylene	HAP/TAP	2.00E-06	lb/hp-hr (4)	5.99E-04	1.50E-04
Highest HAP (Formaldehyde)		8.26E-06	lb/hp-hr (4)	2.48E-03	6.20E-04
Total HAPs				8.13E-03	2.03E-03

Note

¹ NSPS allows for only 100 hrs/yr of non-emergency operation of these engines (not the 500 hours shown). The PTE for the emergency generator is based on 500 hr/yr, though, because the regs allow non-emergency operation and EPA guidance is 500 hr/yr for emergency generators.

² Emissions factors from NSPS Subpart IIII (or 40 CFR 89.112 where applicable) in compliance with post-2009 construction.

³ Sulfur content in accordance with Year 2010 standards of 40 CFR 80.510(a) as required by NSPS Subpart IIII.

⁴ Emission factor obtained from AP-42 Section 3.3, Tables 3.3-1 Table 3.3-2.

⁵ Emission factor for NOx is listed as NOx and NMHC (Non-Methane Hydrocarbons or VOC) in Table 4 of NSPS Subpart IIII. Conservatively assumed entire limit attributable to NOx.

⁶ Benzo(a)pyrene is included as a HAP in Total PAH.

Potential GHG Emissions

Operating Data:

207.00 MMBtu/hr 8,760 hrs/yr Dryer Heat Input Operating Schedule

350 bhp 500 hrs/yr Emergency Generator Output Operating Schedule

16.7 gal/hr¹ No. 2 Fuel Input

2.282 MMBtu/hr² Energy Input

300 bhp 500 hrs/yr Fire Water Pump Output

14.3 gal/hr1 Operating Schedule No. 2 Fuel Input

1.956 MMBtu/hr² Energy Input

Emission Unit ID	Fuel Type	Emission Fa	Emission Factors from Table C-1 (kg/MMBtu)	(kg/MMBtu) ³	ĮĮ.	er 1 Emission	Tier 1 Emissions (metric tons)	(\$1
		C02	CH4	N2O	C02	CH4	N20	N2O Total CO2e
ES-DRYER	Wood and Wood Residuals	9.38E+01	3.20E-02	4.20E-03	187,490	64	20	187,562
ES-GN	No. 2 Fuel Oil (Distillate)	7.40E+01	3.00E-03	6.00E-04	93	3.77E-03	3.77E-03 7.55E-04	93
ES-FWP	No. 2 Fuel Oil (Distillate)	7.40E+01	3.00E-03	6,00E-04	80	3.23E-03	3,23E-03 6.47E-04	80

¹ Fuel consumption calculated using a factor of 0.0476 gal/hr-hp. Advanced Environmental Interface, Inc. (1998).

General Permits for Emergency Engines. INSIGHTS, 98-2, 3.

 $^{^2}$ Energy calculated on a fuel consumption basis, using an energy factor of $0.137\,\mathrm{MMBtu/gal.}$

³ Emission factors from Table C-1 and C-2 of GHG Reporting Rule. Emission factors for methane and N2O already multiplied by their respective GWPs of 21 and 310.

ATTACHMENT 2 Air Dispersion Modeling

North Carolina Modeling Protocol Checklist

The North Carolina Modeling Protocol Checklist may be used in lieu of developing the traditional written modeling plan for North Carolina toxics and criteria pollutant modeling. The protocol checklist is designed to provide the same level of information as requested in a modeling protocol as discussed in Chapter 2 of the *Guideline for Evaluating the Air Quality Impacts of Toxic Pollutants in North Carolina*. The modeling protocol checklist is submitted with the modeling analysis.

Although most of the information requested in the modeling protocol checklist is self explanatory, additional comments are provided, where applicable, and are discussed in greater detail in the toxics modeling guidelines referenced above. References to sections, tables, figures, appendices, etc., in the protocol checklist are found in the toxics modeling guidelines.

INSTRUCTIONS: The modeling report supporting the compliance demonstration should include most of the information listed below. As appropriate, answer the following questions or indicate by check mark the information provided or action taken is reflected in your report.

FACIL	ITY INFORMATION					
Name: Enviva Pellets Northampton, LLC Facility ID: New Facility - TBD Address: Lebanon Church Road (Street Number TBD)	Consultant (if applicable): Trinity Consultants One Copley Parkway Suite 310 Morrisville, NC 27560					
Contact Name: Glenn Gray	Contact Name: Joe Sullivan					
Phone Number: (804) 412-0227 Email: Glenn. Gray@intrinergy.com	Phone Number: (919) 462-9693 Email: jhill@trinityconsultants.com					
	GENERAL					
Description of New Source or Source / Process modified source(s) and a brief discussion of how this cha	s Modification: provide a short description of the new or nge affects facility production or process operation.	Х				
Source / Pollutant Identification: provide a table of type (point, area, or volume), maximum pollutant emission sources, indicate if the stack is capped or non-vertical (C/N	f the affected pollutants, by source, which identifies the source in rates over the applicable averaging period(s), and, for point N).	X				
Pollutant Emission Rate Calculations: indicate mass balance, etc.) and where applicable, provide the calculations.	e how the pollutant emission rates were derived (e.g., AP-42, culations.	Х				
sources, buildings or structures, public right-of-ways, and	ing showing the location of all existing and proposed emission d the facility property (toxics) / fence line (criteria pollutants) e north indicator, and the UTM or latitude/longitude of at least	Х				
Certified Plat or Signed Survey: a certified plat (must be submitted to validate property boundaries model	(map) from the County Register of Deeds or a signed survey ed.	SS				
Topographic Map: A topographic map covering appracility boundaries should be annotated on the map as according to the map as a contract to the map as a contra	proximately 5km around the facility must be submitted. The curately as possible.	Х				
region of influence extending to one or more sources mod	ity impact analysis must be conducted for all structures with a deled to determine if cavity regions extend off property separate cavity analysis is required if using AERMOD. See	N/A				

GENERAL (continued)	
Background Concentrations (criteria pollutant analyses only): Background concentrations must be determined for each pollutant for each averaging period evaluated. The averaged background value used (e.g., high, high-second-high, high-third-high, etc.) is based on the pollutant and averaging period evaluated. The background concentrations are added to the modeled concentrations, which are then compared to the applicable air quality standard to determine compliance.	N/A
Offsite Source Inventories (criteria pollutant analyses only): Offsite source inventories must be developed and modeled for all pollutants for which onsite sources emissions are modeled in excess of the specific pollutant significant impact levels (SILs) as defined in the PSD New Source Review Workshop Manual. The DAQ AQAB must approve the inventories. An initial working inventory can be requested from the AQAB.	N/A

SCREEN LEVEL MODELING	
Model : The latest version of the SCREEN3 model must be used until AERSCREEN is developed and approved. The use of other screening models should be approved by NCDAQ prior to submitting the modeling report.	N/A
Source / Source emission parameters : Provide a table listing the sources modeled and the applicable source emission parameters. See NC Form 3 – Appendix A.	N/A
Merged Sources: Identify merged sources and show all appropriate calculations. See Section 3.3	N/A
GEP Analysis: SCREEN3 – for each source modeled, show all calculations identifying the critical structure used in the model run. See section 3.2 and NC Form 1 - Appendix A.	N/A
Cavity Impact Analysis: A cavity impact analysis using SCREEN3 must be conducted for all structures with a region of influence extending to one or more sources modeled to determine if cavity regions extend off property (toxics) or beyond the fence line (criteria pollutants). See Section 4.2	N/A
Terrain: Indicate the terrain modeled: simple (Section 4.4), and complex (Section 4.5 and NC Form 4 – Appendix A). If complex terrain is within 5 kilometers of the facility, complex terrain must be evaluated. Simple terrain must include terrain elevations if any terrain is greater than the stack base of any source modeled.	N/A
Simple: Complex:	
Meteorology: In SCREEN3, select full meteorology.	N/A
Receptors : SCREEN3 – use shortest distance to property boundary for each source modeled and use sufficient range to find maximum (See Section 4.1 (i) and (j)). Terrain above stack base must be evaluated.	N/A
Modeling Results: For each affected pollutant, modeling results should be summarized, converted to the applicable averaging period (See Table 3), and presented in tabular format indicating compliance status with the applicable AAL, SIL or NAAQS. See NC Form S5 – Appendix A.	N/A
Modeling Files: Either electronic or hard copies of SCREEN3 output must be submitted.	N/A

REFINED LEVEL MODELING	
Model : The latest version of AERMOD should be used, and may be found at http://www.epa.gov/scram001/dispersion_prefrec.htm. The use of other refined models must be approved by NCDAQ prior to submitting the modeling report.	Х
Source / Source emission parameters : Provide a table listing the sources modeled and the applicable source emission parameters. <i>See NC Form 3 - Appendix A</i> .	х
GEP Analysis: Use BPIP-Prime with AERMOD.	Х
Cavity Impact Analysis: No separate cavity analysis is required when using AERMOD as long as receptors are placed in cavity susceptible areas. See Section 4.2 and 5.2.	N/A
Terrain : Use digital elevation data from the USGS NED database (http://seamless.usgs.gov/index.php). Use of other sources of terrain elevations or the non-regulatory Flat Terrain option will require prior approval from DAQ AQAB.	Х
Coordinate System: Specify the coordinate system used (e.g., NAD27, NAD83, etc.) to identify the source, building, and receptor locations. Note: Be sure to specify in the AERMAP input file the correct base datum (NADA) to be used for identifying source input data locations. Clearly note in both the protocol checklist and the modeling report which datum was used.	Х
Receptors: The receptor grid should be of sufficient size and resolution to identify the maximum pollutant impact. <i>See Section 5.3.</i>	Х
Meteorology : Indicate the AQAB, pre-processed, 5-year data set used in the modeling demonstration: (See Section 5.5 and Appendix B)	
AERMOD 1988-1992 Raleigh-Durham / Greensboro If processing your own raw meteorology, then pre-approval from AQAB is required. Additional documentation files (e.g. AERMET stage processing files) will also be necessary. For NC toxics, the modeling demonstration requires only the last year of the standard 5 year data set (e.g., 2005) provided the maximum impacts are less than 50% of the applicable AAL(s).	Х
Modeling Results: For each affected pollutant and averaging period, modeling results should be summarized and presented in tabular format indicating compliance status with the applicable AAL, SIL or NAAQS. See NC Form R5 - Appendix A.	Х
Modeling Files: Submit input and output files for AERMOD. Also include BPIP-Prime files, AERMAP files, DEM files, and any AERMET input and output files, including raw meteorological data.	X

MODELING INPUTS

AERMOD ID	Stack Ht. (m)	Stack Temp. (K)	Stack Vel. (m/s)	Stack Diam. (m)
DRYER	30.48	349.82	20.58	2.26
FWPSTACK	2.13	785.37	109.18	0.08
EMERGEN	1.52	766.48	78.30	0.10

Pollutant	EG Emission Rate (g/s)	FWP Emission Rate (g/s)	Dryer Emission Rate (g/s)
Arsenic	0.000E+00	0.000E+00	4.164E-05
Benzo(a)pyrene	5.809E-08	4.979E-08	6.787E-05
Cadmium	0.000E+00	0.000E+00	7.760E-06
Chlorine	0.000E+00	0.000E+00	2.062E-02
Hexachlorodibenzo-p-dioxin	0.000E+00	0.000E+00	4.177E-05
Hydrogen Chloride	0.000E+00	0.000E+00	4.960E-02
Mercury	0.000E+00	0.000E+00	9.137E-05
Nickel	0.000E+00	0.000E+00	8.615E-04
Vinyl Chloride	0.000E+00	0.000E+00	4.699E-04

FINAL MODELING RESULTS

	Averaging	Max. Modeled Impact	Date/Time of Impact	Location o	f Maximum	AAL	% of AAL	
Pollutant	Period	(μg/m³)	(YYMMDDHH)	UTM-E (m) UTM-N (m)		$(\mu g/m^3)$	(%)	
Arsenic	Annual	1.00E-05	1992	266,073.2	4.043,369.4	2.30E-04	4.35%	
Benzo(a)pyrene	Annual	1.00E-05	1992	266,073.2	4.043,369.4	3.30E-02	0.03%	
Cadmium	Annual	0.00E+00	1992	266,073.2	4.043,369.4	5.50E-03	0.00%	
Chlorine	24-Hour	5.85E-02	92050724	265,518.8	4.042,557.8	3.75E+01	0.16%	
Hexachlorodibenzo-p-dioxin	Annual	1.00E-05	1992	266.073.2	4,043,369.4	7.60E-05	13.16%	
Hydrogen Chloride	1-Hour	2.72E-01	92080420	265,791.0	4.042,519,1	7.00E+02	0.04%	
Mercury	24-Hour	2.60E-04	92050724	265,518.8	4,042,557.8	6.00E-01	0.04%	
Nickel	I-Hour	4.73E-03	92080420	265,791.0	4.042,519.1	6.00E+00	0.08%	
Vinyl Chloride	Annual	1.00E-04	1992	266,073.2	4,043,369.4	3.80E-01	0.03%	

				(4)		*	



6680167

North Carolina Department of Environment and Natural Resources Division of Air Quality

Beverly Eaves Perdue Governor

Sheila C. Holman Director

Dee Freeman Secretary

October 13, 2011

Mr. Norb Hintz Vice President, Engineering Enviva Pellets Northampton, LLC 7200 Wisconsin Avenue, Suite 1100 Bethesda, Maryland 20814

OCT 1 4 2011

ବ୍ୟ ଅନ୍ତର

Dear Mr. Hintz:

Subject:

PSD Completeness Review

Enviva Pellets Northampton, LLC

Gaston, Northampton County, North Carolina

Reference is made to your Prevention of Significant Deterioration (PSD) preconstruction air permit application received August 26, 2011 (6600167.11A) for proposed construction of a wood pellet manufacturing facility.

In accordance with the procedures required pursuant to 15A NCAC 2D .0530(o) and 40 CFR 51.166(q), this office considers your application complete for PSD review purposes. This determination does not prevent the NCDAQ from requesting additional information regarding previously submitted materials and technical issues involved in the application.

The application has been assigned to Kevin Godwin for review. If you have any questions regarding this matter please contact Kevin at (919) 715-6255.

Sincerely,

Donald R. van der Vaart, Ph.D., J.D., P.E.

deela

Chief

c:

Patrick Butler, Supervisor, Raleigh Regional Office

Permitting Section

1641 Mail Service Center, Raleigh, North Carolina 27699-1641 2728 Capital Blvd., Raleigh, North Carolina 27604

Phone: 919-715-6235 / FAX 919-733-5317 / Internet: www.ncair.org

NorthCarolina Naturally



North Carolina Department of Environment and Natural Resources Division of Air Quality

Beverly Eaves Perdue Governor

Sheila C. Holman Director

Dee Freeman Secretary

August 29, 2011

Mr. Norb Hintz Vice President Engineering Enviva Pellets Northampton, LLC 7200 Wisconsin Avenue Suite 1100 Bethesda, MD 20814

SUBJECT: Receipt of Permit Application

Greenfield Facility

Application No. 6600167.11A Enviva Pellets Northampton, LLC

Facility ID: 6600167, Gaston, Northampton County

Dear Mr. Hintz:

Your air permit application (6600167.11A) for Enviva Pellets Northampton, LLC, located in Northampton County, North Carolina was received by this Division on August 26, 2011.

This application submittal did contain all the required elements as indicated and has been accepted for processing. Your application will be considered complete as of August 26, 2011, unless informed otherwise by this office within 60 days.

Should you have any questions concerning this matter, please contact Kevin Godwin at (919) 715-6255.

Sincerely,

Donald van der Vaart, Ph.D., P.E., J.D.

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cc: Raleigh Regional Office Files

6600167

FORM A1

FACILITY (General Information)

AUS 2 0 2011

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[\forall]	Local Zoning Consistency Determination (if required)			✓ Facility	ty Reduction & Recycling Survey Form (Form A4) A Cocation Fee						
					priate Number of Copies of Application P Seal (if required)						
			GEI	NERAL IN	FORMAT	TION					
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Enviva Pell	ets Northampton, L	LC									
911 Address	s) Line 1:	Lebanon C	Church Road (Stree	t Number T	8D)			- (1111			
ine 2:											
Gaston					State:	North Car	olina				
	278	66			County:	Northamp	ton				
e. 70.340			COI	NTACT IN	FORMAT	ION	and the state of t				
ermit/Technical Contact:											
ame/Title: Glenn Gray / Plant Manager											
Mailing Address Line 1: 7200 Wisconsin Avenue											
s Line 2:	Suite 1100										
Bethesda	State:	Maryland	Zip Code:	20814	City:		State:		Zip Code:		
a code)	(757) 274-8377	Fax No. (ar	ea code) (30	1) 657-5567	Phone No.	(area code)		Fax No. (a			
Email Address: Glenn.Gray@envivabiomass.com						ess:					
)fficial/Autl	norized Contact:				Invoice Co	ntact:					
Name/Title: Norb Hintz					Name/Title: same as permit/technical contact						
Mailing Address Line 1: 7200 Wisconsin Avenue					Mailing Address Line 1:						
Line 2:	Suite 1100										
ethesda	State:	Maryland	Zip Code:				State		Zin Code:		
a code)	(301) 657-5567	Fax No. (ar	rea code) (30°			(area code)		Fax No. (a			
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Attach Additional Sheets As Necessary

Comprehensive Application Report for 6600167.11A Enviva Pellets Northampton, LLC - Gaston (6600167)

08/29/2011

Northampton County

Permit/Latest Revision: 10203/

General Information:

Permit code:

Greenfield Facility Engineer/Rev. location: Application type:

Raleigh Regional Office Kevin Godwin/RCO Charles McEachern Regional Contact: Facility location:

Application is COMPLETE Clock is ON

Unknown

Facility classification:

In progress

Status is:

Application Dates

Clock Start Completeness Due

Calculated Issue Due

10/25/2011

08/26/2011 Received

Add. Amt Rcv'd: Date Rcv'd: initial amount: Date received: Amount Due: Fee Information

08/29/2011 Fund type:

\$13488.00

Location rec'd:

Location deposited:

Deposit Slip #:

2331

Contact Information

Norb Hintz, Vice President Engineering Glenn Gray, Plant Manager Technical/Permit Authorized

7200 Wisconsin Avenue 7200 Wisconsin Avenue

City State ZIP

Bethesda, MD 20814 Bethesda, MD 20814

(757) 274-8377 (301) 657-5567

Telephone

Acceptance Criteria

Acceptance Criteria Description Application fee Received? Yes

Appropriate number of apps submitted Zoning Addressed

Yes Yes Yes Yes

Source recycling/reduction form Authorized signature

Completeness Criteria Received?

Complete Item Description

6685167 pro

Northampton County

Comments Complete Due Start Application Events Event

Staff

Regulations Pertaining to this Permit

Reference Rule

Regulation Description

Charles McEachern <u>Editor</u> Mark Cuilla Mark Cuilla 821 (Charles McEachern) New Value PSD (PSD) 10203 Old Value GRNTV (TV-Greenfield) Audit Information Pertaining to this Application Column Name Date Changed 08/29/2011 08/29/2011 08/29/2011 perm_Code permit_No reg_Cont

AUG 3 0 2011

Air Quality Construction and Operating TING PERMIT APPLICATION CO Volume I Enviva Pellets Northampton, LLC • Gaston, North Carolina

Prepared by:

TRINITY CONSULTANTS

One Copley Parkway, Suite 310 Morrisville, North Carolina 27560 919.463.9693 Fax: 919.462.9694

trinityconsultants.com

Prepared for:

ENVIVA PELLETS NORTHAMPTON, LLC Lebanon Church Rd. Gaston, NC 27832

August 2011

Project 113401.0047



AIR QUALITY CONSTRUCTION AND OPERATING PERMIT APPLICATION VOLUME I ENVIVA PELLETS NORTHAMPTON, LLC • GASTON, NORTH CAROLINA

Prepared by:

AUG ? (1 201)

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Prepared for:

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August 2011

Project 113401.0047



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APPENDIX A – NCDAQ APPLICATION FORMS

APPENDIX B – EMISSIONS CALCULATIONS

APPENDIX C - LOCAL ZONING CONSISTENCY DETERMINATION

1.1 EXECUTIVE SUMMARY

Enviva Pellets, LLC (Enviva) is planning to construct and operate a wood pellets manufacturing plant in the town of Gaston, NC.

The proposed plant consists of the following:

- A raw material receiving and processing yard;
- Wood handling equipment;
- One 207 mmBtu/hr green wood direct-fired dryer system with pollution control equipment consisting of a cyclone dust collector and wet electrostatic precipitator (WESP) for particulate matter abatement;
- Four hammermills controlled by fabric filtration systems;
- Wood pellet coolers controlled via cyclones;
- A wood pellet storage silo;
- An emergency electric generator; and
- Fire water pump.

Air emission sources and associated pollution controls are described in detail in Section 2.

This document in its entirety comprises an air quality construction and operating permit application for the project. The project will result in air emissions increases of various compounds that exceed the thresholds triggering the Prevention of Significant Deterioration (PSD) preconstruction permitting program, as well as certain other federal and state regulations. This application fully conforms to all permitting requirements and demonstrates compliance in accordance with those requirements. It should be noted that the project will not cause or contribute to violations of the National and State Ambient Air Quality Standards (NAAQS and SAAQS) and PSD Increments, will not result in adverse impacts to federally protected Class I areas, and will utilize Best Available Control Technology (BACT) for each compound subject to PSD review.

In addition to application report Sections 1 through 6, key elements of this application are provided as the following appendices to this report:

- 1. Permit application forms (Appendix A);
- 2. Emissions calculations (Appendix B); and
- 3. Local Zoning Consistency determination (Appendix C).

Six copies of the application addendum have been provided and two electronic copies of the air dispersion modeling-related files have also been provided.

1.2 ORGANIZATION OF APPLICATION

Six copies of the application have been provided along with the \$13,488 permit application processing fee. This application consists of two (2) volumes, comprised of the following:

Volume I:

- Section 1 provides an Executive Summary,
- Section 2 provides a project description and discusses air emissions,
- Section 3 discusses regulatory applicability, and
- Section 4 summarizes the BACT analysis.
- Appendix A contains air permit application forms,
- Appendix B presents air emissions calculations, and
- Appendix C contains the required local zoning consistency determination.

Volume II: Air Dispersion Modeling Report.

The proposed wood pellets plant is designed to produce up to 500,000 tons per year of wood pellets, assuming a residual 5 percent weight (wt %) moisture content of the pellets. Pellets will typically consist of pressed hardwoods, but could contain up to 10 percent softwoods on an annual basis. This section discusses the Northampton Plant's pelletizing process and associated air emissions. Detailed air emissions calculations are presented for each source discussed in this section in Appendix B. A process flow diagram is presented in Figure 2-1.

2.1 GREEN CHIPPED WOOD HANDLING AND SIZING (ES-GWHS), LOG DEBARKING AND CHIPPING (ES-CHIP-1) AND FUEL STORAGE BIN (ES-GWFB)

"Green" (i.e., wet) wood will be delivered to the facility via trucks as either pre-chipped wood or whole logs (for on-site chipping). Pre-chipped wood will be screened and oversized chips will undergo additional chipping. Whole logs will be chipped and debarked to specification for drying in the on-site electric-powered chipper (ES-CHIP-1). Chipped wood for drying is conveyed to wood storage while wood/bark is conveyed to a green wood dryer fuel storage bin (ES-GWFB).

Green wood contains a high moisture content approaching 50 percent by weight and handling operations for wet wood therefore has negligibly small emissions. The moisture content of wet wood is well above the applicability range of aggregate handling emissions estimation methodologies provided in AP-42, so no emission calculations are included for green wood transfer points.

Emissions estimates for ES-CHIP-1 are based on limited emission factors available for wood chipping. As shown in the attached emissions calculations (Appendix B), VOC emissions from the chipper are calculated using emission factors from NCASI technical bulletins. Methanol emissions are also calculated using factors from AP-42 Sections 10.6.3 and 10.6.4. Particulate matter (PM) emissions will be negligible from the green wood chipper because the exhaust is directed downward towards the ground.

2.2 WOOD DRYER (ES-DRYER)

Green wood is conveyed to a single rotary dryer system. Direct contact heat is provided to the system via a 207 mmBtu/hr total heat input burner system. Air emissions are controlled by a cyclone for bulk particulate removal and additional particulate is removed utilizing a wet electrostatic precipitator (WESP) operating after the cyclones.

Emissions are calculated using a combination of dryer vendor emission guarantees (criteria pollutants only) and AP-42 emissions factors.

¹ NCASI Technical Bulletins containing emission factors for wood-chipping were provided to Trinity Consultants by South Carolina Department of Health and Environmental Control (SC DHEC) in the course of developing emissions for an electric powered chipper.

2.3 DRIED AND SIZED WOOD HANDLING (ES-DWH)

Dried materials are transferred from the dryer via conveyors to hammermills for further size reduction prior to pelletization. In total there are four uncontrolled dried wood transfer points, two occurring prior to the hammermills and two after the hammermills.

The following dried wood transfer points are included in this emissions grouping:

- Drop Point 1 (DP1): Dryer discharger to dryer collection conveyor belt
- DP2: Pre-screen feeder fines overs to hammermills infeed and distribution
- DP3: Hammermills cyclone diverter gates to hammermills system discharge collection conveyor belt
- DP4: Hammermills system discharge collection conveyor belt to pellet mill feed silo infeed screw

As shown in the calculations in Appendix B, emissions from any source within the Dried and Sized Wood Handling emission grouping are insignificant.

2.4 HAMMERMILLS (ES-HM-1, -2, -3, -4)

Prior to pellitization, dried materials are reduced to the appropriate size needed for pelletization using four hammermills operating in parallel. A conveyor system receives the ground wood from the hammermills and sends the ground wood to to the pellet mill feed silo.

Particulate emissions from the hammermills are controlled using four cyclones in series with two bagfilters. A third bagfilter located in the hammermills area controls fugitive dust emissions from a variety of sources (discussed in a separate section to follow). Appendix B summarizes the emissions from each hammermill bagfilter system.

2.5 HAMMERMILL AREA FILTER

A number of dried- and sized-wood transport and transfer point emissions sources are controlled by the Hammermill Area Filter baghouse. Sources controlled by this bagfilter include, but are not limited to, the following sources (indicated by alphabetical designations prescribed in Figure 2-1):

- A, B, C, & D: Emissions from the four dry hammermill metering bins
- E: Hammermills infeed and distribution transfer
- F: Pellet cooler transfer (particulate emissions from pellet cooler cyclones large enough to drop out of entrainment) & pellet screening
- G: Hammermill pre-screen feeder emissions
- H: Pellet screen fines cyclone

Emissions from this bagfilter are calculated assuming an average grain loading factor for the wood particulates and the maximum nominal stack flow rate.

2.6 PELLET MILL FEED SILO (ES-PMFS)

Sized wood from the hammermills is transported on a set of conveyors to the infeed screw for the pellet mill feed silo prior to pelletization. Emissions from the Pellet Mill Feed Silo are controlled using a separate bagfilter.

2.7 PELLET PRESS SYSTEM AND CONVEYORS (ES-PP)

Dried ground wood is mechanically compacted in the presence of water in several screw presses in the Pellet Press System. Exhaust from the Pellet Press and Pellet Presses conveyors are vented to the atmosphere with negligible particulate matter emissions, as shown in Appendix B. No chemical binding agents are needed for pelletization.

2.8 Pellet Coolers (ES-CLR)

Pellet Press conveyors discharge wood pellets through one of six Pellet Coolers. Cooling air is passed through the pellets. At this point, the Pellets contain a small amount of wood fines, which are swept out with the cooling air and are controlled utilizing three cyclones operating in parallel (one for each two coolers) prior to discharge to the atmosphere.

2.9 FINISHED PRODUCT HANDLING (ES-FPH)

Pelletized product is conveyed to storage and load-out operations with no air emissions to the atmosphere.

2.10 EMERGENCY GENERATOR (ES-EG), FIRE WATER PUMP (ES-FWP) AND ASSOCIATED FUEL OIL STORAGE TANKS

The plant will utilize a 350 brake horsepower emergency generator for emergency operations and a 300 brake horsepower fire water pump engine. Both engines will combust diesel fuel. Aside from maintenance and readiness testing, these sources will only be utilized for emergency operations. Diesel for the emergency generator will be stored in up to a 2,500 gallon storage tank and diesel for the fire water pump will be stored in up to a 500 gallon storage tank. Emissions from both fuel oil storage tanks are insignificant.

This section summarizes the applicability and requirements of key federal and state regulations.

3.1 FEDERAL REGULATIONS

3.1.1 PREVENTION OF SIGNIFICANT DETERIORATION (PSD), 40 CFR PART 51.166

North Carolina has implemented most of the federal PSD requirements of 40 CFR 51.166 under North Carolina Regulation 15A NCAC 2D .0530. Under the PSD regulations, a major stationary source for PSD is defined as any source in one of the 28 named source categories with the potential to emit 100 tpy or more of any regulated pollutant, or any source not in one of the 28 named source categories with the potential to emit 250 tpy or more of any regulated pollutant other that GHGs.² Neither wood pellet production nor operation of associated combustion sources qualifies the facility for classification in one of the 28 listed source categories.

Federal PSD requirements for GHGs have been implemented in North Carolina under 15A NCAC 2D .0544, which essentially adopts the U.S. EPA's "GHG Tailoring Rule." The GHG Tailoring Rule establishes higher emission rates triggering PSD review for GHGs with the major source threshold being 100,000 tpy of CO₂ equivalent (CO₂e) and a significant emission rate of 75,000 tpy CO₂e.

As shown in Table 3-1, the proposed project constitutes a major stationary source of CO, VOC and CO₂e. In addition, the facility exceeds the PSD significant emission rates (SERs) for PM, NO_x, and VOC. Therefore, Enviva is submitting this PSD construction and operating permit application in accordance with all federal and state PSD requirements.

3.1.2 TITLE V OPERATING PERMIT PROGRAM, 40 CFR PART 70

40 CFR Part 70 establishes the federal Title V operating permit program. North Carolina has incorporated the provisions of this federal program in its Title V operating permit program under 15A NCAC 2Q .0500. The major source thresholds with respect to the North Carolina Title V operating permit program regulations are 10 tons per year of a single HAP, 25 tpy of any combination of HAP, and 100 tpy of certain other regulated pollutants.

The site will be a major Title V source for only criteria pollutants. Enviva is requesting that the procedures of 15A NCAC 2Q .0504 be applied to this project allowing direct issuance of a construction and operating permit under 15A NCAC 2D .0300. Enviva will submit a permit application for a Title V permit within one year after commencement of operation.

² 40 CFR §52.21(b)(1)(i)

3.1.3 NEW SOURCE PERFORMANCE STANDARDS, 40 CFR PART 60 (15A NCAC 2D .0524 NEW SOURCE PERFORMANCE STANDARDS)

New Source Performance Standards (NSPS), located in 40 CFR Part 60 and implemented in North Carolina Regulation 15A NCAC 2D .0524, require certain categories of new, modified, or reconstructed sources to control emissions to specified levels. Three potentially applicable NSPS are addressed below.

3.1.3.1 NSPS SUBPART IIII

NSPS Subpart IIII applies to owners or operators of compression ignition (CI) internal combustion engines (ICE) manufactured after April 1, 2006 that are not fire pump engines, and fire pump engines manufactured after July 1, 2006. As noted in Section 2, the plant will have a 350 hp emergency generator and a 300 hp fire pump. The emergency generator and fire pump will be manufactured after the dates specified above. Therefore, the emergency generator and fire pump are subject to the provisions of NSPS Subpart IIII.

Under NSPS Subpart IIII, owners and operators of emergency generators manufactured in CY 2007 or later with a maximum engine power greater than or equal to 50 hp are required to comply with the emission limits referenced in 40 CFR §60.4205(b). These limits are as follows: 0.20 g/kW for PM, 3.5 g/kW for CO, and 4 g/kW for NO_x + nonmethane hydrocarbons (NMHC).

Enviva will comply with the emission limits by operating the generator as instructed in the manufacturer's operating manual in accordance with 40 CFR §60.4211(a), and purchasing an engine certified to meet the referenced emission limits in accordance with 40 CFR §60.4211(c). The engine will be equipped with a non-resettable hour meter in accordance with 40 CFR §60.4209(a). Emergency and readiness testing of the unit will be limited to 100 hours per year.

In accordance with NSPS Subpart IIII, owners and operators of fire pump engines manufactured after July 1, 2006 must comply with the emission limits in Table 4 of NSPS Subpart IIII, which are organized based on the size of the unit. These limits are as follows: 0.20 g/kW for PM, 3.5 g/kW for CO, and 4 g/kW for NO_x + nonmethane hydrocarbons (NMHC).

Enviva will comply with these emission limits by operating the fire pump as instructed in the manufacturer's operating manual in accordance with 40 CFR §60.4211(a), and purchasing an engine certified to meet the referenced emission limits in accordance with 40 CFR §60.4211(b). The engine will be equipped with a non-resettable hour meter in accordance with 40 CFR §60.4209(a). Emergency and readiness testing of the unit will be limited to 100 hours per year.

In addition, both the proposed emergency generator and fire pump will be required to comply with the fuel requirements in 40 CFR §60.4207, which limit sulfur to a maximum of 15 ppmw and a cetane index of at least 40.

3.1.3.2 NSPS SUBPARTS DB AND KB

The proposed plant will utilize direct fired drying of chipped wood and, therefore, will not trigger the NSPS Subpart Db (Industrial-Commercial-Institutional Steam Generating Units) regulations. Diesel fuel oil storage tank capacities are well below the NSPS Subpart Kb (Volatile Organic Liquid Storage Vessels, for which construction, reconstruction, or modification commenced after 7/23/1984) applicability storage capacity threshold of approximately 20,000 gallons.

3.1.4 NATIONAL EMISSION STANDARDS FOR HAZARDOUS AIR POLLUTANTS, 40 CFR PART 63 (15A NCAC 2D .1111 MAXIMUM ACHIEVABLE CONTROL TECHNOLOGY)

The National Emission Standards for Hazardous Air Pollutants (NESHAP) listed in 40 CFR Part 63 and implementing North Carolina regulation 15A NCAC 2D .1111 are source category-specific regulations that limit emissions of HAPs. Two potentially applicable NESHAPs are addressed below.

3.1.4.1 40 CFR PART 63 SUBPART ZZZZZ

40 CFR 63 Subpart ZZZZ applies to reciprocating internal combustion engines (RICE) located at a major or area source of HAP emissions. An affected source is any existing, new, or reconstructed stationary RICE located at a major or area source of HAP emissions. Emergency power and limited use units are subject to limited requirements under 40 CFR 63.6590(b)(i) and 40 CFR 63.6590(b)(ii). Emergency stationary RICE are defined in 40 CFR 63.6675 as any stationary RICE that operates in an emergency situation. These situations include engines used for power generation when power from the local utility is interrupted, or engines used to pump water in the case of fire or flood.

The proposed emergency generator and the emergency fire pump at the site will be classified as emergency stationary RICE under the NESHAP and will comply with the requirements listed under this subpart.

3.1.4.2 40 CFR PART 63 SUBPART DDDD

40 CFR Subpart DDDD applies to Plywood and Composite Wood Products facilities classified as major sources of hazardous air pollutants (HAPs), having the potential to emit of 10 tons per year of a single HAP or 25 tons per year aggregate HAP. As indicated in Table 3-2, facility-wide potential HAP emissions are less than the major source threshold.

3.2 NORTH CAROLINA REGULATIONS

For the sources that are included for review in this application package, the North Carolina State Implementation Plan (SIP) rules and regulations have been evaluated for applicability. Applicable rules are identified below.

3.2.1 15A NCAC 02D .0515 PARTICULATES FROM MISCELLANEOUS INDUSTRIAL PROCESSES

Particulate emissions from all emissions sources subject to permitting, including the wood pellet dryer are regulated under 15A NCAC 2D .0515. This regulation limits the particulate emissions based on total throughput. This regulation limits the particulate emissions based on process throughput using the equation $E = 4.10 \times P^{0.67}$, for process rates (P) less than 30 tons per hour (ton/hr) and $E = 55 \times P^{0.11}$ -40 for process rates greater than 30 tons per hour.

All emissions from particulate matter sources are either negligible or well-controlled. The most significant emission unit at the site, the process dryer operating a 61.5 ODT/hr, has an emission limit of 46.5 lb/hr. Maximum emissions from the dryer are approximately 8.5 lb/hr, well below the standard.

3.2.2 15A NCAC 02D .0516 SULFUR DIOXIDE EMISSIONS FROM COMBUSTION SOURCES

Under this regulation, emissions of sulfur dioxide from combustion sources cannot exceed 2.3 pounds of sulfur dioxide per million Btu input. Wood is fired in the dryer and low sulfur diesel is combusted in the two emergency engines, resulting in operation well below regulatory limits.

3.2.3 15A NCAC 02D .0521 CONTROL OF VISIBLE EMISSIONS

Under this regulation, for sources manufactured after July 1, 1971, visible emissions cannot be more than 20 percent opacity when averaged over a six-minute period. However, six-minute averaging periods may exceed 20 percent opacity under the following conditions:

- No six-minute period exceeds 87 percent opacity,
- No more than one six-minute period exceeds 20 percent opacity in any hour, and
- No more than four six-minute periods exceed 20 percent opacity in any 24-hour period.

This rule applies to all processes that may have a visible emission, including the dryer, other particulate matter emissions sources controlled by cyclone and/or baghouse, and the diesel-fired engines.

3.2.4 15A NCAC 02Q .0700 TOXIC AIR POLLUTANT PROCEDURES

This regulation requires that new and modified sources of toxic air pollutants with emissions exceeding specified de minimis values apply for an air toxics permit. Facility-wide emissions of several compounds emitted from the site exceed the permitting de minimis level. A comparison of emissions to de minimis values are summarized in Table 3-3. Modeling for compounds triggering permitting is discussed in Volume 2 of this application.

4.1 Introduction

Any major stationary source or major modification subject to PSD must conduct an analysis to ensure the use of "best available control technology" (BACT). BACT is an emission limitation for NSR-regulated pollutants that applies to each individual new emission unit at a major stationary source when the project, in its entirety, has a significant net emissions increase for that pollutant. Significant emissions thresholds are set forth in 40 C.F.R. §52.21(b)(23). Individual BACT determinations are performed on a unit-by-unit, pollutant-by-pollutant basis taking into account energy, environmental, and economic impacts. This numerical limit can be based on the application of air pollution equipment or specific production processes, methods, systems, or techniques.

4.1.1 APPLICABILITY

The proposed plant is a major PSD source as described in Section 3. The compounds subject to PSD review and for which a BACT analysis is required are:

- Nitrogen oxides (NO_x),
- Particulate matter (PM/PM₁₀/PM_{2.5}),
- Carbon monoxide (CO),
- Volatile organic compounds (VOC), and
- Carbon dioxide equivalent (CO₂e).

The emission units and compounds for which a BACT analysis is required are listed below:

Regulated NSR Pollutants	Dryer System	Emergency Generator	Firewater Pump	Pellet Coolers	Hammermills and Area Filters	Pellet Press Silo
NO _x	х	x	X			
PM/PM ₁₀ /PM _{2.5}	x	X	X	х	X	Х
CO	х	x	X			
VOC	X.	X	X			
CO _{2e}	x	X	х			

4.1.2 TECHNICAL APPROACH

The definition of BACT may be found in Section 169(3) of the Clean Air Act and in the PSD regulations under 40 CFR 52.21(j). BACT is defined as:

"...an emissions limitation (including a visible emission standard) based on the maximum degree of reduction for each pollutant subject to regulation under the Clean Air Act which would be emitted from any proposed major stationary source or

major modification which the Administrator, on a case-by-case basis, taking into account energy, environmental, and economic impacts and other costs, determines is achievable for such source or modification through application of production processes or available methods, systems, and techniques, including fuel cleaning or treatment or innovative fuel combustion techniques for control of such pollutant. In no event shall application of best available control technology result in emissions of any pollutant which would exceed the emissions allowed by any applicable standard under 40 CFR Parts 60 and 61. If the Administrator determines that technological or economic limitations on the application of the measurement methodology to a particular emissions unit would make the imposition of an emissions standard infeasible, a design, equipment, work practice, operational standard, or combination thereof, may be prescribed instead to satisfy the requirement for the application of best available control technology."

On December 1, 1987, the U.S. EPA Assistant Administrator for Air and Radiation issued a memorandum that implemented certain program initiatives to improve the effectiveness of the PSD program within the confines of existing regulations and state implementation plans. Among the initiatives was a "top-down" approach for determining BACT. This "top down" approach was used to determine BACT for all sources indicated in Section 4.1.1.

The first step in this analysis was to identify all possible control options. Next, all technically infeasible or undemonstrated control options were eliminated and the remaining options were ranked in order of control effectiveness. After ranking control options, the most stringent emission level was considered BACT unless economic, energy, or environmental impacts preclude its selection. If adverse impacts precluded selection of the most stringent option, the next most stringent emission level was evaluated. This process continued until a control option could not be eliminated and was selected as BACT.

Control options for each compound for this analysis were developed using information from the following resources:

- RBLC database (RACT/BACT/LAER Clearinghouse) located on EPA's Technology Transfer Network in the EPA electronic bulletin board system,
- Various EPA reports on emissions control technologies,
- Various air pollution control technology vendors,
- Pending permit applications and issued permits for similar facilities, and
- Compilation of Air Pollution Emission Factors (AP-42) published by EPA.

It should be noted that the RBLC only includes one determination for a wood pellet mill, determination VA-0298. This project was permitted a number of years ago using an conceptual "wood-fired RTO" technology for VOC control, but the plant was never constructed because, according the VA Department of Environmental Quality, the project was unable to obtain financing. Therefore, the only RBLC information presented in this application for the proposed facility is for NO_x emissions from the dryer, assumed to be

similar to wood-fired stoker boilers. All other pollutants emitted from the dryer are not believed to be similar to any other types of emission units included in the RBLC. For instance, namely because emissions are directly impacted by the effect of the rotary drying process (even CO is evolved from wood being dried).

4.1.3 PSD IMPACT ANALYSIS OF CONTROL ALTERNATIVES

As mentioned above, the economic, environmental, and energy impacts of technically feasible BACT options were evaluated according to the top-down BACT process. The first step involves a technical feasibility analysis of all potential control options, and the next step involves an evaluation of the economic impacts of feasible control alternatives with primary consideration to the cost effectiveness (dollars per ton of compound removed) for each option. The economic analysis is typically based on vendor quotes and/or established EPA cost estimating procedures. An environmental impact analysis was then performed to determine whether any adverse "non-air" impacts were associated with an alternative. The last analysis involved calculating energy impacts, or increased energy requirements, associated with each option.

4.2 DRYER SYSTEM

Enviva plans to use utilize a rotary drying kiln to reduce wood moisture from approximately 50 percent to 5 to 10 percent prior to pelletization. Direct contact heat will be provided to the system via a 207 mmBtu/hr burner system. Air emissions will be controlled by a multiclone followed by a wet electrostatic precipitator (WESP) operating in series. Emissions are calculated using a combination of dryer vendor emission guarantees (criteria pollutants only) and AP-42 emissions factors. The pollutants emitted from the dryers that are subject to BACT review are NO_x, TSP/PM₁₀/PM_{2.5}, VOC, CO, and CO₂e. The control technology assessment for each compound subject to PSD review is provided below

4.2.1 NITROGEN OXIDES (NO_x)

The formation of NO_x is determined by the interaction of chemical and physical processes occurring within the flame zone of the furnace of the proposed boiler. There are two principal forms of NO_x designated as "thermal" NO_x and "fuel" NO_x . Thermal NO_x formation is the result of oxidation of atmospheric nitrogen contained in the inlet gas in the high-temperature, post-flame region of the combustion zone. The major factors influencing thermal NO_x formation are temperature, concentrations of combustion gases (primarily nitrogen and oxygen) in the inlet air and residence time within the combustion zone. Fuel NO_x is formed by the oxidation of fuel-bound nitrogen. NO_x formation can be controlled by adjusting the combustion process and/or installing post-combustion controls.

4.2.1.1 IDENTIFY CONTROL TECHNOLOGIES

A summary of results from the RBLC is provided in Table 4-1.

Potentially applicable NO_x control technologies are:

- Conventional Selective Catalytic Reduction (SCR),
- Regenerative Selective Catalytic Reduction (RSCR), and
- Selective Non-Catalytic Reduction (SNCR).

Conventional Selective Catalytic Reduction and Regenerative Selective Catalytic Reduction Technologies: Conventional Selective Catalytic Reduction (SCR) is a post combustion NO_x add-on control device that is placed in the flue gas stream following the boiler. SCR involves the injection of ammonia (NH₃) into the flue gas stream ahead of a catalyst bed. On the catalyst surface, ammonia reacts with NO_x contained within the air to form nitrogen gas (N₂) and water (H₂O) in accordance with the following chemical equations:

$$4NH_3 + 4NO + O_2 \rightarrow 4N_2 + 6H_2O$$

 $4NH_3 + 2NO_2 + O_2 \rightarrow 3N_2 + 6H_2O$

The catalyst's active surface is usually either a noble metal (platinum), base metal (titanium or vanadium), or a zeolite-based material. Metal-based catalysts are usually applied as a coating over a metal or ceramic substrate. Zeolite catalysts are typically a homogenous material that forms both the active surface and the substrate. The geometric configuration of the catalyst body is designed for maximum surface area and minimum obstruction of the flue gas flow path in order to achieve maximum conversion efficiency and minimum back pressure. The most common configuration is a "honeycomb" design. In a typical ammonia injection system, ammonia is drawn from a storage tank, vaporized and injected upstream of the catalyst bed. Excess ammonia that is not reacted in the catalyst bed and emitted is referred to as ammonia slip. An important factor that affects the performance of an SCR is operating temperature. The temperature range for standard base metal catalyst is between 400-800°F.

The flue gas in conventional SCR systems in wood-fired systems prior to final particulate matter controls contain alkali metals such as sodium, potassium and zinc and trace heavy metals that poison and "blind" the SCR catalyst. It is believed that there are no conventional SCR systems operating after wood-fired combustion systems in the U.S. There are a few systems reportedly operating in Europe utilizing such systems; however, these are specialized systems operating on power plants utilizing bubbling fluidized bed and circulating fluidized bed boilers and these systems reportedly require unusually high maintenance.

Babcock Power Inc. developed a new SCR system that can be installed after the final particulate matter emissions controls. This relatively new technology, called Regenerative Selective Catalytic Reduction or "RSCR" utilizes beds of ceramic media to raise the temperature of the flue gas after particulate control, to a temperature needed for reaction. The main advantage of an RSCR system is that it operates in a cleaner environmental providing improved catalyst performance and high thermal efficiency. In the RSCR, the gas passes through a preheated bed where it is heated from the temperature

of the exhaust exiting the final PM control device (approximately 170 °F). Burners then raise the flue gas temperature to 470 °F before it flows across the adjacent catalyst canister, where NO_x reduction occurs. The exhaust gas from the catalyst bed then heats an adjacent bed containing heat transfer media. This heated bed then becomes the preheater for the exhaust. Flow direction continues to alternate in this fashion.

Selective Non-Catalytic Reduction: Selective Non-Catalytic Reduction (SNCR) describes a process by which NO_X is reduced to molecular nitrogen (N_2) and water (H_2O) by injecting an ammonia or urea ($CO(NH_2)_2$) spray into the post-combustion area of the unit. Typically, injection nozzles are located in the upper area of the furnace and convective passes. Once injected, the urea or ammonia decomposes into NH_3 or NH_2 free radicals, reacts with NO_X molecules, and reduces to nitrogen and water. The ammonia and urea reduction equations are provided below. These reactions are endothermic and use the heat of the burners as energy to drive the reduction reaction:

$$2NO + 2NH_3 + \frac{1}{2}O_2 \longrightarrow 2N_2 + 3H_2O$$

 $2NO + CO(NH_2)_2 + \frac{1}{2}O_2 \longrightarrow 2N_2 + CO_2 + 2H_2O$

Both ammonia and urea have been successfully employed as reagents in SNCR systems and have certain advantages and disadvantages. Ammonia is less expensive than urea and results in substantially less operating costs at comparable levels of effectiveness. Urea, however, is able to penetrate further into flue gas streams, making it more effective in larger scale burners and combustion units with high exhaust flow rates.

SNCR is considered a selective chemical process because, under a specific temperature range, the reduction reactions described above are favored over reactions with other flue gas components. Although other operating parameters such as residence time and oxygen availability can significantly affect performance, temperature remains one of the most prominent factors affecting SNCR performance.

The SNCR process requires the installation of reagent storage facilities, a system capable of metering and diluting the stock reagent into the appropriate solution, and an atomization/injection system at the appropriate locations in the combustion unit. The reagent solution is typically injected along the post-combustion section of the combustion unit. Injection sites around the unit must be optimized for reagent effectiveness and must balance residence time with flue gas stream temperature.

For ammonia, the optimum reaction temperature range is approximately 880 to 1,100 degrees Celsius (°C) (1,615 to 2,000 °F). Below the SNCR operating temperature range, the NH_3/NO_x reaction will not occur. The unreacted NH_3 will either be emitted as NH_3 slip or it will react with SO_3 to form ammonium salts. Above the optimal temperature range, the amount of NH_3 that oxidizes to NO_x increases and NO_x reduction performance deteriorates.

4.2.1.2 ELIMINATE TECHNICALLY INFEASIBLE OPTIONS

Conventional SCR and Regenerative SCR: As discussed in the previous section, there are substantial technical concerns about poisoning/blinding of catalysts utilized within a conventional SCR system and our research indicates that there are no such systems operating on source similar to the wood-fired dryer burner system anywhere in the world. RSCR has not been demonstrated on a wood chip dryer in the past. Potential impacts of salts carry over from the WESP needed for particulate matter control may poison catalyst and, furthermore, the low temperate of the exhaust from the WESP (~170 °F) makes reheat necessary for appropriate catalyst operating temperature impracticable. Thus, both conventional SCR and RSCR are both considered undemonstrated/technically infeasible technologies for wood dryers.

4.2.1.3 RANK REMAINING CONTROL TECHNOLOGIES BY EFFECTIVENESS

There is one technically feasible NO_x control technologies for the rotary dryer – SNCR. After collaboration between Enviva and a major SNCR vendor, an SNCR control option of 0.515 lb/ODT (equivalent to 0.15 lb/mmBtu) was determined to be the lowest achievable emission rate due to inherent limitations on the effectiveness of this control device in the proposed burner system.

4.2.1.4 EVALUATE MOST EFFECTIVE CONTROL OPTION (IMPACTS ANALYSIS)

4.2.1.4.1 SNCR (0.515 LB/ODT)

Economic Impacts

As shown in Tables 4-3 and 4-4, the SNCR can achieve a NO_x level of 0.515 lb/mmBtu at approximately \$6,701/ton of NO_x reduction. This cost is considered prohibitive and, thus, SNCR is rejected from consideration in the BACT analysis.

Energy Impacts

Energy requirements for an SNCR system primarily consist of the power needed for ammonia injection. It is estimated that the energy impact associated with SNCR control is approximately 2.54 x 10⁴ KWH/yr. Enviva Pellets, LLC does not consider this quantity of electric generation capacity to be a significant "adverse impact."

Environmental Impacts

There are no major adverse environmental impacts.

4.2.1.5 SELECT BACT

The baseline emission rate proposed by the dryer vendor of 0.79 lb/ODT utilizing good combustion practices and optimal burner design is proposed as BACT.

4.2.2 PARTICULATE MATTER (TSP/PM₁₀/PM_{2.5})

Particulate matter (TSP/PM $_{10}$) is emitted as both filterable and condensable particulate matter. Enviva has designed the rotary dryer system with a multiclone, considered the baseline level of control, for particulate matter removal.

4.2.2.1 IDENTIFY CONTROL TECHNOLOGIES

Potentially applicable TSP/PM₁₀ add-on control technologies (in addition to the base multiclone) are:

- Baghouse and
- WESP.

Baghouse: A fabric filtration device (baghouse) consists of a number of filtering elements (bags) along with a bag cleaning system contained in a main shell structure incorporating dust hoppers. Fabric filters use fabric bags as filters to collect particulate matter. The particulate-laden gas enters a fabric filter compartment and passes through a layer of particulate and filter bags. The collected particulate forms a cake on the bag, which enhances the bag's filtering efficiency. However, excessive caking will increase the pressure drop across the fabric filter and reduce its efficiency. A phenomenon known as "blinding" occurs when cake builds up to the point that air can no longer pass through the baghouse during normal operation or the baghouse becomes clogged with wet and/or resinous compounds.

The particulate removal efficiency of fabric filters is dependent upon a variety of particle and operational characteristics. Particle characteristics that affect the collection efficiency include particle size distribution, particle cohesion characteristics, and particle electrical resistivity. Operational parameters that affect fabric filter collection efficiency include air-to-cloth ratio, operating pressure loss, cleaning sequence, interval between cleanings, cleaning method, and cleaning intensity. In addition, the particle collection efficiency and size distribution can be affected by certain fabric properties (e.g., structure of fabric, fiber composition, and bag properties).

Wet Electrostatic Precipitator: WESPs remove particles from a gas stream through the use of electrical forces. Discharge electrodes apply a negative charge to particles passing through a strong electrical field. These charged particles then migrate to a collecting electrode having an opposite, or positive, charge. Collected particles are removed from the collecting electrodes by washing utilizing a mild hydroxide solution to prevent buildup of resinous materials present in the dryer exhaust. Wet ESPs versus dry ESPs are utilized in the forest products industries for control of emissions from similar dryer sources because dry ESPs cannot reliably operate due to resin buildup on collection electrodes.

4.2.2.2 ELIMINATE TECHNICALLY INFEASIBLE OPTIONS

Although an effective form of particulate control in many applications, use of a baghouse is technically infeasible due to condensation of resinous compounds on the baghouse leading to blinding. Wood chip dryers are optimized for thermal efficiency to recirculate as much air through the system without leading to excess moisture and condensation problems within the drying system. However, as the exhaust leaves the process it is sufficiently laden with moisture and resinous compounds that condensation in a baghouse occurs readily.

4.2.2.3 RANK REMAINING CONTROL TECHNOLOGIES BY EFFECTIVENESS

There is only one feasible control technology for the rotary dryer, a WESP.

4.2.2.4 EVALUATE MOST EFFECTIVE CONTROL OPTION (IMPACTS ANALYSIS)

Enviva does not consider the cost of WESP control excessive. Based on their extensive experience with the wood products industry, use of a WESP is a reliable method of excellent PM control. There are numerous sources utilizing this method of control on forest products dryers, so there are no adverse energy impacts. Wastewater is pretreated prior to permitted discharge to the local wastewater treatment plant, so there will be no adverse environmental impacts.

4.2.2.5 SELECT BACT

Since the baghouse was deemed cost prohibitive the plant will utilize the current process design controls of multiclones followed by WESP to minimize total PM emissions. Although WESPs control filterable and condensable PM, the degree to which condensable PM is controlled is not well characterized and cannot be estimated with confidence. Since WESP control efficiency for filterable PM in a wood-fired application is well-characterized, but condensable PM is not, Enviva proposes a filterable PM limit of 0.09 lb/MM Btu, equivalent to approximately 0.007 gr/cubic foot of exhaust. It should be noted that for conservatism, condensable PM from the dryer included in air dispersion modeling included in the application was based on AP-42.

4.2.3 CARBON MONOXIDE (CO) AND VOLATILE ORGANIC COMPOUNDS (VOC)

Carbon monoxide and VOC emissions result due to imperfect combustion of carbonaceous material in the fuel. CO is a by-product of the combustion process in which carbon is not fully oxidized to CO₂. Likewise, VOC is emitted when the carbonaceous matter in the fuel is not converted to CO₂ or CO. Control of both species involves forcing the oxidation of carbon to CO₂.

The VOC emissions from a wood pellet mill are almost entirely from the wood drying process. Enviva will design the pellet milling equipment to utilize at least 90 percent hardwood. Hardwood species emit far less VOC than the more common softwood species and it is anticipated that the plant would emit almost 70 percent less VOC than a traditional softwood mill. It should be noted that wood chip drying systems such as the

one proposed recirculate approximately 30 percent of dryer air into the combustion makeup air for the burner to optimize thermal efficiency and partial VOC destruction.

A variety of forest products industries sometimes utilize VOC and CO oxidation abatement equipment. Use of such controls is often fraught with operational difficulties requiring regular, significant capital investments to replace various equipment in the oxidation system. The following analysis ignores these additional costs; however, the useful economic life of oxidation controls has been assumed to be 10 years, which is still conservatively long because experience with the forest products industry has shown that the major components of these systems are typically replaced at a more frequent schedule such that essentially the entire cost of an oxidation system will occur more frequently than 10 years.

4.2.3.1 IDENTIFY CONTROL TECHNOLOGIES

VOC and CO emissions from the wood drying kiln can be controlled by process design and/or VOC and CO add-on oxidation technologies. Based upon a search of RBLC results and commercially demonstrated technology, only the following control technologies were considered in this evaluation:

- Process design,
- Regenerative thermal oxidation (RTO),
- Regenerative catalytic oxidation (RCO),
- Thermal Catalytic Oxidation (TCO),
- Packed-Bed Catalytic Wet Scrubber, and
- Bio-oxidation / Bio-filtration.

PROCESS DESIGN: Enviva will design the pellet milling equipment to utilize at least 90 percent hardwood species. Utilizing 90% hardwood for pellet production would achieve a VOC emission rate of 1.50 lb/oven-dried ton (ODT), which equates to a 68 percent reduction in VOC compared to the AP-42³ emission factor of 4.7 lbs/ODT for comparable rotary dryer utilizing softwood.

REGENERATIVE THERMAL OXIDATION: RTOs use a high-density media such as a ceramic-packed bed still hot from a previous cycle to preheat an incoming VOC-laden waste gas stream. The preheated, partially oxidized gases then enter a combustion chamber where they are heated by auxiliary fuel (natural gas) combustion to a final oxidation temperature typically between 760 to 820 °C (1400 to 1500 °F) and maintained at this temperature to achieve maximum VOC destruction. The purified, hot gases exit this chamber and are directed to one or more different ceramic-packed beds cooled by an earlier cycle. Heat from the purified gases is absorbed by these beds before the gases are exhausted to the atmosphere. The reheated packed-bed then begins a new cycle by heating a new incoming waste gas stream.

³ US EPA Compilation of Air Pollutant Emission Factors, Chapter 10.6 Table 10.6.2-3.

REGENERATIVE CATALYTIC OXIDATION: Regenerative catalytic oxidation (RCO) technology is widely used in the reduction of VOC emissions. It operates in the same fashion as the RTO, but it requires only moderate reheating to the operating range of the catalyst, approximately 450 °F. Furthermore, RCOs can achieve a high thermal efficiency of 95% because they utilize a ceramic bed to recapture the heat of the stream exiting the combustion zone. Particulate control must be placed upstream of an RCO.

THERMAL CATALYTIC OXIDATION: Operating much in the same fashion as an RCO, thermal catalytic oxidation (TCO), passes heated gases through a catalyst without the regenerative properties attributed by the ceramic bed used to recapture heat.

PACKED-BED CATALYTIC WET SCRUBBER: This technology was considered for its ability to oxidize the volatile organic hazardous air pollutants (HAPs) formaldehyde and methanol, which comprise a considerable portion of the VOC emissions. This technology, combined with the existing wet scrubbing system, is reportedly capable of achieving 90 percent control efficiency of either compound and roughly 30 percent overall VOC control efficiency.

BIO-OXIDATION / BIO-FILTRATION: Bio-filtration offers an alternative to costly thermal or catalytic units. It is an air pollution control technology – offering upwards of 80% or more control efficiency – in which VOCs are oxidized using living micro-organisms on a media bed (sometimes referred to a "bioreactor"). A fan is typically used to collect or draw contaminated air from a building or process. If the air is not properly conditioned (heat, humidity, solids), then pretreatment may be a necessary step to obtain optimum gas stream conditions before introducing it into the bioreactor. As the emissions flow through the bed media, the pollutants are absorbed by moisture on the bed media and come into contact with the microbes. The microbes consume and metabolize the excess organic pollutants, converting them into CO₂ and water, much like a traditional oxidation process.

"Mesophilic" microbes are typically used in these systems. Mesophilic microbes can survive and metabolize VOC materials at conditions up to 110°F to 120°F. One company is attempting to develop a commercial-scale technology that employs "thermophilic" microbes, but that technology has only been demonstrated on a single pilot scale installation that has a similar – but not exactly the same – exhaust stream profile as Enviva. Thermophilic microbes live and metabolize VOC at higher operating temperatures (~160°F).

4.2.3.2 ELIMINATE TECHNICALLY INFEASIBLE OPTIONS

As indicated in the previous subsection, there are a variety of combustion techniques that can be used to control VOC. However, the following technologies are not practical for VOC control at the Enviva plant:

- Packed Bed Catalytic Scrubber, and
- Bio-oxidation / Bio-filtration.

PACKED BED WET SCRUBBER: This technology is still within a startup mode of operation at its first full-scale demonstration in Moncure, NC. Until the technology can demonstrated to operate reliably with an established VOC control efficiency over an extended period of time, this technology is not considered to be a clearly feasible control technology.

BIO-OXIDATION / BIO-FILTRATION: In the case of the bio-oxidation or bio-filtration, many questions still remain on the technology's efficacy to remove VOC and HAP emissions at the Enviva plant.

A primary problem with this technology is the sensitivity of the microbes to stream conditions. At the normal exhaust temperature ranges (~170°F) after a wet ESP that would be used for PM control, mesophilic microbes would die. To cool the exhaust stream to conditions in which mesophiles live, Enviva would need to install a recirculating water heat exchanger which is ineffective during the hotter summer months. At such a high operating temperature, use of thermophilic microbes would be required. However, this technology has only been demonstrated on the pilot scale to date. Additionally, questions still remain as to how to "feed" the thermophiles during common two week downtimes, or during other non-operational periods. Therefore, use of a bio-filtration system is not considered a technically feasible means of VOC control for the Enviva plant.

REGENERATIVE CATALYTIC/THERMAL OXIDATION: Even though RTO and RCO are assumed to be technically feasible it is important to note that other facilities have had problems with RTO/RCOs in the past. Even with efficient PM/PM₁₀ control, catalyst blinding/poisoning reduces catalyst life. There are also corrosion problems that currently occur in both the RTO and RCO.

4.2.3.3 RANK REMAINING CONTROL TECHNOLOGIES BY EFFECTIVENESS

After eliminating the technically infeasible control options, Enviva has determined the following options remain and has ranked them in order of greatest to least control of VOC emissions:

- Regenerative thermal oxidation (RTO) designed for 90% control efficiency
- Regenerative catalytic oxidation (RCO) designed for 70% control efficiency

4.2.3.4 EVALUATE MOST EFFECTIVE CONTROL OPTION (IMPACTS ANALYSIS)

4.2.3.4.1 REGENERATIVE THERMAL OXIDATION (0.150 LB/ODT VOC AND 0.116 LB/ODT CO)

Economic Impacts

Results of the economic impacts evaluation for operation of the RTO are presented in Tables 4-5, 4-7 and 4-8. Capital and operating costs were based on vendor quotes, OAQPS Manual, and past permitting experience. Other cost impacts were estimated using EPA cost methodologies. Table 4-5 presents a breakout of costs used in the economic impacts evaluation. A detailed discussion of key cost estimates is provided in the following text.

Capital Costs for the RTO were provided to Enviva by GEOENERGY. Economic Life of the RTO of 10 years was also supplied by the vendor, which is also consistent with Trinity experience.

As shown in Tables 4-7 and 4-8, the cost-effectiveness of continued operation of the RTO is approximately \$5,566/ton VOC and \$8,023/ton CO, which is considered cost prohibitive.

Energy Impacts

The additional energy required to operate the RTO is about 3,560,000 kW-hr/yr.

Environmental Impacts

There are no adverse impacts from the operation of an RTO, except for increased emissions of criteria pollutants and GHGs emitted as byproducts of natural gas used for supplemental fuel.

4.2.3.4.2 REGENERATIVE CATALYTIC OXIDATION (0.450 LB/ODT VOC AND 0.348 LB/ODT CO)

Economic Impacts

Results of the economic impacts evaluation for operation of the RCO are presented in Tables 4-6 through 4-8. Capital and operating costs were based on vendor quotes and the OAQPS Manual. Other cost impacts were estimated using EPA cost methodologies. Table 4-7 presents a breakout of costs used in the economic impacts evaluation. A detailed discussion of key cost estimates is provided in the following text.

As shown in Tables 4-7 and 4-8, the cost-effectiveness of the RCO is approximately \$7,197/ton VOC and \$10,375, which is considered cost prohibitive.

Energy Impacts

The additional energy required to operate the RCO is approximately 3,600,000 kW-hr/yr.

Environmental Impacts

There are no adverse impacts from the operation of a RCO, except for increased emissions of criteria pollutants and GHGs emitted as byproducts of natural gas used for supplemental fuel.

4.2.3.4.3 PROCESS DESIGN (1.50 LB/ODT VOC & 1.16 LB/ODT CO)

There are no adverse economic, energy, or environmental impacts associated with designing the process to utilize at least 90% hardwood. Use of primarily hardwood has been used to establish baseline emissions and results in an approximate 68% VOC reduction compared to a traditional softwood mill.

4.2.3.5 SELECT BACT

Since both RTO and RCO add-on abatement technologies were deemed cost prohibitive, the plant would utilize process design to minimize total VOC emissions to 1.50 lb/ODT and CO emissions to 1.16 lb/ODT.

4.2.4 GREENHOUSE GAS EMISSIONS (CO2, CH4, N2O)

On July 1, 2011, EPA signed the Deferral for CO₂ Emissions from Bioenergy and Other Biogenic Sources under the Prevention of Significant Deterioration (PSD) and Title V Programs. The final rule becomes effective immediately upon the date of its publication in the Federal Register, which is expected to follow the rule signing by one to two weeks. However, the applicability and effective date of this deferral in a particular state will vary. The deferral is optional for any state, local, or tribal permitting authorities that implement the Title V and PSD permitting programs (i.e., SIP-approved programs). Though not mandatory, EPA encourages states that expect to receive permit applications from a number of biomass facilities to submit the necessary SIP revisions or Title V program revisions to implement this three-year deferral. Since Enviva is submitting this application prior to North Carolina amending its own SIP-approved program to reflect the deferred rule, Enviva is addressing the CO₂ emissions from the new facility. Based on future developments of the updated SIP, Enviva will discuss any permitting implications with NCDAQ at that time.

Therefore, since there will be significant emissions increases from the project, a BACT analysis for GHG is being conducted on the dryer. From a combustion unit, GHG emissions of CO, CH₄, and N₂O are anticipated as a result of the combustion processes; therefore, a BACT review must be conducted for each of these pollutants. The following sections outline Steps 1 through 5 of the BACT analysis for CO₂.

On November 10, 2010 (and later with a revision in March 2011), U.S. EPA issued several new guidance documents related to the completion of GHG BACT analyses. The following guidance documents were utilized as resources in completing the GHG BACT evaluation for the proposed project:

- ▲ PSD and Title V Permitting Guidance For Greenhouse Gases (hereafter referred to as General GHG Permitting Guidance)⁴
- ▲ Available and Emerging Technologies for Reducing Greenhouse Gas Emissions from Industrial, Commercial, and Institutional Boiler (hereafter referred to as GHG BACT Guidance for Boilers)⁵

To complete the GHG BACT evaluation, Enviva also relied on additional resources such as:

- Specifications provided by the dryer system vendor
- ▲ RBLC database Searching the newly enhanced RBLC database returned no results on permitting decisions for biomass furnaces for GHGs. ⁶
- ▲ GHG Mitigation Strategies Database The GHG Mitigation Strategies Database did not contain any green wood furnaces and dryer system installations for the forest products industry comparable to this project. ⁷

4.2.4.1 IDENTIFY CONTROL TECHNOLOGIES

CO₂: The following potential CO₂ control strategies for the dryer system were considered as part of this BACT analysis:

- ▲ Selection of the lowest carbon fuel
- ▲ Installation of energy efficient options for the Dryer System

SELECTION OF LOWEST CARBON FUEL: For GHG BACT analyses, low-carbon intensity fuel selection is the primary control option that can be considered a lower emitting process. The dryer system's furnace will combust biomass (green wood) as the primary fuel.

Firing natural gas as a primary fuel is considered an available option, as natural gas is a lower emitting GHG fuel on a direct carbon basis than biomass (not accounting for the life cycle carbon neutral benefits of biomass combustion). Other "clean fuels" options are not required to be considered according to the General GHG Permitting Guidance since that would fundamentally redefine the source by requiring the permit applicant to

⁴ U.S. EPA, Office of Air and Radiation, Office of Air Quality Planning and Standards, (Research Triangle Park, NC: U.S. EPA EPA-HQ-OAR-2010-0841-0001, November 2010). http://www.epa.gov/nsr/ghgdocs/epa-hq-oar-2010-0841-0001.pdf

⁵ U.S. EPA, Office of Air and Radiation, Office of Air Quality Planning and Standards, (Research Triangle Park, NC: October 2010). http://www.epa.gov/nsr/ghgdocs/iciboilers.pdf

⁶ http://cfpub.epa.gov/RBLC/

⁷ http://ghg.ie.unc.edu:8080/GHGMDB/

switch to a primary fuel type other than the type of fuel that the applicant proposes to use for its combustion processes.⁸

INSTALLATION OF ENERGY EFFICIENCY OPTIONS: Operating practices that increase energy efficiency are a potential control option for improving the fuel efficiency of the Dryer System and therefore, providing benefit with respect to GHG emissions.

In November 2010, the U.S. EPA provided a white paper that addresses control technologies, energy efficiency measures, and fuel switching options for industrial, commercial and institutional boilers. Several of the energy efficiency options for boilers discussed in this document were also listed in the U.S. EPA's white paper specifically directed to the pulp and paper industry, which has some relevant sections for the forest products industry. These options primarily focus on improved process control, reduced heat loss, and improved heat recovery, and are expected to be part of the design of "state-of-the-art boiler systems." The energy efficiency options (applicable to a wood chip drying system) listed in the GHG BACT Guidance for the Pulp and Paper Industry are:

- Furnace maintenance
- Furnace process control
- Heat recovery
- Reduction of excess air

Note that additional options were recognized in the GHG BACT Guidance documents such as condensate return and minimizing boiler blow down, but were not included above since these features do not apply to a furnace and drying system such as the one proposed for the Northampton facility.

 $\underline{\text{CH}_4}$ and $\underline{\text{N}_2}$ O Options: Available control options for minimizing CH₄ emissions from the Dryer System include operating practices that promote energy efficiency to reduce fuel usage.

 N_2O catalysts have been used in nitric/adipic acid plant applications to minimize N_2O emissions. ¹⁰ Tailgas from the nitric acid production process is routed to a reactor vessel with a N_2O catalyst followed by ammonia injection and a NO_X catalyst.

Energy efficient operating practices are additionally available control technology options for N_2O reduction.

10 http://www.catalysts.basf.com/Main/mediaroom/10years_worldscale_experience_in_reducing_nitrous_.be

⁸ US EPA, Office of Air Quality Planning and Standards, "PSD and Title V Permitting Guidance for Greenhouse Gases", March 2011, p. 29.

⁹ U.S. EPA Office of Air and Radiation, Office of Air Quality Planning and Standards, Available and Emerging Technologies for Reducing Greenhouse Gas Emissions from the Pulp and Paper Manufacturing Industry, October 2010, http://www.epa.gov/nsr/ghgdocs/pulpandpaper.pdf, p. 11-16.

4.2.4.2 ELIMINATE TECHNICALLY INFEASIBLE OPTIONS

<u>CO</u>₂:

SELECTION OF THE LOWEST CARBON FUEL: Additional firing of a lower carbon fuel (natural gas) is a technically feasible option for CO₂ control of the Dryer System.

INSTALLATION OF ENERGY EFFICIENCY OPTIONS ON THE NO. 3 BIOMASS BOILER: Each of the aforementioned energy efficiency options in Step 1 is technically feasible for CO₂ control of the Dryer System.

<u>CH₄ and N₂O Options</u>: Energy efficient operating practices are the only technically feasible control options for reducing CH₄ emissions from the Dryer System.

 N_2O catalysts have not been used to control N_2O emissions in industrial applications as yet. In addition, the very low N_2O concentrations present in the Dryer System exhaust stream would make installation of N_2O catalysts technically infeasible. In comparison, the application of a catalyst in the nitric acid industry sector has been effective due to the high (1,000-2,000 ppm) N_2O concentration in those exhaust streams. N_2O catalysts are eliminated as a technically feasible option for the proposed project.

With N_2O catalysts eliminated, energy efficient operating practices are the only available and technically feasible control options for N_2O reduction from the Dryer System.

4.2.4.3 RANK REMAINING CONTROL TECHNOLOGIES BY EFFECTIVENESS

 $\underline{CO_2}$: Lower carbon fuel selection and installation of energy efficient options are the remaining technically feasible control options for minimizing CO_2 emissions from the Dryer System. It is unclear which option has a more significant impact on emissions of CO_2 from the facility.

<u>CH₄ and N₂O</u>: Energy efficient operating practices are the only remaining control option for reducing CH₄ and N₂O emissions from the Dryer System.

4.2.4.4 EVALUATE MOST EFFECTIVE CONTROL OPTION (IMPACTS ANALYSIS)

<u>CO</u>₂:

4.2.4.4.1 SELECTION OF THE LOWEST CARBON FUEL

While natural gas may be a lower emitting carbon fuel than biomass, combustion of clean biomass (as a primary fuel), is a renewable fuel that has clean energy and GHG benefits, and has financial benefits to the facility in terms of cost reductions. This assertion is supported by U.S. EPA in the General GHG Permitting Guidance:

Even before EPA takes further action, however, permitting authorities may consider, when carrying out their BACT analyses for GHG, the environmental, energy and economic benefits that may accrue from the use of certain types of biomass and other biogenic sources (e.g., biogas from landfills) for energy generation, consistent with existing air quality standards. In particular, a variety of federal and state policies have recognized that some types of biomass can be part of a national strategy to reduce dependence on fossil fuels and to reduce emissions of GHGs.

The General GHG Permitting Guidance goes on to state that combustion of biomass can be considered carbon neutral.¹¹ The combustion of biomass as a fuel is environmentally beneficial since biomass is a renewable fuel source and contributes to additional renewable energy on the grid. Reliance on natural gas as the primary fuel would eliminate the renewable energy benefits of the overall project as this would simply mean the displacement of one fossil-fuel with another fossil fuel, as opposed to allowing for the increased reliance on a renewable energy source.

Therefore, combustion of biomass demonstrates significant environmental and energy benefits when considering the impacts to climate change, GHG emissions, and renewable energy generation.

<u>CH₄ and N₂O</u>: No adverse energy, environmental, or economic impacts are associated with good combustion/operating practices for reducing CH₄ and N₂O emissions from the wood-fired furnace.

4.2.4.4.2 Installation of Energy Efficiency Options

<u>CO</u>₂: No adverse energy, environmental, or economic impacts are associated with energy efficient operating practices for reducing CO₂ emissions from the Dryer System.

The environmental benefits include fuel savings and reduction of GHG emissions, as well as other criteria pollutant emissions, due to the efficiency gains.

<u>CH₄ and N₂O</u>: Energy efficient operating practices resulting in minimized fuel consumption are the only technically feasible control options for reducing CH_4 and N_2O emissions from the Dryer System.

¹¹ US EPA, Office of Air Quality Planning and Standards, "PSD and Title V Permitting Guidance for Greenhouse Gases", March 2011, p 9.

4.2.4.5 SELECT BACT

<u>CO</u>₂: Therefore, biomass is the best fuel selection for the facility from a renewable source. With respect to energy efficiency, the drying system has been designed for optimal thermal efficiency, recirculating about 30 percent of the dryer air as combustion makeup air in the burners. Excess combustion air will be optimized to further improve thermal efficiency of the system and the dryer system will be regularly maintained (e.g., burner maintenance) according to a regular schedule, taking into account manufacturer's recommendations, to maintain the high thermal efficiency of the system.

 $\underline{\text{CH}_4 \text{ and N}_2\text{O}}$: Enviva is implementing the energy efficiency efforts as described above. Through these efforts to maximize the unit's efficiency, $N_2\text{O}$ emissions from the dryer system are inherently reduced and kept to a minimum.

Since there is some potential variability in final thermal efficiency of the system, establishing a specific emissions limitation, such as a lb CO_2e per ODT is impractical. Instead, Enviva proposes the following design/work practice standards:

- Biomass to be utilized for drying system fuel,
- Energy-efficient design (which is considered by Enviva to be self-implementing and necessary as part of the inherent design of the equipment since thermal energy supplied to the dryer is the most significant operating cost at the facility), and
- Regular maintenance at minimum intervals to be established taking into account manufacturer's recommendations and standard industry practices.

4.3 Pellet Coolers

Pellet Press conveyors discharge wood pellets through one of six Pellet Coolers. Cooling air is passed through the pellets. At this point, the Pellets contain a small amount of wood fines, which are swept out with the cooling air and are controlled utilizing three high cyclones operating in parallel (one for every two coolers) prior to discharge to the atmosphere. These cyclones will not only provide high-efficiency PM control, but are also inherent process equipment because they are needed to effect cooling through the intimate mixing of air through the pellets. The only pollutant emitted from the pellet coolers that are subject to BACT review is TSP/PM₁₀/PM_{2.5}. The control technology assessment for each compound subject to PSD review is provided below.

4.3.1 PARTICULATE MATTER (TSP/PM₁₀)

Particulate matter (TSP/PM₁₀/PM_{2.5}) is emitted as a both filterable and condensable particulate matter. As stated earlier, Enviva has designed the pellet coolers dual high efficiency cyclones operating in parallel (one for every two coolers) prior to discharge to the atmosphere. Therefore, baseline emissions are based on use of the cyclones.

4.3.1.1 IDENTIFY CONTROL TECHNOLOGIES

Potentially applicable PM add-on control technologies are:

- Baghouse and
- Electrostatic Precipitator (ESP).

Baghouse: A fabric filtration device (baghouse) consists of a number of filtering elements (bags) along with a bag cleaning system contained in a main shell structure incorporating dust hoppers. Fabric filters use fabric bags as filters to collect particulate matter. The particulate-laden gas enters a fabric filter compartment and passes through a layer of particulate and filter bags. The collected particulate forms a cake on the bag, which enhances the bag's filtering efficiency. However, excessive caking will increase the pressure drop across the fabric filter and reduce its efficiency.

Electrostatic Precipitator: Electrostatic precipitators (ESPs) remove particles from a gas stream through the use of electrical forces. Discharge electrodes apply a negative charge to particles passing through a strong electrical field. These charged particles then migrate to a collecting electrode having an opposite, or positive, charge. Collected particles are removed from the collecting electrodes by periodic mechanical rapping.

4.3.1.2 ELIMINATE TECHNICALLY INFEASIBLE OPTIONS

Baghouses and ESPs are not designed to operate under conditions in which the gas stream contains water vapor or other moist/sticky elements. Because of the nature of the moist, sticky exhaust stream from the pellet coolers, baghouses are anticipated to provide it would be expected to see particulate agglomeration on dry ESPs and baghouses. Therefore both the dry ESP and baghouse is technically infeasible to control PM.

4.3.1.3 IMPACTS ANALYSIS

The annualized costs of WESP control for the pellet cooler cyclones is approximately \$1,065,000, as presented in Table 4-9. Baseline emissions from the cooler cyclones is 61.95 tpy at 0.022 grains per actual cubic foot (gr/acf) outlet grain loading. The WESP system presented in Table 4-9 is estimated to reduce emissions to 0.008 gr/acf, which would result in a control efficiency of approximately 63.6%, equivalent to a 39.4 tpy emission reduction. Thus, the cost effectiveness of WESP control is estimated to be approximately \$27,000/ton, clearly cost prohibitive.

4.3.1.4 SELECT BACT

The proposed BACT emission rate for the pellet cooler cyclones is 0.022 gr PM/acf, a level considered near the lowest levels reliably achieved via cyclone control.¹²

¹² Air & Waste Management Association, Table 4 - Cyclone and Fabric Filter Performance, "Air Pollution Control Manual," 2000.

4.4 DIESEL ENGINES

One 350 kW emergency generator and a 300 hp fire pump powered by diesel will be installed as part of this project. Other than for use during emergency service, both engines are limited to a maximum of 100 hours per year of operation for maintenance and readiness testing under the NSPS standards of Subpart IIII. Add-on controls are impractical given the intermittent operation of these sources. Accordingly, Enviva proposes the NSPS IIII standards as BACT for NO_x, PM, and CO for these engines.

GHG emissions will be limited by limiting the use of the NSPS-compliant engines to maintenance, readiness testing and emergency use only. The only appropriate method of reducing GHG emissions is selection of fuel-efficient engines, which obviously minimizes CO₂, CH₄, and N₂O emissions. Since new, NSPS-compliant engines will be utilized, the engines will be fuel efficient. Since ultimate engine selection must necessarily take into account reliability in emergency operation, instead of a specific emissions standard Enviva proposes a work practice standard of limiting operation of the engines to maintenance, readiness testing and emergency use only.

4.5 HAMMERMILLS/ HAMMERMILL AREA BAGHOUSE/ PELLET PRESS SILO

TSP/PM₁₀/PM_{2.5} emissions from the hammermills, hammermills area bagfilter, and pellet press silo will be controlled with fabric filtration sytems. Baghouses are capable of achieving the lowest achievable emission rates of potentially applicable particulate matter control devices for filterable PM. The proposed BACT is based on an outlet grain loading factor of 0.005 gr/acf, which is essentially approaching the lowest emission levels reliably achieved using fabric filter control.

4.6 SUMMARY OF PROPOSED BACT EMISSION LIMITS

A summary of proposed BACT emission levels and associated control technologies for each emission source is provided in Table 4-10.

TABLES

TABLE 3-1
PSD APPLICABILITY SUMMARY
ENVIVA PELLETS NORTHAMPTON, LLC

Source Description	Unit ID	CO (tpy)	NOx (tpy)	TSP (tpy)	PM-10 (tpy)	PM-2.5 (tpy)	SO2 (tpy)	VOC (tpy)	CO _{2e} (tpy)
Dryer System	ES-DRYER	275.50	187.63	36.79	36.79	36.79	22.67	356.25	158,566.84
Emergency Generator	ES-EG	0.50	0.58	0.03	0.03	0.03	0.00	0.00	93.04
Fire Water Pump	ES-FWP	0.43	0.49	0.05	0.02	0.02	0.00	0.00	79.75
Hammermills	ES-HM-1, -2, -3, -4	1	•	15.02	15.02	15.02	•	•	1
Hammermills Area Filter	ES-HMA	*	,	7.04	7.04	7.04	•	•	,
Pellet Mill Feed Silo	ES-PMFS	1	1	0.47	0.47	0.47		ı	,
Pellet Coolers	ES-CLR	1	1	61.95	61.95	61.95	,	,	-
Log Debarking/Chipping	ES-CHIP-1	ı	1	,	1	1	,	1.25	1
Diesel Storage Tanks	TK1 & TK2	ı	1	0)	*:	1	1	3.79E-03	1
Total Proje	Total Project Emission Increases	276.44	188.69	121.31	121.31	121.31	22.67	357.51	158,739.64
PSD Signi	PSD Significant Emission Rates	100	40	25	10	15	40	40	100,000
ď	PSD Review Required?	Yes	Yes	Yes	Yes	Yes	No	Yes	Yes

TABLE 3-2 FACILITYWIDE HAP EMISSIONS SUMMARY ENVIVA PELLETS NORTHAMPTON, LLC

Description	ES-DRYER (tpy)	ES-EG (tpy)	ES-FWP (tpy)	ES-CHIP-1 (tpy)	Total (tpy)
1.3-Butadiene	-	2.39E-05	2.05E-05	-	4.45E-05
Acetaldehyde	2.60	4.70E-04	4.03E-04	1	2.60
Acrolein	08.0	5.67E-05	4.86E-05	-	0.80
Benzene	0.26	5.71E-04	4.90E-04	1	0.26
Chloroform	3.47E-03	-	-	1	3.47E-03
Cumene	0.07	1	ı	t	0.07
Formaldehyde	4.85	7.23E-04	6.20E-04	1	4.85
m-,p-Xylene	0.17	1.75E-04	1.50E-04	1	0.17
Methanol	3.81	1	-	0.24	3.81
Methyl isobutyl ketone	0.24	1	-	1	0.24
Methylene chloride	90.0	1	-	1	90'0
o-Xylene	0.02	ı	-	1	0.02
Phenol	0.97	-	1	1	0.97
Propionaldehyde	0.45	1	-	ľ	0.45
Styrene	0.01	t	t	-	0.01
Toluene	0.45	2.51E-04	2.15E-04	1	0.45
Total PAH (POM)	•	1.03E-04	8.82E-05	-	1.91E-04
TOTAL HAP	14.77	2.37E-03	2.03E-03	0.24	14.77

TABLE 3-3 DETERMINATION OF POLLUTANTS SUBJECT TO AIR TOXICS PERMITTING ENVIVA PELLETS NORTHAMPTON, LLC

TAP Emissions

Pollutant (Dryer		Eme	Emergency Generator	ator	-	Fire Water Pump	du		Total	
1.3-Butadiene	CAS Number	(lb/hr)	(Ib/day)	(lb/yr)	(Ib/hr)	(lb/day)	(lb/yr)	(lb/hr)	(lb/day)	(lb/vr)	(lb/hr)	(Ib/dav)	(lh/vr)
	106-99-0						4.79E-02			4.11E-02			8 90F-02
Acetaldehyde	75-07-0	4.61E+00			1.88E-03			1.61E-03			4 62E+00		2000
Acrolein	107-02-8	1.41E+00			2.27E-04			1.94E-04			141F+00		
Benzene	71-43-2			5.27E+02			1.14E+00			9.80E-01			\$ 29E+02
Benzo(a)pyrene	50-32-8						2.30E-04			1 97E-04			1 20E 04
Chloroform	67-66-3			6 93E+00									4.20E-04
													6.93E+00
Formaldehyde	20-00-0	8.61E+00			2.89E-03			2.48E-03			8.62E+00		
Xylene	1330-20-7	3.23E-01	7.75E+00		6.98E-04	1.68E-02		5.99E-04	1.44F-02		3.24E-0.1	7 78E+00	
Methyl isobutyl ketone	108-10-1	4.24E-01	1.02E+01								4 245 01	10.00.0	
Methylene chloride	75-09-2	1.11E-01		1.25E+02							111501	1.02220.1	00 230 1
Phenol	108-95-2	1.72E+00									1 775100		1.23E±02
Styrene	100-42-5	2.21E-02									2.72E:00		
Tohuene	108-88-3		1.92E+01			2.40E-02			2 06E-02		40-014-0	1 00 5 101	

TPER Comparison Table

			Total		-	TPER (2Q .0711)	2	Modeling
Pollutant	CAS Number	(lb/hr)	(Ib/day)	(lb/yr)	(lb/hr)	(Ib/day)	(lb/yr)	Required?
1,3-Butadiene	0-66-901			8.90E-02			1.10E+01	Š
Acetaldehyde	75-07-0	4.62E+00			6.80E+00			ž
Acrolein	107-02-8	1.41E+00			2.00E-02			Yes
Benzene	71-43-2			5.29E+02			8 10F+00	Ves
Benzo(a)pyrene	50-32-8			4.28E-04			2.20E+00	S. N
Chloroform	67-66-3			6.93E+00			2.90E+02	2
Formaldehyde	50-00-0	8.62E+00			4.00E-02			Yes
Xylene	1330-20-7	3.24E-01	7.78E+00		1.64E+01	5.70E+01		S. S.
Methyl isobutyl ketone	108-10-1	4.24E-01	1.02E+01		7.60E+00	5.20E+01		S N
Methylene chloride	75-09-2	1.11E-01		1,25E+02	3.90E-01		1 60F+03	S Z
Phenol	108-95-2	1.72E+00			2.40E-01			Ver
Styrene	100-42-5	2.21E-02			2.70E+00			Z
Toluene	108-88-3		1.92E+01			9.80E+01		N.

TABLE 4-1 DRYER BACT INPUT PARAMETERS AND EMISSIONS ESTIMATES ENVIVA PELLETS NORTHAMPTON, LLC

Operating Assumptions:

Total Dryer heat input capacity = Operating hours and days =

WESP Outlet flow rate =

WESP Outlet flow rate =

Total Plant estimated heat input =

Dryer Temperature =

Dryer Production =

Annual Dried Wood Throughput of Dryer =

Nominal Hourly Dried Wood Throughput of Dryer =

Maximum Hourly Dried Wood Throughput of Dryer =

Percent Hardwood

Percent Softwood

207 MMBtu/hr

8,760 hrs/yr

175,000 ACFM

146,389 SCFM assuming 171 deg. F

1,813,320 MMBtu/yr

171 deg. F

500,000 tons/year

475,000 ODT/year

54.22 ODT/hr

61.50 ODT/hr

90%

10%

Criteria Pollutant Calculations:

Pollutant	Biomass Emission Factor	Biomass Emission Factor	Emission Factor Source	Total Po Emiss	
ronutan	(lb/MMBtu)	(lb/ODT)		(lb/hr)	(tpy)
со		1.16	Calculated from Guaranteed WESP Specifications	71.34	275.5
NO _x		0.79	Calculated from Guaranteed WESP Specifications ^{1,4}	48.59	187.6
PM/PM ₁₀ /PM _{2.5} Condensable Fraction	0.017		AP-42, Section 1.6 ²	3.52	15.4
TSP (Filterable)		0.09	Calculated from Guaranteed WESP Specifications ¹	5.54	21.4
Total TSP (Filterable+ Condensable)				9.05	36.8
PM ₁₀ (Filterable)		0.09	Calculated from Guaranteed WESP Specifications ¹	5.54	21.4
Total PM ₁₀ (Filterable+ Condensable)				9.05	36.8
PM _{3.5} (Filterable)		0.09	Calculated from Guaranteed WESP Specifications ¹	5.54	21.4
Total PM25(Filterable+ Condensable)				9.05	36.8
SOn	0.025		AP-42, Section 1.6 ³	5.18	22.7
VOC		1,50	Calculated from Guaranteed WESP Specifications ¹	92.25	356.3

- 1. CO, NO_x, VOC, and filterable PM/PM₁₀ emission factors were provided by the dryer system vendor. The PM_{2.5} filterable emission factor is assumed to be the same as PM and PM₁₀.
- 2. The vendor only provided the filterable fraction of particulate matter in the emission factors. The condensable fraction of particulate matter from a rotary dryer controlled by a WESP is not provided in AP-42, Section 10.6.2. Enviva has conservatively calculated the condensable fraction based upon the heat input of the dryer burners using an emission factor for wood combustion from AP-42, Section 1.6.
- 3. No emission factor is provided in AP-42, Section 10.6.2 for SO₂ for rotary dryers. Enviva has conservatively calculated SO2 emissions based upon the heat input of the dryer burners using an emission factor for wood combustion from AP-42, Section 1.6.
- 4. Equivalent to a 0.235 lb/MM Btu level at the rated burner capacity of 207 mmBtu/br.

STOKER BOILER NO_X DATA FROM RBLC ENVIVA PELLETS NORTHAMTON, LLC

Company	Location	Boiler (MMBtu/hr)	Limit (lb/MMBtu)	NOx Control Technology
SIERRA PACIFIC INDUSTRIES	Grays Harbor, WA	310	0.15 (24-hour) 0.1 (annual)	Spreader Stoker, SNCR
MULTITRADE OF	Virginia	373.3	0.1 (30-Day Roll)	Spreader Stoker Boilers, SNCR
DARRINGTON ENERGY LLC	Washington	403	0.12 (24-hr ave)	SNCR
SIERRA PACIFIC	Washington	430	0.13	SNCR
DISTRICT ENERGY ST.	Ramsey, MN	550	0.15	SNCR
BEAVER- ASHLAND ALTERNATIVE ENERGY	Maine	534	0.15	SNCR
ADM NORTHERN SUN	North Dakota	280	0.2 (30-day roll)	Combustion Controls
SD WARREN	Somerset, ME	1,300	0.2	Multi-fuel boiler, SNCR
BORALEX CHATEAUGAY	Arkansas	275	0.23	
DEL-TIN FIBER, LLC	Union, AR	291	0.3	Closed Loop Gasification System gasifies biomass fuel in a rotary kiln to produce a combustible gas used as fuel in a secondary combustion chamber. Lovy NO _X combustors, SNCR.
CLEWISTON SUGAR MILL AND REFINERY	Florida	812	0.31	Boiler #7 Spreader Stoker
MEADWESTVACO	Wickliffe, KY	631	0.4	Multi-fuel boiler, including NCGs
INLAND PAPERBOARD AND PACKAGAING	Louisiana	787.5	0.45	OFA,LNB, Good Combustion

Trinity Consultants File: Enviva BACT Calculations 8.14.11 Sheet: Table 2 NOx RBLC

TABLE 4-3
SELECTIVE NON-CATALYTIC REACTOR COST ANALYSIS FOR ROTARY DRYER ENVIVA PELLETS NORTHAMPTON, LLC

Cost Item		Notes	Reference
Direct Capital Costs			
Total Equipment Cost	\$575,468		2(a), 4
Installation Estimate	\$1,056,250		2(b)
Fotal Capital Investment	\$1,631,718		
Operating Cost			
Direct Annual Costs Capacity Factor For Direct Annual Costs	88.2%		3(a)
Operation and Maintenance Costs	\$25,000		2(c)
Reagent Costs (50% Urea Solution)			
Reagent Consumption	8.15	gph	2(d), 5
Reagent Cost	\$2.00	(\$/gal)	2(d)
Total	\$125,935		
Compressed Air			
Compressed Air	41	scfm	2(e), 5
Air Price	\$0.15	\$/1000 ft ³ air	
Total	\$2,869		
Water Consumption			2/0 5
Water	162	gph	2(f), 5 3(b)
Water Price	\$1.65	\$/1000 gallons	3(0)
Total	\$2,059		
Electricity		l	2(-) 5
Power	3	kW	3(c), 5
Unit Cost	\$0.075	\$/kWh	
Total	\$1,671		
Total Direct Annual Costs	\$157,534		
Indirect Annual Costs			
Administrative Charges	\$32,634	2% of TCI	
Property tax	\$16,317	1% of TCI	
Insurance	\$16,317	1% of TCI	
Annual Interest Rate	10%		
Economic life of SNCR	15		
Capital Recovery Factor	0.131		1(b)
Total Capital Recovery Cost	\$214,528		
Total Indirect Annual Costs	\$279,797		
Total Annual Cost	\$437,331		

TABLE 4-3 SELECTIVE NON-CATALYTIC REACTOR COST ANALYSIS FOR ROTARY DRYER ENVIVA PELLETS NORTHAMPTON, LLC

- 1. U.S. EPA OAQPS, EPA Air Pollution Control Cost Manual (6th Edition), March 2003, Section 4.2, Chapter 2.
 - " No taxes, Insurance, Admin applies (OAQPS 1-37)
 - ^b Equation 1.34 for CFI (OAQPS 1-38)
- Fuel Tech Vendor Quote provided for Hertford Renewable Energy PSD Application (Hertford, North Carolina). Submitted 2008, Approved 2009.
 - a Cost of SNCR System
 - b BOP Interface Design Engineering and Erection Assumes Install = 1.25 x Mat'l & Engineering
 - c Estimated Value, Parts and Labor
 - d Reagent Consumption (gph) and Cost (\$/gal) from vendor-90% Capacity
 - e Plant air + instrument air, based on \$0.15 per 1000 cubic feet of air
 - f Assumes I gpm per injector total flow and \$2.50 per 1000 gallons filtered water
- 3 Sources as follows:
 - a Capacity factor calculated as 8760 times the average hourly annual throughput divided by maximum hourly throughput (54.22 ODT/hr / 61.5 ODT/hr)
 - b Base water price from Hertford Renewable Energy PSD Application (Hertford, North Carolina). Submitted 2008, Approved 2009.
 - c Base electricity price from Hertford Renewable Energy PSD Application (Hertford, North Carolina). Submitted 2008, Approved 2009.
- Scale-up capital cost factor from Ulrich, Gael D. Chemical Engineering Process Design and Economics, 2004 (C1*(S2/S1)^{0.6}) where S1 is Hertford boiler flow rate of 331,969 ACFM and S2 is the flow rate of 175,000 ACFM
- 5. Scaled original quoted reagent consumption based on the Herford NOx emissions reduction at 762.5 MMBTU/hr versus the dryer heat input rating of 175 MMBtu/hr. Herford had a reduction from a NOx reduction from 0.30 lb/MMBTU to 0.15 lb/MMBTU at 762.5 MMBTU/hr or
- 114.4 lb/hr reduction. The dryer will have a NOx reduction of 0.23 lb/mmBtu to 0.15 lb/mmBtu or 16.56 lbs/hr reduction.

Thus, multiply the Hertford quote by 16.56/114.4, which is equal to

0.145

Electricity, Water, and Compressed air were also scaled accordingly

TABLE 4-4
NO, BACT IMPACTS SUMMARY FOR ROTARY DRYER
ENVIVA PELLETS NORTHAMPTON, LLC

									Environmental
					Fcono	Economic Impacts		Energy Impacts	Impacts
									Adverse
Control	Baseline	Control	Emissions	Total Capital	Annual	Cost Effectiveness	Incremental Cost Effectiveness	Increase Over Baseline	Environmental Impacts?
Options (lb/ODT)	Emissions (tons/yr)	Efficiency	(tons/year)	(S)	(\$/year)	(\$/ton)	(\$/ton)	(kW*hr/yr)	(Yes/No)
SNCR = 0.515 lb/ODT (0.15	187.63	34 8%	65.3	\$1.631.718	\$437,331	\$6,701	\$6,701	3.56E+06	No
ID/MIM But)	10.701	20.00							
Baseline = 0.79 lb/ODT	187 63	Υ/Z	V/A	N/A	N/A	N/A	N/A	3598469.789	No
(mid MIMI/01 cc2.0)	20.701								

Trinity Consultants File: Enviva BACT Calculations 8.14.11 Sheet: Table 4 NOx Summary

TABLE 4-5 REGENERATIVE THERMAL OXIDATION COST ANALYSIS FOR ROTARY DRYER ENVIVA PELLETS NORTHAMPTON, LLC

Cost Item		Notes	Reference
Direct Costs			
Purchased Equipment Costs			
RTO Price+ Freight+Instrumentation	\$2,950,000	A	2(a)
Sales Tax Purchased Equipment Cost, PEC	\$88,500	0.03A B	1(a)
i dichased Equipment Cost, FEC	\$3,038,500	P	
Direct Installation Costs			
Foundations and Support	\$243,080	0.08B	1(a)
Handling & Erection Electrical	\$425,390 \$121,540	0.14B 0.04B	1(a)
Piping	\$60,770	0.02B	1(a) 1(a)
Insulation for ductwork	\$30,385	0.01B	1(a)
Painting	\$30,385	0.01B	1(a)
Direct Installation Costs	\$911,550		
Total Direct Costs, DC	\$3,950,050		
Indirect Costs (Installation)			
Engineering Construction and field expenses	\$303,850	0.10B	1(a)
Construction and field expenses Contractor Fees	\$151,925 \$303,850	0.05B 0.10B	1(a) 1(a)
Start-up	\$60,770	0.02B	1(a) 1(a)
Performance test	\$30,385	0.01B	1(a)
Contingencies	\$91,155	0.03B	1(a)
Total Indirect Costs, IC	\$941,935		
Total Capital Investment	\$4,891,985	TCI = DC + IC	
Operating Cost			
Direct Annual Costs			
Capacity Factor For Direct Annual Costs	88.2%	used to establish hours/yr of operation	
Operating Labor			
Operator	\$24,753	0.5 hr/s, 3 s/d, d/yr, \$51.26/hr, CF	1(b), 3(a)
Supervisor	\$3,713	15% of operator	1(b)
Total	\$28,466		
Maintenance			
Labor	\$24,753	0.5 hr/s, 3 s/d, d/yr, \$51.26/hr, CF	1(b), 3(a)
Material	\$24,753	100% of maintenance labor	1(b)
Total	\$49,506		
Electricity			
Total Requirement	461	KW	2(c)
Unit cost	\$0.075	\$/kW-hr	2(c)
Total	\$267,155		
Fuel			
Natural Gas Cost	8.64 \$6.00	MMBTU/hr \$/MMBtu	3(a)
Total	\$400,735	2. MINISTU	2(b)
Total Direct Annual Costs	\$745,863		
Indirect Annual Costs			
Overhead	\$46,784	60% of operating labor + maintenance	1(b)
Administrative Charges	\$97,840	2% of TCI	1(b)
Property tax	\$48,920	1% of TCI	1(b)
Insurance	\$48,920	1% of TCI	1(b)
Annual Interest Rate	10%		
Economic life of RTO	10		
Capital Recovery Factor	0.163		
Total Capital Recovery Cost	\$796,148		
Total Indirect Annual Costs	\$1.038.611		

TABLE 4-5 REGENERATIVE THERMAL OXIDATION COST ANALYSIS FOR ROTARY DRYER ENVIVA PELLETS NORTHAMPTON, LLC

- 1. U.S. EPA OAQPS, EPA Air Pollution Control Cost Manual (6th Edition), September 2000, Section 3, Chapter 2.
 - ^a Table 2.8: Capital Cost Factors for Thermal and Catalytic Incinerators (OAQPS 2-42); Vendor quote usually includes instrumentation
 - ^b Table 2.10: Annual Costs for Thermal and Catalytic Incinerators Example Problem (OAQPS 2-45)
- 2. Provided to Wallace Lasonde of Enviva by Steve Jassund from GEOENERGY Division of A.H. Lundberg Associates, Inc on March 21, 2011.
 - a RTO Price/Quote
 - b Natural Gas Cost and usage.
 - c Electricity cost and power requirement.
- 3. Taken from Methodology for Estimating Control Costs for Industrial, Commercial, Institutional Boilers and Process Heaters Nation Emissions Standards for Hazardous Air Pollutants -- Major Source ERG Memo April 2010.
 - a Conservative estimate of loaded hourly wage
 - b Compressed Air Cost from Memo
- 4. U.S. EPA OAQPS, EPA Air Pollution Control Cost Manual (6th Edition), July 2002, Section 6, Chapter 2.
 - a Equation 2.40 for fan HP (OAQPS 2-42)

TABLE 4-6 REGENERATIVE CATALYTIC OXIDATION COST ANALYSIS FOR ROTARY DRYER ENVIVA PELLETS NORTHAMPTON, LLC

Cost Item		Notes	Reference
Direct Costs			
Purchased Equipment Costs			
RCO Price + auxiliary equipment + freight	\$3,881,854	A	2(a), 6
Sales Tax	\$116,456	0.03A	1(a)
Purchased Equipment Cost, PEC	\$3,998,309	В	
Direct Installation Costs			
Foundations and Support	\$319,865	0.08B	1(-)
Handling & Erection	\$559,763	0.14B	l(a) l(a)
Electrical	\$159,932	0.04B	1(a) 1(a)
Piping	\$79,966	0.02B	l(a)
Insulation for ductwork	\$39,983	0.01B	l(a)
Painting	\$39,983	0.01B	1(a)
Direct Installation Costs	\$1,199,493	1	
Total Direct Costs, DC	\$5,197,802		
Indirect Costs (Installation)			
Engineering	\$399,831	0.10B	l(a)
Construction and field expenses	\$199,915	0.05B	1(a)
Contractor Fees	\$399,831	0.10B	1(a)
Start-up	\$79,966	0.02B	l(a)
Performance test	\$39,983	0.01B	1(a)
Contingencies	\$119,949	0.03B	1(a)
Total Indirect Costs, IC	\$1,239,476		
Total Capital Investment	\$6,437,278	TCI = DC + IC	
Operating Cost			
Direct Annual Costs			
Capacity Factor For Direct Annual Costs	88.2%	used to establish hours/yr of operation	
Operating Labor			
	\$34 TE2	0.5 halo 2 a/d disc 001 000	103 103
Operator	\$24,753	0.5 hr/s, 3 s/d, d/yr, \$51.26/hr, CF	I(b), 4(a)
Supervisor	\$3,713	15% of operator	1(b)
Total	\$28,466		
Maintenance			
Labor	\$24,753	0.5 hr/s, 3 s/d, d/yr, \$51.26/hr, CF	1(b), 4(a)
Material	\$24,753	100% of maintenance labor	1(b)
Total	\$49,506	J. Managarana A.	*(0)
Electricity	.,		
Combustion Air Fan	16	HP	2(a), (d), 7
Hydraulic Power unit	5	HP	
Misc./Instruments, Hydraulic Heaters	8	KW	2(a), (d), 7
•	ð		2(a), (d), 7
Fan Power to Overcome Catalyst Pressure	593	HP (14 iwc), Assumed 65% Efficiency, Flowrate 87,222 ACFM	2(d), 5(a)
Total Requirement	466	KW	
Unit cost	\$0.075	S/kW-hr	3(b)
Total	\$269,885		3(0)
Fuel			
Natural Gas or fuel	1,6	MBTU/br	3(a), 7
Cost	\$6.00	\$/MMBtu	5(a), 7
Conversion	1020	Btu/ft ³	· ·
Total	\$80,591		
Compressed Air			
Requirement	38	SCFM	2(a) 4(b) 7
Cost	\$0.31	\$/1000 ft ³ air	2(a), 4(b), 7
Total	\$5,394	J TOOU IL BII	4(b)
Catalyst Costs	100 1		
Catalyst Cost (Present Value)	\$421,726		2(b), 7
Catalyst Life	2		2(b), 7 2(b)
Catalyst Cost (Future Value)	\$451,669	F/P, 3.5%, 2 years	2(0)
Catalyst Cost (Annualized) Total	\$215,085	A/F, 10%, 2 years	

TABLE 4-6 REGENERATIVE CATALYTIC OXIDATION COST ANALYSIS FOR ROTARY DRYER ENVIVA PELLETS NORTHAMPTON, LLC

Cost Item		Notes	Reference
Indirect Annual Costs			
Overhead	\$46,784	60% of operating labor + maintenance	1(b)
Administrative Charges	\$128,746	2% of TCI	1(b)
Property tax	\$64,373	1% of TCI	1(b)
Insurance	\$64,373	1% of TCI	1(b)
Annual Interest Rate	10%		
Economic life of RCO	10		
Capital Recovery Factor	0.163		
Total Capital Recovery Cost	\$1,047,637		
Total Indirect Annual Costs	\$1,351,912		
Total Annual Cost	\$2,000,839	TAC = DAC + IDAC	

- 1. U.S. EPA OAQPS, EPA Air Pollution Control Cost Manual (6th Edition), September 2000, Section 3, Chapter 2.
 - Table 2.8: Capital Cost Factors for Thermal and Catalytic Incinerators (OAQPS 2-42), Vendor quote usually includes instrumentation
 - ^b Table 2.10: Annual Costs for Thermal and Catalytic Incinerators Example Problem (OAQPS 2-45)
- 2. Hertford Renewable Energy PSD Application (Hertford, North Carolina). Submitted 2008, Approved 2009.
 - a RCO Price/Quote
 - b Catalyst costs and life
 - c Fuel Requirement was 2.5 MBTU/hr
 - d 14 iwc for pressure drop and RCO electricity and utility usage were similar to RSCR
- 3. Enviva Vendor
 - a Natural Gas Cost
 - b Electricity cost
- 4. Takeu from Methodology for Estimating Control Costs for Industrial, Commercial, Institutional Boilers and Process Heaters Nation Emissions Standards for Hazardous Air Pollutants -- Major Source ERG Memo April 2010.
 - a Conservative estimate of loaded hourly wage
 - b Electricity and Compressed Air Cost from Memo
- 5. U.S. EPA OAQPS, EPA Air Pollution Control Cost Manual (6th Edition), July 2002, Section 6. Chapter 2.
 - a Equation 2.40 for fan HP (OAQPS 2-42)
- 6. Scale-up capital cost factor from Ulrich, Gael D. Chemical Engineering Process Design and Economics, 2004 (C1*(S2/S1)^{0.6}) where S1 is Hertford boiler flow rate of 279,736ACFM and S2 is the Enviva boiler flow rate of 175,000 ACFM
- 7. Scaled up Direct Annual Costs linearly based on Hertford Application boiler flow rate of 279,736 ACFM and Enviva flow rate of of 175,000 ACFM. The resulting Qnew/Qinitial =

TABLE 4-7
VOC BACT IMPACTS SUMMARY FOR ROTARY DRYER
ENVIVA PELLETS NORTHAMPTON, LLC

								Environmental
					Economic Impacts		Energy Impacts	Impacts
								Adverse
Control	Uncontrolled	Control	Emissions	Total Capital	Annual	Cost	Increase Over	Environmental
Options	Emissions	Efficiency	Reduction	Cost	Cost	Effectiveness	Baseline	Impacts?
(lb/ODT)	(tons/yr)		(tons/year)	(\$)	(\$/year)	(\$/ton)	(kW*hr/yr)	(Yes/No)
0.15 (RTO)	356.25	%06	320.6	\$4,891,985	\$1,784,474	\$5,566	3.56E+06	No
0.45 (RCO)	356.25	20%	249.4	\$6,437,278	\$2,000,839	\$8,023	3.60E+06	No
1 50 lh/ODT (Pracess Design) ²	356.25	Α/Z	A/N	V.Z	Ø/N	N/A	N/A	ž

¹ For purposes of streamlining this evaluation, use of at least 90% hardwood species is assumed to be "baseline." However, it should be recognized that emissions are estimated to be approximately 68% less than a traditional softwood mill. Trinity Consultants File: Enviva BACT Calculations 8.14.11 Sheet: 7 VOC Summary

TABLE 4-8
CO BACT IMPACTS SUMMARY FOR ROTARY DRYER
ENVIVA PELLETS NORTHAMPTON, LLC

									Environmental
					Econol	Economic Impacts		Energy Impacts	Impacts
									Adverse
En Br	Baseline Emissions (tons/yr)	Control	Emissions Reduction (tons/year)	Total Capital Cost (\$)	Annual Cost (\$/year)	Cost Effectiveness (\$/ton)	Incremental Cost Effectiveness (\$/ton)	Increase Over Baseline (kW*hr/yr)	Environmental Impacts? (Yes/No)
								İ	ST.
	· ·	,000	0.000	\$4 801 985	\$1 784.474	\$7,197	\$7,197	3.56E+06	ON
7	275.50	9/0/	240.0	44.074,702		11000	270 275	3 40E±06	Z
	V	7007	10.0	\$6 437 278	\$2,000,839	\$10,375	\$10,575	3.005.00	
. ~1	275.50	0/0/	172.7	2011		4444	A11.A	N/A	Š
1	00 000	NIA	N/A	N/A	A/Z	N/A	N/A	17/1/	
7	00.012	C/A	1777						

TABLE 4-9 WET ESP COST ANALYSIS FOR PELLET COOLERS ENVIVA PELLETS NORTHAMPTON, LLC

Cost Item		Notes .	Ref.
al Capital Investment			
Direct Costs			
Purchased Equipment Costs			
ESP	\$1,832,031	A	1, 11
Freight Estimate	\$164,539		1(a), 11
Instrumentation	\$183,203	0.10A	2
Sales Tax	\$54,961	0.03A	2
Purchased Equipment Cost, PEC	\$2,234,733	В	
Direct Installation Costs			
Foundations and Support	\$89,389	0.04B	2
Handling & Erection	\$1,117,367	0.50B	2
Electrical	\$178,779	0.08B	2
Piping	\$22,347	0.01B	2
Insulation for ductwork	\$44,695	0.02B	2
	\$44,695	0.02B	2
Painting <i>Total</i>	\$1,497,271	0.045	
Total Direct Costs, DC	\$3,732,005	DC = B + 0.67 * B	
Indirect Costs (Installation)			
Engineering	\$446,947	0.20B	2
Construction and field expenses	\$446,947	0.20B	2
Contractor Fees	\$223,473	0.10B	
	\$22,347	0.01B	2
Start-up	\$22,347	0.01B	2
Performance test	\$44,695	0.02B	2 2 2 2
Model study Contingencies	\$67,042	0.03B	2
Total Indirect Costs, IC	\$1,273,798	IC = 0.57 * B	
Total Capital Investment	\$5,005,803	TCI = DC + IC	
Operating Cost			
Direct Annual Costs			
Capacity Factor For Direct Annual Costs	88.2%	used to establish hours/yr of operati	on
Operating Labor			
Operator	\$49,506	3 hr/d * d/y * \$51.26/hr	3(a), 5
Supervisor	\$7,426	15% of operator	3(b)
Coordinator	\$16,502	1/3 of operator	3(c)
Total	\$73,434		-
Maintenance		,	
Labor	\$1,031	0.825*ESP Plate Area (ft ²)	4, 12
Material	\$22,347		3(d)
Total	\$23,378		
Electricity Costs			
Requirement	94	kw/HR	6(a), 9, 11
Unit cost	\$0.070	\$/kW-hr	9
Total	\$50,704		
Water Costs			
Wastewater Disposal	\$954	1	6(b), 7

TABLE 4-9 WET ESP COST ANALYSIS FOR PELLET COOLERS ENVIVA PELLETS NORTHAMPTON, LLC

Cost Item		Notes	Ref.
Municipal Water Usage Total Direct Annual Costs	\$159 \$1,113 <i>\$148,629</i>		6(b), 8
Indirect Annual Costs Overhead Administrative Charges Property tax Insurance Annual Interest Rate Economic life of ESP Capital Recovery Factor Total Capital Recovery Cost Total Indirect Annual Costs	\$58,088 \$100,116 \$50,058 \$50,058 10.0% 15 0.1315 \$658,132	60% * (operating labor + maintenance) 2% of TCI 1% of TCI 1% of TCI	3(e) 3(e) 3(e) 3(e) 10 10 10
l Annual Cost	\$1,065,081	TAC = DAC + IDAC	

- 1. Cost estimate of \$3.3 provided by TurboSonic (6/22/2010) for Unilin wood products dryer (PSD application processed by NCDAQ).
 - a Email from Rod Pennington (TurboSonic) to Joe Sullivan (Trinity) June 26, 2010 that stated additional freight costs not included.
- 2. Direct and Indirect capital costs associated with the purchase of the ESP determined in accordance with EPA OAQPS APCCM Sec.6, Ch.3, Table 3.16
- 3. EPA OAQPS APCCM Sec.6, Ch.3, Table 3.21
 - (a) Operator costs calculated @ 3 hr per day and 88.2% operating factor
 - (b) Supervisor labor costs calculated @ 15% of operator cost as per APCCM guidance
 - (c) Coordinator costs calculated @ 1/3 of operator costs as per APCCM guidance
 - (d) Maintenance material(s) calculated @ 1% of purchased equipment cost as per APCCM guidance
 - (e) Indirect annual costs calculated in accordance with APCCM guidance
- 4. EPA OAQPS APCCM Sec.6, Ch.3, Equation 3.45 for Maintenance Materials
- 5. US Dept. of Labor Bureau of Labor Statistics \$51.26/hr (Stationary Engineers and Boiler Operators, 2008 dollars)
- 6. Provided by TurboSonic, ESP supplier/vendor
 - (a) Electrical power requirements
 - (b) Wastewater blowdown rate (0.6 gallons / minute); assumes water usage (blowdown rate + 50% sump vol); assumes 6,000 hrs of operation.
- 7. Waste water disposal cost \$0.0054/gal provided by Air Compliance Advisor User Guide -
- 8. Municipal water usage cost \$0.0006 /gal provided by Electric Power Research Institute
- 9. Electricity unit cost provided by the Energy Information Administration (Electrical costs calculated assuming 88.2% operating factor)
- 10. Capital recovery calculated assuming 20 years of equipment life @ a recovery rate of 13.5% Capital Recovery Factor (CRF)
 - = $(IR*(1+IR)^n)/((1+IR)^n 1) = 0.1315$
- 11. Scale-up capital cost factor from Ulrich, Gael D. Chemical Engineering Process Design and Economics, 2004 (C1*(S2/S1)^{0.6}) where S1 is Unilin heating plant flow rate and S2 is Enviva pellet cooler cyclone flow rate.
- 12. Scaled up Direct Annual Costs linearly based on initial flow rate of 200,000 ACFM and pellet cooler cyclones flow rate 0.38 of 75,000 ACFM. The resulting Qnew/Qinitial

TABLE 4-10 SUMMARY OF PROPOSED BACT LIMITS ENVIVA PELLETS, LLC

Source	Pollutant	Control/Operation	Proposed Emission
	NO _x	Good combustion practices/design	0.79 lb/ODT
Rotary Dryer System	PM/PM ₁₀ /PM _{2.5}	Process Design (multiclones + WESP)	0.09 lb/ODT (filterable only)
Rotary Dryer System	VOC/CO	Process Design	1.50 lb/ODT VOC & 1.16 lb/ODT CO
	$\mathrm{CO}_{2\mathrm{e}}$	Biomass-fired / Energy Efficient Operation	N/A
Emergency Generator and Firewater Pump	$PM/PM_{10}/PM_{2.5}, NO_x,$ VOC, CO	Good combustion practices/design, minimize	NSPS Subpart IIII
Pellet Cooler	PM/PM ₁₀ /PM _{2.5}	Cyclones	0.022 gr/cf
Hammermills, Hammermill Area Filter, Pellet Press Silo	PM/PM ₁₀ /PM _{2.5}	Fabric filter	0.005 gr/cf

FIGURES

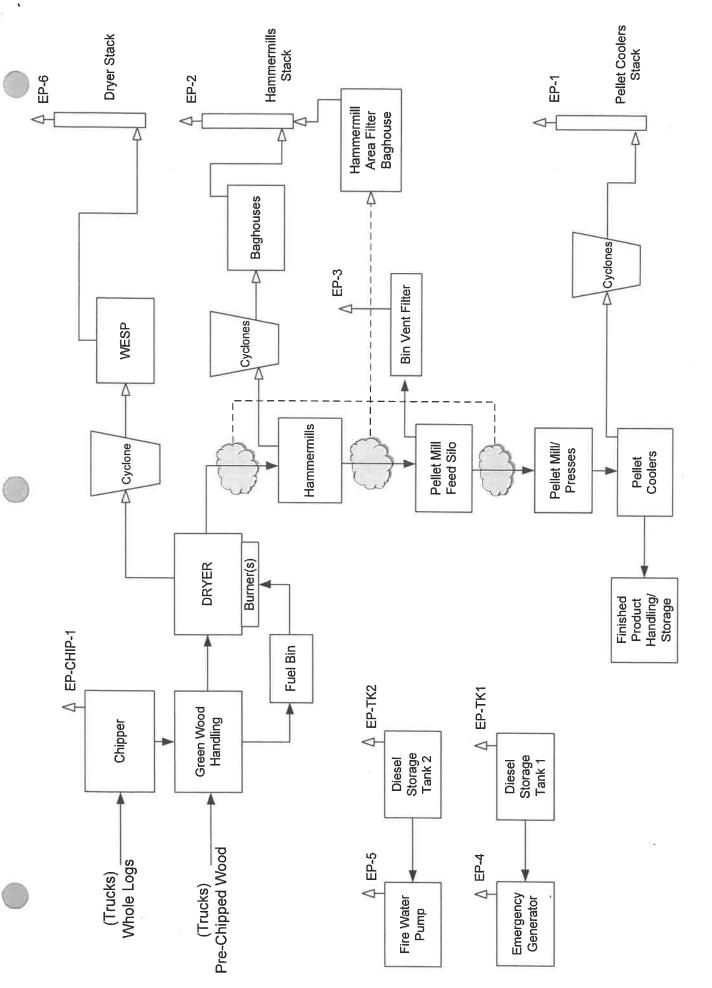


Figure 2-1. Process Flow Diagram

FORM A1

•			FURI	LAL			AL EVE		
		FACILITY	Y (Gener	al Infor	mation)	Palen		Office [
EVISED 11/01/02	NC	DENR/Division of Air Quality	- Applicatio	n for Air Pe	rmit to Construc	ct/Operate		Maries	A1
	NOTE- A	PPLICATION WILL NO	T BE PRO	CESSED	WITHOUT TI	HE FOLLOW	VING:	<u> </u>	-BYE! - 1
		cy Determination (if required)	✓ Facility R	eduction &	Recycling Survey	Form (Form A4) A ca	tion Fee	
		thorized Contact Signature	✓ ppropria	ite Number	of Copies of Appli	cation F	Seal (if req	uired)	
			IERAL INF	ORMATI	ON		- 1		*4
egal Corporate/Owner	Name: F	Enviva Pellets Northampton,	LLC		-				
ite Name: Enviva Pell								J-2	
ite Address (911 Addres		ebanon Church Road (Stree	t Number TE	3D)				ite Cellis	
	s) Lile 1.								C.
ite Address Line 2: City: Gaston				State:	North Carolina		4	UG 2 6 200	
	27866			County:	Northampton		Airo.	- 2011)
ip Code:	21000	COI	NTACT IN	ORMATI	ON		* 3	UG 2 6 2011	
	at.			Facility/Ins	pection Contact:			a	רכיו
Permit/Technical Contact lame/Title: Glenn Gray				Name/Title:	same as perm	it/technical co			
Mailing Address Line 1:	7200 Wisconsin Ave	niie			Iress Line 1:				
Mailing Address Line 1:	Suite 1100			Mailing Add	Iress Line 2:				
		Maryland Zip Code:	20814	City:		State:		Zip Code:	
City: Bethesda	0.0.10.		1) 657-5567	Phone No. I	(area code)		Fax No. (are	a code)	
Phone No. (area code) Email Address:	Glenn.Gray@enviva			Email Addre					
Responsible Official/Au				Invoice Co.	ntact:				
				Name/Title:	same as perm	it/technical co	ntact		
Name/Title: Norb Hint	7200 Wisconsin Ave	anua .			dress Line 1:				
Mailing Address Line 1:	Suite 1100	situo			dress Line 2:				
Mailing Address Line 2:		Maryland Zip Code:	20814	-		State:		Zip Code:	
City: Bethesda	(301) 657-5567		01) 657-5567	Phone No.	(area code)		Fax No. (are:	a code)	
Phone No. (area code)	Norb.Hintz@enviva			Email Addr					
Email Address:	NOID.THILE@ell4140	APPLICA	ATION IS	BEING M	ADE FOR				
	New Non-permitted Faci	lity/Greenfield Mod	lification of Fa	acility (permi	itted)	Rene	wal with Modif	ication	
	, , , , , , , , , , , , , , , , , , ,		Renewal	(TV Only)					
	F	ACILITY CLASSIFICAT	ION AFTE	R APPLIC	ATION (Chec	k Only One)		
Beneral	[]mall []	Prohibitory Small		Synthetic Mir		√ Title V			
		FACILIT	Y (Plant S	ite) INFO	RMATION				
Describe nature of (plan	t site) operation(s): Fa	cility ID No.: (t	to be assigne	ed)					
Wood pellet manufactu		and the second section of the second section is the second section of the second section of the second section of the second section is the second section of the second section of the second section section is the second section of the second section section is the second section of the second section							
Primary SIC/NAICS Cod	te: 2499 (Wood Produ	cts, Not Elsewhere Classified	d)	Current/Pr	evious Air Permit	No.	N/A	Expiration Date	e N/A
Facility Coordinates:	Latitude:	256,700 UTM E		Longitude:	4,042,900 UT	M N			
Does this application co		YES		√NO					
		PERSON OR FI	RM THAT	PREPAR	ED APPLICAT	rion			
Person Name:	Joe Sullivan			Firm Name	e: Trinity Const	ultants, Inc.			
Mailing Address Line 1:		ray		Mailing Ad	idress Line 2:	Suite 310	-		
City: Morrisvil		State: North Carolina	а	Zip Code:	27560		County:	Wake	
Phone No. (919) 462	-9693	Fax No. (919) 462-9694	4	Email Add			nityconsultant	s.com	
		SIGNATURE OF RESPO	ONSIBLE C	OFFICIAL	/AUTHORIZE	D CONTACT			
Name (typed):	North Hintz			Title:		ent Engineering			
X Signature(Blue lnk):	11/1			Date:	1	18,2	011		
	1 hup				17 -	,,,,	- / /		

Attach Additional Sheets As Necessary

FORMs A2, A3

EMISSION SOURCE LISTING FOR THIS APPLICATION - A2

112r APPLICABILITY INFORMATION - A3

SED 04/10/07	NCDENR/Division of Air Quality - Applic	L Burnianaly Linner	mitted Replaced Deleted	
(2)	EMISSION SOURCE LISTING: New, Modified	CONTROL DEVICE	CONTROL DEVICE	
MISSION SOURCE	EMISSION SOURCE	ID NO.	DESCRIPTION	
ID NO.	DESCRIPTION uipment To Be ADDED By This Application	New Previously		
	uipment To Be ADDED By This Application	CD-DC	Single Cyclone	
S-DRYER	Green Wood Direct-Fired Dryer System	CD-WESP	Wet Electrostatic Precipitator	
	2 (250 lov. 250 hbp)	N/A	N/A	
S-GN	Emergency Generator (250 kw, 350 bhp)	N/A	N/A	
S-FWP	Fire Water Pump (300 bhp)	CD-HM-CYC-1	Single Cyclone	
S-HM-1,-2,-3,-4	Four (4) Hammermills	CD-HM-CYC-2	Single Cyclone	
		CD-HM-CYC-3	Single Cyclone	
		CD-HM-CYC-4	Single Cyclone	
		CD-HM-BF1	Bagfilter	
		CD-HM-BF2	Bagfilter	
		CD-HMA-BF	Bagfilter	
S-HMA	Hammermill Area Filter	CD-PPS-BV	Bin vent filter	
S-PPS	Pellet Mill Feed Silo		Pellet Cooler Cyclone	
ES-CLR-1,2,3,4,5, 6	Six (6) Pellet Coolers	CD-CLR-1	Pellet Cooler Cyclone	
		CD-CLR-2	Pellet Cooler Cyclone	
		CD-CLR-3	Pellet Cooler Systems	
	Existing Permitted Equipment To	BeMODIFIED By	This Application	
MARKENSER	Existing 1 crimited Equipment			
	1			
		-		
			+	
	Furthers To Po DEL	ETED By This Apr	olication	
	Equipment To Be DEL	ETED By This App	olication	
	Equipment To Be DEL	ETED By This App	plication	
	Equipment To Be DEL	ETED By This App	blication	1000 400
	Equipment To Be DEL	ETED By This App	blication	
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	Equipment To Be DEL	ETED By This App	blication	
	Equipment To Be DEL	ETED By This App	blication	
	Equipment To Be DEL	ETED By This App	blication	
	112(r) APPLICAL	BILITY INFORMA	TION	1000
is your facility subject to	112(r) APPLICAL 40 CFR Part 68 "Prevention of Accidental Releases" - Section	BILITY INFORMA	TION	AS
s your facility subject to		BILITY INFORMA	TION	1007

Yes No Specify required RMP submittal date: B. Are you using administrative controls to subject your facility to a lesser 112(r) program standard? If yes, please specify:

Yes e No e

If submitted, RMP submittal date:

FORM A4								
SURVE	EY OF AIR EMISSION	NS AND FACILITY - WI	DE REDUCTION &	RECYCLING ACTIVITI	ES			
DATE:	Does facility have	an environmental mar	ngement system in	place?()YES(X)NO	If so, is facility ISO 1400	0 Certified? () YES (X) N	0	
Facility Name:	Enviva Pellets No				Permit Number:	N/A		
lity ID:	N/A (to be assigned)	County:	Northampton		Environmental Contact:	Glenn Gray / Plant Manag	јег	
Mailing Address		Lebanon Church Ro	- 4					
Mailing Address		Lebation Church Ro	au		Phone No. () Zip Code:	(804) 412-0227	Fax No. ()	(804) 412-0229
City:	Gaston	State:	North Carolina		Email Address:	27866 Glenn.Gray@envivabiomass.co	County:	Northampton
AID FAMORIOUS	2011							
AIR EMISSIONS	SOURCE REDUCTI		Any Air Emission	s Source Reductions i	n the past year? () YES ()			
		Enter Code for	Date Reduction	Quantity Emitted	Quantity Emitted	Has reduction activity	Addition deta	il about source
Source	Air Pollutant	Contact - Deduction		_		been		
Description and		Emission Reduction	Option Implemented	from prior annual	from current annual	discontinued? If so,		
ID			implemented			when		
		Option (See Codes)	(mo/yr)	report to DAQ (lb/yr)	report to DAQ (lb/yr)	was it discontinued?		
NI/A					(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	(mo/yr)		
N/A								
1								
Comments:								
CILITY MADE	BEDUCTIONS * OF	777797979797979						· ·
THE COUNTY	Pollutant	ECYCLING ACTIVITIES Enter Code for		Any Reductions or Re	ecycling Activities in the pa	st year? () YES (X) NO		
	, onotant	Litter Code for	Date Reduction	Quantity Emitted	Quantity Emitted	Has reduction activity	Addition detail	about source
			1			been		
Source	or	Emission Reduction	Option	from prior annual	from current annual	discontinued? If so,		
Description or Activity			Implemented			when		
7.0.71.9	Recycled or	Option (See Codes)	(mo/yr)					
	Reduced Materials	Option (occ codes)	(mo/yr)	report	report	was it discontinued?		
						(mo/yr)		
N/A								
				1				
					11			

Comments:
The requested information above shall be used for fulfilling the requirements of North Carolina General Statute 143-215.108(g). The permit holder shall submit to the Department a written description of current and projected plans to reduce the emissions of air pollutants by source reduction or recycling. The written description shall accompany any application for a new permit, modification of an existing permit and for each annual air quality permit fee payment. Source reduction is defined as reducing the amount of any hazardous substance, pollutant, or contaminant entering any waste stream or otherwise released into the environment (including fugitive emissions) prior to recycling, treatment, or disposal. If no activity has taken place since the previous report, simply indicate so by checking the no box in that section.



FORM D1

FACILITY-WIDE EMISSIONS SUMMARY

D₁ NCDENR/Division of Air Quality - Application for Air Permit to Construct/Operate **REVISED 12/01/01** CRITERIA AIR POLLUTANT EMISSIONS INFORMATION - FACILITY-WIDE OTENTIAL EMISSION POTENTIAL EMISSIONS EXPECTED ACTUAL EMISSIONS (AFTER CONTROLS / BEFORE CONTROLS (AFTER CONTROLS / LIMITATIONS) LIMITATIONS) LIMITATIONS) tons/yr tons/yr AIR POLLUTANT EMITTED tons/yr See Table 3-1 in the accompanying application document PARTICULATE MATTER (PM) PARTICULATE MATTER < 10 MICRONS (PM 10) PARTICULATE MATTER < 2.5 MICRONS (PM 2.5) SULFUR DIOXIDE (SO2) NITROGEN OXIDES (NOx) CARBON MONOXIDE (CO) VOLATILE ORGANIC COMPOUNDS (VOC) LEAD OTHER HAZARDOUS AIR POLLUTANT EMISSIONS INFORMATION - FACILITY-WIDE OTENTIAL EMISSION POTENTIAL EMISSIONS **EXPECTED ACTUAL EMISSIONS** (AFTER CONTROLS / (AFTER CONTROLS / BEFORE CONTROLS LIMITATIONS) LIMITATIONS) LIMITATIONS) tons/yr tons/yr CAS NO. tons/yr HAZARDOUS AIR POLLUTANT EMITTED See Table 3-2 in the accompanying application document TOXIC AIR POLLUTANT EMISSIONS INFORMATION - FACILITY-WIDE INDICATE REQUESTED ACTUAL EMISSIONS AFTER CONTROLS / LIMITATIONS. EMISSIONS ABOVE THE TOXIC PERMIT EMISSION RATE (TPER) IN 15A NCAC 2Q .0711 MAY REQUIRE AIR DISPERSION MODELING. USE NETTING FORM D2 IF NECESSARY. Modeling Required? lb/year lb/day CAS NO. lb/hr TOXIC AIR POLLUTANT EMITTED See Table 3-3 in the accompanying application document COMMENTS:

FORM D4

EXEMPT AND INSIGNIFICANT ACTIVITIES SUMMARY

REVISED: 12/01/01

NCDENR/Division of Air Quality - Application for Air Permit to Construct/Operate

D4

		XEMPTED PER 2Q .	
	INSIGNIFICANT ACTIVITIE	S PER 2Q .0503 FO	PRITILE V SOURCES
	DESCRIPTION OF EMISSION SOURCE	SIZE OR PRODUCTION RATE	BASIS FOR EXEMPTION OR INSIGNIFICAN ACTIVITY
(a)	Green Wood Handling and Sizing Operations ES-GWHS	~900,000 tpy	15A NCAC 02Q .0102 (c)(2)(E) - no quantifiable emissions
	Green Wood Fuel Bin ES-GWFB	~150,000 tpy	15A NCAC 02Q .0102 (c)(2)(E) - no quantifiable emissions
.	Dried Wood Handling ES-DWH	520,951 tpy	15A NCAC 02Q .0102 (c)(2)(E) - no quantifiable emissions
i.	Pellet Presses ES-PP	520,951 tpy	15A NCAC 02Q .0102 (c)(2)(E) - no quantifiable emissions
	Final Product Handling ES-FPH	451,128 tpy	15A NCAC 02Q .0102 (c)(2)(E) - no quantifiable emissions
i.	Emergency Generator Diesel Fuel Tank TK1	2,500 gallons	15A NCAC 02Q .0102 (c)(1)(D)
	Fire Water Pump Diesel Fuel Tank TK2	500 gallons	15A NCAC 02Q .0102 (c)(1)(D)
3.	Electric Powered Wood Chipper - EPWC	950,000 wet wood	15A NCAC 02Q .0102 (c)(2)(E) - low emissions, see Appendix B
).			~~ =
0.			

FORM D

TECHNICAL ANALYSIS TO SUPPORT PERMIT APPLICATION

REVISED: 12/01/01

NCDENR/Division of Air Quality - Application for Air Permit to Construct/Operate

D5

PROVIDE DETAILED TECHNICAL CALCULATIONS TO SUPPORT ALL EMISSION, CONTROL, AND REGULATORY DEMONSTRATIONS MADE IN THIS APPLICATION: INCLUDE A COMPREHENSIVE PROCESS FLOW DIAGRAM AS NECESSARY TO SUPPORT AND CLARIFY CALCULATIONS AND ASSUMPTIONS. ADDRESS THE FOLLOWING SPECIFIC ISSUES ON SEPARATE PAGES:

	NECESSARY TO SUPPORT AND CLARIFY FOLLOWING SPECIFI	C.ISSUES ON SEPARATE PAGES:
	A SPECIFIC EMISSIONS SOURCE (EMISSION INFORMATION) (FORM B) - BALANCES, AND/OR OTHER METHODS FROM WHICH THE POLLUTAN OF POTENTIAL BEFORE AND, WHERE APPLICABLE, AFTER CONTROL NEEDED TO SUPPORT MATERIAL BALANCE CALCULATIONS.	SHOW CALCULATIONS USED, INCLUDING EMISSION FACTORS, MATERIAL T EMISSION RATES IN THIS APPLICATION WERE DERIVED. INCLUDE CALCULATION S. CLEARLY STATE ANY ASSUMPTIONS MADE AND PROVIDE ANY REFERENCES AS
В	INDIVIDUAL SOURCES AND THE FACILITY AS A WHOLE. INCLUDE A C REQUIREMENTS) FOR COMPLYING WITH APPLICABLE REGULATIONS RATES OR OTHER OPERATIONAL PARAMETERS. PROVIDE JUSTIFIC SIGNIFICANT DETERIORATION (PSD), NEW SOURCE PERFORMANCE	22 - TITLE V ONLY) - PROVIDE AN ANALYSIS OF ANY REGULATIONS APPLICABLE TO DISCUSSION OUTING METHODS (e.g. FOR TESTING AND/OR MONITORING E, PARTICULARLY THOSE REGULATIONS LIMITING EMISSIONS BASED ON PROCESS ATION FOR AVOIDANCE OF ANY FEDERAL REGULATIONS (PREVENTION OF STANDARDS (NSPS), NATIONAL EMISSION STANDARDS FOR HAZARDOUS AIR THE FEDERAL REGULATIONS WHICH WOULD OTHERWISE BE APPLICABLE TO THIS THE ANY REGULATIONS. INCLUDE EMISSION RATES CALCULATED IN ITEM "A" ABOVE, RT THESE CALCULATIONS.
С	LISTED ON SECTION C FORMS, OR USED TO REDUCE EMISSION RAT PARAMETERS (e.g. OPERATING CONDITIONS, MANUFACTURING REC	ALUATION WITH SUPPORTING REFERENCES FOR ANY CONTROL EFFICIENCIES FES IN CALCULATIONS UNDER ITEM "A" ABOVE. INCLUDE PERTINENT OPERATING COMMENDATIONS, AND PARAMETERS AS APPLIED FOR IN THIS APPLICATION) DEVICES). INCLUDE AND LIMITATIONS OR MALFUNCTION POTENTIAL FOR THE DETAIL PROCEDURES FOR ASSURING PROPER OPERATION OF THE CONTROL BE PERFORMED.
D	D PROCESS AND OPERATIONAL COMPLIANCE ANALYSIS - (FORM E3 - PROCESS, OPERATIONAL, OR OTHER DATA TO DEMONSTRATE COMINITEM "B" WHERE APPROPRIATE. LIST ANY CONDITIONS OR PARACOMPLIANCE WITH THE APPLICABLE REGULATIONS.	TITLE V ONLY) - SHOWING HOW COMPLIANCE WILL BE ACHIEVED WHEN USING MPLIANCE. REFER TO COMPLIANCE REQUIREMENTS IN THE REGULATORY ANALYSIS AMETERS THAT CAN BE MONITORED AND REPORTED TO DEMONSTRATE
E	E PROFESSIONAL ENGINEERING SEAL - PURSUANT TO 15A N A PROFESSIONAL ENGINEER REGISTERED IN NORTH CAROLINA SE NEW SOURCES AND MODIFICATIONS OF EXISTING SOURCES. (SEE	CAC 2Q .0112 "APPLICATION REQUIRING A PROFESSIONAL ENGINEERING SEAL," HALL BE REQUIRED TO SEAL TECHNICAL PORTIONS OF THIS APPLICATION FOR E INSTRUCTIONS FOR FURTHER APPLICABILITY).
	I, Joe Sullivan, attest the has been review in the engineering plans, calculations, and all other supporting docknowledge the proposed design has been prepared in accordance package may have been developed by other professionals, inclusing the support of the professionals.	ed this application forEnviva Pellets Northampton, LLC ed by me and is accurate, complete and consistent with the information supplied sumentation to the best of my knowledge. I further attest that to the best of my with the applicable regulations. Although certain portions of this submittal ion of these materials under my seal signifies that I have reviewed this material te: In accordance with NC General Statutes 143-215.6A and 143-215.6B, any , or certification in any application shall be guilty of a Class 2 misdemeanor which sup to \$25,000 per violation.
	(PLEASE USE BLUE INK TO COMPLETE THE FOLLOWING) NAME: DATE: COMPANY: ADDRESS: Morrisville, NC 27560 TELEPHONE: SIGNATURE: PAGES CERTIFIED: Trinity Consultants, Inc. One Copley Parkway, Suite 310 Morrisville, NC 27560 (919) 462-9693 All ceptrol device application forms ("C Forms)	PLACE NORTH CAROLINA SEAL HERE SEAL 023037
	(IDENTIFY ABOVE EACH PERMIT FORM AND AT	TACHMENT

THAT IS BEING CERTIFIED BY THIS SEAL)

SPECIFIC EMISSIONS SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 12/01/01 NCDENR/Division (of Air Quality - A	Application to	or Air Permit	to Construct	t/Operate		D
EMISSION SOURCE DESCRIPTION:			EMISSION S	OURCE ID N	O:	ES-DRYER	
Green Wood Direct-Fired Dryer System			CONTROL D	EVICE ID NO)(S):	CD-DC, CD-	WESP
OPERATING SCENARIO OF	1		EMISSION P	OINT (STAC	K) ID NO(S):		EP-6
DESCRIBE IN DETAILTHE EMISSION SOURCE PROCES Green wood is conveyed to either a rotary dryer system emissions are controlled by cyclones for bulk particulat (WESP) operating after the cyclones.	. Direct contact	heat is prov	rided to the s				
TYPE OF EMISSION SOURCE (CHECK A	AND COMPLETE	APPROPRI	ATE FORM B	1-B9 ON THE	FOLLOWING	PAGES):	
■ Coal,wood,oil, gas, other burner (Form B1) □ Woodv	vorking (Form B4)	Manufact	t. of chemical	s/coatings/inks	(Form B7)	
☐ Int.combustion engine/generator (Form B2) ☐ Coating	g/finishing/printin	g (Form B5)	Incinerati	ion (Form B8)		
☐ Liquid storage tanks (Form B3) ☐ Storag	e silos/bins (Forn	n B6)	Other (Fo	orm B9)			
START CONSTRUCTION DATE: TBD OPERATION	ON DATE:	TBD	DATE MANU	FACTURED:		TBD	
MANUFACTURER / MODEL NO.: TBD		EXPECTED	OP. SCHEDU	LE: <u>24</u> HF	R/DAY 7	DAY/WK	52_ WK/YR
IS THIS SOURCE SUBJECT TO? NSPS (SUBPART?):	NESH.	AP (SUBPAF	RT?):	MACT	(SUBPART?):_		
PERCENTAGE ANNUAL THROUGHPUT (%): DEC-FEB	25% MAR-N	MAY 25%	JUN-AU	3 25 %	SEP-NO\	25%	
EXPECTED ANNUAL HOURS OF OPERATION 8,70	60 VISIBLE STA	CK EMISSIO	NS UNDER N	ORMAL OPE	RATION: <2	0 % OPA	CITY
CRITERIA AIR POLLUT	ANT EMISSIO	ONS INFO	RMATION F	OR THIS	SOURCE		
	SOURCE OF	EXPECTE	D ACTUAL		POTENTIAL	EMSSIONS	
	EMISSION	(AFTER CONT	ROLS / LIMITS)	(BEFORE CON	NTROLS / LIMITS)	(AFTER CON	TROLS / LIMITS)
AIR POLLUTANT EMITTED	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)	See Emission	n Calculation	ns in Appendi	х В			
PARTICULATE MATTER<10 MICRONS (PM 10)							
PARTICULATE MATTER<2.5 MICRONS (PM 2.5)							
SULFUR DIOXIDE (SO2)							
NITROGEN OXIDES (NOx)							
CARBON MONOXIDE (CO)							
VOLATILE ORGANIC COMPOUNDS (VOC)							
LEAD							
OTHER							
HAZARDOUS AIR POLLU	JTANT EMISS	SIONS INF	ORMATION	I FOR THI	SSOURCE		
	SOURCE OF	EXPECTE	D ACTUAL		POTENTIAL	EMSSIONS	
	EMISSION	(AFTER CON	TROLS / LIMITS)	(BEFORE CO	NTROLS / LIMITS)	(AFTER CON	TROLS / LIMITS
HAZARDOUS AIR POLLUTANT AND CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
	See Emissio	n Calculatio	ns in Append	ix B			
					-		-
							<u> </u>
	-						-
TO/40 AID DOL (1771	NT ENDOUG	MO MEGO	MATION TO	D TUO C	OUDOE		
TOXIC AIR POLLUTA							
INDICATE EXPECTE							
TOXIC AIR POLLUTANT AND CAS NO.	EF SOURCE		o/hr		/day	ı	b/yr
	See Emissio	n Calculatio	ns in Append	ix B			
				-			
Attachments: (1) emissions calculations and supporting documentation							

and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

COMPLETE THIS FORM AND COMPLETE AND ATTACH APPROPRIATE B1 THROUGH B9 FORM FOR EACH SOURCE

EMISSION SOURCE (WOOD, COAL, OIL, GAS, OTHER FUEL-FIRED BURNER)

Green Wood Direct-Fired Dryer System OPERATING SCENARIO: DESCRIBE USE: PROCESS HEAT CONTINUOUS USE SPACE HEAT CONTINUOUS USE STAND BY/EMERGENCY HEATING MECHANISM: MOOD TYPE: BARK WOOD/BARK WOOD/BARK PERCENT MOISTURE OF FUEL: 20 to 50% UNCONTROLLED UNCONTROLLED FUEL FEED METHOD: METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER IF OTHER DESCRIBE:	DRY WOOD & CON STEAM AIR DER STOKER	RATION
CONDERATING SCENARIO: 1 OF 1 EMISOR SPACE HEAT DESCRIBE USE: PROCESS HEAT STAND BY/EMERGENCY HEATING MECHANISM: INDIRECT DIRECT MAX. FIRING RATE (MMBTU/HOUR): 207 WOOD-FIRED BURNE WOOD TYPE: BARK WOOD/BARK NET WOOD PERCENT MOISTURE OF FUEL: 20 to 50% UNCONTROLLED CONTROLLED WITH FLYASH REINJECTION FUEL FEED METHOD: HEAT TRANSFER MEDIA: TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED UNCONTROLLED DIROCHTOLLED UNCONTROLLED DRY BED CONTROLLED FLYASH REIN FILYASH REIN FILYASH REIN FILYASH REIN FILYASH REIN	ER DRY WOOD STEAM ST	O(S): EP-6 RATION D: OTHER (DESCRIBE): TROLLED W/O REINJECTION
PERATING SCENARIO: 1 OF 1 SPACE HEAT © SPACE HEAT © CONTINUOUS USE © STAND BY/EMERGENCY HEATING MECHANISM: © INDIRECT MAX. FIRING RATE (MMBTU/HOUR): PERCENT MOISTURE OF FUEL: 20 to 50% © UNCONTROLLED EUEL FEED METHOD: METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER PULVERIZED OVERFEED STOKER PULVERIZED OVERFEED STOKER UNCONTROLLED © CONTROLLED © UNCONTROLLED UNCONTROLLED FUEL BED & UNCONTROLLED OVERFEED STOKER UNDERFEED STOKER UNDERFEED STOKER UNDERFEED STOKER UNCONTROLLED © FLYASH REIN FLYASH REIN FLYASH REIN FLYASH REIN	ER DRY WOOD CON STEAM AIR	RATION DESCRIBE STROLLED W/O REINJECTION
PROCESS HEAT O CONTINUOUS USE O STAND BY/EMERGENCY STAND BY/EMERGENCY DIRECT TAX. FIRING RATE (MMBTU/HOUR): WOOD-FIRED BURNE WOOD TYPE: O BARK O WOOD/BARK PERCENT MOISTURE OF FUEL: 20 to 50% UNCONTROLLED O CONTROLLED WITH FLYASH REINJECTION HEAT TRANSFER MEDIA: METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER UNCONTROLLED O FLYASH REIN OF FLYASH REIN	OTHER (DESCRIBE ER DRY WOOD CON STEAM AIR DER STOKER	OTHER (DESCRIBE): TROLLED W/O REINJECTION
CONTINUOUS USE STAND BY/EMERGENCY HEATING MECHANISM: INDIRECT DIRECT MAX. FIRING RATE (MMBTU/HOUR): 207 WOOD-FIRED BURNE WOOD TYPE: BARK WOOD/BARK WET WOOD PERCENT MOISTURE OF FUEL: 20 to 50% UNCONTROLLED CONTROLLED WITH FLYASH REINJECTION HEAT TRANSFER MEDIA: METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED UNCONTROLLED UNCONTROLLED DRY BED CONTROLLED CONTROLLED FLYASH REIN	ER DRY WOOD CON STEAM AIR DER STOKER	OTHER (DESCRIBE):TROLLED W/O REINJECTION
HEATING MECHANISM: INDIRECT OF DIRECT MAX. FIRING RATE (MMBTU/HOUR): 207 WOOD-FIRED BURNE WOOD TYPE: BARK WOOD/BARK WET WOOD PERCENT MOISTURE OF FUEL: 20 to 50% UNCONTROLLED CONTROLLED WITH FLYASH REINJECTION HEAT TRANSFER MEDIA: TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED UNCONTROLLED UNCONTROLLED DRY BED CONTROLLED CONTROLLED FLYASH REIN	DRY WOOD & CON STEAM AIR DER STOKER	TROLLED W/O REINJECTION
WOOD TYPE: BARK WOOD/BARK WET WOOD PERCENT MOISTURE OF FUEL: 20 to 50% UNCONTROLLED CONTROLLED WITH FLYASH REINJECTION HEAT TRANSFER MEDIA: WETHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED UNCONTROLLED CONTROLLED UNCONTROLLED DRY BED CONTROLLED CONTROLLED FLYASH REIN FLYASH REIN WOOD-FIRED BURNE COAL-FIRED BURNE UNCONTROLLED FLYASH REIN FLYASH REIN	DRY WOOD & CON STEAM AIR DER STOKER	TROLLED W/O REINJECTION
WOOD-FIRED BURNE WOOD TYPE: BARK WOOD/BARK WET WOOD PERCENT MOISTURE OF FUEL: 20 to 50% UNCONTROLLED CONTROLLED WITH FLYASH REINJECTION HEAT TRANSFER MEDIA: METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED UNCONTROLLED UNCONTROLLED DRY BED CONTROLLED CONTROLLED FLYASH REIN	DRY WOOD & CON STEAM AIR DER STOKER	TROLLED W/O REINJECTION
WOOD TYPE: BARK WOOD/BARK WET WOOD PERCENT MOISTURE OF FUEL: 20 to 50% UNCONTROLLED CONTROLLED WITH FLYASH REINJECTION HEAT TRANSFER MEDIA: METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED UNCONTROLLED UNCONTROLLED DRY BED CONTROLLED CONTROLLED FLYASH REIN	DRY WOOD & CON STEAM AIR DER STOKER	TROLLED W/O REINJECTION
PERCENT MOISTURE OF FUEL: 20 to 50% UNCONTROLLED CONTROLLED WITH FLYASH REINJECTION HEAT TRANSFER MEDIA: METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED UNCONTROLLED UNCONTROLLED DRY BED CONTROLLED CONTROLLED FLYASH REIN	STEAM AIR ER DER STOKER	TROLLED W/O REINJECTION
UNCONTROLLED CONTROLLED WITH FLYASH REINJECTION FUEL FEED METHOD: METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED UNCONTROLLED UNCONTROLLED DRY BED CONTROLLED CONTROLLED FLYASH REIN	ER DER STOKER	
FUEL FEED METHOD: METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED & UNCONTROLLED UNCONTROLLED UNCONTROLLED DRY BED & CONTROLLED FLYASH REIN	ER DER STOKER	
METHOD OF TUBE CLEANING: N/A COAL-FIRED BURNE TYPE OF BOILER IF OTHER DESCRIBE: PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD □ WET BED ② UNCONTROLLED ② UNCONTROLLED ② UNCONTROL □ DRY BED ② CONTROLLED ② CONTROLLED ③ FLYASH REIN	DER STOKER	OTHER
COAL-FIRED BURNE TYPE OF BOILER IF OTHER DESCRIBE: PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD □ WET BED	DER STOKER	
TYPE OF BOILER IF OTHER DESCRIBE: PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD □ WET BED	DER STOKER	
PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD □ WET BED	n,	
PULVERIZED OVERFEED STOKER UNDERFEED STOKER SPREAD WET BED & UNCONTROLLED & UNCONTROLLED UNCONTROLLED DRY BED & CONTROLLED CONTROLLED FLYASH REIN	n,	
□ WET BED Ø UNCONTROLLED Ø UNCONTROLLED Ø UNCONTROLLED □ DRY BED Ø CONTROLLED Ø FLYASH REIN	ı.	FLUIDIZED BED
□ DRY BED & CONTROLLED & CONTROLLED & FLYASH REIN	LLED Ů	CIRCULATING
DEKT BED & CONTREETED &	NJECTION &	RECIRCULATING
5 NOTEWISH		
METHOD DE LOADING: & CYCLONE & HANDFIRED & TRAVELING		DESCRIBE):
METHOD OF LOADING: & CTCLONE S TWINDS INCE		
METHOD OF TUBE CLEANING: OIL/GAS-FIRED BURN		
DUTILITY DINDUSTRIAL DICOMMERCIAL DR	RESIDENTIAL	
TYPE OF BOILER:		
TYPE OF FIRING.		
METHOD OF TUBE CLEANING: CLEANING SCHE OTHER FUEL-FIRED BU		
OTHER FUEL-FIRED BO	JKIYEK	
TYPE OF FUEL: PERCENT MOISTURE:	DECIDENTIAL	
TYPE OF BOILER:	RESIDENTIAL	
TYPE OF FIRING: TYPE OF CONTROL (IF ANY):		FUEL FEED METHOD:
METHOD OF TUBE CLEANING: CLEANING SCH		
FUEL USAGE (INCLUDE STARTUP)		A PARTY OF PARTY
MAXIMUM DES	SIGN	REQUESTED CAPACITY
FUEL TYPE UNITS CAPACITY (UNI	NIT/HR)	LIMITATION (UNIT/HR)
Bark/Wet Wood Tons Nominal 10.).9 (bark basis)	
FUEL CHARACTERISTICS (COMPLETE ALI	L THAT ARE APPLICA	ABLE)
SPECIFIC	SULFUR CONTENT	ASH CONTENT
FUEL TYPE BTU CONTENT	(% BY WEIGHT)	(% BY WEIGHT)
Bark/Wet Wood Nominal 4,200 BTU/lb	0.011	
Bark/Wet Wood Nominal 4,200 B10/10		
	(S: YES)	NO
SAMPLING PORTS, COMPLIANT WITH EPA METHOD 1 WILL BE INSTALLED ON THE STACK		

			FOI	RM C4					
CONT	ROL DEVICE (CYCLON	E, MUL	TICYCLON	E, OR OTH	ER I	MECHAN	IICAL)	
REVISED 12/01/01	NCDENR/Di	vision of Air Q	uality - Ap	plication for Air	Permit to Const	ruct/0	perate	,	C4
CONTROL DEVICE ID NO:	CD-DC	CONTROLS	EMISSION	S FROM WHICH	EMISSION SOUR	RCE ID	NO(S):	ES-DRYER	
EMISSION POINT (STACK) ID N	IO(S): EP-6	POSITION IN	SERIES O	F CONTROLS	NO.	1	OF 2	UNITS	
MANUFACTURER: TBD1			MODEL N	IO:					
DATE MANUFACTURE TBD			PROPOSI	ED OPERATION	DATE: TBD				
OPERATIN	IG SCENARIO:		PROPOSI	ED START CONS	STRUCTION DAT	E:	TBD		
1	OF1		P.E. SEAL	REQUIRED (PE	R 2Q .0112)?		· é YES	é NO	
DESCRIBE CONTROL SYSTEM Three identical convential effic		equipped to th	e discharg	ge of the rotary of	lryer system to d	aptur	e bulk PM en	nissions.	
Emissions from each the cyclo	nes are combined in	ito a common							
The parameters presented here	e are per each cyclor	ne:				_			
POLLUTANT(S) COLLECTED:			PM	PM ₁₀	PM _{2.5}	-		-	
BEFORE CONTROL EMISSION	RATE (LB/HR):					-		-	
CAPTURE EFFICIENCY:			98.5	% 98.5	5 % 98.5	5 %		_%	
CONTROL DEVICE EFFICIENCY	Y:			%	_%	_ %		_%	
CORRESPONDING OVERALL E	FFICIENCY:			%	_ %	_ %		_%	
EFFICIENCY DETERMINATION	CODE:					-		_	
TOTAL EMISSION RATE (LB/HF	R):					_		_	
PRESSURE DROP (IN. H ₂ 0):	MIN MAX 6	5.0" W	ARNING AI	LARM? ∉ YES	€ NO				
INLET TEMPERATURE (°F):	MIN MAX	Nominal 400		OUTLET TEMP	ERATURE (°F):	MIN	MAX	Nominal 400	
INLET AIR FLOW RATE (ACFM)	95,000			BULK PARTICLI	E DENSITY (LB/F	T³):	3.43E-05		
POLLUTANT LOADING RATE (C	GR/FT ³ 0.24								
SETTLING CHAMBER		74. 4	CYCLONE		148181	16	M	ULTICYCLONE	s Maria
LENGTH (INCHES):	INLET VELOCITY (F	FT/SEC):	95	d CIRCULAR	RECTANGLE	NO.	TUBES:		
WIDTH (INCHES):	DIMENSIONS (INC	CHES) See inst	ructions	IF WET SPR	AY UTILIZED	DIAI	METER OF T	UBES:	
HEIGHT (INCHES):	H:	Dd:		LIQUID USED:		HOF	PPER ASPIRA	ATION SYSTEM?	
VELOCITY (FT/SEC.):	W:	Lb:	217"	FLOW RATE (G	PM):	é	YES	€ NO	
NO. TRAYS:	De: 74"	Lc:	254*	MAKE UP RATE	(GPM):	LOU	VERS?		
NO. BAFFLES:	D: 149"	S:				e	YES	é NO	
	TYPE OF CYCLONE	€ CONVENT	IONAL)	€ HIGH	EFFICIENCY	ę	OTHER		
DESCRIBE MAINTENANCE PRO						PART	ICLE SIZE D	ISTRIBUTION	MAL)
Periodic inspection of m as specified by manufact	_	ity during p	lant out	ages	SIZE (MICRONS)	1	EIGHT % F TOTAL	CUMULAT %	IVE
							TOTAL		
The flue gas from the dry		ınd distribu	ted thro	unh a set of	0-1	-		Unknown	
three cyclones before en					1-10				
stream will be combined	-			-, J		-			
point.	into a single aa	ot and anec	ica to ti	ie arron litte		-			
					50-100	-			
					>100	-		TOTAL = 100	
DESCRIBE ANY MONITORING I	DEVICES, GAUGES 1	TEST PORTS	ETC:			_		TOTAL = 100	
None				HE CONTDOL OF	SVICE TO ITE EN	II GOLO	N SOUPEE	2).	
ON A SEPARATE PAGE, ATTAC	IT A DIAGRAM OF TH	TE RELATIONS	SHIP OF TH	HE CONTROL DE	VICE TO ITS EM	ISSIO	N SOURCE(S	S):	

Attach Additional Sheets As Necessary

¹Final equipment selection has not yet occurred but will be similar in design to specifications shown.

FORM C2

CONTROL DEVICE (Electrostatic Precipitator)

VISED 12/01/01	NCDENR/Divisi	on of Air Quality - Applic	ation for Air Permit to Construct/Operate		
	CD-WESP		CONTROLS EMISSIONS FROM WHICH E	EMISSION SOURCE ID NO	ES-DRYER
NTROL DEVICE ID NO: SSION POINT (STACK) ID NO(S):	EP-6		POSITION IN SERIES OF CONTROLS:	NO. 2 OF 2	UNITS
			MODEL NO. SonicKleen V	VESP-304L-567-12H19	
INDI AOTORER			PROPOSED OPERATION DATE:	TBD	
NUFACTURE DATE: TBD	G SCENARIO:		PROPOSED START CONSTRUCTION DA	ATE: TBD	
	OF		P.E. SEAL REQUIRED (PER 2Q .0112)?	YES (NO
	SPECIFICATIONS		GAS DISTRIBUTION GRIDS: & YE	ES) é NO	
	é I		SINGLE-STAGE	TWO-STAGE	
PE: (WET)		29,904		TOR PLATE PER FIELD:	567 tubes
OTAL COLLECTION PLATE AREA (FT		WIDTH:	SPACING BETWEEN COLLECTOR PLAT	ES (INCHES):	12" hextube
DLLECTOR PLATES SIZE (FT): LEN		9"-0"		2.054E-04 Poise	
OTAL DISCHARGE ELECTRODE LEN	10111(1.1)	567	NUMBER OF COLLECTING ELECTRODE	E RAPPERS:	none
JMBER OF DISCHARGE ELECTRO			PARTICLE MIGRATION VELOCITY (FT/S		0.234
AXIMUM INLET AIR FLOW RATE (AC		190,000	BULK PARTICLE DENSITY (LB/FT 3):	45 lb/cu.	ft.
INIMUM GAS TREATMENT TIME (SE		2.3 COLLECTING: N/A	CORONA POWER (WATTS/1000 CFM):		4000
ELD STRENGTH (VOLTS) CHARGIN		COLLECTING. N/A	CORONAL OWER (WILLIAM)		
LECTRICAL USAGE (kw/HOUR):	141.5	L DI ATE MUDDATING	WASHING OTHER		
LLANING I NOOLD G. III	RAPPING	€ PLATE VIBRATING	2" MAX 2" WARNING ALAR	M? ØYES	∮ NO ()
OPERATING PARAMETERS		ROP (IN. H20): MIN		TYPE OF AGENT (IF YES	5):
ESISTIVITY OF POLLUTANT (OHM-	Oltrij.	N/A	OUTLET GAS TEMPERATURE (°F):	MIN 150 MAX 190	
ALET GAS TEMM ETCHOLIE (17		X 300	INLET MOISTURE PERCENT:	MIN 40% MAX 50	%
OLUME OF GAS HANDLED (ACFM):		185,000		YES # NO)
POWER REQUIREMENTS			EACH TRANSFORMER (kVA)	EACH RECTIFIER K	/ Ave/Peak Ma Dc
FIELD NO. NO.	OF SETS	CHARGING	118	83 / 1265	
1	1		118	83 / 1265	
2	1		110		
POLLUTANT(S) COLLECTED:	Р	M / PM ₁₀ / PM _{2.5}		-	_
BEFORE CONTROL EMISSION RATI	E (LB/HR):	125.00		%	~
CAPTURE EFFICIENCY:		%	% 	-	— ″ %
CONTROL DEVICE EFFICIENCY:		%	%		— ″ %
		%	%	%	
CORRESPONDING OVERALL EFFIC	CIENCY:				
					_
EFFICIENCY DETERMINATION COL		See calculations in App	pendix B		_
CORRESPONDING OVERALL EFFICE EFFICIENCY DETERMINATION COLTOTAL EMISSION RATE (LB/HR): PARTICLE	DE:		pendix B DESCRIBE STARTUP PROCEDURES:		
EFFICIENCY DETERMINATION COL TOTAL EMISSION RATE (LB/HR): PARTICLE	DE: SIZE DISTRIBUT				_
EFFICIENCY DETERMINATION COL TOTAL EMISSION RATE (LB/HR): PARTICLE SIZE	DE:	ION	DESCRIBE STARTUP PROCEDURES:		
EFFICIENCY DETERMINATION COE TOTAL EMISSION RATE (LB/HR): PARTICLE SIZE (MICRONS)	SIZE DISTRIBUT NEIGHT % OF TOTAL	CUMULATIVE	DESCRIBE STARTUP PROCEDURES:		
EFFICIENCY DETERMINATION COE TOTAL EMISSION RATE (LB/HR): PARTICLE SIZE (MICRONS) 0-1 Unkno	SIZE DISTRIBUT NEIGHT % OF TOTAL	CUMULATIVE	DESCRIBE STARTUP PROCEDURES: See attached		
EFFICIENCY DETERMINATION COE TOTAL EMISSION RATE (LB/HR): PARTICLE SIZE (MICRONS) 0-1 Unkno 1-10	SIZE DISTRIBUT NEIGHT % OF TOTAL	CUMULATIVE	DESCRIBE STARTUP PROCEDURES: See attached DESCRIBE MAINTENANCE PROCEDU See attached	JRES:	
EFFICIENCY DETERMINATION COE TOTAL EMISSION RATE (LB/HR): PARTICLE SIZE (MICRONS) 0-1 Unkno 1-10 10-25	SIZE DISTRIBUT NEIGHT % OF TOTAL	CUMULATIVE	DESCRIBE STARTUP PROCEDURES: See attached DESCRIBE MAINTENANCE PROCEDU	JRES:	HE CONTROL
EFFICIENCY DETERMINATION COE TOTAL EMISSION RATE (LB/HR): PARTICLE SIZE (MICRONS) 0-1 Unkno 1-10 10-25 25-50	SIZE DISTRIBUT NEIGHT % OF TOTAL	CUMULATIVE	DESCRIBE STARTUP PROCEDURES: See attached DESCRIBE MAINTENANCE PROCEDU See attached	JRES:	HE CONTROL
EFFICIENCY DETERMINATION COE TOTAL EMISSION RATE (LB/HR): PARTICLE SIZE (MICRONS) 0-1 Unkno 1-10 10-25 25-50 50-100	SIZE DISTRIBUT NEIGHT % OF TOTAL	CUMULATIVE	DESCRIBE STARTUP PROCEDURES: See attached DESCRIBE MAINTENANCE PROCEDU See attached DESCRIBE ANY AUXILIARY MATERIA	JRES:	HE CONTROL
EFFICIENCY DETERMINATION COE TOTAL EMISSION RATE (LB/HR): PARTICLE SIZE (MICRONS) 0-1 Unkno 1-10 10-25 25-50	SIZE DISTRIBUT NEIGHT % OF TOTAL	CUMULATIVE %	DESCRIBE STARTUP PROCEDURES: See attached DESCRIBE MAINTENANCE PROCEDU See attached DESCRIBE ANY AUXILIARY MATERIA SYSTEM:	JRES:	HE CONTROL
EFFICIENCY DETERMINATION COE TOTAL EMISSION RATE (LB/HR): PARTICLE SIZE (MICRONS) 0-1 Unkno 1-10 10-25 25-50 50-100	SIZE DISTRIBUT WEIGHT % OF TOTAL wn	CUMULATIVE % AL = 100	DESCRIBE STARTUP PROCEDURES: See attached DESCRIBE MAINTENANCE PROCEDU See attached DESCRIBE ANY AUXILIARY MATERIA SYSTEM: NOAH	JRES:	HE CONTROL

SPECIFIC EMISSIONS SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 12/01/01 NCDENR/Division o	f Air Quality -	Application f	or Air Permit	to Construc	t/Operate		В
EMISSION SOURCE DESCRIPTION: Four (4) Hammermills			EMISSION S	OURCE ID N	10:	ES-HM-1,-2	,-3,-4
, ,			CONTROL D	EVICE ID NO	D(S):	CD-HM-BV	1,-BV2
OPERATING SCENARIO 1 OF	1		EMISSION F	OINT (STAC	K) ID NO(S):	EP-2	
DESCRIBE IN DETAILTHE EMISSION SOURCE PROCESS Dried materials are reduced to the appropriate size needs				ills			
TYPE OF EMISSION SOURCE (CHECK AI	ND COMPLETE	E APPROPRI	ATE FORM B	1-B9 ON THE	FOLLOWING	PAGES):	
Coal,wood,oil, gas, other burner (Form B1) Woodwo					s/coatings/ink	-	
☐ Int.combustion engine/generator (Form B2) ☐ Coating.	/finishing/printir	ng (Form B5)				(,	
I —	silos/bins (For		Other (F		,		
START CONSTRUCTION DATE: TBD OPERATION	N DATE:	TBD	DATE MANU	FACTURED:		TBD	
MANUFACTURER / MODEL NO.: TBD		EXPECTED	OP. SCHEDU		R/DAY 7	DAY/WK	52 WK/YR
IS THIS SOURCE SUBJECT TO? NSPS (SUBPART?):		IAP (SUBPAR			(SUBPART?):		
PERCENTAGE ANNUAL THROUGHPUT (%): DEC-FEB	25% MAR-I		JUN-AU		SEP-NO'		
EXPECTED ANNUAL HOURS OF OPERATION 8,760	VISIBLE STA	CK EMISSIO	NS UNDER N	ORMAL OPE	RATION: <	20 % OPA	ACITY
CRITERIA AIR POLLUTA	NT EMISSI	ONS INFO	RMATION H	OR THIS	SOURCE		
	SOURCE OF	EXPECTE	D ACTUAL		POTENTIAL	. EMSSIONS	
	EMISSION	(AFTER CONT	ROLS / LIMITS)	(BEFORE CON	TROLS / LIMITS)	1	TROLS / LIMITS)
AIR POLLUTANT EMITTED	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)	See Emissio	n Calculation	s in Appendi	x B			
PARTICULATE MATTER<10 MICRONS (PM 10)							
PARTICULATE MATTER<2.5 MICRONS (PM _{2.5})							
SULFUR DIOXIDE (SO2)							
NITROGEN OXIDES (NOx)							
CARBON MONOXIDE (CO)							
VOLATILE ORGANIC COMPOUNDS (VOC)							
LEAD							
OTHER							
HAZARDOUS AIR POLLU	TANT EMISS	SIONS INFO	ORMATION	FOR THIS	SOURCE		
	SOURCE OF		D ACTUAL			EMSSIONS	
HAZARROUG AIR ROLL HTANK AND GARNO	EMISSION		ROLS / LIMITS)		TROLS / LIMITS)	(AFTER CON	TROLS / LIMITS)
HAZARDOUS AIR POLLUTANT AND CAS NO. N/A	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
IN/A							
	 						
1101							
TOXIC AIR POLLUTAN	T EMISSION	VS INFORM	ATION FO	R THIS SE	HIRCE	CHILD CHO	
INDICATE EXPECTED							
TOXIC AIR POLLUTANT AND CAS NO.	EF SOURCE		hr		day	n	Shire
N/A		101	111	ID/	uay	IK.	o/yr
÷							
Attachments: (1) emissions calculations and supporting documentation:	(2) indicate all red	Tuested state an	nd federal enforc	aabla narmit lim	its (o.g. bours of	anarotion amia	ninn materia

Attachments: (1) emissions calculations and supporting documentation; (2) indicate all requested state and federal enforceable permit limits (e.g. hours of operation, emission rates and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

EMISSION SOURCE (OTHER)

VISED: 12/01/01 NCDENR/Division of Air Quality - A	oppiication ic	or Air Permit to Construct/Operate	В9
ISSION SOURCE DESCRIPTION: Four (4) Hammermills			-HM-1,-2,-3,-4
			-HM-BV1,-BV2
ERATING SCENARIO: 1 OF 1		EMISSION POINT (STACK) ID NO(S	S): EP-2
SCRIBE IN DETAIL THE PROCESS (ATTACH FLOW DIAGRAM): Dried materials are reduced to the appropriate size needed for p	elletization u	ising four hammermills.	
PROCESS CONTINUOUS PROCESS	9	MAX. DESIGN	REQUESTED CAPACITY
MATERIALS ENTERING PROCESS - CONTINUOUS PROCES	UNITS	CAPACITY (UNIT/HR)	LIMITATION(UNIT/HR)
TYPE		68.3	
Dried Wood	Tons	00.3	
MATERIALS ENTERING PROCESS - BATCH OPERATION TYPE	UNITS	MAX. DESIGN CAPACITY (UNIT/BATCH)	REQUESTED CAPACITY LIMITATION (UNIT/BATCH)
MAXIMUM DESIGN (BATCHES / HOUR):			
REQUESTED LIMITATION (BATCHES / HOUR):	(BATCHES/\		ILIEN. ALIA
FUEL USED: N/A		IMUM FIRING RATE (MILLION BTU	
MAX. CAPACITY HOURLY FUEL USE: N/A COMMENTS:	REQUESTE	D CAPACITY ANNUAL FUEL USE:	N/A

rrol Device NCDENR YC-1,-2,-3,-4 EP-2 SCENARIO: F1_ Coarse hammermills to cyclones. Pre (LB/HR): CIENCY: DDE: N MAX 6.0"	CONTROL:	Air Quality - Appli S EMISSIONS FRO IN SERIES OF COI MODEL NO: PROPOSED OF PROPOSED ST P.E. SEAL REG OULK PM emissions PM 34,000 98.0%	ication for MM WHICH NTROLS PERATION FART CON MUIRED (PI	EMISSION I DATE: ISTRUCTIC ER 2Q .011	t to Construct/C N SOURCE ID N NO. 1 TBD DN DATE: 12)? m the cyclone : PM _{2.5} 34,000 98.0%	O(S): OF 2 TBD YES are routed to a	ES-H UNIT	
YC-1,-2,-3,-4 EP-2 SCENARIO: F1_ Coarse hammermills to cyclones. Per each cyclone. FE (LB/HR): CCIENCY: DDE:	CONTROL	S EMISSIONS FRO IN SERIES OF COI MODEL NO: PROPOSED OF PROPOSED ST P.E. SEAL RECO DUIK PM emissions PM 34,000 98.0%	M WHICH NTROLS PERATION FART CON PUIRED (PI The emi-	EMISSION DATE: ISTRUCTIC ER 2Q .011 ssions from PM 10 34,000 98.0% %	N SOURCE ID N NO. 1 TBD DN DATE: 12)? m the cyclone : PM _{2.5} 34,000 98.0%	O(S): OF 2 TBD YES are routed to a	UNIT) # NO a bagfilter. E	S
EP-2 SCENARIO: F1_ coarse hammermills to cyclones. Experiment by the per each cyclone. FE (LB/HR): CCIENCY: CODE:	POSITION	MODEL NO: PROPOSED OF PROPOSED ST P.E. SEAL RECOULT PM 34,000 98.09	PERATION PART CON PUIRED (PI	I DATE: ISTRUCTIC ER 2Q .011 Ssions from PM 10 34,000 98.0% %	NO. 1 TBD DN DATE: 12)? m the cyclone : PM _{2.5} 34,000 98.0%	OF 2 TBD YES are routed to a	UNIT) # NO a bagfilter. E	S
SCENARIO: OF1 coarse hammermills to cyclones. One per each cyclone. OF1 OF1 COENCY: OF1 CIENCY: ODE:	3850	MODEL NO: PROPOSED OF PROPOSED ST P.E. SEAL RECOULT PM 34,000 98.09	PERATION PART CON PUIRED (PI	ER 2Q .011 ssions fro PM 10 34,000 98.0% %	TBD ON DATE: 112)? m the cyclone : PM _{2.5} 34,000 98.0%	TBD YES are routed to) ≠ NO a bagfilter. E %	
occarse hammermills to cyclones. a per each cyclone. TE (LB/HR): ICIENCY:	to capture b	PROPOSED OF PROPOSED ST P.E. SEAL RECORD PM 34,000 98.0%	ART CON PLANTS OF THE CONTROL OF THE	ER 2Q .011 ssions fro PM 10 34,000 98.0% %	PM _{2.5} 34,000 98.0%	y YES	a bagfilter. E	iach
occarse hammermills to cyclones. a per each cyclone. TE (LB/HR): ICIENCY:	to capture b	PROPOSED ST P.E. SEAL REC Pulk PM emissions PM 34,000 98.0%	ART CON PLANTS OF THE CONTROL OF THE	ER 2Q .011 ssions fro PM 10 34,000 98.0% %	PM _{2.5} 34,000 98.0%	y YES	a bagfilter. E	ach
occarse hammermills to cyclones. a per each cyclone. TE (LB/HR): ICIENCY:	to capture b	P.E. SEAL REG	The emis	PM ₁₀ 34,000 98.0% %	PM _{2.5} 34,000 98.0%	y YES	a bagfilter. E	Each
coarse hammermills to cyclones. a per each cyclone. ITE (LB/HR): ICIENCY:	to capture b	PM 34,000 98.0%	. The emis	PM ₁₀ 34,000 98.0% %	PM _{2.5} 34,000	are routed to	a bagfilter. E	ach
o cyclones. a per each cyclone. TE (LB/HR): ICIENCY:	to capture b	PM 34,000 98.0%		PM ₁₀ 34,000 98.0% %	PM _{2.5} 34,000 98.0%	%	%	ach
TE (LB/HR): ICIENCY: IDE:		34,000 98.0%	 - % _	34,000 98.0% %	34,000			
CIENCY:		98.0%	<u>%</u> %	98.0% %	98.0%			
CIENCY:			_ %	%				
DDE:			_			%	%	
DDE:		-	_% _ _, _	%				
		·			<u> </u>	%	%	
MAX 60"						-		
MAX 60"		68	0	680	680	_		
1 1717-010	WAF	RNING ALARM?			é NO			
N 1€	60 Ambient		_			MIN MA	AX Ambi	ent
20,00	00		BULK P.	ARTICLE [DENSITY (LB/FT	⁻³): 2.8	3E-02	
/FT³): 198.3	33						MIN TICK	VOI ONE
36 1 == -1 1 7 =		CYCLONE					MULTIC	CLONE
INLET VELOCITY (F	FT/SEC):	90	4 e CIR	CULAR)	RECTANGLE	NO. TUBES:		
DIMENSIONS	(INCHES) S	Gee instructions	IF W	VET SPRA	Y UTILIZED			
H: 48"	Dd:	24"	LIQUID	USED:		1 .	SPIRATION S	
W: 22"	Lb:	68"	FLOW	RATE (GPI	M):	_		€ NO
De: 57"	Lc:	192"	MAKE	UP RATE (GPM):	1		
D: 120"	S:	67"						€ NO
TYPE OF CYCLONE	E: (& CON	VENTIONAL)		é HIGH E				
CEDURES:				1	0175			CUMULATIVE
	y during p	lant outages					- 1	%
rer						1	Unk	nown
AM:	done und	or nonative pre	SCHIPA	The		-	1	
i inrough the cyc	ole ctre	m and the sire	will					
material from the	e air strea	discharge to a	tmoenhe	ere				
a pag filter prior	្រេង២:= =:	uischarge to a	anospiic	,			_	
imon to all fitters	s in this ai	red.						
					- 100		TOTA	L = 100
EVICES, GAUGES, TI	EST PORTS	, ETC:					TOTA	AL = 100
	INLET VELOCITY (DIMENSIONS H: 48" W: 22" De: 57" D: 120" TYPE OF CYCLON EDURES: Chanical integrity For and the domain of the domain of the cycles and the domain of the domain of the domain of the cycles EVICES, GAUGES, T	INLET VELOCITY (FT/SEC): DIMENSIONS (INCHES) S H: 48" Dd: W: 22" Lb: De: 57" Lc: D: 120" S: TYPE OF CYCLONE: & CON SEDURES: Chanical integrity during parer AM: I through the cyclone und material from the air stread d bag filter prior to being mon to all fitlers in this a	INLET VELOCITY (FT/SEC): 90 DIMENSIONS (INCHES) See instructions H: 48" Dd: 24" W: 22" Lb: 68" De: 57" Lc: 192" D: 120" S: 57" TYPE OF CYCLONE: & CONVENTIONAL SEDURES: Chanical integrity during plant outages are AM: I through the cyclone under negative prematerial from the air stream and the air of the day filter prior to being discharge to a form on to all fitlers in this area.	INLET VELOCITY (FT/SEC): DIMENSIONS (INCHES) See instructions IF V	INLET VELOCITY (FT/SEC): 198.33 198.33 198.33 190.4	CYCLONE INLET VELOCITY (FT/SEC): DIMENSIONS (INCHES) See instructions H: 48" Dd: 24" Liquid used: W: 22" Lb: 68" FLOW RATE (GPM): De: 57" Lc: 192" MAKE UP RATE (GPM): TYPE OF CYCLONE: Chanical integrity during plant outages rer AM: I through the cyclone under negative pressure. The material from the air stream and the air will d bag filter prior to being discharge to atmosphere mon to all fitlers in this area. EVICES, GAUGES, TEST PORTS, ETC:	TINLET VELOCITY (FT/SEC): 198.33	TYPE OF CYCLONE: de CONVENTIONAL de HIGH EFFICIENCY de OTHER PARTICLE SIZE DISTRICULAR CONTROL DE SIZE CHANGLE INTOLOGRA CONTROL DE SIZE CHANGLE NO. TUBES: 198.33

Attach Additional Sheets As Necessary

¹Final equipment selection has not yet occurred but will be similar in design to specifications shown.

		RM C1				
	CONTROL DEV	ICE (FABRIC	FILTER)			C1
VISED 12/01/01 NCDEN	R/Division of Air Qualit	ty - Application for Ai	r Permit to Con	struct/Operate	S LIM 1 .2 .3 .4	101
NTROL DEVICE ID NO: CD-HM-BF1 & CD-HM-BF.	2 CONTROLS EMIS	SIONS FROM WHICH	EMISSION SO	NO.	2 OF 2 UN	NITS
ISSION POINT (STACK) ID NO(S): EP-2	POSITION IN SER	MODEL NO: TE				
NUFACTURER: TBD ¹		MODEL TO		- RD		
TE MANUFACTURED: TBD		PROPOSED OPERA			BD	
OPERATING SCENARIO:		P.E. SEAL REQUIRE		JIV DITTE		NO
1OF1		P.E. SEAL REGUINE	D (FER 2Q .OT	12).		
ESCRIBE CONTROL SYSTEM: ro (2) bagfilters will be utilized for emission control of	on four of the hammer	mill cyclones. Two ha	mmermili cylco	ones will be routed	to a single bagh	ouse.
TO THE PROPERTY OF THE PROPERT		PM	PM-10	PM-2.5		
OLLUTANT(S) COLLECTED:		1,750	1,750	1,750		
EFORE CONTROL EMISSION RATE (LB/HR):			~99.9	% ~99.9	% 9,	/a
APTURE EFFICIENCY:			- 33.3			/6
ONTROL DEVICE EFFICIENCY:		%			~	
ORRESPONDING OVERALL EFFICIENCY:		%		%	%	Vo
FFICIENCY DETERMINATION CODE:						
		See calculations in	n Appendix B			
OTAL EMISSION RATE (LB/HR):				ARNING ALARM?	(YES)	NO
PRESSURE DROP (IN. H ₂ 0): MIN: MAX: 6"	GAUGI					
BULK PARTICLE DENSITY (LB/FT³): 7.3	29E-04	INLET TEMPERAT				
POLLUTANT LOADING RATE: 5.10 %	B/HR GR/FT	OUTLET TEMPER				
NLET AIR FLOW RATE (ACFM): 40,000		FILTER MAX OPE	RATING TEMP.	(°F): N/A LENGTH OF BAG	/INI >: 144	
NO. OF COMPARTMENTS: 1 NO. OF	BAGS PER COMPART			FILTER SURFACE		7,442
DIAMETER OF BAG (IN.): 5.75 DRAFT			D/POS.	€ WOVEN		
AIR TO CEOTITION.	MATERIAL: Polyester	r or equivalent			CLE SIZE DISTR	
DESCRIBE CLEANING PROCEDURES:				SIZE	WEIGHT %	CUMULATIV
e AIR PULSE	e sonic	O COLLADEE		(MICRONS)	OF TOTAL	%
@ REVERSE FLOW	€ SIMPLE BA			0-1	Unl	known
MECHANICAL/SHAKER	e RING BAC	G COLLAPSE		1-10		
⊕ OTHER				10-25		
DESCRIBE INCOMING AIR STREAM:				25-50		
The air stream will contain wood dust particles. La	rger particles will have	been		50-100		
removed by the upstream cyclone. The filters will	discharge to a commo	n stack. This		>100		
stack will also accept the discharge air flow from a	third bag filter (CD-HN	IA-BF)			TOT	AL = 100
(located in this area.)						
METHOD FOR DETERMINING WHEN TO CLEAN:						
AUTOMATIC	ANUAL					
METHOD FOR DETERMINING WHEN TO REPLACE		MISSION Á	OTHER			
é ALARM é INTERNAL INSPECT	ION & VISIBLE E	MISSION				
SPECIAL CONDITIONS: None	L RESISTIVITY	∮ OTHER				
E MOISTORE DELITION	L REGIOTIVITI					
EXPLAIN: DESCRIBE MAINTENANCE PROCEDURES: Per m	anufacturer recommer	ndations				
DESCRIBE MAINTENANCE PROCEDURES. Per in						

Attach Additional Sheets As Necessary

¹Final equipment selection has not yet occurred but will be similar in design to specifications shown.

SPECIFIC EMISSIONS SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

EVISED 12/01/01 NCDENR/Division	of Air Quality - A	pplication fo	or Air Permit	to Construct	/Operate	1	В	
VISED 12/01/01 NCDENR/Division of Air Quality - Application for Air Permit to Construct/Operate ISSION SOURCE DESCRIPTION: ES-HMA						S-HMA		
ammermill Area Filter	_	CONTROL DEVICE ID NO(S): CD-HMA-BV						
PERATING SCENARIO 1 OF		EMISSION POINT (STACK) ID NO(S): EP-2						
ESCRIBE IN DETAILTHE EMISSION SOURCE PROCES	SS (ATTACH FLO							
and of common offer the hammermille franchings	material to the p	ellet press s	ilo. A secon	d set of conv	eyors transp	orts the mat	erial from th	
ellet press silo to the pellet presses. Particulate emis	sions are routed	to a commo	n dust collec	tion system.	See main rep	port for full o	description.	
	AND AGUEL ET	ADDDODDI	ATE FORM D	4 DO ON THE	EOU OWING	PAGES).		
TYPE OF EMISSION SOURCE (CHECK			Manufact	of chemicals	/coatings/inks	(Form B7)		
Coal,wood,oil, gas, other burner (Form B1) ☐ Wood Int.combustion engine/generator (Form B2) ☐ Coatin	working (Furil D4)	(Form B5)			,	(, , , , ,		
Int.combustion engine/generator (Form B2)	ge silos/bins (Form	1 B6)	Other (Fo	rm B9)				
	ON DATE:		DATE MANUI			TBD		
777111 001101110011011011					DAY 7 D	AY/WK 5	2 WK/YR	
MANOTATION TO THE PROPERTY OF		AP (SUBPAR			(SUBPART?):			
S THIS SOURCE SUBJECT TO? NSPS (SUBPART?):_			JUN-AUG		SEP-NOV	25%		
PERCENTAGE ANNUAL THROUGHPUT (%): DEC-FEB	760 VISIBLE STAC				RATION: <20	% OPAC	CITY	
EXPECTED ANNUAL HOURS OF OPERATION 8,7 CRITERIA AIR POLLUT						- FAREE	A40.04	
CRITERIA AIN I OLLO	SOURCE OF	EXPECTE			POTENTIAL	EMSSIONS		
	EMISSION	(AFTER CONTI		(BEFORE CON	TROLS / LIMITS)		ROLS / LIMITS)	
	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr	
AIR POLLUTANT EMITTED	See Emission				10170177			
PARTICULATE MATTER (PM)	See Lillission	Calculation	із пі дрропа					
PARTICULATE MATTER<10 MICRONS (PM ₁₀) PARTICULATE MATTER<2.5 MICRONS (PM ₂₅)								
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx) CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS (VOC)								
LEAD								
OTHER								
HAZARDOUS AIR POLL	UTANT EMISS	SIONS INF	ORMATIO	FOR THE	S SOURCE		Burrelli .	
	SOURCE OF		D ACTUAL			EMSSIONS		
	EMISSION	(AFTER CONT	ROLS / LIMITS)			(AFTER CON	(AFTER CONTROLS / LIMITS	
HAZARDOUS AIR POLLUTANT AND CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr	
N/A								
107.								
TOXIC AIR POLLUT								
INDICATE EXPEC	TED ACTUAL EM	ISSIONS AF	TER CONTRO	DLS / LIMITAT	TONS			
TOXIC AIR POLLUTANT AND CAS NO.	EF SOURCE	1	b/hr	lt.	o/day		b/yr	
N/A								

Attachments: (1) emissions calculations and supporting documentation; (2) indicate all requested state and federal enforceable permit limits (e.g. nours of operation, emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

EMISSION SOURCE (OTHER)

ES-HMA CD-HMA-BF EP-2 ors transports collection system.						
EP-2						
ers transports						
ers transports						
collection system.						
REQUESTED CAPACITY						
LIMITATION(UNIT/HR)						
REQUESTED CAPACITY LIMITATION (UNIT/BATCH)						
TOTAL MAXIMUM FIRING RATE (MILLION BTU/HR): N/A						
REQUESTED CAPACITY ANNUAL FUEL USE: N/A						

	FORM C1	EII TED\			
	EVICE (FABRIC		actruatiOnarata		C1
	MISSIONS FROM WHICH			FS-HMA	01
The state of the s	SERIES OF CONTROLS	T E MOOIGIT DI	NO.		UNITS
MANUFACTURER: TBD ¹	MODEL NO: T	BD			
DATE MANUFACTURED: TBD	PROPOSED OPERA	ATION DATE:	TBD		
OPERATING SCENARIO:	PROPOSED START	CONSTRUCT	ON DATE:	TBD	
1OF1	P.E. SEAL REQUIR	eD (PER 2Q .0	112)? @	YES	ė NO
DESCRIBE CONTROL SYSTEM: This bagfilter will be utilized for emission control of sources described in	B forms.				
POLLUTANT(S) COLLECTED:	PM	PM ₁₀	PM _{2.5}		
BEFORE CONTROL EMISSION RATE (LB/HR):	1,500	1,500	1,500		
CAPTURE EFFICIENCY:	-99.9 %	-99.9	% -99.9	%	%
CONTROL DEVICE EFFICIENCY:	%		%	%	%
CORRESPONDING OVERALL EFFICIENCY:	%		%	%	%
EFFICIENCY DETERMINATION CODE:					, -
TOTAL EMISSION RATE (LB/HR):	See calculations in	Appendix B			,
PRESSURE DROP (IN. H₂0): MIN: MAX: 6" GAU	GE? (YES	NO W	ARNING ALARM?	(YES)	NO
BULK PARTICLE DENSITY (LB/FT³): 6.67E-04	INLET TEMPERATU	JRE (°F): 120)		
POLLUTANT LOADING RATE: 4.67 & LB/HR & GR/FT	OUTLET TEMPERA	TURE (°F): 10)		
INLET AIR FLOW RATE (ACFM): 37,500	FILTER MAX OPER	ATING TEMP.	°F): N/A		
NO. OF COMPARTMENTS: 1 NO. OF BAGS PER COMPAR	RTMENT: 412		LENGTH OF BAG	(IN.): 144	
DIAMETER OF BAG (IN.): 5.75 DRAFT: # INDUCED	NEG. FORCED	POS.	FILTER SURFACI	E AREA (FT²):	7,442
AIR TO CLOTH RATIO: 6.00 FILTER MATERIAL: Polyeste	er or equivalent		€ WOVEN	# FELTE	D
DESCRIBE CLEANING PROCEDURES:			PARTIC	CLE SIZE DISTR	
₹ AIR PULSE ₹ SONIC			SIZE	WEIGHT %	CUMULATIVE
	AG COLLAPSE		(MICRONS)	OF TOTAL	%
	G COLLAPSE		0-1	Uni	known
₹ OTHER			1-10		
DESCRIBE INCOMING AIR STREAM:			10-25 25-50		
The air stream will contain wood dust particles. Larger particles will have			50-100	ļ	
removed by the upstream cyclone. This filter will discharge to a common	n stack (same		>100		
stack as CD-HM-BF1 & BF2).			>100	TOT	AL = 100
METHOD FOR DETERMINING WHEN TO CLEAN:					
(AUTOMATIC) & TIMED & MANUAL					
METHOD FOR DETERMINING WHEN TO REPLACE THE BAGS:					
& ALARM & INTERNAL INSPECTION & VISIBLE E	EMISSION & OT	THER			
SPECIAL CONDITIONS: None					
é MOISTURE BLINDING é CHEMICAL RESISTIVITY	∮ OTHER				
EXPLAIN:					
DESCRIBE MAINTENANCE PROCEDURES: Per manufacturer recommen	ndations				
ON A SEPARATE PAGE, ATTACH A DIAGRAM SHOWING THE RELATION	SHIP OF THE CONTROL	DEVICE TO IT	S EMISSION SOU	RCE(S):	

Attach Additional Sheets As Necessary

¹Final equipment selection has not yet occurred but will be similar in design to specifications shown.

SPECIFIC EMISSIONS SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

NCDENE/Division C	f Δir Quality - Appli	cation for	Air Permit to	Construct/O	perate		B	
VIOLE ILIVIE	N SOURCE DESCRIPTION: EMISSION SOURCE ID NO.							
IISSION SOURCE DESCRIPTION:	OURCE DESCRIPTION. CD-PMFS-							
Het Mill Feed Silo	4		EMISSION POINT (STACK) ID NO(S): EP-3					
PERATING SCENARIO 1 OF	1							
SCRIBE IN DETAILTHE EMISSION SOURCE PROCESS pellet press silo stores dried ground wood prior to trai	nsport to the penet	presses.				2.050		
TYPE OF EMISSION SOURCE (CHECK A	AND COMPLETE AP	PROPRIAT	E FORM B1	B9 ON THE F	OLLOWING I	PAGES):		
Woody	vorking (Form B4)		Mariuraci.	Or Chemicals.	coatings/inks	(Form B7)		
Int.combustion engine/generator (Form B2)	g/finishing/printing (F	orm B5)	☐ Incineratio	n (Form B8)				
Liquid storage tanks (Form B3)	e silos/bins (Form Bi	5)	Other (For	rm B9)				
TART CONSTRUCTION DATE: TBD OPERATION	ON DATE:		ATE MANUF			TBD	a MIKOVO	
IANUFACTURER / MODEL NO.: TBD	EXI	PECTED OI	P. SCHEDUL	E: <u>24</u> HR/I		DAY/WK <u>5</u>	2_WK/YR	
STHIS SOURCE SUBJECT TO? NSPS (SUBPART?):	NESHAP	(SUBPART	?):	MACT (S	SUBPART?):_			
THE CHOURT WAY DECKER	25% MAR-MAY	25%	JUN-AUG		SEP-NOV			
TON 97	60 VISIBLE STACK	EMISSION	S UNDER NO	ORMAL OPER	ATION: <2	0 % OPA	CITY	
XPECTED ANNUAL HOURS OF OPERATION 8,7 CRITERIA AIR POLLUT	ANT EMISSION	S INFOR	MATION F	OR THIS S	DURCE		SALVEL SILL	
ONTENANCE	SOURCE OF	EXPECTED	ACTUAL		POTENTIAL			
		AFTER CONTR	OLS / LIMITS)	(BEFORE CONT	ROLS / LIMITS)	(AFTER CONT	ROLS / LIMITS)	
	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr	
AIR POLLUTANT EMITTED	See Emission C	alculations	in Appendi	х В				
PARTICULATE MATTER (PM)								
PARTICULATE MATTER<10 MICRONS (PM 10) PARTICULATE MATTER<2.5 MICRONS (PM 2.5)								
SULFUR DIOXIDE (SO2)								
NITROGEN OXIDES (NOx)								
CARBON MONOXIDE (CO)								
VOLATILE ORGANIC COMPOUNDS (VOC)								
LEAD								
OTHER HAZARDOUS AIR POLE	UTANT EMISSI	ONS INFO	ORMATIO	N FOR THIS	SOURCE			
HAZAKDOOG AIKT GE	SOURCE OF	EXPECTE	D ACTUAL		POTENTIA	L EMPORIONS		
			ROLS / LIMITS)	1		(AFTER CON	CONTROLS / LIMITS	
TO STANT AND CAS NO	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr	
HAZARDOUS AIR POLLUTANT AND CAS NO.							-	
N/A							1	
TOXIC AIR POLLU	TANT EMISSION	S INFOR	MATION F	OR THIS S	OURCE			
INDICATE EXPEC	TED ACTUAL EMIS	SIONS AFT	ER CONTRO	DLS / LIMITAT	IONS			
	EF SOURCE		b/hr		o/day		lb/yr	
TOXIC AIR POLLUTANT AND CAS NO.	El GGG.							
N/A								
	1 1							

Attachments: (1) emissions calculations and supporting documentation; (2) indicate all requested state and federal enforceable permit limits (e.g. hours of operation, emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

FORM B6 EMISSION SOURCE (STORAGE SILO/BINS)

EVISED 12/01/01	NCDENR/D	Division of Air Quality - A	Applicatio	n for Air Pe	rmit to Cor	nstruct/Opera	ate		B6	
ISSION SOURCE DESCRIP	TION: Pellet Mill	Pellet Mill Feed Silo			SSION SO	ES-PMFS				
9				CONTROL DEVICE ID NO(S): CD-PMFS			CD-PMFS-B	ву		
PERATING SCENARIO:		OF		EMISSION POINT(STACK) ID NO(S): EP-3				EP-3		
ESCRIBE IN DETAIL THE PRI		FLOW DIAGRAM):	the pellet	presses.						
MATERIAL STORED:				DENSITY C	F MATERI	AL (LB/FT3):		40		
CAPACITY	CUBIC FEET:	TBD		TONS:	TBD					
DIMENSIONS (FEET)	HEIGHT:	DIAMETER:	(OR)	LENGTH:		WIDTH:	HEIG	ŧΤ:		
ANNUAL PRODUCT THR	-		•	MAX	XIMUM DE:	SIGN CAPAC	ITY:			
PNEUMATICALLY F		MECHANI	CALLY FI					ED FROM		
ේ BLOWER ඒ COMPRESSOR ඒ OTHER:		BELT CONVEYOR BUCKET ELEVATOR	>	МОТС	R HP:	d TRU	DRAGE PILE			
		Ø OTHER:				(d 01	THER:	Conveyor		
NO. FILL TUBES:		∜ OTHER:				(o	THER:	Conveyor		
XIMUM ACFM:		♡ OTHER:				01	HER:	Conveyor		
XIMUM ACFM: MATERIAL IS FILLED TO: BY WHAT METHOD IS MATER		ROM SILO?				01	HER:	Conveyor		
XIMUM ACFM: MATERIAL IS FILLED TO: BY WHAT METHOD IS MATER		ROM SILO?	~75				HER:	Conveyor		
1	RATE OF MATERIAL	ROM SILO? L (TONS/HR):	~75 ~75				HER:	Conveyor		

FORM C1

CONTROL DEVICE (FABRIC FILTER)

VISED 12/01/01 NTROL DEVICE ID NO: CD-PPS-BV CONTROL	S EMISSIONS FROM WHICH	EMISSION S	OURCE ID NO(S):	ES-PPS	NIITO
SSION POINT (STACK) ID NO(S): EP-7 POSITION	IN SERIES OF CONTROLS		NO	. 1 OF 1 U	NITS
	MODEL NO:	TBD			
NOFACTORER.	PROPOSED OPE			TBD	
TE MANUFACTURED: TBD OPERATING SCENARIO:	PROPOSED STA			TBD	10
1_OF_1_	P.E. SEAL REQU	RED (PER 20	2 .0112)?	e YE)	NO
SCRIBE CONTROL SYSTEM: A bin vent filter collects dust from when wood enters or exit	s the silo and displaces air.				
OLLUTANT(S) COLLECTED:	PM	PM ₁	PM _{2.5}		
EFORE CONTROL EMISSION RATE (LB/HR):	~99.9 %		~99.9 %~99	.9 %	%
APTURE EFFICIENCY:			——————————————————————————————————————	%	%
ONTROL DEVICE EFFICIENCY:	%	-			%
ORRESPONDING OVERALL EFFICIENCY:	%		%	%	,v
EFFICIENCY DETERMINATION CODE:					
	See calculation	s in Appendix	кВ		
OTAL EMISSION RATE (LB/HR):	GAUGE? (YES	é NO	WARNING ALARM	P € YES € N	0
RESSURE DROP (IN. H ₂ 0): MIN: TBD MAX: TBD	INLET TEMPER	ATURE (°F):	Ambient		
BULK PARTICLE DENSITY (LB/FT 3): 1.43E-06	GR/FT ³) OUTLET TEMF		F): Ambient		
POLLUTANT LOADING RATE. 0.02	FILTER MAX C				
NLET AIR FLOW RATE (ACFM): 2,500 NO. OF BAGS PER COMPARTMENT: TBD NO. OF BAGS PER COM				AG (IN.): TBD	
NO. OF COMPACTMENT	UCED/NEG. FORC	ED/POS.	FILTER SURFA	ACE AREA (FT 2):	rbd
DIAMETER OF BAG (IN.):	OCEDINEO.		∮ WO.		
AIR TO CLOTH RATIO: TBD FILTER MATERIAL:			P	ARTICLE SIZE DISTR	
DESCRIBE CLEANING PROCEDURES:	NIC		SIZE	WEIGHT %	CUMULATIVI
e AIR PULSE	IPLE BAG COLLAPSE		(MICRONS) OF TOTAL	%
© REVERSE FLOW	NG BAG COLLAPSE		0-1		
WECHANIOALION WALL			1-10		
(d OTHER			10-25		
DESCRIBE INCOMING AIR STREAM: The air stream will contain wood dust particles			25-50		
HUG SIT PRESENT AND CONTROL ASSOCIATION			50-100		
			>100		TAL = 400
				ТО	TAL = 100
SPECIAL CONDITIONS: # MOISTURE BLINDING # CHEMICAL RESISTIVITY EXPLAIN: **EXPLAIN:** **EXPLAIN:*	SIBLE EMISSION	· OTHER		-	
Per manufacturer recommendations or common industry pract	ices.				

SPECIFIC EMISSIONS SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

EVISED 12/01/01 NCDENR/Division o	f Air Quality - Appl	ication fo	or Air Permit to	Construct/	Operate		В
MISSION SOURCE DESCRIPTION:			EMISSION SO			ES-CLR-1,2	3,4,5, 6
ellet Coolers		1	CONTROL DE			CD-CLR-1,-	
	1		EMISSION PC			EP-1	
PERATING SCENARIO1 OF							
hree Pellet Coolers follow the pellet presses to cool the	e newly formed pel	lets down	to an accepta				
TYPE OF EMISSION SOURCE (CHECK A	ND COMPLETE AF	PROPRIA	ATE FORM B1	B9 ON THE	FOLLOWING	PAGES):	
□ Coal,wood.oil, gas, other burner (Form B1) □ Woodw	orking (Form B4)		Manufact.	of chemicals	/coatings/inks	(Form B7)	
☐ Int.combustion engine/generator (Form B2) ☐ Coating	g/finishing/printing (f						
Liquid storage tanks (Form B3)	e silos/bins (Form B	6)	Other (Fo	rm B9)			
START CONSTRUCTION DATE: TBD OPERATION		TBD	DATE MANUF			TBD	
MANUFACTURER / MODEL NO.: TBD	EX	PECTED	OP. SCHEDUL			DAY/WK _	52 WK/YR
S THIS SOURCE SUBJECT TO? NSPS (SUBPART?):	NESHAP	(SUBPAF	RT?):	MACT (SUBPART?):_		
PERCENTAGE ANNUAL THROUGHPUT (%): DEC-FEB	25% MAR-MA		JUN-AUG		SEP-NOV		
EXPECTED ANNUAL HOURS OF OPERATION 8,76	VISIBLE STACK	EMISSIO	NS UNDER NO	RMAL OPER	RATION: <2	0 % OP	ACITY
CRITERIA AIR POLLUT	ANT EMISSION	S INFO	RMATION F	OR THIS S	OURCE		
			D ACTUAL		POTENTIAL	EMSSIONS	6
	EMISSION (AFTER CON	rrols/LIMITS)	(BEFORE CON	TROLS / LIMITS)	(AFTER CO	TROLS / LIMITS
AIR POLLUTANT EMITTED	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
PARTICULATE MATTER (PM)	See Emission C	alculation	ns in Appendi	х В			
PARTICULATE MATTER (FM) PARTICULATE MATTER < 10 MICRONS (PM 10)	T						
PARTICULATE MATTER<2.5 MICRONS (PM _{2.5})							
SULFUR DIOXIDE (SO2)							
NITROGEN OXIDES (NOx)							
CARBON MONOXIDE (CO) VOLATILE ORGANIC COMPOUNDS (VOC)							
LEAD							
OTHER HAZARDOUS AIR POLL	UTANT EMISSION	ONS INF	ORMATION	FOR THIS	SOURCE	ye i- ji ii	i ingila
THE PART OF THE PA	SOURCE OF	EXPECT	ED ACTUAL ITROLS / LIMITS)		POTENTIAI	(AFTER CO	NTROLS / LIMITS
HAZARDOUS AIR POLLUTANT AND CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
N/A							
						-	
							4
					.		
TOXIC AIR POLLUT.	ANT EMISSION	S INFOR	RMATION F	OR THIS S	OURCE		VIEW BON
INDICATE EXPECT	ED ACTUAL EMISS	SIONS AF	TER CONTRO	LS / LIMITAT	IONS		
TOXIC AIR POLLUTANT AND CAS NO.	EF SOURCE		lb/hr	ll li	o/day		lb/yr
N/A							
ATU.						-1	

Attachments: (1) emissions calculations and supporting documentation; (2) indicate all requested state and federal enforceable permit limits (e.g. hours of operation, emission rates and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

EMISSION SOURCE (OTHER)

TIOLD, INVIET	Application f	or Air Permit to Construct/Operate	B9
EVISED: 12/01/01 NCDENR/Division of Air Quality - A MISSION SOURCE DESCRIPTION:		EMISSION SOURCE ID NO:	ES-CLR-1,2,3,4,5, 6
ellet Coolers		CONTROL DEVICE ID NO(S):	CD-CLR-1,-2,-3
PERATING SCENARIO: 1 OF 1		EMISSION POINT (STACK) ID NO(S)): EP-1
ESCRIBE IN DETAIL THE PROCESS (ATTACH FLOW DIAGRAM): Three Pellet Coolers follow the pellet presses to cool the newly	formed pello	ets down to an acceptable storage to	emperature.
MATERIALS ENTERING PROCESS - CONTINUOUS PROCES	S	MAX. DESIGN	REQUESTED CAPACITY
TYPE	UNITS	CAPACITY (UNIT/HR)	LIMITATION(UNIT/HR)
Dried Wood	Tons	72.8	
		MAY DEGICAL	REQUESTED CAPACITY
MATERIALS ENTERING PROCESS - BATCH OPERATION TYPE	UNITS	MAX. DESIGN CAPACITY (UNIT/BATCH)	LIMITATION (UNIT/BATCH)
TOTAL PARTIES (HOUR).			
MAXIMUM DESIGN (BATCHES / HOUR): REQUESTED LIMITATION (BATCHES / HOUR):	(BATCHES/	YR):	
FUEL USED: N/A		(IMUM FIRING RATE (MILLION BTU/	HR): N/A
MAX. CAPACITY HOURLY FUEL USE: N/A		D CAPACITY ANNUAL FUEL USE:	N/A

CONT	ROL DEVI	CE (CYC		ULTIC	I C 4 YCLONE, O	R OTHER N	/IECHANIC	AL)	
REViSED 12/01/01					cation for Air Pen			-,	C4
CONTROL DEVICE ID NO: CD-CLR-			1		S FROM WHICH I			ES-CLR-1,2,3,4,5	5. 6
EMISSION POINT (STACK) ID NO(S):	EP-1				OF CONTROLS	NO.	1 OF 1	UNITS	,, 0
MANUFACTURER: TBD ¹				MODEL	NO:				
DATE MANUFACTURED: TBD				PROPOS	SED OPERATION I	DATE: TBD			
OPERATIN	G SCENARIO:			PROPOS	SED START CONS	TRUCTION DATI	E: TBD		
1_	OF1			P.E. SEA	L REQUIRED (PE	R 2Q .0112)?	a (YES	NO è NO	
DESCRIBE CONTROL SYSTEM: Three identical dual high efficiency of three cyclones. The cyclones will op	yclones are to erate under ne	be used to egative pres	capture bulk i	PM emiss ameters p	ions from six (6) poresented here are	ellet coolers. T	wo coolers ven	t to each of the cyclone.	
POLLUTANT(S) COLLECTED:				PM	PM ₁₀	PM _{2.5}			
BEFORE CONTROL EMISSION RATE	(LB/HR):			30	0 300	300)		
CAPTURE EFFICIENCY:				98-99	98-99	% 98-99	%	%	
CONTROL DEVICE EFFICIENCY:					%	%	%	%	
CORRESPONDING OVERALL EFFICIE	ENCY:				_%	%	%	%	
EFFICIENCY DETERMINATION CODE	is								
TOTAL EMISSION RATE (LB/HR):				See Emi	ssions Calculation	ns in Appendix E	3		
PRESSURE DROP (IN. H ₂ 0); MIN	MAX 6.	.0" V	VARNING ALA	RM?	€ YES	é NO			
INLET TEMPERATURE (°F): MIN	MAX		Ambient		OUTLET TEMPE	RATURE (°F):	MIN MA	Ambient	
INLET AIR FLOW RATE (ACFM):	12,500 per Cy	clone/25,000	0 per Dual Cyc	ci. Sys.	BULK PARTICLE	DENSITY (LB/F			
POLLUTANT LOADING RATE (GR/FT ³		1.40				`	, 0,000		
SETTLING CHAMBER	THE RES	181 194	CY	CLONE				MULTICYCLONE	
LENGTH (INCHES):	INLET VELOC	CITY (FT/SEC	58		& CIRCUI AR	é RECTANGLE	NO. TUBES:		
WIDTH (INCHES):			ES) See instruc		IF WET SPRA		DIAMETER OF	TUBES:	
HEIGHT (INCHES):		6"	Dd:	12"	LIQUID USED:	., ., ., .,		IRATION SYSTEM?	
VELOCITY (FT/SEC.):		4.25"	Lb:	72"	FLOW RATE (GF	PM):	# YES	€ NO	
NO. TRAYS:	De: 36	0"	Lc:	84"	MAKE UP RATE		LOUVERS?	0 110	
NO. BAFFLES:	D: 56	0"	S:	39"	0.11.0	(Or my.	& YES	€ NO	
	TYPE OF CYC	LONE:	& CONVENT		& HIGH	EFFICIENC	€ OTHER	9 110	
DESCRIBE MAINTENANCE PROCEDU	-							DISTRIBUTION	F/45 19
Periodic inspection of mechanical in as specified by manufacturer	tegrity during p	plant outage	s			SIZE (MICRONS)	WEIGHT %	CUMULATI	VE
							OFTOTAL	%	
DESCRIBE INCOMING AIR STREAM: The dual cyclones used for particula	te capture the	pellet cooler	s will be duct	ed to		1-10		Unknown	_
a discharge stack. The stack will be									
_		- copi		. •		10-25			
						25-50			
						50-100			
						>100		7074	
DESCRIBE ANY MONITORING DEVIC None	ES, GAUGES, 1	TEST PORTS	S, ETC:					TOTAL = 100	
ON A SEPARATE PAGE, ATTACH A D	IAGRAM OF T	IE DEL ATIO	NGUID OF THE	- CONTE	N DEMOS TO TO	EMBORON SCH	DOE(O)		
S JEI MEUTE I AGE, ATTAON A	NOIVINI OF IF				ets As Neces		RUE(S):		
¹ Final equipment selection has	not yet occui								

SPECIFIC EMISSIONS SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

REVISED 12/01/01 NCDENR/Division or	f Air Quality - Ap	plication for	r Air Permit t	o Construct/0	Operate		B
MISSION SOURCE DESCRIPTION:				URCE ID NO		ES-EG	
mergency Generator (250kw, 350 bhp)			CONTROL DE	VICE ID NO(S):	N/A	
PERATING SCENARIO 1OF	1	- I	EMISSION PO	DINT (STACK)) ID NO(S):	EP-4	
ESCRIBE IN DETAILTHE EMISSION SOURCE PROCESS	(ATTACH FLOV	V DIAGRAM):				
iesel-fired internal combustion generator to provide po	wer in the case of	of an emerge	ency.				
lesel-med internal combastion government.							
TYPE OF EMISSION SOURCE (CHECK A	ND COMPLETE	APPROPRIA	TE FORM B1	-B9 ON THE	FOLLOWING	PAGES):	
Coal,wood,oil, gas, other burner (Form B1) Woodw	orkina (Form B4)		Manufact	. of chemicals	/coatings/inks	(Form B7)	
Int.combustion engine/generator (Form B2)	/finishing/printing	(Form B5)	Incinerati	on (Form B8)			
	silos/bins (Form		Other (Fo	rm B9)			
			DATE MANU	FACTURED:		TBD	
START CONSTRUCTION DITTE:				E: <u>24</u> HR	/DAY	DAY/WK	52 WK/YR
MANUFACTURER / MODEL NO.: TBD S THIS SOURCE SUBJECT TO? NSPS (SUBPART?):II		(SUBPART?			JBPART?):_Z	777	
	25% MAR-M		JUN-AU	3 25%	SEP-NO	√ 25%	
PERCENTAGE ANNUAL PHROOGH OT (70). DEG TE	O VISIBLE STAC		S UNDER N	ORMAL OPER	RATION: <2	20_ % OPA	CITY
EXPECTED ANNUAL HOURS OF OPERATION 50 CRITERIA AIR POLLUT.	ANT FMISSIO	NS INFOR	RMATION F	OR THIS S	OURCE		A
CRITERIA AINT OLLOT	SOURCE OF	EXPECTE			POTENTIAL	EMSSIONS	
	FMISSION		ROLS / LIMITS)	(BEFORE CON	TROLS / LIMITS)	•	TROLS / LIMITS)
	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
AIR POLLUTANT EMITTED	See Emission				toriary		
PARTICULATE MATTER (PM)	See Emission	Calculation	S III Append				
PARTICULATE MATTER<10 MICRONS (PM 10)							
PARTICULATE MATTER<2.5 MICRONS (PM 2.5)	-						
SULFUR DIOXIDE (SO2)	-						
NITROGEN OXIDES (NOx)							
CARBON MONOXIDE (CO)							
VOLATILE ORGANIC COMPOUNDS (VOC)	_						
LEAD						1	
OTHER HAZARDOUS AIR POLL	ITANT ENICS	NONE INE	OPMATIO	V FOR THIS	SOURCE		E.S. 1505 V.
HAZARDOUS AIR POLLI				TORTIN	DOTENTIA	L EMSSIONS	
	SOURCE OF		D ACTUAL	(BEEGDE 60)	TROLS / LIMITS)	1	YTROLS / LIMITS
	EMISSION		ROLS / LIMITS)	Ib/hr	tons/yr	ib/hr	tons/yr
HAZARDOUS AIR POLLUTANT AND CAS NO.	FACTOR	lb/hr	tons/yr	1	toris/yi	10/11/	tonerj.
	See Emissio	n Calculatio	ns in Append	T B	-		
							+
			-	-	-		
			-	-	-	1	
			+	-	+	-	
						+	+
		110 11/1505	MATION E	OD TUIC C	OUDCE		
TOXIC AIR POLLUTA	ANT EMISSIO	NS INFUR	MATION F	LC LIMITAT	IONS		
INDICATE EXPECT						1	lb/ur
TOXIC AIR POLLUTANT AND CAS NO.	EF SOURCE		b/hr		o/day		lb/yr
	See Emission	on Calculation	ns in Appen	dix B			- 55
				-			
				-		-	
				-		-	
						-	
				-		-	
					imits (e.a. hours	of appropriate and	mission rates)
			and fodoral onfo	arceable nermit l	imits le a bolits	or operation, et	masion rates)

Attachments: (1) emissions calculations and supporting documentation; (2) indicate all requested state and federal enforceable permit limits (e.g. hours of operation, emission rates and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

EMISSION SOURCE (INTERNAL COMBUSTION ENGINES/GENERATORS)

ES-GN N/A): EP-4 SYR): DUAL FUEL ENGIN OTHER Pete below) TURBINE SE): LLYTIC REDUCTION NTROLLED
DUAL FUEL ENGIN OTHER TURBINE LYTIC REDUCTION
DUAL FUEL ENGIN OTHER TURBINE SE): LLYTIC REDUCTION
DUAL FUEL ENGIN OTHER TURBINE EE: LLYTIC REDUCTION
DUAL FUEL ENGIN OTHER TURBINE EE: LLYTIC REDUCTION
DUAL FUEL ENGIN OTHER TURBINE EE: LLYTIC REDUCTION
DUAL FUEL ENGIN OTHER TURBINE EE: LLYTIC REDUCTION
ete below) TURBINE SE): LLYTIC REDUCTION
ete below) ### TURBINE BE): LLYTIC REDUCTION
ete below) ### TURBINE BE): LLYTIC REDUCTION
ete below) ### TURBINE BE): LLYTIC REDUCTION
€ TURBINE BE): ILYTIC REDUCTION
€ TURBINE BE): ILYTIC REDUCTION
BE):
LYTIC REDUCTION
LYTIC REDUCTION
TINGELED
THE HERETER
ED CARACITY
ED CAPACITY ON (UNIT/HR)
ID CONTENT
JR CONTENT WEIGHT)
N
OC OTHER
70C OTTLER

SPECIFIC EMISSIONS SOURCE INFORMATION (REQUIRED FOR ALL SOURCES)

EVISED 12/01/01 NCDENR/Division of	Air Quality - Ap	olication for	Air Permit to	Construct/C	perate		В
EVISED 12/01/01 NCDENR/Division of MISSION SOURCE DESCRIPTION:		E	MISSION SO	URCE ID NO	ES	S-FWP	
re Water Pump (300 bhp)			CONTROL DE			A	
	1		MISSION PC			P-5	
PERATING SCENARIO 1 OF ESCRIBE IN DETAILTHE EMISSION SOURCE PROCESS							
ESCRIBE IN DETAILTHE EMISSION SOURCE? ROOLSS iesel-fired internal combustion pump to provide water in	n the case of a fi	re emergen	cy.				
lesel-tired internal combustion pump to provide							
TYPE OF EMISSION SOURCE (CHECK A	ND COMPLETE A	PPROPRIA	TE FORM B1	B9 ON THE I	OLLOWING P	AGES):	
Coal,wood,oil, gas, other burner (Form B1) Woodw	orking (Form B4)		Manufact.	of chemicals	coatings/inks (F	Form B7)	
Int.combustion engine/generator (Form B2)	/finishing/printing	(Form B5)	☐ Incineration	n (Form B8)			
Int.combustion engine/generation (Form B2) Liquid storage tanks (Form B3)	silos/bins (Form	B6)	Other (Fo	rm B9)			
Liquid storago tarino (. 1111 - 17			DATE MANUF	ACTURED:	Т	BD	
START CONSTRUCTION BATE: 125		XPECTED C	P. SCHEDUL	E: 24 HR/	DAY	AY/WK5	2 WK/YR
MANUFACTURER / MODEL NO.: TBD S THIS SOURCE SUBJECT TO? NSPS (SUBPART?): III		SUBPART?		MACT (SU	BPART?): ZZZ	77	
PERCENTAGE ANNUAL THROUGHPUT (%): DEC-FEB	25% MAR-M		JUN-AUG	25%	SEP-NOV	25%	
HOURD OF OPERATION 10	VISIBLE STAC	K EMISSION	NS UNDER NO	ORMAL OPER	RATION:<20	% OPA	CITY
EXPECTED ANNUAL HOURS OF OPERATION 10 CRITERIA AIR POLLUTA	ANT EMISSIO	NS INFOR	RMATION F	OR THIS S	OURCE		A ST ST
OMILIAN AIRS CLOSE	SOURCE OF	EXPECTE	DACTUAL		POTENTIAL E	EMSSIONS	
	EMISSION	(AFTER CONT		(BEFORE CON	TROLS / LIMITS)	(AFTER CONT	ROLS / LIMITS)
	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
AIR POLLUTANT EMITTED	See Emission	Calculation	s in Appendi	х В			
PARTICULATE MATTER (PM)							
PARTICULATE MATTER (10 MICRONS (PM 10)							
PARTICULATE MATTER<2.5 MICRONS (PM 2.5)							
SULFUR DIOXIDE (SO2)							
NITROGEN OXIDES (NOx)							
CARBON MONOXIDE (CO) VOLATILE ORGANIC COMPOUNDS (VOC)							
LEAD							
OTHER HAZARDOUS AIR POLL	UTANT EMISS	IONS INF	ORMATIO	FOR THIS	SOURCE		
IMENIO	SOURCE OF	EXPECTE	D ACTUAL		POTENTIAL		
	EMISSION	(AFTER CON	TROLS / LIMITS)	(BEFORE COM	TROLS / LIMITS)	(AFTER CON	TROLS / LIMITS
HAZARDOUS AIR POLLUTANT AND CAS NO.	FACTOR	lb/hr	tons/yr	lb/hr	tons/yr	lb/hr	tons/yr
HAZARDOUS AIR POLEUTANT AND GAS ITS.	See Emissio	n Calculatio	ns in Append	ix B			
							-
							4
							-
TOXIC AIR POLLUTA	ANT EMISSIO	NS INFOR	MATION F	OR THIS S	OURCE		
INDICATE EXPECT	ED ACTUAL EMI	SSIONS AF	TER CONTRO	LS / LIMITAT	IONS		
TOXIC AIR POLLUTANT AND CAS NO.	EF SOURCE		lb/hr	1	b/day		lb/yr
TOMO AIR TOLLOTARY THE CITE TO	See Emission	n Calculation	ons in Appen	dix B			
						-	
							mission rates)

Attachments: (1) emissions calculations and supporting documentation; (2) indicate all requested state and federal enforceable permit limits (e.g. hours of operation, emission rates) and describe how these are monitored and with what frequency; and (3) describe any monitoring devices, gauges, or test ports for this source.

EMISSION SOURCE (INTERNAL COMBUSTION ENGINES/GENERATORS)

ALL THAT APPLY	REVISED 12/01/01	NCDENR/Division of Air Qualit	y - Application for Air Perm	it to Construct/Operate	B2
ING SCENARIO: 1 OF 1 SPACE HEAT	MISSION SOURCE DESCRIPTION:	Fire Water Pump (300 bhp)		EMISSION SOURCE ID NO:	ES-FWP
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## PLAK SHMVER ## OTHER (DESCRIBE): ANTICIPATED ACTUAL HOURS OF OPERATION AS PEAK SHAVER (HRSYYR): COUTPUT (HYP):			SPACE HEAT	ELECTRICAL GENERATION	
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COUTPUT (IIP): E: É GASOLINE ENGINE GASOLINE ENGINE OTHER (DESCRIBE): TYPE OTHER (DESCRIBE): TYPE OTHER (DESCRIBE): TYPE OTHER (DESCRIBE): TYPE OTHER (DESCRIBE): ON REDUCTION MODIFICATIONS OTHER (DESCRIBE): OTH				OPERATION AS PEAK SHAVER (HRS	
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# ORSCHILL STORY Complete below # OTHER (DESCRIBE): (complete below) TYPE		DIEGEL ENGINE IND	TO COOLID & DIESE	ENGINE OPEATED THAN 800 HP	DUAL FUEL ENGIN
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STATIONARY GAS TURBINE (complete below) NATURAL GAS				NITION CHAMPED COMPILISTION	d OTHER
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	COMMENTS:				

Rotary Dryer - Criteria Pollutant Emissions

Dryer Inputs

Dryer Throughput (@ Dryer Exit)	527,778	tons/year @ 10% moisture
Annual Dried Wood Throughput of Dryer	475,000	ODT/year
Max. Hourly Dried Wood Throughput of Dryer	61.50	ODT/hr
Burner Heat Input	207.0	MMBtu/hr
Percent Hardwood	90%	
Percent Softwood	10%	
Potential Operation	8,760	hr/yr

Criteria Pollutant Calculations:

Pollutant	Biomass Emission Factor	Units	Emission Factor Source	Total Po Emiss	
1 Ollutuilt	(lb/ODT)			(lb/hr)	(tpy)
СО	1.16	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	71.34	275.5
NO _X	0.79	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	48.59	187.6
PM/PM ₁₀ /PM _{2.5} Condensible Fraction	0.017	lb/MMBtu	AP-42, Section 1.6 ²	3.52	15.4
TSP (Filterable)	0.090	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	5.54	21.4
Total TSP (Filterable + Condensible)				9.05	36.8
PM ₁₀ (Filterable)	0.090	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	5.54	21.4
Total PM ₁₀ (Filterable + Condensible)				9.05	36.8
PM _{2.5} (Filterable)	0.090	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	5.54	21.4
Total PM _{2.5} (Filterable + Condensible)				9.05	36.8
SO ₂	0.025	lb/MMBtu	AP-42, Section 1.6 ³	5.18	22.7
VOC	1.50	lb/ODT	Calculated from Guaranteed WESP Specifications ¹	92.25	356.3
Lead	0.00	N/A	N/A	0.00	0.0

Note

 $^{^{1}}$ CO, NO_x, VOC, and filterable PM/PM₁₀ emission factors were provided by the dryer system vendor. The PM_{2.5} filterable emission factor is assumed to be the same as PM and PM₁₀.

² The vendor only provided the filterable fraction of particulate matter in the emission factors. The condensible fraction of particulate matter from a rotary dryer controlled by a WESP is not provided in AP-42, Section 10.6.2. Enviva has conservatively calculated the condensible fraction based upon the heat input of the dryer burners using an emission factor for wood combustion from AP-42, Section 1.6.

³ No emission factor is provided in AP-42, Section 10.6.2 for SO₂ for rotary dryers. Enviva has conservatively calculated SO2 emissions based upon the heat input of the dryer burners using an emission factor for wood combustion from AP-42, Section 1.6.

Rotary Dryer - Federal Hazardous Air Pollutant (HAP) and North Carolina Toxic Air Pollutant (TAP) Emissions

Calculation Inputs:

Dryer Throughput (Ton/yr)	527,778
ODT/yr	475,000
ODT/hr	61.50
Hardwood Composition	%06
Softwood Composition	10%

HAP & TAP Emission Calculations:

				Direct w	Direct wood-fired, hardwood	rdwood	Green, Direct	reen, Direct wood-fired (inlet moistu content >5 <u>0</u> %, dry basis), softwood [†]	Green, Direct wood-fired (inlet moisture content >50%, dry basis), softwood ¹		
HAP/TAP Pollutant	CAS Number	HAP	NC TAP	Emission Factor ²	Emiss	Emissions ³	Emission Factor	Emiss	Emissions ³	MAXIMUM TOTAL EMISSIONS	1 TOTAL
		(Yes/No)	(Yes/No)	(Ib/ODT)	(lb/hr)	(tpy)	(lp/ODT)	(Ib/hr)	(tpy)	(lb/hr)	(tpy)
Acetaldehyde	75-07-0	Yes	Yes	3.83E-03	2.36E-01	8.19E-01	7.50E-02	4.61E+00	1.78E+00	4.61E+00	2.60E+00
Acrolein	107-02-8	Yes	Yes	1.17E-03	7.22E-02	2.51E-01	2.30E-02	1.41E+00	5.46E-01	1.41E+00	7.97E-01
Benzene	71-43-2	Yes	Ves	3.88E-04	2.39E-02	8.30E-02	7.60E-03	4.67E-01	1.81E-01	4.67E-01	2.63E-01
Chloroform	67-66-3	Yes	Yes	5.11E-06	3.14E-04	1.09E-03	1.00E-04	6.15E-03	2.38E-03	6.15E-03	3.47E-03
Cumene	98-82-8	Yes	No	1.02E-04	6.28E-03	2.18E-02	2.00E-03	1.23E-01	4.75E-02	1.23E-01	6.93E-02
Formaldehyde	20-00-0	Yes	Yes	7.15E-03	4.40E-01	1.53E+00	1.40E-01	8.61E+00	3.33E+00	8.61E+00	4.85E+00
m-,p-Xylene	1330-20-7	Yes	Yes	2.45E-04	1.51E-02	5.24E-02	4.80E-03	2.95E-01	1.14E-01	2.95E-01	1.66E-01
Methanol	67-56-1	Yes	No	5.62E-03	3.45E-01	1.20E+00	1.10E-01	6.77E+00	2.61E+00	6.77E+00	3.81E+00
Methyl isobutyl ketone	108-10-1	Yes	Yes	3.52E-04	2.17E-02	7.53E-02	6.90E-03	4.24E-01	1.64E-01	4.24E-01	2.39E-01
Methylene chloride	75-09-2	Yes	Yes	9.19E-05	5.65E-03	1.96E-02	1.80E-03	1.11E-01	4.28E-02	1.11E-01	6.24E-02
o-Xylene	95-47-6	Yes	No	2.30E-05	1.41E-03	4.91E-03	4.50E-04	2.77E-02	1.07E-02	2.77E-02	1.56E-02
Phenol	108-95-2	Yes	Yes	1.43E-03	8.79E-02	3.06E-01	2.80E-02	1.72E+00	6.65E-01	1.72E+00	9.71E-01
Propionaldehyde	123-38-6	Yes	No	6.64E-04	4.08E-02	1.42E-01	1.30E-02	8.00E-01	3.09E-01	8.00E-01	4.51E-01
Styrene	100-42-5	Yes	Yes	1.84E-05	1.13E-03	3.93E-03	3.60E-04	2.21E-02	8.55E-03	2.21E-02	1.25E-02
Toluene	108-88-3	Yes	Yes	6.64E-04	4.08E-02	1.42E-01	1.30E-02	8.00E-01	3.09E-01	8.00E-01	4.51E-01
									Total HAP	2.62E+01	1.48E+01

Note:

¹ HAP & TAP emission factors for "green, direct wood-fired (inlet moisture content >50%, dry basis" softwood were obtained from AP-42, Section 10.6.2, Table 10.6.2-3.

² To account for hardwood HAP & TAP emissions, factors were conservatively calculated by taking the AP-42 HAP factors for 100% softwood (green) and multiplying by the ratio of the total listed VOC emission factors for hardwood and softwood (0.24 / 4.7).

³ Short-term HAP & TAP emissions were calculated based upon a worst-case scenario of 100% hardwood or softwood firing (in which case, softwood is always the overall worst case).

Emergency Generator Emissions (ES-EG)

Equipment and Fuel Characteristics

Engine Output	0.26	MW
Engine Power	350	hp (brake)
Hours of Operation	500	hr/yr¹
Heating Value of Diesel	19,300	Btu/lb
Power Conversion	2,545	Btu/hr/hp

Criteria Pollutant Emissions

				Potential En	issions
Pollutant	Category	Emission Factor	Units	lb/hr	tpy
TSP	PSD	4.41E-04	lb/kW-hr (2)	0.12	2.88E-0
PM ₁₀	PSD	4.41E-04	lb/kW-hr (2)	0.12	2,88E-0
PM _{2.5}	PSD	4.41 E-04	lb/kW-hr (2)	0.12	2.88E-0
NO _x	PSD	8.82E-03	lb/kW-hr (5)	2,30	5.75E-0
SO_2	PSD	15	ppmw (3)	1.38E-03	3.46E-0
CO	PSD	7.72E-03	lb/kW-hr (2)	2.01	5.40E-0 5.03E-0
VOC (NMHC)	PSD	2.51E-03	lb/MMBtu (4)	2.24E-03	5.59E-0
Acrolein	HAP/TAP HAP/TAP	5.37E-06	lb/hp-hr (4)	1.88E-03	4.70E-0
Benzene		6.48E-07	lb/hp-hr (4)	2.27E-04	5.67E-0
	HAP/TAP	6.53E-06	lb/hp-hr (4)	2.29E-03	5.71E-0
Benzo(a)pyrene ⁶	HAP/TAP	1.32E-09	lb/hp-hr (4)	4.61E-07	1.15E-0
1,3-Butadiene	HAP/TAP	2.74E-07	lb/hp-hr (4)	9.58E-05	2.39E-0.
Formaldehyde	HAP/TAP	8.26E-06	1b/hp-hr (4)	2.89E-03	7.23E-0
Total PAH (POM)	HAP	1.18E-06	lb/hp-hr (4)	4.12E-04	1.03E-0
Toluene	HAP/TAP	2.86E-06	Ib/hp-hr (4)	1.00E-03	2.51E-0
Xylene	HAP/TAP	2.00E-06	lb/hp-hr (4)	6.98E-04	1.75E-0
Highest HAP (Formaldehyde)		8.26E-06	lb/hp-hr (4)	2.89E-03	7.23 E-04
Total HAPs				9.49E-03	2.37E-03

Note

NSPS allows for only 100 hrs/yr of non-emergency operation of these engines (not the 500 hours shown). The PTE for the emergency generator is based on 500 hr/yr, though, because the regs allow non-emergency operation and EPA guidance is 500 hr/yr for emergency generators.

² Emissions factors from NSPS Subpart IIII (or 40 CFR 89.112 where applicable) in compliance with post-2009 construction.

³ Sulfur content in accordance with Year 2010 standards of 40 CFR 80.510(a) as required by NSPS Subpart IIII.

 $^{^{\}rm 4}$ Emission factor obtained from AP-42 Section 3.3, Tables 3.3-1 Table 3.3-2.

⁵ Emission factor for NOx is listed as NOx and NMHC (Non-Methane Hydrocarbons or VOC) in Table 4 of NSPS Subpart IIII. Conservatively assumed entire limit attributable to NOx.

⁶ Benzo(a)pyrene is included as a HAP in Total PAH.

Firewater Pump Emissions (ES-FWP)

Equipment and Fuel Characteristics

Educhien		
Engine Output	0.22	MW
Engine Power	300	hp
Hours of Operation	500	hr/yr ^l
Heating Value of Diesel	19,300	Btu/lb
Power Conversion	2,545	Btu/hr/hp

iteria Pollutant Emissions				Potential Em	issions
Pollutant	Category	Emission Factor	Units	lb/hr	tpy
	PSD	4.41E-04	lb/kW-hr (2)	0.10	2.47E-02
TSP	PSD	4.41E-04	lb/kW-hr (2)	0.10	2.47E-02
PM ₁₀	PSD	4.41E-04	lb/kW-hr (2)	0.10	2.47E-03
PM _{2.5}	PSD	8.82E-03	lb/kW-hr (5)	1.97	4.93E-0
NO _x	1	15	ppinw (3)	1.19E-03	2.97E-0
SO ₂	PSD	7.72E-03	lb/kW-hr (2)	1.73	4.32E-0
CO	PSD PSD	2.51E-03	lb/MMBtu (4)	1.92E-03	4.79E-0
VOC (NMHC)	130	1 2.012 00			
Acetaldehyde	HAP/TAP	5.37E-06 6.48E-07	lb/hp-hr (4) lb/hp-hr (4)	1.94E-04	4.86E-0
oxic/Hazardous Air Pollutant Emissio		5.37E-06	lb/hp-hr (4)	1.61E-03	4.03E-0
Acrolein	HAP/TAP	6.53E-06	lb/hp-hr (4)	1.96E-03	4.90E-0
Benzene	HAP/TAP	1	1 1	3.95E-07	9.87E-0
Benzo(a)pyrene ⁶	HAP/TAP	1.32E-09	lb/hp-hr (4)	8.21E-05	2.05E-0
1.3-Butadiene	HAP/TAP	2.74E-07	lb/hp-hr (4)		6.20E-0
Formaldehyde	HAP/TAP	8.26E-06	lb/hp-hr (4)	2.48E-03	8.82E-0
Total PAH (POM)	HAP	1.18E-06	lb/hp-hr (4)	3.53E-04	8.82E-V 2.15E-V
Toluene	HAP/TAP	2.86E-06	lb/hp-hr (4)	8.59E-04	
	27 4 D (D 4 D	2.00E-06	lb/hp-hr (4)	5.99E-04	1.50E-(
Xylene	HAP/TAP				
Xylene Highest HAP (Formaldehyde)	HAP/TAP	8.26E-06	lb/hp-hr (4)	2.48E-03 8.13E-03	6.20E-(2.03E-

Note:

¹ NSPS allows for only 100 hrs/yr of non-emergency operation of these engines (not the 500 hours shown). The PTE for the emergency generator is based on 500 hr/yr, though, because the regs allow non-emergency operation and EPA guidance is 500 hr/yr for emergency generators.

² Emissions factors from NSPS Subpart IIII (or 40 CFR 89.112 where applicable) in compliance with post-2009 construction.

³ Sulfur content in accordance with Year 2010 standards of 40 CFR 80.510(a) as required by NSPS Subpart IIII.

⁴ Emission factor obtained from AP-42 Section 3.3, Tables 3.3-1 Table 3.3-2.

⁵ Emission factor for NOx is listed as NOx and NMHC (Non-Methane Hydrocarbons or VOC) in Table 4 of NSPS Subpart IIII. Conservatively assumed entire limit attributable to NOx.

⁶ Benzo(a)pyrene is included as a HAP in Total PAH.

Dust Control Systems PM Emissions

		Wilter Vent or-		Pollutant	Annual					Potential Emissions	Emissions		
	Fmission	Cyclone	Flowrate	Loading ²	Operation	% PM	% PM that is	Ь	PM	PM ₁₀	3 10	PM _{2.5}	3.5
A STATE OF THE STA	Source ID	QI O	(cfm)	(gr/cf)	(hours)	PM_{10}	PM _{2.5}	(lb/hr)	(tby)	(lb/hr)	(tpy)	(lb/hr)	(tpy)
Emission Cum	D 1 0 1 4	CD UM BE!	40.000	0000	8.760	100%	100%	1.71	7.51	1.71	7.51	1.71	7.51
Hammermills Bagfiffer 1	E3-HIVI-1, -2, -3, -4	CD-INIT-DI I	2000		0/= 0	1000	1000/	10.	7.51	171	751	171	7.51
Hammermills Barfilter 2	ES-HM-1, -2, -3, -4	CD-HM-BF2	40,000	0.005	8,760	100%	100%	1.71	10.7	1./1	10.1	77.77	10.7
Downsermill Area Fifter	FS-HMA	CD-HMA-BF	37,500	0.005	8,760	100%	100%	1.61	7.04	1.61	7.04	1.61	7.04
Dalingiani Area rinoi													
Pellet Mill Feed Silo Bin Vent	ES-PMFS	CD-PMFS-BV	2,500	0.005	8,760	100%	100%	0.11	0.47	0.11	0.47	0.11	0.47
Filter										1	27.00		27.00
Dellat Coolers Cyclone 1	FS-CLR	CD-CLR-1	25,000	0.022	8,760	100%	100%	4.71	20.65	4.71	20.65	4.71	50,02
Patter Contract Contract	210-01	CD-CLR-2	25.000	0.022	8,760	100%	100%	4.71	20.65	4.71	20.65	4.71	20.65
Pellet Coolers Cyclone 2	4 5 54	CD-C1 P.3	25,000	0.022	8.760	100%	100%	4.71	20.65	4.71	20.65	4.71	20.65
Pellet Coolers Cyclone 3	ES-CLN	CDCCRC	2005				TOTA1	19 29	84.47	19.29	84.47	19.29	84.47
							TOTAL	17:47	04:47	17.00			

¹ Filter, Vent, and Cyclone inlet flow rate (cfin) provided by design engineering firm (Mid-South Engineering Co.). The exit flowrate was conservatively assumed to be the same as the inlet flowrate.

² Unless otherwise specified, pollutant (PM) loading conservatively assumed to be 0.005 gr/dscf.

¹ It was conservatively assumed that PM₁₀ and PM_{2,5} equal PM emissions.

Fugitive PM Emissions

Emissions for PM ₁₀ Emissions for (1b/hr) (tpy) (1b/hr) (1b/h						Throu	Throughput				P u	Datastiol Ilu	Controlled
ENTISSUE SOUTCE STORY Conveyor Belt ES-DWH Conveyor Belt to Pelet ES-DWH Collection Conveyor Belt to Pelet Es-DWH Collection Conveyor Belt to Pelet Es-DWH Collection Conveyor Belt to Pelet Enclosed Reduction to 2 mph 68.29 527,778 5.2E-03 2.0E-03 2.3E-03 3.3E-04 3.5E-04 3				Control	Control Description	Max.	Max.	Potential U Emissions	ncontrolled s for PM ³	Potential Un Emissions	controlled for PM ₁₀	Emissions f	or PM _{2.5}
ES-DWH Conveyor Belt Collection Conveyor Belt to Pelet Es-DWH Conveyor Belt to Pelet Es-DWH Conveyor Belt to Pelet Mannermills System Discharge Collection Conveyor Belt to Pelet Mill Feed Silo Infeed Screw Mill Feed Silo Infeed Screw Mill Feed Silo Infeed Screw Conveyor Belt to Pelet Collection Conveyor Belt Collection Conveyor Belt Collection Conveyor Belt to Pelet Collection Conveyor Belt to Pelet Collection Conveyor Belt Collection Conveyor Belt to Pelet Collection Conveyor Collection Conve	2	Emission Source Group				(toh)	(tpy)	(lb/hr)	(tpy)	(lb/hr)	(tpy)	(Jb/hr)	(tpy)
ES-DWH Pre-screen Feeder Fines Overs to Hammermills Infeed and Distribution ES-DWH Hammermills System Discharge ES-DWH Hammermills System Discharge Es-DWH Collection Conveyor Belt to Pellet Enclosed Reduction to 2 mph 61.83 477.850 4.7E-03 1.8E-02 2.2E-03 8.5E-03 3.3E-04 3.5E-04 3.5E-05 3.3E-04 3.3E-05 3.3E-04 3.3E-05 3.3E-0	Idci	ES-DWH	Dryer Discharger to Dryer Collection	_		68.29	527,778	5.2E-03	2.0E-02	2.4E-03	9.4E-03	3.7E-04	1,4E-03
ES-DWH			The second second										40.00
Hammermills System Discharge Enclosed Reduction to 2 mph 61.83 477,850 4.7E-03 1.8E-02 2.2E-03 3.3E-04 Reduction Conveyor Belt Collection Conveyor Belt to Pellet Enclosed Reduction to 2 mph 68.29 527,778 5.2E-03 2.0E-02 2.4E-03 3.7E-04 Reduction to 2 mph 68.29 527,778 5.2E-03 7.3E-03 3.7E-04 Mill Feed Silo Infeed Screw Mill Feed Screw	DP2	ЕЅ-ЪМН	Pre-screen Feeder Fines Overs to Hammermills Infeed and Distribution		Reduction to 2 mph mean wind speed	6.46	49,928	4.9E-04	1.9E-03	2.3E-04	8.9E-04	3.5E-05	1.4E-04
Hammermills Cyclone Diverter Gates Lector of Collection Conveyor Belt Collection Conveyor Belt to Pellet Collection Conveyor Belt to Pellet Collection Convey													
Hammermills System Discharge Eachosed Collection Conveyor Belt to Pellet Enclosed Mill Feed Silo Infeed Screw Mill Feed	DP3	ES-DWH	Hammermills Cyclone Diverter Gates to Hammermills System Discharge		Reduction to 2 mph mean wind speed		477,850	4.7E-03	1.8E-02	2.2E-03	8.5E-03	3.3E-04	1.3E-03
Hanmermills System Discharge			Collection conveyor con-										
Mill Feed Silo Infeed Screw 4. EP 17 7.3R-03 2.8E-02 1.1E-03	DP4	ES-DWH	Hammermills System Discharge Collection Conveyor Belt to Pellet	Enclosed	Reduction to 2 mph mean wind speed		527,778	5.2E-03	2.0E-02	2.4E-03	9.4E-03	3.7E-04	1.4E-03
	i		Mill Feed Silo Infeed Screw				TOT	1 CE 03	6.0E-02	7.3E-03	2,8E-02	1.1E-03	4.3E-03

² Max hourly rates based upon maximum calculated throughput rates and moistures contents provided in mass balance provided by Mid-South Engineering Company, June 17, 2011. ¹ Fugitive emissions are not included in facility-wide PTE because the Northampton Pellet Mill does not belong to one of the listed 28 source categories.

³ Based emission factors calculated per AP-42 Section 13.2.4, September 2006.

where: $E = emission \ factor \ (lb/lon)$ $k = particle \ size \ multiplier \ (dimensionless) \ for \ PM$ $k = particle \ size \ multiplier \ (dimensionless) \ for \ PM_{10}$

k= particle size multiplier (dimensionless) for $PM_{2,5}$

2.00 U = mean wind speed (mph)
M = material moisture content (%)
E for PM (lb/ton) =

10

7.6E-05 E for PM_{10} (lb/ton) = 3.6E-05 E for $PM_{2.5}$ (lb/ton) = 5.4E-06

Tank VOC Emissions

Tank Description		Tank D	Tank Dimensions				I AINKS 4.0	0.4.0
	Volumo	Diamotor	Height/Length Orientation Throughput	Orientation	Throughput	Turnovers	VOC E	VOC Emissions
	(graf)	(fi)	(#)		(gal/yr)		(lb/yr)	(tpy)
	(ear)					, 00	200	2 670 02
Tomb?	2 500	9	12	Vertical	12,000	4.80	0.37	3.3 / E-U3
TK01 Emergency Generator Fuel Oil Latin	2,,700	,			000	07.00	0.42	2 15E-04
Elle Woter Dump Fire Oil Tank	200	57	10	Horizontal	10,300	70.07	- 1	4.13L1.2
IKUZ FIIE Water rump ruch our rum.	200					TOTAL	0.80	3.79E-03

Note:

¹ Conservative design specifications.

² Throughput based on fuel consumption and 500 hours of operation per year. Fuel consumption data provided by pump engine vendors.

Electric Powered Chipper (ES-CHIP-1) Emissions

Annual Throughput of Chipper 475,000 tons/year (dry wood)¹
Short-term Throughput of Chipper 61.50 tons/hr (dry wood)¹
Maximum Annual Operation 8,760 hours

	Emission Factors	Emissi	ons ⁶
Pollutant	(lb/dry wood tons)	(lb/hr)	(tpy)
THC as Carbon ²	0.0041	2.522E-01	1.10
THC as alpha-Pinene ³	0.0047	2.862E-01	1.25
PM ⁴	N/A	N/A	N/A
Methanol ²	0.0010	6.150E-02	0.24

It is assumed that the wood received at the facility has a nominal water content of 50%.
The annual throughput used for the chipper is the same as the annual throughput of the dryer; while the short-term throughput is based upon the maximum hourly throughput of the dryer.

² Emission factor obtained from available emissions factors for chippers in AP-42 Section 10.6.3, Table 7 and Section 10.6.4, Tables 7 and 9. Emission factors for THC and Methanol are the same across all three tables.

³ The THC/VOC makeup of wood is primarily composed of terpenes (C₅H₈)_n[where n = 2, 3, or 4 typically] but to convert from carbon to the equivalent weight in THC/VOC, the assumption was that alphapinene (AP) would be the representative THC/VOC (molecular weight = 136.2 lb/lb-mol). The following equation shows the conversion:

lb VOC/ODT = lb C/ODT * (136.2 lb/mol AP / 12 lb/mol C) * (1 mol AP / 10 mol C)

⁴ PM emission factor is not applicable as the chipper emissions are routed downward to the ground.

⁵ Short term emissions were based upon the annual throughput of the chipper (dry wood) divided by the total hours of operation.

Potential GHG Emissions

Operating Data:

Dryer Heat Input 175.00 MMBtu/nr
Operating Schedule 8,760 hrs/yr
Emergency Generator Output 350 bhp
Operating Schedulc 500 hrs/yr

No. 2 Fuel Input 16.7 gal/hr¹
Energy Input 2.282 MMBtu/hr²

Fire Water Pump Output 300 bhp Operating Schedule 500 hrs/yr

14.3 gal/hr¹ 1.956 MMBtu/hr²

Energy Input

No. 2 Fuel Input

				ANTHORNIA 3	Į.	Tier 1 Emissions (metric tons)	s (metric ton	(\$
		Emission Fac	Emission Factors from Table C-1 (Rg/MIMDEU)	(g/MMDtu)				i
61 22 22	Enol Tune			0.00	200	PHU	CCZ	N2O Total COZe
Emission Unit 1D	adá rana	C02	CH4	NZO	200			
						, ,	r	150 567
derived on	Wood and Wood	9.38E+01	3.20E-02	4.20E-03	158,506	54	,	100,001
ES-DKY EK	Daeiduale							
	Nestana					00 1100	NO 023 7	03
	No. 2 Fuel Oil	7 40F+01	3.00E-03	6.00E-04	93	3.77E-U3	3.77E-U3 7.33E-U4	(/)
ND-SH	Distillate							
	Piprinter				0	CO Troc	A 77E OA	08
	No. 2 Fuel Oil	7 40F±01	3.00E-03	6.00E-04	08	3.23E-U3	0.47E=04	2
ES-FWP	Distillate	0.00						
	Distillate							

¹ Fuel consumption calculated using a factor of 0.0476 gal/hr-hp. Advanced Environmental Interface, Inc. (1998).

General Permits for Emergency Engines. INSIGHTS, 98-2, 3.

² Energy calculated on a fuel consumption basis, using an energy factor of 0.137 MMBtu/gal.

³ Emission factors from Table C-1 and C-2 of GHG Reporting Rule. Emission factors for methane and N2O already multiplied by their respective GWPs of 21 and 310.



One Copley Parkway, Suite 310, Morrisville, North Carolina 27560 U.S.A. • (919) 462-9693 • Fax (919) 462-9694

August X, 2011

William Flynn
Planning and Zoning Director
Northampton County Planning and Zoning
102 West Jefferson Street
Jackson, NC 27845

Subject: Air Permit Application Zoning Consistency Determination Request

Enviva Pellets Northampton, LLC

Dear Mr. William Flynn,

This letter is a request for a determination of whether planned construction project of a wood pellet manufacturing facility located at Lebanon Church Road in Gaston, NC is consistent with current local zoning requirements. A copy of the air permit application being submitted to the North Carolina Division of Air Quality (NCDAQ) is attached.

Your confirmation of zoning consistency is needed by the NCDAQ prior to issuance of the air quality construction permit. Please complete the attached form and send to the address shown on the form as soon as possible. In the interim, we would appreciate it if you would stamp this cover letter with your department's seal, sign and date next to your seal and return the sealed cover letter via FAX to my attention at (919) 462-9694. This stamp is needed to be considered administratively complete by the NC Division of Air Quality. Should you require additional information to complete your review, please do not hesitate to contact me at (919) 462-9693.

Sincerely,

Joe Sullivan, PE, CM Managing Consultant

Goe W. Sullivan

Attachment

Zoning Consistency Determination

D-:!!tr Nome	Enviva Pellets Northampton, LLC
Facility Name	Lebanon Church Road (Street Number TBD)
Facility Street Address	
Facility City	Gaston
Description of Process	Wood pellet manufacturing facility
SIC Code/NAICS	SIC – 2499 ; NAICS - 321999
Facility Contact	Glenn Gray
Phone Number	(804) 412-0227
Mailing Address	1309 East Cary Street, Suite 200
Mailing City, State Zip	Richmond, Virginia 23219
Based on the information given	ven above:
I have received a copy o	f the air permit application (draft or final) AND
The proposed operation The proposed operation	IS NOT consistent with applicable zoning and subdivision ordinances Als NOT consistent with applicable zoning and subdivision ordinances By of the rules in the package sent to the air quality office)
The determination is per	nding further information and can not be made at this time
Cother:	
Agency	
Name of Designated Offic	ial
Title of Designated Officia	al
Signature	
Date	

Please forward to the mailing address listed above and the air quality office at the appropriate address as checked on the back of this form.

Courtesy of the Small Business Assistance Program toll free at 1-877-623-6748 or on the web at www.envhelp.org/sb

All PSD and Title V Applications

X Attn: Dr. Donald van der Vaart, PE DAQ – Permitting Section 1641 Mail Service Center Raleigh, NC 27699-1641

Local Programs

- □ Attn: David Brigman
 Western NC Regional Air Quality Agency
 49 Mount Carmel Road
 Asheville, NC 28806
 (828) 250-6777
- □ Attn: Donald R. Willard
 Mecklenburg County Air Quality
 700 N. Tryon Street, Suite 205
 Charlotte, NC 28202-2236
 (704) 336-5500

□ Attn: Robert R. Fulp Forsyth County Environmental Affairs Department 537 N. Spruce Street Winston-Salem, NC 27101-1362 (336) 703-2440

Division of Air Quality Regional Offices

- Attn: Paul Muller
 Asheville Regional Office
 2090 U.S. Highway 70
 Swannanoa, NC 28778
 (828) 296-4500
- □ Attn: Steven Vozzo
 Fayetteville Regional Office
 225 Green Street Suite 714
 Fayetteville, NC 28301
 (910) 433-3300
- □ Attn: Ron Slack
 Mooresville Regional Office
 610 East Center Avenue, Suite 301
 Mooresville, NC 28115
 (704) 663-1699
- Attn: Patrick Butler, PE Raleigh Regional Office 1628 Mail Service Center Raleigh, NC 27699-1628 (919) 791-4200

- Attn: Robert Fisher
 Washington Regional Office
 943 Washington Square Mall
 Washington, NC 27889
 (252) 946-6481
- □ Attn: Wayne Cook
 Wilmington Regional Office
 127 Cardinal Drive Extension
 Wilmington, NC 28405
 (910) 796-7215
- □ Attn: Margaret Love, PE
 Winston-Salem Regional Office
 585 Waughtown Street
 Winston-Salem, NC 27107
 (336) 771-5000

Courtesy of the Small Business Assistance Program toll free at 1-877-623-6748 or on the web at www.envhelp.org/sb